



CH2M HILL
2485 Natomas Park Drive
Suite 600
Sacramento, CA 95833
Tel 916.920.0300
Fax 916.920.8463

November 13, 2006

Mr. Lorne Prescott
Project Manager
California Energy Commission
1516 Ninth Street
Sacramento, CA 95814

DOCKET 05-AFC-2	
DATE	NOV 13 2006
RECD.	NOV 13 2006

Re: Supplement IV in Response to Data Requests and Workshop Queries in Support of the Application for Certification for the Walnut Creek Energy Park (05-AFC-02)

Dear Mr. Prescott:

Attached are one original and 12 copies of Walnut Creek Energy, LLC's Supplement IV in Response to Data Requests 1 through 104 and April 25 Workshop Queries in Support of the Application for Certification for the Walnut Creek Energy Park (05-AFC-02).

If you have any questions about this matter, please contact me at (916) 286-0278 or Jenifer Morris at (714) 841-7522.

Sincerely,

Douglas M. Davy, Ph.D.
AFC Project Manager

Attachment

cc: T. McCabe
L. Kostrzewa
J. Morris
S. Galati
V. Yamada

Contents

Contents	1
Introduction	3
Transmission System Engineering	5
WSQ8 Generation Tie-Line Route.....	5
Visible Plume Modeling	11
DR77 Visible Plume Modeling Results.....	13
Visual Resources	17
DR91 Landscape and Irrigation Plan.....	19

Introduction

The following is Walnut Creek Energy, LLC (WCE's) fourth supplemental filing in response to Data Requests for the Walnut Creek Energy Park (WCEP) (05-AFC-02) and other information requests from staff and other parties. Additional staff questions have arisen subsequent to the Staff's filing of formal Data Requests, and these are called workshop queries, for convenience. Some workshop queries resulted from the April 25, 2006, Data Request Response Workshop. Others have arisen through subsequent discussions with Staff. Responses or information submittals such as this one are numbered consistently with the Data Request numbers (for example, DR-15 is a response to Staff Data Request number 15), or are given a unique and sequential number with the WSQ prefix (for "workshop query").

Transmission System Engineering

Generation Tie-Line Route

WSQ-8 *Has Southern California Edison clarified their role in developing a finalized routing for the generation tie line between the WCEP and the Walnut Substation? If so, please provide this information.*

Response: During further discussions with Southern California Edison (SCE) in connection with SCE's interconnection study process, SCE has identified two generation tie-line options instead of the project design option as described in the Application for Certification. These options are shown in Attachment TSE-1, Figure WSQ-11.

Both of these options involve a connection to the northwest corner of the Walnut Substation, rather than the southeast corner. Option 1 runs due west from the WCEP within the existing SCE transmission corridor for about 700 feet, then turns south to cross the Union Pacific Railroad and connect with the northwest corner of the Walnut Substation. The length of this tie-line would be approximately 1,170 feet.

Option 2 would run first south from the WCEP, across the railroad, then turn west to run just north of the northern boundary of the substation to the northwest corner of the substation, turning south to connect. The length of this tie-line would be approximately 1,220 feet.

Each of these options would involve crossing over or under a number of different 66 kV transmission lines. These crossings could also be made by placing the lines underground. Figure WSQ-11 indicates the locations of transmission towers necessary to make these crossings. The towers would not be needed if the line were placed underground.

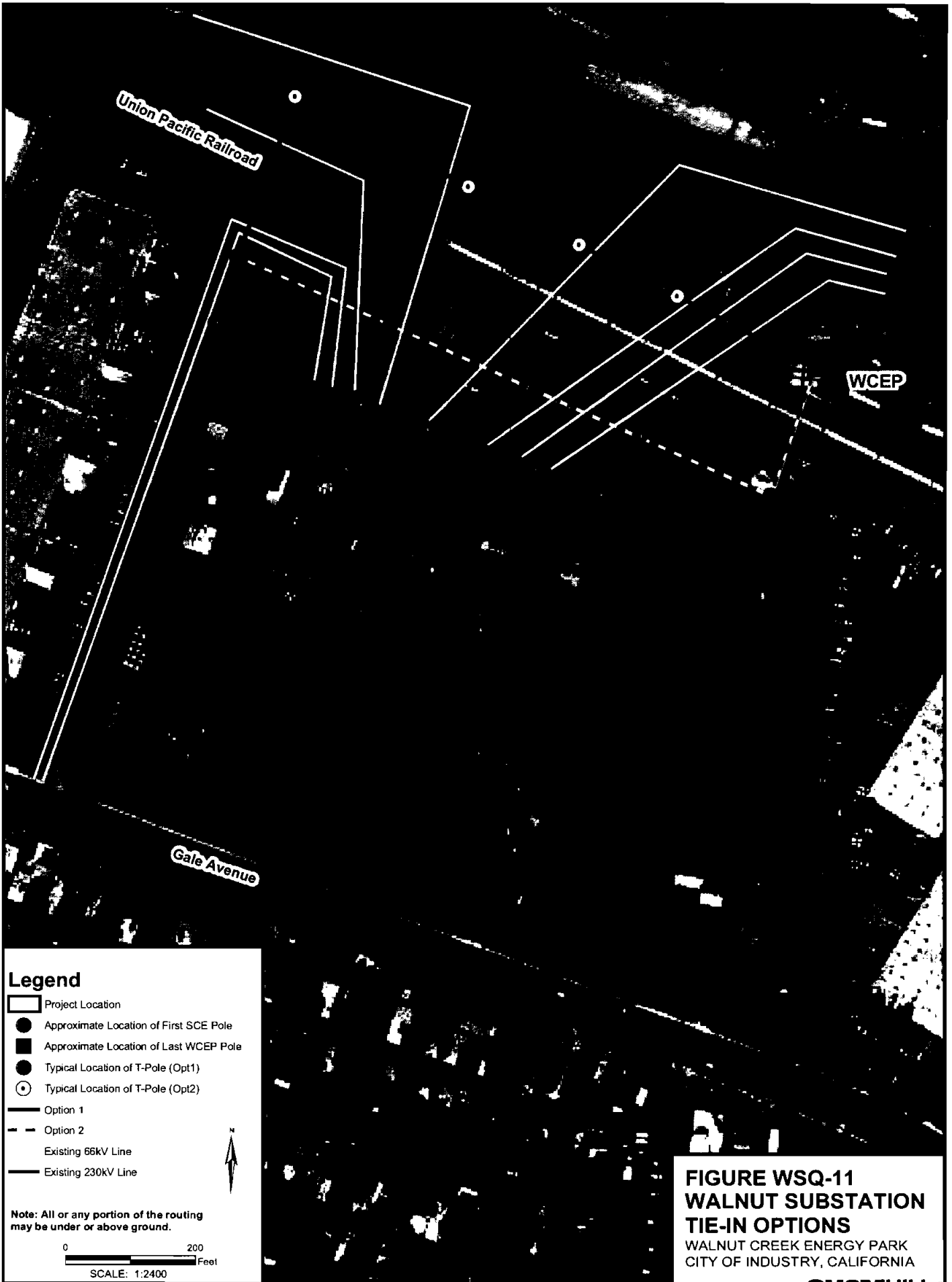
It is our understanding currently that WCE would be responsible for the generation tie connection as far as the Walnut Substation fence line and that SCE would construct and own the tie-line within the substation. The final choice of generation tie route will be made by SCE.

In terms of environmental effects, both options are nearly identical to the existing project design. The only significant difference is that these options would require more towers than the existing line, because of the need to cross the existing 66 kV lines. The additional towers would have a negligible effect, from a visual resources point of view, because the substation area is already congested with towers and transmission lines, and the new towers would not block any scenic or protected viewsheds.

Portions of both options are within the area surveyed for biological and cultural resources, and portions of these routes (on the western end) were not previously surveyed. Significant resources are not likely to be located in these areas.

Attachment TSE-1

SCE Interconnection Option

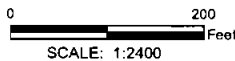


Legend

- Project Location
- Approximate Location of First SCE Pole
- Approximate Location of Last WCEP Pole
- Typical Location of T-Pole (Opt1)
- Typical Location of T-Pole (Opt2)
- Option 1
- Option 2
- Existing 66kV Line
- Existing 230kV Line



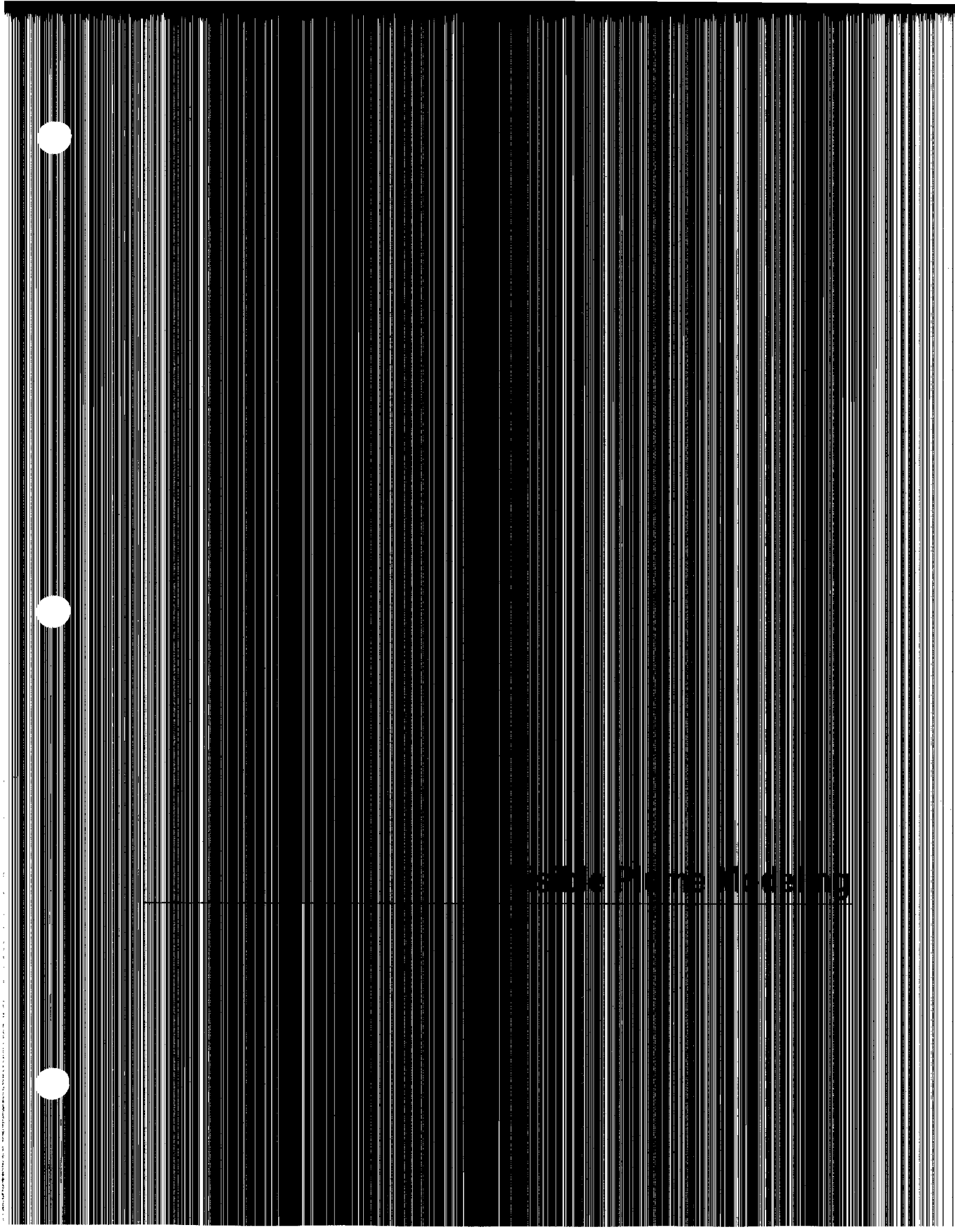
Note: All or any portion of the routing may be under or above ground.



SCALE: 1:2400

**FIGURE WSQ-11
WALNUT SUBSTATION
TIE-IN OPTIONS**

WALNUT CREEK ENERGY PARK
CITY OF INDUSTRY, CALIFORNIA



Visible Plume Modeling

Visible Plume Modeling Results

DR77. *If the applicant performed a visible plume modeling analysis in support of the AFC Visual Resources conclusion, please provide:*

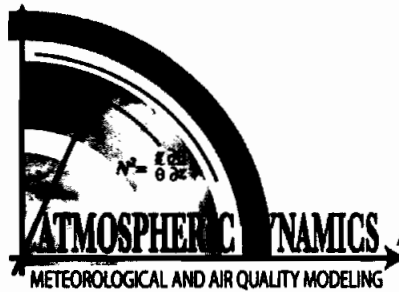
- a. the modeling results;*
- b. any meteorological data used in the analysis;*
- c. a full discussion of all assumptions;*
- d. the name and version of the model used; and*
- e. all model input and output files.*

Response: The visual plume modeling analysis is included as Attachment VP-1.

Attachment VP-1

Visible Plume Analysis

Cooling Tower Plume Modeling Analysis for the Edison Mission Energy Walnut Creek Energy Park



Prepared by:

Atmospheric Dynamics, Inc.
2925 Puesta del Sol Rd.
Santa Barbara, CA 93105

November 9, 2006

Cooling Tower Plume Modeling Analysis Edison Mission Energy – Walnut Creek Energy Park

Introduction

This report was prepared to summarize an analysis of the potential for the formation of visible water vapor plumes from cooling towers at the proposed Walnut Creek Project (WCEP). This study was conducted to support the visual resources assessment, which will involve a separate analysis of the visual resources impacts of cooling tower plumes, if they are present.

Edison Mission Energy (EME) is proposing to use a five (5) cell wet mechanical-draft cooling tower to reject heat to the atmosphere. The air leaving the cooling towers is usually saturated with moisture and warmer than the ambient air, causing a wet exhaust plume to be created. The saturated exhaust plume may be or may not be visible, depending on the specific meteorological conditions. The potential for visible plume formation is also based on cooling tower operational factors that can occur in conjunction with existing meteorological conditions. Visible plume formation from the five (5) natural gas-fired turbines is not expected to occur since the turbine exhaust is hot and contains very little moisture.

Potential issues associated with cooling tower plumes include the presence of visible plumes and the occurrence of ground level fogging and/or icing episodes that involve the ground contact of visible plumes. In order to evaluate the effects on the local and regional environment, a modeling analysis was conducted to simulate the cooling tower plumes from the proposed project using five (5) years of meteorological data.

The modeling analysis presented below is conservative because it does not take into account the likely conditions in which the power plant would actually operate. Specifically, WCEP is a peaking power plant that is expected to operate primarily during peak power demand periods. Peak power demands generally occur during mid-day hours, particularly during hot summer or fall months, when the climatic conditions that result in visible plume formation are not present. However, since the computer modeling technique does not easily segregate the specific hours during which the peak power demand would occur, the results of the vapor plume modeling analysis assumed continuous operation of the power plant during all daylight/non-rain hours. The results presented below considerably over-predict the project's creation of visible plumes and do not represent the true operational profile of this project.

Modeling Techniques

The Seasonal/Annual Cooling Tower Impact Program (SACTI, Version 11-01-90) was used to
Cooling Tower Plume Analysis

assess potential for the WCEP cooling tower to form visible vapor plumes. SACTI was developed by Argonne National Laboratory¹ for the Electric Power Research Institute (EPRI) to address the following potential adverse impacts of cooling towers:

- plume visibility
- deposition of cooling tower drift
- ground-level fogging and icing
- shadowing by the plume & reduction of solar energy

SACTI contains algorithms for both natural- and mechanical-draft cooling towers arranged singly or in clusters. Plume merging and associated enhanced plume rise are treated by the routines contained in the model. While the SACTI model does not have any official regulatory endorsement, this model has been applied for a large number of projects where cooling tower impact assessments were required. The characteristics of the tower and the preparation of the meteorological data set are discussed below.

The characteristics of the proposed cooling tower are listed in Table 1. These input parameters were obtained from EME's engineering consultant based on preliminary seasonal design data for the facility.

A five (5) year meteorological data set was constructed using hourly surface observations from the Ontario International Airport meteorological station, which is located near the proposed project location, for the years 2001 through 2005. As discussed below, night-time hours were removed from the meteorological data set, as were day-time hours for which weather or other phenomena would impair visibility. Figure 1 displays a wind rose constructed from all hours of the five (5) year data. The average wind speed is 3.5 m/s and high winds greater than 6 m/s occur 11 percent for the five year data set. Wind speeds either missing or less than the threshold of the anemometer at Ontario occur for 33 percent of the time period. A lack of precision for light winds is not expected to unduly influence the outcome of the modeling for ground-level fogging, however, because such fogging effects require plume touchdown and would typically be associated with high wind conditions.

Given the length of time of the data used in the SACTI analysis, the data used are considered representative of the climatic conditions of the project area where plume formation can occur. Even with this representative data set, short-term variability in conditions can affect the prediction of cooling tower plume impacts. Therefore, the results of the analysis are considered an indicator of likely occurrence and not an absolute predictor of events.

Modeling Results

Cooling Tower

The SACTI model was applied to simulate plumes from the proposed cooling towers using the

¹Argonne National Laboratory, 1984. Users Manual: Cooling-Tower -Plume Prediction Code. Prepared for Electric Power Research Institute, 3412 Hillview Avenue, Palo Alto, CA 9404, EPRI CS-3403-CCM, April, 1984.

five (5) year meteorological data set and tower design characteristics described below. Default options were assumed for the input variables controlling the model's operation. The five (5) year data set was input into SACTI to produce a five (5) year average frequency distribution for condensed plume length, condensed plume height, plume shadowing, and ground-level fogging. Although the model provides information on plume shadowing and drift deposition, the focus of our analysis and the discussion that follows is on visible plume dimensions and ground based fogging.

Table 1. Cooling Tower Input Parameters

Parameter	Value
Type	linear mechanical draft 1 tower, 5 cells
Heat Dissipation Rate (MW)	190
Circulation Rate (gpm)	32,500
Total Tower Air Flow (kg/s)	1262 – 1300
Max Drift Rate (%)	0.0005
Salt Concentration (gm/gm)	2.03E-3
Orientation	One banks of 5 in-line cells aligned east to west
Height (m)	12.2
Equivalent Total Cell Diameter (m)	20.4
Exit Velocity & Temperature	variable, calculated by the model assuming saturation conditions

Conditions favoring a long condensed plume occur more frequently in the fall and winter seasons, as atmospheric conditions, such as lower air temperature and higher relative humidity, are more favorable during these periods for plume formation. Also, plume formation tends to occur more frequently during night-time hours and during adverse weather conditions. Since EME has committed to a lighting plan that minimizes illumination, cooling tower plumes would not be visible at night. Unless illuminated by on-site sources, the cooling tower plumes would not be visible. The SACTI meteorological data set was therefore modified by removing all nocturnal hours, which accounted for 50 percent of all the hours in the five (5) year data set. In addition, daytime observations with fog, precipitation, visibility less than 3 miles, or ceiling heights less than 500 feet were excluded from the meteorological data set as, under these conditions, a visible plume from the cooling tower would be obscured by these local weather phenomena. For the Ontario meteorological data set, these adverse weather conditions account

for 8.8 percent of the total valid (daylight hours) observations. Table 2 summarizes these statistics.

Table 2	Total hours	Day hours	Night Hours Removed from Analysis	Limited Visibility Hours Removed from Analysis	Total Hours Modeled With SACTI
Year					
2001	3275	1522	1753	156	1366
2002	8578	4295	4283	315	3680
2003	8607	4332	4275	259	4073
2004	8630	4320	4310	501	3819
2005	8659	4361	4293	423	3938

Thus, the five (5) year meteorological data set was modified by removing both night-time hours and hours with weather obscuring phenomena. In total, these conditions accounted for 54 percent of all the hours (day, night, and obscuring weather) in the data set. The SACTI was then applied to the remaining data to assess the potential for the formation of cooling tower plumes under daytime conditions when a condensed plume would most likely also be a visible plume. Of particular interest was the analysis of visible plume formation during the months when formation of larger and more visible plumes is most likely, namely the fall and winter seasons. The occurrence of low temperatures coupled with high(er) relative humidity occurs with a greater frequency during these seasons. Plume formation is favored during these types of low temperature/high humidity conditions because, under these conditions, the ability of the atmosphere to absorb water vapor is greatly reduced, as the air mass is at or near saturation.

The results of the cooling tower analysis are summarized in Attachments 1-5 for the tower for the annual and seasonal seasons. The attachments present the frequency distributions of one of the primary model output variables, namely plume length and height, which are depicted by downwind sector and radial distance from the center of the cooling tower array.

Cooling Tower Plume Formation

The SACTI results are summarized below on an annual basis, and for each of the four seasons. The annual summary values indicate that the majority of visible plumes will be less than 300 meters (984 feet) in length. Modeling results indicate that, based on total hours, plume formation will occur 20 percent of the time during valid visible hours at locations up to 2000 meters from the site. Larger downwind visible plume lengths are possible and are predicted during the spring and winter seasons, but the downwind visible plume length will be less than 400 meters (1300 feet) for 62 percent of all the hours where a visible plume will form. SACTI also predicts that the visible plume height will average 175 meters, and have a median radius of 40 meters (131 feet) on an annual basis. For the winter season, the average plume length (when visible) will be longer, at 325 meters (1066 feet). For winter, SACTI predicts an average visible plume height of 175 meters with a median radius of 45 meters, similar to the annual averages.

The level of visibility of the modeled plumes was also assessed, based upon the opacity of the predicted visible plumes. SACTI does not directly calculate plume opacity, but it does calculate the total hours of cooling tower plume shadowing. Assuming that a plume with sufficient

opacity will cause a shadow, the modeling shows that plumes with enough opacity to cause shadowing would be longer than 60 meters less than 20 percent of the time on an annual basis. Thus, a majority of the plumes that do form will not be opaque enough to cause shadowing at distances beyond 60 meters and most plumes that do form at distances greater than 60 meters could have less opacity such that ground shadowing would occur on a less frequent basis.

TABLE 3 Seasonal Plume Characteristics from SACTI

	<i>Annual</i>	<i>Winter</i>	<i>Spring</i>	<i>Summer</i>	<i>Fall</i>
Plume Characteristics (meters)					
Median Length	300	325	400	250	250
Median Height	175	175	200	150	150
Median Radius	40	45	45	35	40
Limit of Shadowing ^a	60	100	25	150	50

a- 80% of visible plumes

Ground level fogging

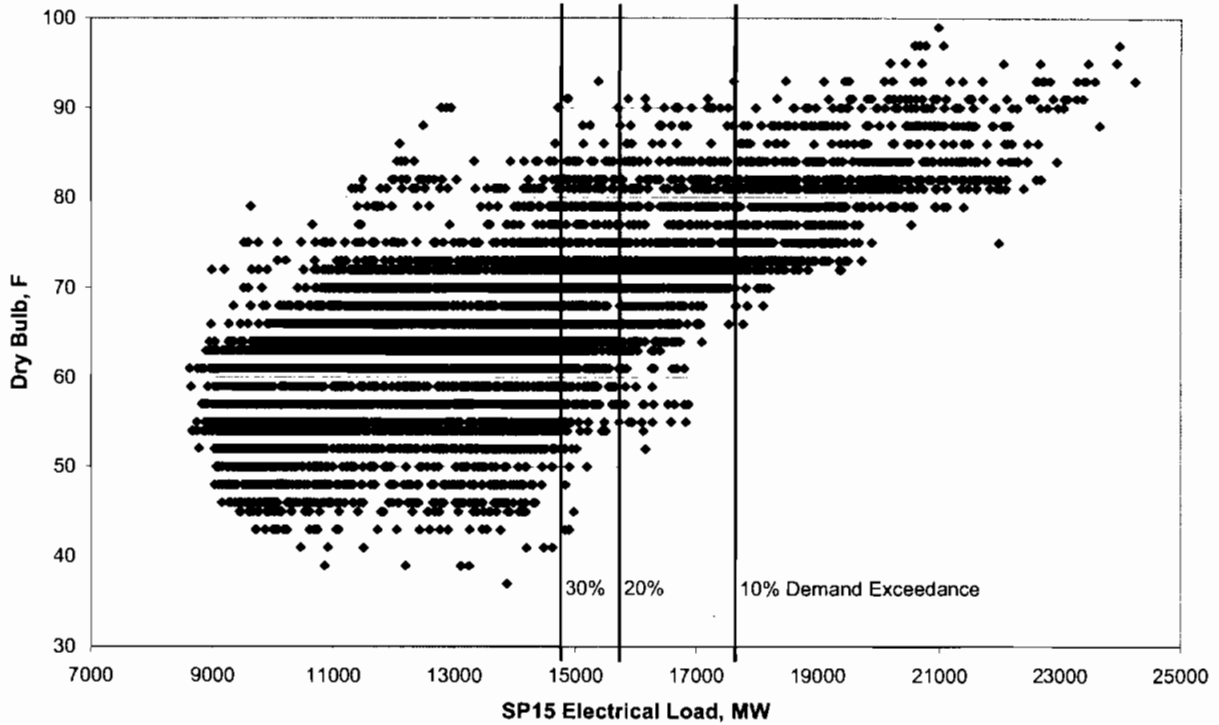
The potential for ground-level fogging on nearby areas was also assessed with SACTI. Potential fogging conditions can occur when atmospheric conditions allow the cooling tower plume to generate a cloud that contacts the ground. This can occur under periods of high humidity or high wind speed and favorable temperatures and stabilities with the fog being nucleated or generated by the cooling tower plume. Should fog be generated across a highway or other thoroughfare, it may become a potential hazard, and mitigation measures such as signs and traffic assistance may be needed. In order for fogging to affect roadway operations, the cooling tower plume must touchdown on the road surface and be condensed. This requires high winds (low plume rise), the right wind direction, low dew-point depression, and low temperatures.

SACTI was run with all hours of the five (5) year data base, including nighttime and low-visibility hours. There were no hours of predicted fogging from the cooling tower, considering all wind directions and all hours. Thus, the potential for fogging is nearly zero.

Project Operation

The SACTI model was modified to produce an output listing of the meteorological conditions that produced a visible plume. The SACTI cooling tower plume modeling output shows that a visible plume generally only occurs when relative humidity exceeds 85 percent. In order to evaluate the likelihood of this atmospheric condition coinciding with plant operation, hourly electric load data from the California ISO for the SP15 zone (effectively SCE's and SDG&E's service area) for the period of November 2002 through October 2003 was obtained, and hourly weather data for Fullerton, CA for the same period was obtained. As one would expect, regional electrical loads are highest when dry bulb temperatures are highest due to air-conditioner use on hot summer days, as illustrated in the chart below.

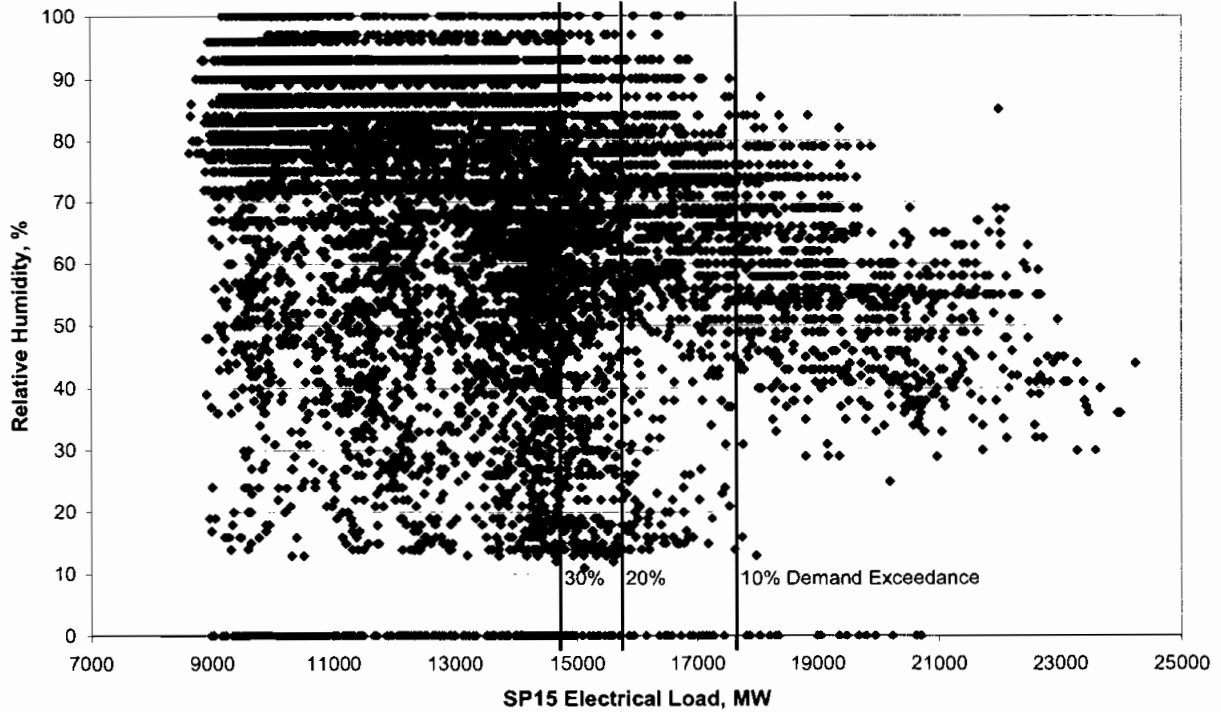
November 2002 - October 2003 Electrical Demand vs Weather Data for Fullerton, CA



The vertical red lines indicate the SP15 electrical loads that are exceeded 10 percent, 20 percent and 30 percent of the time (i.e., 10 percent, 20 percent and 30 percent of the data points are to the right of the respective lines). Although a peaking powerplant may occasionally be called on to run to alleviate a power grid emergency or unexpected outage of a baseload powerplant, almost all operation of peaking powerplants will be during the highest electrical loads.

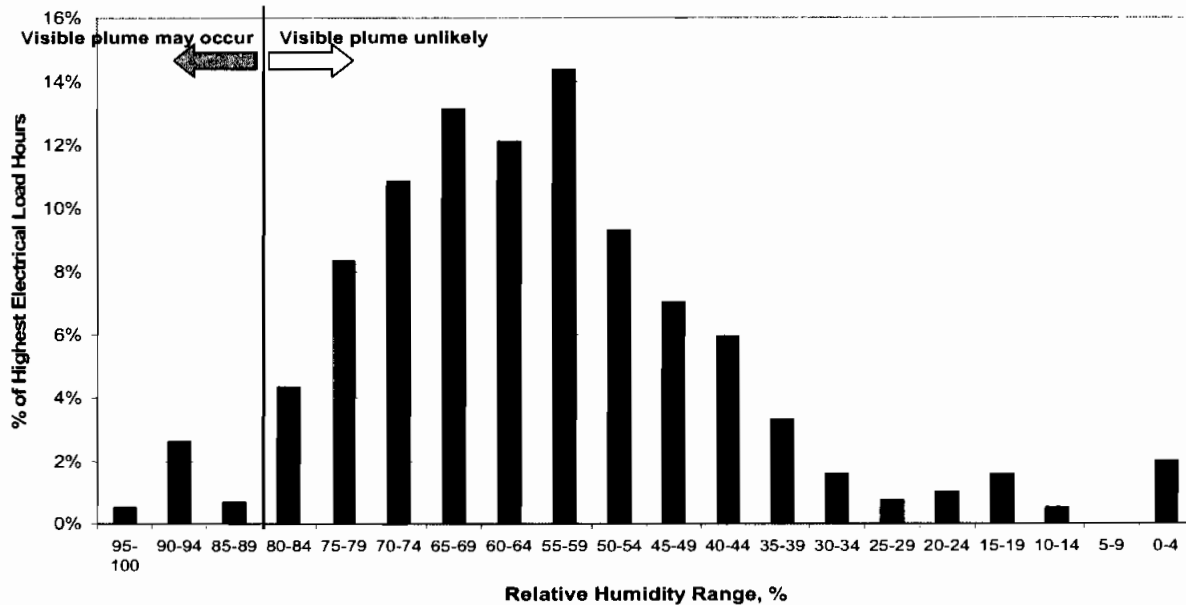
On hot summer days, as dry bulb temperatures (and corresponding electrical loads) increase to afternoon peaks, relative humidity naturally decreases due to the increased moisture-holding ability of the warmer air. It would be expected, then, that high electrical loads would correlate negatively with high relative humidity. The chart below is a plot of the same electrical loads as those in the preceding chart, but versus the relative humidity prevailing at the time of those loads, and illustrates the expected negative correlation.

November 2002 - October 2003 Electrical Demand vs Weather Data for Fullerton, CA



The chart below is a frequency distribution of the relative humidity during the hours corresponding to the highest 20 percent of electrical loads. Relative humidity only exceeds the 85 percent level at which visible plume may occur during one percent of the hours in which the highest 20 percent of electrical loads occurred during the one year period for which data was obtained. Expressed as a percent of the entire year, one percent of 20 percent of the year is an incidence of less than 0.2 percent.

Relative Humidity for Fullerton, CA During Top 20% Electrical Loads, Nov. 02 - Oct. 03



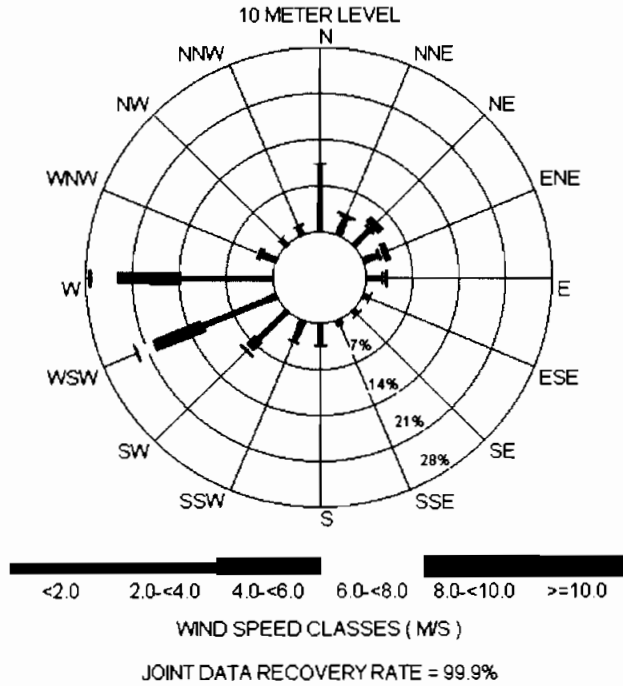
Summary

A cooling tower modeling analysis was conducted using SACTI and five (5) years of Ontario Airport meteorological data. Since there is no realistic method to run the model during the hours of typical peaker plant operation, all daylight/non-rain hours were included in the analysis, which thereby assumes that the project would be in operation at all times. With this highly unlikely profile, modeling results indicate that plume formation could result 20 percent of the time during valid, visible hours—justly barely meeting the CEC’s previously established significance criteria for base-loaded power projects. However, this result would require that the WCEP peaker operate during 100% of the daylight hours—historically unprecedented for peaking power project. As described in the AFC, the WCEP is expected to have an annual capacity factor of 30 percent. Even if the project operated during 50% of the daylight hours, this would reduce the predicted plume formation to 10 percent of the time during valid, visible hours, well below the CEC’s 20 percent criteria for potential significance. Moreover, the previous section, Project Operation, provides a detailed analysis based on real operational experience and predicted the vastly reduced incidence of 0.8 percent of the year for operation during the highest 20% of electrical loads when the relative humidity exceed 85%.

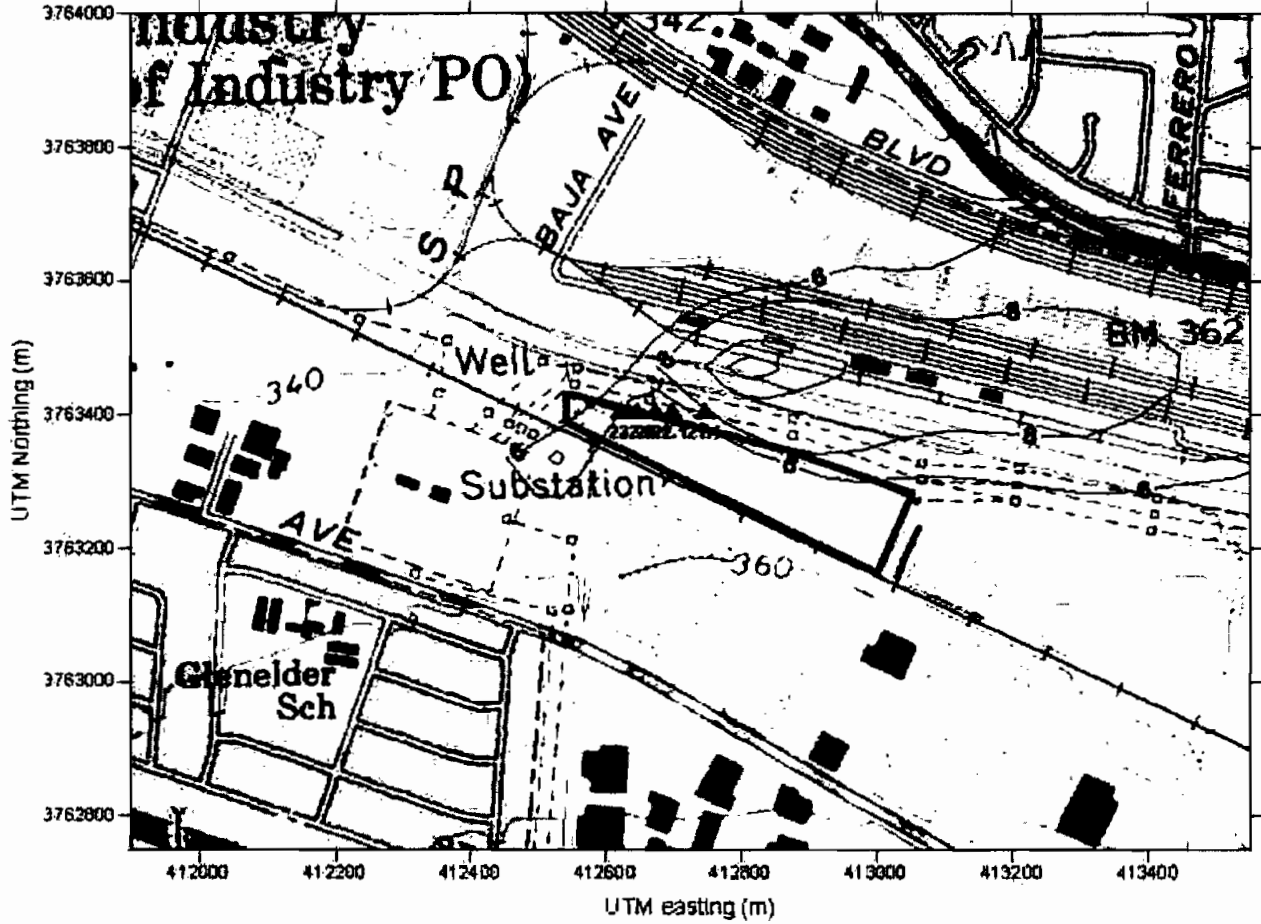
Model simulations also indicate that when plumes are visible, they are more likely not to have enough opacity to cause a ground-based shadow. Thus, the plume may not have enough opacity to be considered a significant visual plume. No plume fogging is predicted to occur in the general vicinity of the project site.

Figure 1
Annual Wind Rose (2001-2005)
Ontario, CA Airport

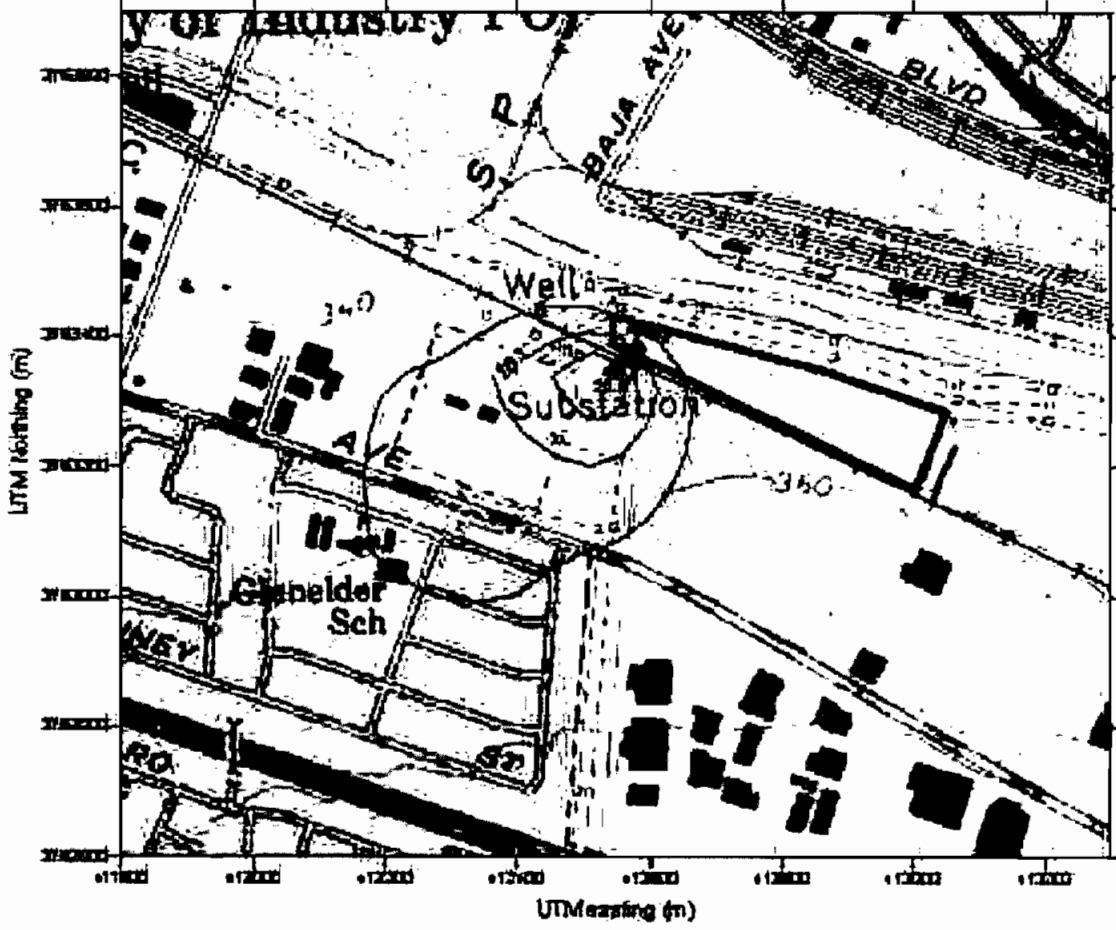
ontario DATA CA
 AIR QUALITY MONITORING SITE
 JANUARY 1, 2001 THRU DECEMBER 31, 2005 FOR HOURS 0.00 THRU 23.00



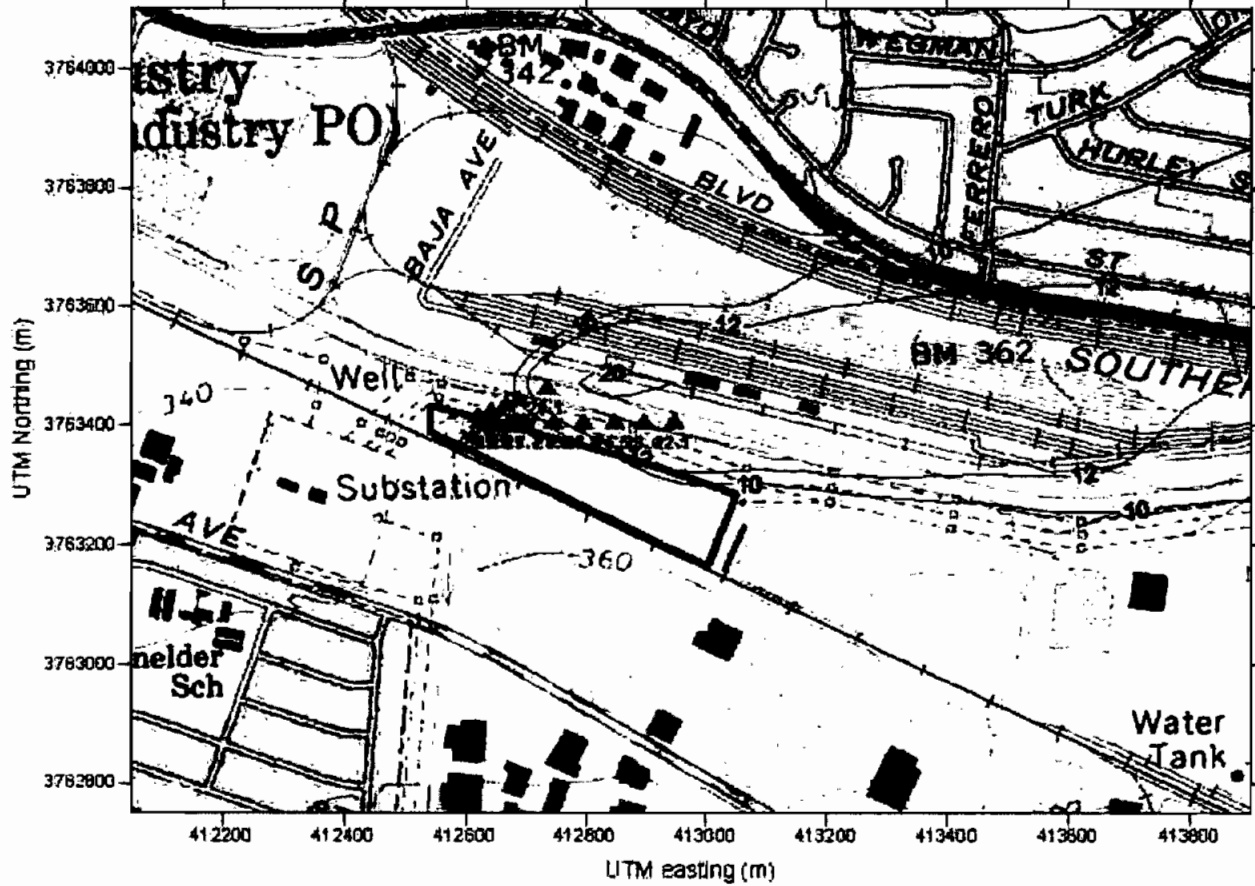
Walnut Creek Cooling Tower
Plume Modeling Analyses
PLUME LENGTH
% Hours/Annual (Good Visible Hrs)
Using Ontario, CA Met data
RED = 20% or more



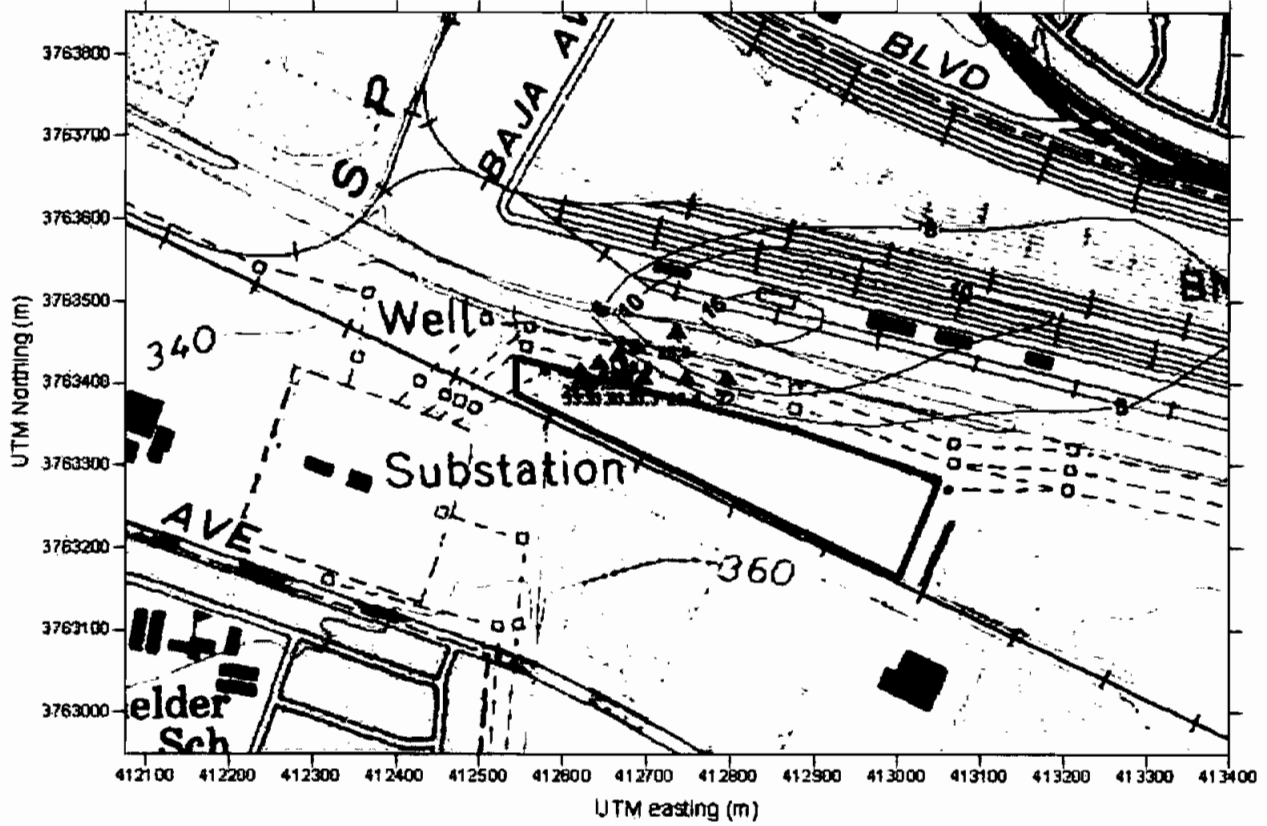
Without Desk Cooling Tower
Plume Modeling Analyses
PLUME LENGTH
% Hours/Year (Good Visible Hrs)
Using Ontario, CA Met data
RED = 20% or more



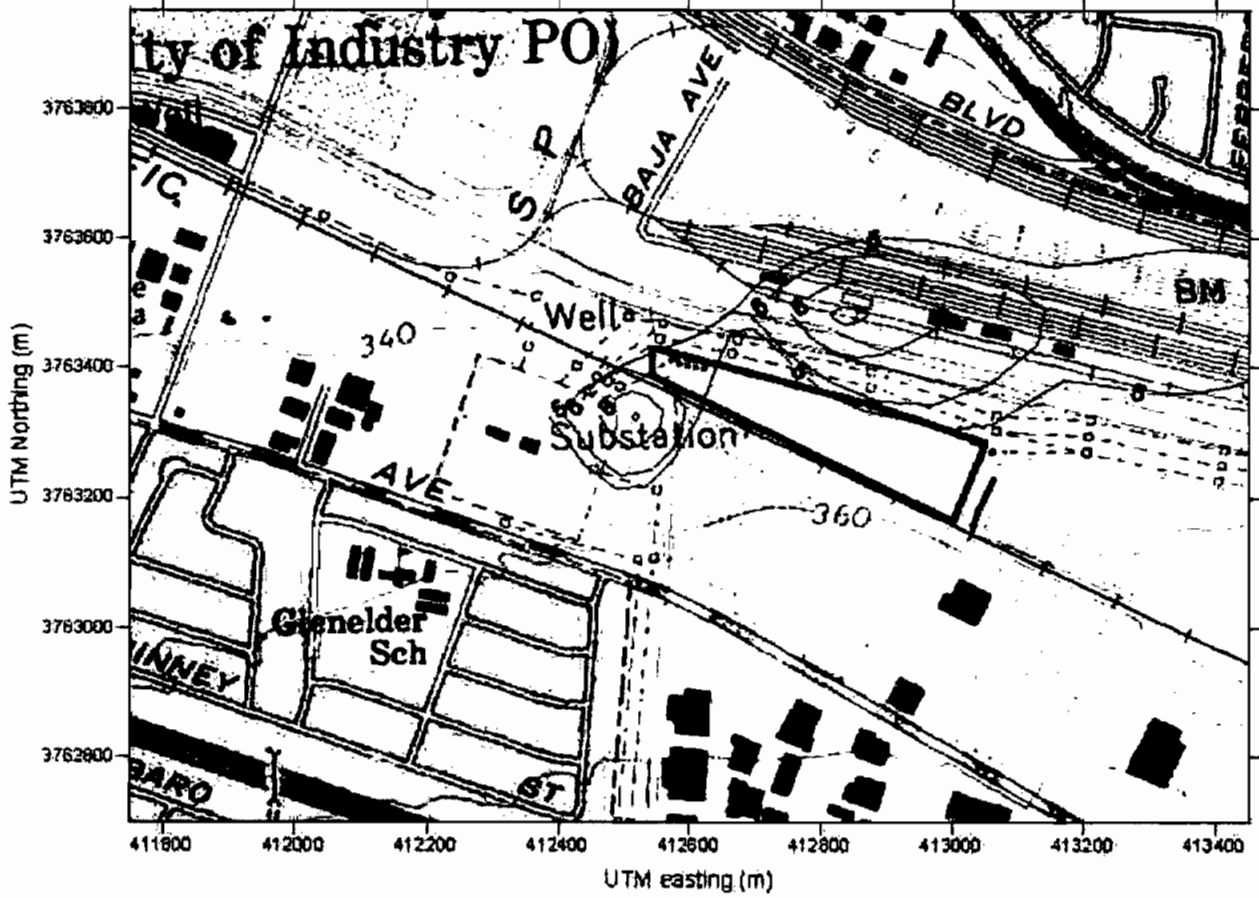
Walnut Creek Cooling Tower
Plume Modeling Analysis
PLUME LENGTH
% Hours/Spring (Good Visible Hrs)
Using Ontario, CA Met data
RED = 20% or more



Walnut Creek Cooling Tower
Plume Modeling Analyses
PLUME LENGTH
% Hours/Summer (Good Visible Hrs)
Using Ontario, CA Met data
RED = 20% or more



Walnut Creek Cooling Tower
Plume Modeling Analyses
PLUME LENGTH
% Hours/Fail (Good Visible Hrs)
Using Ontario, CA Met data
RED = 20% or more





SECRET

Visual Resources

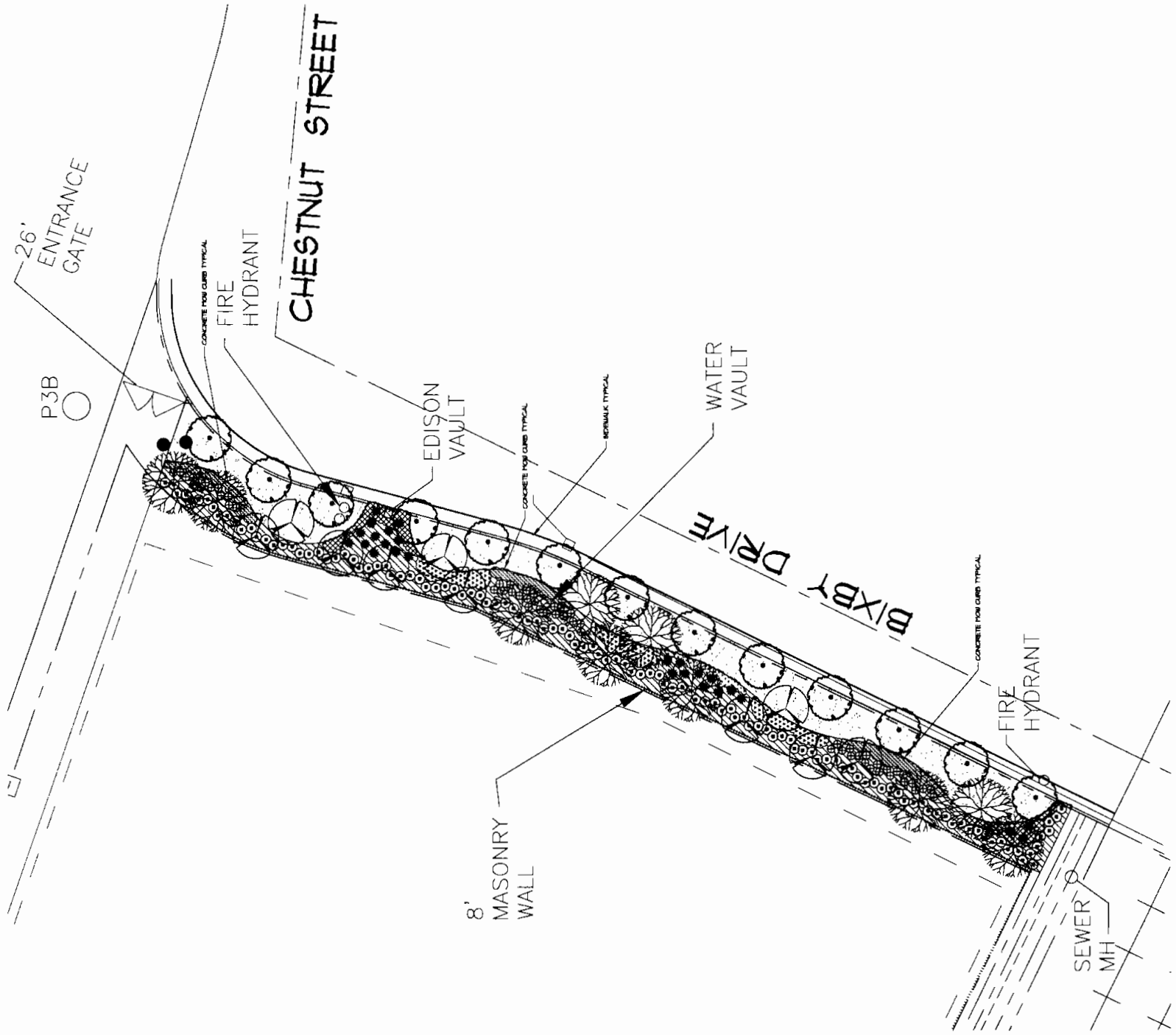
Landscape and Irrigation Plan

DR91. Please provide a landscape and irrigation plan that contains all the components required by the City.

Response: The landscape and irrigation plans are included as Attachment VIS-1.

Attachment VIS-1

Landscape and Irrigation Plans



PLANT LEGEND

TREES	BOTANICAL	COMMON	SIZE	QTY
	PLATANUS SPINOSA (VERTICAL EVERGREEN TREE)	LETOX IDENTIFIED QRT	14" BOX	3
	ULMUS ELAENAGUS (VERTICAL EVERGREEN BUTTER TREE)	ELDMORGA PINE	14" BOX	10
	PLATANUS ACERIFOLIA (DECIDUOUS VERTICAL TREE)	LORDEX PLANE STYLANDER	8 GAL	10

SHRUBS	BOTANICAL	COMMON	SIZE	QTY
	NANDINA DOMESTICA	NEW ZEALAND FLAX	9 GAL	24
	PHOTINIA	PHOTINIA	9 GAL	10
	NANDINA DOMESTICA	NANDINA	9 GAL	36

GROUND COVER	BOTANICAL	COMMON	SIZE	SPACING
	HEPEROCALLIS HYBRID	DATELY	1 GAL	TRIANGULAR SPACE BY OC
	LANTANA MONTEVIDENSIS	TRAINING LANTANA FOR PINK AND WHITE	1 GAL	TRIANGULAR SPACE BY OC
	NANDINA DOMESTICA	DWARF NANDINA	1 GAL	TRIANGULAR SPACE BY OC
	TULBAGHIA VIOLACEA	VARIEGATED SOCIETY GARLIC	1 GAL	TRIANGULAR SPACE BY OC
	NANDINA DOMESTICA	ROSEMARY	PLANT	TRIANGULAR SPACE BY OC
	HEPEROCALLIS HYBRID	HAWAIIAN HYDRANGEA 0 LBS / 1000 SF	PLANT	TRIANGULAR SPACE BY OC

NOTE:
 1. ALL PLANTS ARE TO BE PLANTED IN ALL PLANTERS.
 2. ALL PLANTS ARE TO BE PLANTED IN ALL PLANTERS.
 3. PLANTING SHALL BE IN ACCORDANCE WITH THE CITY OF SAN JOSE PLANTING SPECIFICATIONS.

MULCH NOTE:
 1. ALL PLANTERS SHALL BE MULCHED WITH 2" OF MULCH.
 2. MULCH SHALL BE APPLIED TO ALL PLANTERS.
 3. MULCH SHALL BE APPLIED TO ALL PLANTERS.

WATER USAGE CALCULATIONS

WATER (THE MAXIMUM APPLIED WATER ALLOWANCE) = (1.0 PLANT FACTOR) / (0.017) (CONVERSION FACTOR TO GALLONS)
 WWA = 54.5 x 8 x 113.78 SF x 82 = 331,402 GAL/YR
 ESTIMATED WATER USAGE
 EWU (THE ESTIMATED WATER USAGE) = (1.0 PLANT FACTOR) / (0.017) (CONVERSION FACTOR TO GALLONS)
 EWU = 54.5 x 8 x 113.78 SF x 82 = 331,402 GAL/YR
 TOTAL = 331,402 GAL/YR



SHEET TITLE: PLANTING PLAN
 PROJECT NAME: EDISON MISSION ENERGY
 DRAWN BY: BPK
 DATE: 7/21/06
 JOB NO.: CH2MHILL
 SHEET NO.: L-3
 OF 6 SHEETS

CH2MHILL
 Lockwood Greene
 Irvine, CA

ENVIRON, INC.
 LANDSCAPE ARCHITECTURE
 224 W. Foothill Blvd., Suite 7
 Claremont, CA 91711

WALNUT CREEK ENERGY PARK • CITY OF INDUSTRY, CA

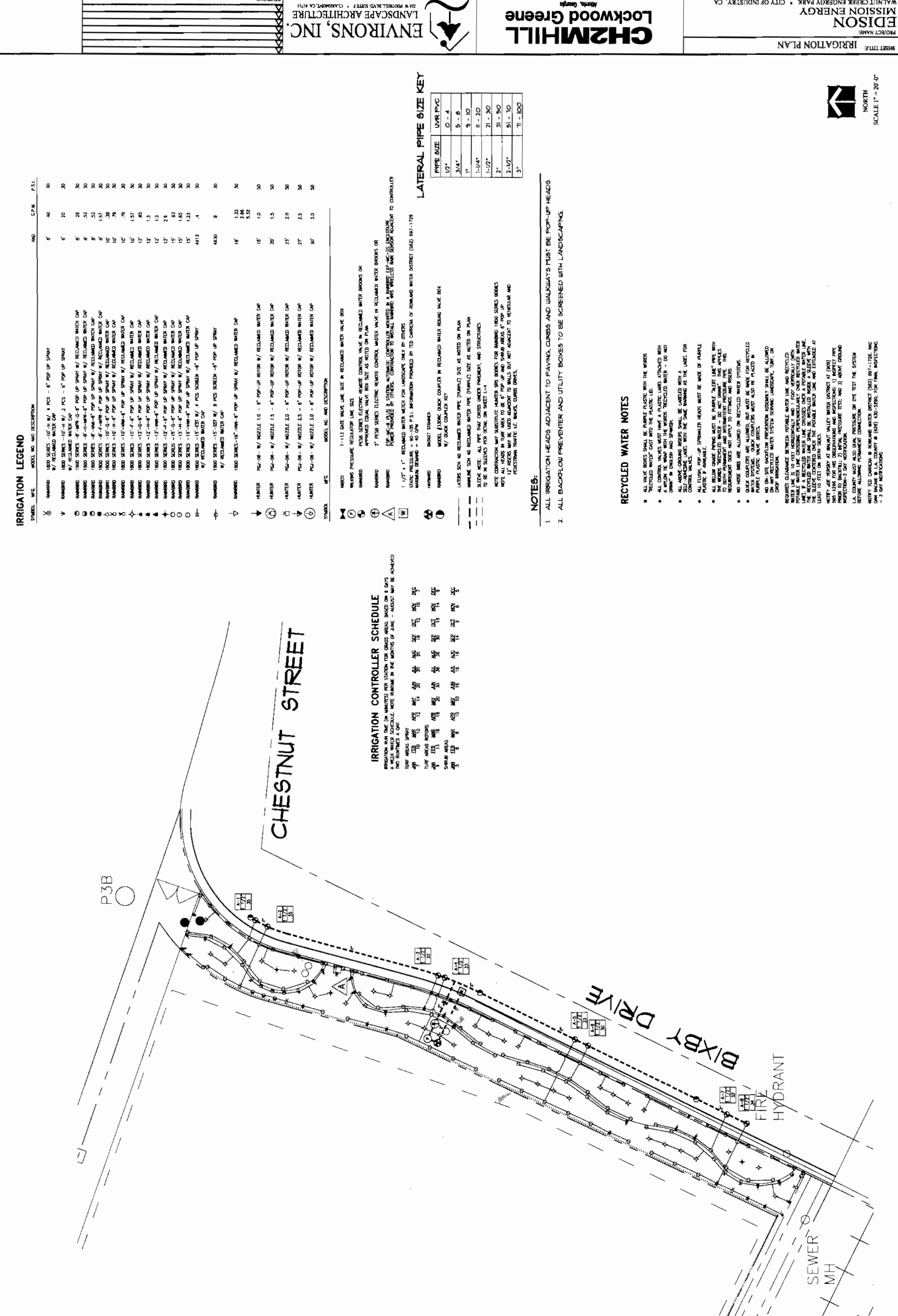
IRRIGATION LEGEND

SYMBOL	W.P.	MODEL NO. AND DESCRIPTION	REQ.	Q.P.M.	P.S.I.
⊙	1800	1800 SERIES - 10"-11" W/ 4 PCS - 8" POP UP SPRAY W/ RECLAIMED WATER CAP	8	40	30
⊙	1800	1800 SERIES - 10"-11" W/ 3 PCS - 8" POP UP SPRAY W/ RECLAIMED WATER CAP	8	20	30
⊙	1800	1800 SERIES - 8"-10" W/ 4 PCS - 8" POP UP SPRAY W/ RECLAIMED WATER CAP	8	20	30
⊙	1800	1800 SERIES - 8"-10" W/ 3 PCS - 8" POP UP SPRAY W/ RECLAIMED WATER CAP	8	20	30
⊙	1800	1800 SERIES - 6"-8" W/ 4 PCS - 8" POP UP SPRAY W/ RECLAIMED WATER CAP	8	20	30
⊙	1800	1800 SERIES - 6"-8" W/ 3 PCS - 8" POP UP SPRAY W/ RECLAIMED WATER CAP	8	20	30
⊙	1800	1800 SERIES - 4"-6" W/ 4 PCS - 8" POP UP SPRAY W/ RECLAIMED WATER CAP	10	20	30
⊙	1800	1800 SERIES - 4"-6" W/ 3 PCS - 8" POP UP SPRAY W/ RECLAIMED WATER CAP	10	20	30
⊙	1800	1800 SERIES - 3"-4" W/ 4 PCS - 8" POP UP SPRAY W/ RECLAIMED WATER CAP	10	20	30
⊙	1800	1800 SERIES - 3"-4" W/ 3 PCS - 8" POP UP SPRAY W/ RECLAIMED WATER CAP	10	20	30
⊙	1800	1800 SERIES - 2"-3" W/ 4 PCS - 8" POP UP SPRAY W/ RECLAIMED WATER CAP	12	20	30
⊙	1800	1800 SERIES - 2"-3" W/ 3 PCS - 8" POP UP SPRAY W/ RECLAIMED WATER CAP	12	20	30
⊙	1800	1800 SERIES - 1.5"-2" W/ 4 PCS - 8" POP UP SPRAY W/ RECLAIMED WATER CAP	12	1.5	30
⊙	1800	1800 SERIES - 1.5"-2" W/ 3 PCS - 8" POP UP SPRAY W/ RECLAIMED WATER CAP	12	1.5	30
⊙	1800	1800 SERIES - 1.0"-1.5" W/ 4 PCS - 8" POP UP SPRAY W/ RECLAIMED WATER CAP	15	1.5	30
⊙	1800	1800 SERIES - 1.0"-1.5" W/ 3 PCS - 8" POP UP SPRAY W/ RECLAIMED WATER CAP	15	1.5	30
⊙	1800	1800 SERIES - 0.75"-1.0" W/ 4 PCS - 8" POP UP SPRAY W/ RECLAIMED WATER CAP	15	1.5	30
⊙	1800	1800 SERIES - 0.75"-1.0" W/ 3 PCS - 8" POP UP SPRAY W/ RECLAIMED WATER CAP	15	1.5	30
⊙	1800	1800 SERIES - 0.5"-0.75" W/ 4 PCS - 8" POP UP SPRAY W/ RECLAIMED WATER CAP	15	1.5	30
⊙	1800	1800 SERIES - 0.5"-0.75" W/ 3 PCS - 8" POP UP SPRAY W/ RECLAIMED WATER CAP	15	1.5	30
⊙	1800	1800 SERIES - 0.25"-0.5" W/ 4 PCS - 8" POP UP SPRAY W/ RECLAIMED WATER CAP	4812	1.4	30
⊙	1800	1800 SERIES - 0.25"-0.5" W/ 3 PCS - 8" POP UP SPRAY W/ RECLAIMED WATER CAP	4812	1.4	30
⊙	1800	1800 SERIES - 1.5"-2.0" W/ 8 PCS SCREEN - 8" POP UP SPRAY W/ RECLAIMED WATER CAP	4820	8	30
⊙	1800	1800 SERIES - 1.5"-2.0" W/ 6 PCS SCREEN - 8" POP UP SPRAY W/ RECLAIMED WATER CAP	18	1.5	30
⊙	1800	1800 SERIES - 1.5"-2.0" W/ 4 PCS SCREEN - 8" POP UP SPRAY W/ RECLAIMED WATER CAP	18	1.5	30
⊙	1800	1800 SERIES - 1.5"-2.0" W/ 2 PCS SCREEN - 8" POP UP SPRAY W/ RECLAIMED WATER CAP	18	1.5	30
⊙	1800	1800 SERIES - 1.5"-2.0" W/ 1 PCS SCREEN - 8" POP UP SPRAY W/ RECLAIMED WATER CAP	20	1.5	30
⊙	1800	1800 SERIES - 1.5"-2.0" W/ 0 PCS SCREEN - 8" POP UP SPRAY W/ RECLAIMED WATER CAP	25	2.0	30
⊙	1800	1800 SERIES - 1.5"-2.0" W/ 0 PCS SCREEN - 8" POP UP SPRAY W/ RECLAIMED WATER CAP	27	2.5	30
⊙	1800	1800 SERIES - 1.5"-2.0" W/ 0 PCS SCREEN - 8" POP UP SPRAY W/ RECLAIMED WATER CAP	30	3.0	30

IRRIGATION CONTROLLER SCHEDULE

PROVIDE THE (IN UNITS) P.S.I. STATION FOR EACH AREA BASED ON 8 DAYS A WEEK SCHEDULE. NOTE: RUNNING IN THE MONTHS OF JUNE - AUGUST MAY BE ADJUSTED BY THE USER.

AREA	1	2	3	4	5	6	7	8	9	10	11	12
1	1.5	1.5	1.5	1.5	1.5	1.5	1.5	1.5	1.5	1.5	1.5	1.5
2	1.5	1.5	1.5	1.5	1.5	1.5	1.5	1.5	1.5	1.5	1.5	1.5
3	1.5	1.5	1.5	1.5	1.5	1.5	1.5	1.5	1.5	1.5	1.5	1.5
4	1.5	1.5	1.5	1.5	1.5	1.5	1.5	1.5	1.5	1.5	1.5	1.5
5	1.5	1.5	1.5	1.5	1.5	1.5	1.5	1.5	1.5	1.5	1.5	1.5
6	1.5	1.5	1.5	1.5	1.5	1.5	1.5	1.5	1.5	1.5	1.5	1.5
7	1.5	1.5	1.5	1.5	1.5	1.5	1.5	1.5	1.5	1.5	1.5	1.5
8	1.5	1.5	1.5	1.5	1.5	1.5	1.5	1.5	1.5	1.5	1.5	1.5
9	1.5	1.5	1.5	1.5	1.5	1.5	1.5	1.5	1.5	1.5	1.5	1.5
10	1.5	1.5	1.5	1.5	1.5	1.5	1.5	1.5	1.5	1.5	1.5	1.5
11	1.5	1.5	1.5	1.5	1.5	1.5	1.5	1.5	1.5	1.5	1.5	1.5
12	1.5	1.5	1.5	1.5	1.5	1.5	1.5	1.5	1.5	1.5	1.5	1.5



LATERAL PIPE SIZE KEY

PIPE SIZE	UNITS PVC
1/2"	0 - 4
3/4"	5 - 9
1"	9 - 10
1-1/4"	11 - 20
1-1/2"	21 - 30
2"	31 - 90
2-1/2"	91 - 110
3"	11 - 100

NOTES:

1. ALL IRRIGATION HEADS ADJACENT TO FAYNS, CURBS AND WALKWAYS MUST BE POP-UP HEADS
2. ALL BACKFLOW PREVENTER AND UTILITY BOXES TO BE SCREENED WITH LANDSCAPING.

RECYCLED WATER NOTES

- ALL VALVE BOXES SHALL BE POLYPROPYLENE WITH THE WORDS "RECYCLED WATER" CAST INTO THE PLASTIC LID.
- ALL CONTROL VALVES MUST HAVE A PLASTIC LABEL ATTACHED WITH THE WORDS "RECYCLED WATER" IN ENGLISH AND SPANISH.
- ALL ABOVE-GROUND PIPES SHALL BE LABELED WITH A SELF-ADHESIVE LABEL WITH THE SAME WORDING AS THE LABEL FOR POLYPROPYLENE VALVE BOXES.
- ALL BELOW-GROUND PIPES MUST BE MADE OF POLYPROPYLENE PLASTIC & AVAILABLE.
- ALL BELOW-GROUND PIPING MUST BE PURPLE "NIGHT LINE" PIPE WITH THE WORDS "RECYCLED WATER" AND "RECYCLED WATER" IN ENGLISH AND SPANISH. THE REQUIREMENT DOES NOT APPLY TO FITTINGS AND JOINTS.
- NO HOSE LINES ARE ALLOWED ON RECYCLED WATER SYSTEMS.
- QUICK COUPLERS ARE ALLOWED, BUT MUST BE MADE FOR RECYCLED WATER. ALL QUICK COUPLERS MUST ALSO BE PLACED IN PURPLE PLASTIC VALVE BOXES.
- NO ON-SITE BACKFLOW PREVENTION ASSEMBLY SHALL BE ALLOWED ON ANY RECYCLED WATER SYSTEM SERVING LANDSCAPE, TURF, OR OTHER RECREATIONAL PURPOSES. RECYCLED WATER USE AND RECYCLED WATER LINE CROSSING JURISDICTIONS SHALL BE INSTALLED WITHIN THE RECYCLED WATER LINE SHALL BE INSTALLED INSIDE A SLEEVE WITH A LABEL IDENTIFYING THE RECYCLED WATER LINE AND EXTENDED AT LEAST 10 FEET BEYOND THE JURISDICTION.
- VERIFY ALL WORK AT RECYCLED WATER DISTRICT (RWD) 697-1726 AND 505-1256 FOR THE OBSERVATIONS AND INSPECTIONS: 1) INSPECT PIPE INSTALLATION AND JOINTS; 2) PRESSURE TEST; AND 3) ABOVE-GROUND INSPECTIONS SHALL BE PERFORMED.
- L.A. COUNTY MUST ALSO OBTAIN PRESSURE OR DYE TEST THE SYSTEM BEFORE ALLOWING PERMANENT CONNECTION.
- NOTIFY THE CARSON & SOUTHWEST WATER DISTRICT (CSW) 697-1726 AND DUM BROWN & S.A. COUNTY @ (818) 430-3306 FOR FINAL INSPECTIONS - 7 DAY NOTIFICATION.

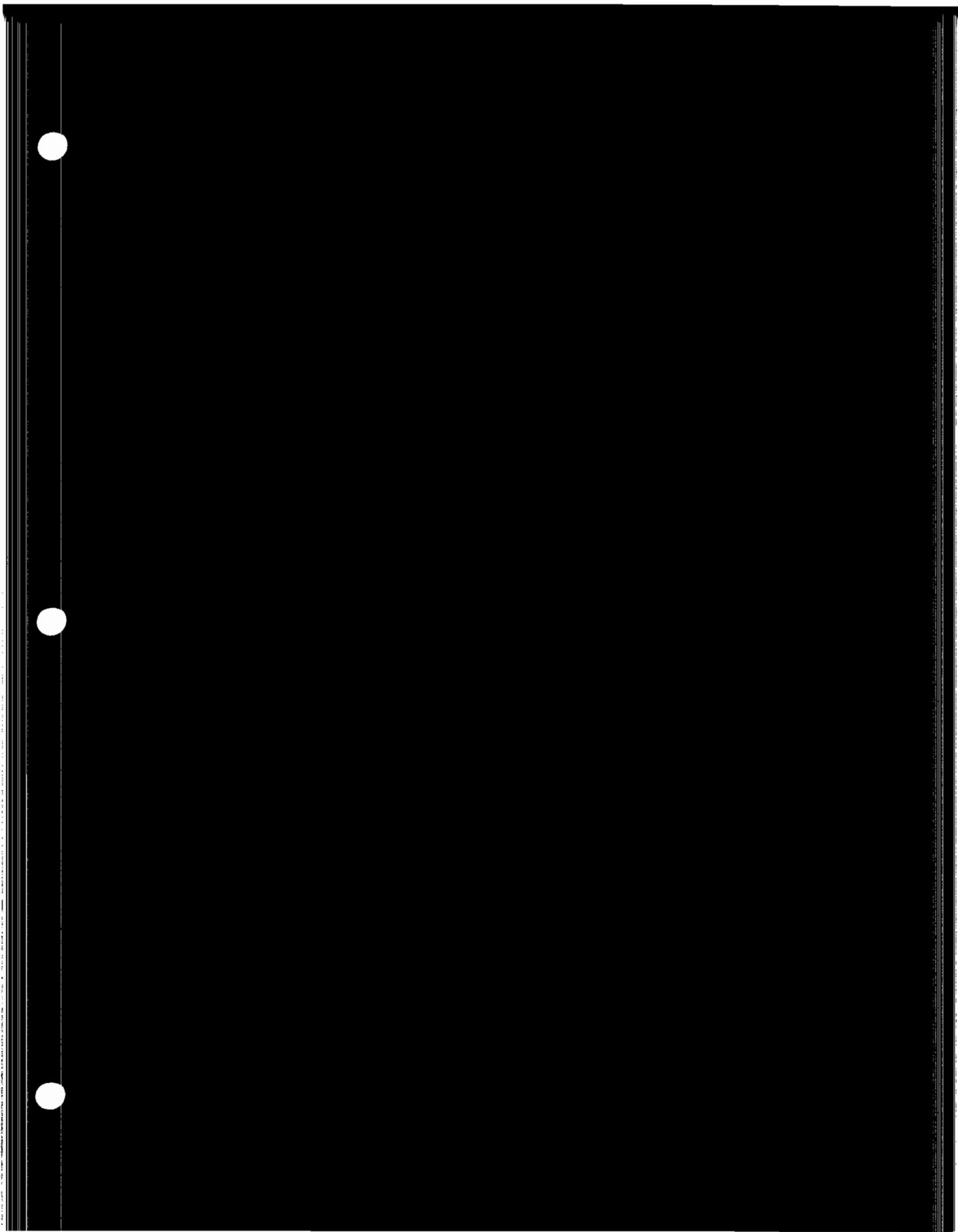
ENVIRONS, INC.
LANDSCAPE ARCHITECTURE
25 W. FOOTBLD BLDG 5000 S. CLAYMONT, CA 91711

CH2MHILL
Lockwood Greene
Atlanta, Georgia

PROJECT NAME: IRRIGATION PLAN
SHEET TITLE: IRRIGATION PLAN
EDISON MISSION ENERGY
WALNUT CREEK ENERGY PARK • CITY OF INDUSTRY, CA

DRAWN BY: CH2MHILL
DATE: 7/21/06
JOB NO.: CH2MHILL
SHEET NO.: L-2
OF 6 SHEETS

SCALE 1" = 20'-0"
NORTH



BEFORE THE ENERGY RESOURCES CONSERVATION AND DEVELOPMENT COMMISSION
OF THE STATE OF CALIFORNIA

APPLICATION FOR CERTIFICATION
FOR THE WALNUT CREEK ENERGY PARK
(WCEP)

DOCKET No. 05-AFC-2

(Revised 2/23/06)

PROOF OF SERVICE LIST

DOCKET UNIT

Send the original signed document plus the required 12 copies to the address below:

CALIFORNIA ENERGY COMMISSION
DOCKET UNIT, MS-4
*Attn: Docket No. 05-AFC-2
1516 Ninth Street
Sacramento, CA 95814-5512
docket@energy.state.ca.us

* * * *

In addition to the documents sent to the Commission Docket Unit, also send individual copies of any documents to:

APPLICANT

Lawrence Kostrzewa, Project Director
Edison Mission Energy
18101 Von Karman Avenue, Suite 1700
Irvine, CA 92612-1046
lkostrzewa@EdisonMission.Com

Douglas Davy
CH2M Hill
2485 Natomas Park Drive, Suite 600
Sacramento, CA 95833
ddavy@ch2m.com

*Jenifer Morris
NJ Resources, LLC
7240 Heil Avenue
Huntington Beach, CA 92647
jenifer@njr.net

*Thomas McCabe
Edison Mission Energy
18101 Von Karman Ave., Suite 1700
Irvine, CA 92612-1046
tmccabe@edisonmission.com

**Revisions to POS List, i.e. updates, additions and/or deletions
WALNUT CREEK ENERGY PARK DOCKET NO.05-AFC-2*

COUNSEL FOR APPLICANT

Scott Galati
Galati & Blek, LLP
555 Capitol Mall, Suite 600
Sacramento, CA 95814
sgalati@gb-llp.com

INTERESTED AGENCIES

No agencies to date.

INTERVENORS

***California Unions for Reliable
Energy (CURE)
C/O Marc D. Joseph
Gloria D. Smith
Adams Broadwell Joseph & Cardozo
601 Gateway Boulevard, Suite 1000
South San Francisco, CA 94080
mdjoseph@adamsbroadwell.com
gsmith@adamsbroadwell.com**

DECLARATION OF SERVICE

I, Jeannette Harris, declare that on November 13, 2006, I deposited copies of the attached Supplement IV in Response to Data Requests and Workshop Queries in Support of the Application for Certification for the Walnut Creek Energy Park (05-AFC-02) in the United States mail at Sacramento, CA with first class postage thereon fully prepaid and addressed to those identified on the Proof of Service list above. Transmission via electronic mail was consistent with the requirements of California Code of Regulations, title 20, sections 1209, 1209.5, and 1210. I declare under penalty of perjury that the foregoing is true and correct.


[signature]