DOCKETED	
Docket Number:	23-OPT-02
Project Title:	Darden Clean Energy Project
TN #:	254675
Document Title:	Data Response Set 1 Appendix A - Geotechnical Report Vol 1 Part 2
Description:	Volume 1 Part 2 of the geotechnical report provided in response to DR GEO-1 as part of Appendix A of Response Set 1.
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Organization:	Rincon Consultants
Submitter Role:	Applicant Consultant
Submission Date:	2/23/2024 5:09:26 PM
Docketed Date:	2/26/2024

Data Response Set 1 - Appendix A

DR GEO-1 Geotechnical Engineering Report - Volume 1, Part 2

Terracon
23041 Avenida De La Carlota
Ste 350
Laguna Hills, CA

Boring Log No. B-99

Graphic Log	Location: See Exploration Plan Depth (Ft.)	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	EXPANSION INDEX	Water Content (%)	Dry Unit Weight (pcf)	Atterberg Limits LL-PL-PI	Percent Fines
	LEAN CLAY WITH SAND (CL), brown			✋						
	2.5									
	LEAN CLAY (CL), trace sand, very stiff			⧗	6-11-14		20.2	100		
	4.0									
	CLAYEY SAND (SC), brown			✋						
	medium dense	5		⊠	5-5-7 N=12					
	7.5									
	LEAN CLAY (CL), trace sand, brown, very stiff			⧗	10-13-14		21.1	95		
	medium stiff	10		⊠	3-3-4 N=7					
	stiff	15		⊠	3-6-7 N=13					
	medium stiff	20		⊠	3-2-3 N=5					
	21.5									
	Boring Terminated at 21.5 Feet									

See Exploration and Testing Procedures for a description of field and laboratory procedures used and additional data (If any).

See Supporting Information for explanation of symbols and abbreviations.

Notes

Water Level Observations
Groundwater not encountered

Advancement Method
Hollow Stem Auger

Abandonment Method
Boring backfilled with bentonite slurry and auger cuttings upon completion.

Drill Rig
CME 75 (track)

Hammer Type
Automatic

Driller
CalPac Drilling

Logged by
AT

Boring Started
01-24-2023

Boring Completed
01-24-2023

Darden Solar Facility
Cantua Creek | Fresno, CA
Terracon Project No. 60225172

Terracon
23041 Avenida De La Carlota
Ste 350
Laguna Hills, CA

Boring Log No. B-100

Graphic Log	Location: See Exploration Plan Depth (Ft.)	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	EXPANSION INDEX	Water Content (%)	Dry Unit Weight (pcf)	Atterberg Limits LL-PL-PI	Percent Fines
▨	**LEAN CLAY WITH SAND (CL)**, brown									
				✋						74
	very stiff			☒	10-11-13 N=24					
	4.0									
▨	**LEAN CLAY (CL)**, trace sand, brown									
				✋						
	stiff	5		⧗	6-8-8		21.9	80		
	medium stiff			☒	3-3-3 N=6					91
	stiff	10		⧗	3-6-11		33.8	84		
		15		☒	3-3-6 N=9					
		20		☒	5-7-6 N=13					
	21.5									
	Boring Terminated at 21.5 Feet									

See Exploration and Testing Procedures for a description of field and laboratory procedures used and additional data (If any).

See Supporting Information for explanation of symbols and abbreviations.

Notes

Water Level Observations
Groundwater not encountered

Advancement Method
Hollow Stem Auger

Abandonment Method
Boring backfilled with bentonite slurry and auger cuttings upon completion.

Drill Rig
CME 75 (track)

Hammer Type
Automatic

Driller
CalPac Drilling

Logged by
AT

Boring Started
01-25-2023

Boring Completed
01-25-2023

Terracon
23041 Avenida De La Carlota
Ste 350
Laguna Hills, CA

Boring Log No. B-101

Graphic Log	Location: See Exploration Plan Depth (Ft.)	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	EXPANSION INDEX	Water Content (%)	Dry Unit Weight (pcf)	Atterberg Limits LL-PL-PI	Percent Fines
▨	**LEAN CLAY WITH SAND (CL)**, brown									
				✋						76
	very stiff			⧗	12-12-12		17.4	97		
	4.0									
▨	**LEAN CLAY (CL)**, trace sand, brown									
	very stiff	5		✋ ☒	5-12-16 N=28					
				⧗	4-8-11		23.1	95		
	stiff	10		☒	3-3-6 N=9					
	stiff	15		☒	3-5-5 N=10					
	soft to medium stiff	20		☒	1-2-2 N=4					
	21.5									
	Boring Terminated at 21.5 Feet									

See Exploration and Testing Procedures for a description of field and laboratory procedures used and additional data (If any).

See Supporting Information for explanation of symbols and abbreviations.

Notes

Water Level Observations
Groundwater not encountered

Advancement Method
Hollow Stem Auger

Abandonment Method
Boring backfilled with bentonite slurry and auger cuttings upon completion.

Drill Rig
CME 75 (track)

Hammer Type
Automatic

Driller
CalPac Drilling

Logged by
AT

Boring Started
01-25-2023

Boring Completed
01-25-2023

Darden Solar Facility
Cantua Creek | Fresno, CA
Terracon Project No. 60225172

23041 Avenida De La Carlota
Ste 350
Laguna Hills, CA

Boring Log No. B-102

Graphic Log	Location: See Exploration Plan Depth (Ft.)	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	EXPANSION INDEX	Water Content (%)	Dry Unit Weight (pcf)	Atterberg Limits LL-PL-PI	Percent Fines
	LEAN CLAY WITH SAND (CL), brown									
	stiff				6-10-8					
	5.0									
	LEAN CLAY (CL), trace sand, brown, stiff	5			2-5-6 N=11					
	7.5									
	FAT CLAY (CH), dark brown, stiff				3-5-8		22.1	91		
	medium stiff	10			2-2-4 N=6					
		15			1-2-3 N=5					
		20	▽		1-1-4 N=5					
	21.5									
	Boring Terminated at 21.5 Feet									

See Exploration and Testing Procedures for a description of field and laboratory procedures used and additional data (If any).

See Supporting Information for explanation of symbols and abbreviations.

Water Level Observations
▽

Drill Rig
Diedrich D-50 (track)

Hammer Type
Automatic

Driller
Terracon

Logged by
AH

Boring Started
04-05-2023

Boring Completed
04-05-2023

Notes

Advancement Method
Hallow Stem Auger

Abandonment Method
Boring backfilled with bentonite slurry and auger cuttings upon completion.

23041 Avenida De La Carlota
Ste 350
Laguna Hills, CA

Boring Log No. B-103

Graphic Log	Location: See Exploration Plan Depth (Ft.)	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	EXPANSION INDEX	Water Content (%)	Dry Unit Weight (pcf)	Atterberg Limits LL-PL-PI	Percent Fines
▨	**LEAN CLAY (CL)**, dark brown									
▨				✋						
▨	very stiff			⧗	7-9-11		13.3	106		
▨	5.0			✋						
🟩	**FAT CLAY (CH)**, dark browm, medium stiff to stiff	5		☒	1-3-5 N=8 .5 (HP)					
🟩	stiff			⧗	3-5-9 3 (HP)		31.7	82		
🟩	sandy, soft to medium stiff	10		☒	1-2-2 N=4 1 (HP)					
🟩		15		☒	1-1-3 N=4					
🟩	20.0		▽							
🟨	**POORLY GRADED SAND (SP)**, very loose	20		☒	0-1-2 N=3					
🟨	21.5									
	Boring Terminated at 21.5 Feet									

See Exploration and Testing Procedures for a description of field and laboratory procedures used and additional data (If any).

See Supporting Information for explanation of symbols and abbreviations.

Notes

Water Level Observations
▽ While drilling

Advancement Method
Hallow Stem Auger

Abandonment Method
Boring backfilled with bentonite slurry and auger cuttings upon completion.

Drill Rig
Diedrich D-50 (track)

Hammer Type
Automatic

Driller
Terracon

Logged by
AH

Boring Started
04-06-2023

Boring Completed
04-06-2023

Boring Log No. B-104

Graphic Log	Location: See Exploration Plan Depth (Ft.)	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	EXPANSION INDEX	Water Content (%)	Dry Unit Weight (pcf)	Atterberg Limits LL-PL-PI	Percent Fines
▨	**LEAN CLAY WITH SAND (CL)**, brown									
				✋			15.7			81
	very stiff			☒	11-11-14 N=25					
▨	4.0 **LEAN CLAY (CL)**, trace sand, brown									
	very stiff			✋						
		5		⧗	4-8-11		27.2	85		
	stiff			☒	5-7-7 N=14					
		10		⧗	4-6-9		17.0	101		
	medium stiff	15		☒	2-2-3 N=5					
▨	20.0 **CLAYEY SAND (SC)**, brown, loose	20	▽	☒	5-4-5 N=9					
	21.5 ***Boring Terminated at 21.5 Feet***									

See Exploration and Testing Procedures for a description of field and laboratory procedures used and additional data (If any).

See Supporting Information for explanation of symbols and abbreviations.

Notes

Water Level Observations
▽ While drilling

Advancement Method
Hollow Stem Auger

Abandonment Method
Boring backfilled with bentonite slurry and auger cuttings upon completion.

Drill Rig
CME 75 (track)

Hammer Type
Automatic

Driller
CalPac Drilling

Logged by
AT

Boring Started
01-25-2023

Boring Completed
01-25-2023

Terracon
23041 Avenida De La Carlota
Ste 350
Laguna Hills, CA

Boring Log No. B-105

Location: See Exploration Plan

Graphic Log	Depth (Ft.) / Description	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	EXPANSION INDEX	Water Content (%)	Dry Unit Weight (pcf)	Atterberg Limits LL-PL-PI	Percent Fines
▨	**LEAN CLAY WITH SAND (CL)**, light brown									
▨				✋						
▨	stiff			⧗	5-6-6		15.5	88		
▨	5.0									
▨	**FAT CLAY (CH)**, brown, stiff	5		✋ ☒	2-3-6 N=9 1.5 (HP)					
▨				⧗	2-8-8 1 (HP)		28.8	85		
▨	soft to medium stiff	10		☒	1-2-2 N=4					
▨	medium stiff	15		☒	0-2-4 N=6					
▨	soft	20		☒	0-1-2 N=3 1.5 (HP)					
▨	21.5									
	Boring Terminated at 21.5 Feet									

See Exploration and Testing Procedures for a description of field and laboratory procedures used and additional data (If any).

See Supporting Information for explanation of symbols and abbreviations.

Notes

Water Level Observations
Groundwater not encountered

Advancement Method
Hallow stem Auger

Abandonment Method
Boring backfilled with bentonite slurry and auger cuttings upon completion.

Drill Rig
Diedrich D-50 (track)

Hammer Type
Automatic

Driller
Terracon

Logged by
AH

Boring Started
04-06-2023

Boring Completed
04-06-2023

Terracon
23041 Avenida De La Carlota
Ste 350
Laguna Hills, CA

Boring Log No. B-106

Graphic Log	Location: See Exploration Plan Depth (Ft.)	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	EXPANSION INDEX	Water Content (%)	Dry Unit Weight (pcf)	Atterberg Limits LL-PL-PI	Percent Fines
▨	**LEAN CLAY (CL)**, trace sand, brown									
▨	medium stiff			☒	1-2-3 N=5				44-15-29	89
▨		5		⧗	2-3-3		25.2	89		
▨	dark brown			☒	2-3-4 N=7					
▨	stiff	10		⧗	2-5-6		23.1	96		
▨			▽							
▨	soft to medium stiff	15		☒	1-2-2 N=4					
▨	20.0 **CLAYEY SAND (SC)**, light brown, very loose 21.5	20		☒	0-1-1 N=2					
	Boring Terminated at 21.5 Feet									

See Exploration and Testing Procedures for a description of field and laboratory procedures used and additional data (If any).

See Supporting Information for explanation of symbols and abbreviations.

Notes

Water Level Observations
▽

Advancement Method
Hollow Stem Auger

Abandonment Method
Boring backfilled with bentonite slurry and auger cuttings upon completion.

Drill Rig
Diedrich D-50 (track)

Hammer Type
Automatic

Driller
Terracon

Logged by
JB

Boring Started
04-13-2023

Boring Completed
04-13-2023

Terracon
23041 Avenida De La Carlota
Ste 350
Laguna Hills, CA

Boring Log No. B-107

Graphic Log	Location: See Exploration Plan Depth (Ft.)	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	EXPANSION INDEX	Water Content (%)	Dry Unit Weight (pcf)	Atterberg Limits LL-PL-PI	Percent Fines
▨	**SANDY LEAN CLAY (CL)**, brown									
				✋					42-15-27	57
	very stiff			⧗	13-18-19		7.8	100		
	4.0									
▨	**LEAN CLAY (CL)**, trace sand, brown									
	very stiff	5		✋ ☒	6-8-10 N=18					
	very stiff			⧗	6-6-10		31.9	85		
	stiff	10		☒	2-3-6 N=9					
	medium stiff	15		☒	3-3-3 N=6					
	soft	20		☒	2-1-1 N=2					
	21.5									
	Boring Terminated at 21.5 Feet									

See Exploration and Testing Procedures for a description of field and laboratory procedures used and additional data (If any).

See Supporting Information for explanation of symbols and abbreviations.

Notes

Water Level Observations
Groundwater not encountered

Advancement Method
Hollow Stem Auger

Abandonment Method
Boring backfilled with bentonite slurry and auger cuttings upon completion.

Drill Rig
CME 75 (track)

Hammer Type
Automatic

Driller
CalPac Drilling

Logged by
AT

Boring Started
01-26-2023

Boring Completed
01-26-2023

23041 Avenida De La Carlota
Ste 350
Laguna Hills, CA

Boring Log No. B-108

Graphic Log	Location: See Exploration Plan Depth (Ft.)	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	EXPANSION INDEX	Water Content (%)	Dry Unit Weight (pcf)	Atterberg Limits LL-PL-PI	Percent Fines
	LEAN CLAY (CL), light brown									
	stiff				2-3-6 N=9					
	brown	5			5-6-5		25.3	86		100
	very stiff				1-25-4 N=29					
	medium stiff	10			2-3-4		26.2	93		
			▽							
		15			1-2-3 N=5					
	20.0 **POORLY GRADED SAND WITH CLAY (SP-SC)**, loose	20			1-2-2 N=4					
	21.5 ***Boring Terminated at 21.5 Feet***									

See Exploration and Testing Procedures for a description of field and laboratory procedures used and additional data (If any).

See Supporting Information for explanation of symbols and abbreviations.

Notes

Water Level Observations
▽

Advancement Method
Hollow Stem Auger

Abandonment Method
Boring backfilled with bentonite slurry and auger cuttings upon completion.

Drill Rig
Diedrich D-50 (track)

Hammer Type
Automatic

Driller
Terracon

Logged by
JB

Boring Started
04-13-2023

Boring Completed
04-13-2023

Darden Solar Facility
Cantua Creek | Fresno, CA
Terracon Project No. 60225172

Terracon
23041 Avenida De La Carlota
Ste 350
Laguna Hills, CA

Boring Log No. B-109

Graphic Log	Location: See Exploration Plan Depth (Ft.)	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	EXPANSION INDEX	Water Content (%)	Dry Unit Weight (pcf)	Atterberg Limits LL-PL-PI	Percent Fines
▨	**LEAN CLAY (CL)**, trace sand, light brown									
▨	stiff			⧗	2-7-7		21.6	92		92
▨	medium stiff	5		✋ ⧖	2-3-3 N=6					
▨	very stiff			⧗	5-10-11		23.4	100		
▨	medium stiff	10		⧖	1-3-3 N=6					
▨	soft	15		⧖	1-1-1 N=2					
▨			▽							
▨	20.0	20								
▨	**POORLY GRADED SAND WITH CLAY (SP-SC)**, very loose			⧖	1-1-1 N=2					
	21.5									
	Boring Terminated at 21.5 Feet									

See Exploration and Testing Procedures for a description of field and laboratory procedures used and additional data (If any).

See Supporting Information for explanation of symbols and abbreviations.

Notes

Water Level Observations
▽

Advancement Method
Hollow Stem Auger

Abandonment Method
Boring backfilled with bentonite slurry and auger cuttings upon completion.

Drill Rig
Diedrich D-50 (track)

Hammer Type
Automatic

Driller
Terracon

Logged by
JB

Boring Started
04-13-2023

Boring Completed
04-13-2023

Darden Solar Facility
Cantua Creek | Fresno, CA
Terracon Project No. 60225172

Terracon
23041 Avenida De La Carlota
Ste 350
Laguna Hills, CA

Boring Log No. B-110

Graphic Log	Location: See Exploration Plan Depth (Ft.)	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	EXPANSION INDEX	Water Content (%)	Dry Unit Weight (pcf)	Atterberg Limits LL-PL-PI	Percent Fines
▨	**LEAN CLAY (CL)**, trace sand, brown									
▨				✋						
▨	very stiff			☒	4-9-12 N=21					
▨		5		✋						
▨				⧗	6-8-11		23.4	93		
▨	medium stiff			☒	3-3-4 N=7					
▨	very stiff	10		⧗	4-8-12		18.3	100		
▨	stiff	15		☒	2-4-6 N=10					
▨	20.0									
▩	**CLAYEY SAND (SC)**, brown, medium dense	20		☒	4-5-11 N=16					
▩	21.5									
	Boring Terminated at 21.5 Feet									

See Exploration and Testing Procedures for a description of field and laboratory procedures used and additional data (If any).

See Supporting Information for explanation of symbols and abbreviations.

Notes

Water Level Observations
Groundwater not encountered

Advancement Method
Hollow Stem Auger

Abandonment Method
Boring backfilled with bentonite slurry and auger cuttings upon completion.

Drill Rig
CME 75 (track)

Hammer Type
Automatic

Driller
CalPac Drilling

Logged by
AT

Boring Started
01-25-2023

Boring Completed
01-25-2023

Boring Log No. B-111

Location: See Exploration Plan

Graphic Log	Depth (Ft.)	Description	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	EXPANSION INDEX	Water Content (%)	Dry Unit Weight (pcf)	Atterberg Limits LL-PL-PI	Percent Fines
▨		**SANDY SILT (ML)**, brown								NP	
		hard			✋						
					⧗	13-23-31		17.4	103		
▨	5.0	**SANDY LEAN CLAY (CL)**, brown, medium stiff to stiff	5		✋ ⊠	3-3-5 N=8					
		very stiff			⧗	5-8-12		20.5	95		
		stiff	10		⊠	3-4-8 N=12					
▨	15.0	**CLAYEY SAND (SC)**, brown, medium dense	15		⧗	3-10-17		7.9	97		
			20		⊠	2-2-8 N=10					13
	21.5	***Boring Terminated at 21.5 Feet***									

See Exploration and Testing Procedures for a description of field and laboratory procedures used and additional data (If any).

See Supporting Information for explanation of symbols and abbreviations.

Notes

Water Level Observations
Groundwater not encountered

Advancement Method
Hollow Stem Auger

Abandonment Method
Boring backfilled with bentonite slurry and auger cuttings upon completion.

Drill Rig
CME 75 (track)

Hammer Type
Automatic

Driller
CalPac Drilling

Logged by
AT

Boring Started
01-25-2023

Boring Completed
01-25-2023

Darden Solar Facility
Cantua Creek | Fresno, CA
Terracon Project No. 60225172

23041 Avenida De La Carlota
Ste 350
Laguna Hills, CA

Boring Log No. B-112

Graphic Log	Location: See Exploration Plan Depth (Ft.)	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	EXPANSION INDEX	Water Content (%)	Dry Unit Weight (pcf)	Atterberg Limits LL-PL-PI	Percent Fines
▨	**LEAN CLAY WITH SAND (CL)**, brown			✋						
	very stiff			☒	4-6-10 N=16					85
	stiff	5		✋ ⧗	5-5-8		24.3	88		
	medium stiff			☒	2-3-4 N=7					
	stiff	10		⧗	4-5-7		28.9	90		
		15		☒	3-4-5 N=9					
	soft to medium stiff	20		☒	2-2-2 N=4					
	21.5									
	Boring Terminated at 21.5 Feet									

See Exploration and Testing Procedures for a description of field and laboratory procedures used and additional data (If any).

See Supporting Information for explanation of symbols and abbreviations.

Notes

Water Level Observations
Groundwater not encountered

Advancement Method
Hollow Stem Auger

Abandonment Method
Boring backfilled with bentonite slurry and auger cuttings upon completion.

Drill Rig
CME 75 (track)

Hammer Type
Automatic

Driller
CalPac Drilling

Logged by
AT

Boring Started
01-25-2023

Boring Completed
01-25-2023

Darden Solar Facility
Cantua Creek | Fresno, CA
Terracon Project No. 60225172

23041 Avenida De La Carlota
Ste 350
Laguna Hills, CA

Boring Log No. B-113

Graphic Log	Location: See Exploration Plan Depth (Ft.)	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	EXPANSION INDEX	Water Content (%)	Dry Unit Weight (pcf)	Atterberg Limits LL-PL-PI	Percent Fines
▨	**SANDY LEAN CLAY (CL)**, brown			✋					42-15-27	66
▨	very stiff			⧗	6-9-10		16.6	101		
▨		5		✋ ☒	6-9-10 N=19					
▨	7.5									
▨	**LEAN CLAY (CL)**, trace sand, stiff			⧗	5-5-6		24.2	87		
▨	medium stiff	10		☒	2-2-3 N=5					
▨	soft to medium stiff	15		☒	2-2-2 N=4					
▨	very stiff	20		☒	4-6-7 N=13					
▨	21.5									
	Boring Terminated at 21.5 Feet									

See Exploration and Testing Procedures for a description of field and laboratory procedures used and additional data (If any).

See Supporting Information for explanation of symbols and abbreviations.

Notes

Water Level Observations
Groundwater not encountered

Advancement Method
Hollow Stem Auger

Abandonment Method
Boring backfilled with bentonite slurry and auger cuttings upon completion.

Drill Rig
CME 75 (track)

Hammer Type
Automatic

Driller
CalPac Drilling

Logged by
AT

Boring Started
01-26-2023

Boring Completed
01-26-2023

Boring Log No. B-114

Graphic Log	Location: See Exploration Plan Depth (Ft.)	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	EXPANSION INDEX	Water Content (%)	Dry Unit Weight (pcf)	Atterberg Limits LL-PL-PI	Percent Fines
▨	**LEAN CLAY (CL)**, brown			✋						
▨	2.5 **FAT CLAY (CH)**, bluish gray, stiff			☒	5-6-5 N=11					
				✋						
▨	5.0 **LEAN CLAY (CL)**, brown, very stiff	5		⧗	7-12-17					
	white veins, stiff			☒	3-4-6 N=10					
		10		⧗	4-5-5					
		15		☒	2-4-6 N=10					
			▽							
▨	20.0 **CLAYEY SAND (SC)**, brown, very loose 21.5	20		⧗	2-2-3		32.0	88		
	Boring Terminated at 21.5 Feet									

See Exploration and Testing Procedures for a description of field and laboratory procedures used and additional data (If any).

See Supporting Information for explanation of symbols and abbreviations.

Notes

Water Level Observations
▽ While drilling

Advancement Method
Hollow Stem Auger

Abandonment Method
Boring backfilled with bentonite slurry and auger cuttings upon completion.

Drill Rig
Diedrich D-50 (track)

Hammer Type
Automatic

Driller
Terracon

Logged by
DD

Boring Started
02-14-2023

Boring Completed
02-14-2023

Boring Log No. B-115

Graphic Log	Location: See Exploration Plan Depth (Ft.)	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	EXPANSION INDEX	Water Content (%)	Dry Unit Weight (pcf)	Atterberg Limits LL-PL-PI	Percent Fines
	CLAYEY SAND WITH GRAVEL (SC), brown									
	loose				5-7-9		4.2		37-20-17	27
	5.0 **FAT CLAY (CH)**, brown, medium stiff	5			3-3-4 N=7					
	very stiff				7-12-13		23.5	97		
	10.0 **LEAN CLAY (CL)**, brown, medium stiff	10			2-3-3 N=6					
	brownish gray with white veins	15			2-3-4 N=7					
	20.0 **POORLY GRADED SAND WITH CLAY (SP-SC)**, brownish gray, medium dense	20	▽		2-3-7 N=10					
	21.5 ***Boring Terminated at 21.5 Feet***									

See Exploration and Testing Procedures for a description of field and laboratory procedures used and additional data (If any).

See Supporting Information for explanation of symbols and abbreviations.

Notes

Water Level Observations
▽ While drilling

Advancement Method
Hollow Stem Auger

Abandonment Method
Boring backfilled with bentonite slurry and auger cuttings upon completion.

Drill Rig
Diedrich D-50 (track)

Hammer Type
Automatic

Driller
Terracon

Logged by
DD

Boring Started
02-14-2023

Boring Completed
02-14-2023

Boring Log No. B-116

Depth (Ft.)	Location: See Exploration Plan	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	EXPANSION INDEX	Water Content (%)	Dry Unit Weight (pcf)	Atterberg Limits LL-PL-PI	Percent Fines
	LEAN CLAY (CL), brown			✋			19.2			
	stiff			☒	4-4-5 N=9					
		5		✋ ⧗	8-8-9		18.4	103		
				☒	3-5-6 N=11					
11.5	very stiff	10		⧗	8-11-11		21.3	100		
	SILTY CLAYEY SAND (SC-SM), medium dense	15		☒	4-5-6 N=11				22-18-4	16
20.0			▽							
21.5	**LEAN CLAY (CL)**, brown, soft	20		☒	0-0-2 N=2					
	Boring Terminated at 21.5 Feet									

See Exploration and Testing Procedures for a description of field and laboratory procedures used and additional data (If any).

See Supporting Information for explanation of symbols and abbreviations.

Notes

Water Level Observations
▽ While drilling

Advancement Method
Hollow Stem Auger

Abandonment Method
Boring backfilled with bentonite slurry and auger cuttings upon completion.

Drill Rig
Diedrich D-50 (track)

Hammer Type
Automatic

Driller
Terracon

Logged by
DD

Boring Started
02-14-2023

Boring Completed
02-14-2023

Darden Solar Facility
Cantua Creek | Fresno, CA
Terracon Project No. 60225172

Terracon
23041 Avenida De La Carlota
Ste 350
Laguna Hills, CA

Boring Log No. B-117

Graphic Log	Location: See Exploration Plan Depth (Ft.)	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	EXPANSION INDEX	Water Content (%)	Dry Unit Weight (pcf)	Atterberg Limits LL-PL-PI	Percent Fines
▨	**FAT CLAY (CH)**, brown with white veins			✋						
▨	very stiff			⧗	4-16-25		16.5	104		
▨	5.0 **LEAN CLAY (CL)**, brown with white veins, stiff	5		✋ ☒	3-4-6 N=10					
▨	very stiff			⧗	4-7-12		30.1	94		
▨	10.0 **SANDY LEAN CLAY (CL)**, brown, medium stiff	10		☒	2-2-4 N=6				32-21-11	62
▨	stiff	15		☒	3-5-6 N=11					
▨	20.0 **SILT WITH SAND (ML)**, brown, soft to medium stiff	20	▽	☒	0-0-4 N=4					
	25.0	25								

See Exploration and Testing Procedures for a description of field and laboratory procedures used and additional data (If any).

See Supporting Information for explanation of symbols and abbreviations.

Notes

Water Level Observations
▽ While drilling

Advancement Method
Hollow Stem Auger

Abandonment Method
Boring backfilled with bentonite slurry and auger cuttings upon completion.

Drill Rig
Diedrich D-50 (track)

Hammer Type
Automatic

Driller
Terracon

Logged by
DD

Boring Started
02-14-2023

Boring Completed
02-14-2023

Terracon
23041 Avenida De La Carlota
Ste 350
Laguna Hills, CA

Boring Log No. B-117

Graphic Log	Location: See Exploration Plan Depth (Ft.)	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	EXPANSION INDEX	Water Content (%)	Dry Unit Weight (pcf)	Atterberg Limits LL-PL-PI	Percent Fines
▨	**POORLY GRADED SAND WITH CLAY (SP-SC)**, brown, medium dense			☒	2-5-6 N=11					
		30		☒	4-6-5 N=11					
▨	31.0 31.5 **LEAN CLAY (CL)**, brown, stiff									
	Boring Terminated at 31.5 Feet									

See Exploration and Testing Procedures for a description of field and laboratory procedures used and additional data (If any).

See Supporting Information for explanation of symbols and abbreviations.

Notes

Water Level Observations
▽ While drilling

Advancement Method
Hollow Stem Auger

Abandonment Method
Boring backfilled with bentonite slurry and auger cuttings upon completion.

Drill Rig
Diedrich D-50 (track)

Hammer Type
Automatic

Driller
Terracon

Logged by
DD

Boring Started
02-14-2023

Boring Completed
02-14-2023

Terracon
23041 Avenida De La Carlota
Ste 350
Laguna Hills, CA

Boring Log No. B-118

Graphic Log	Location: See Exploration Plan Depth (Ft.)	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	EXPANSION INDEX	Water Content (%)	Dry Unit Weight (pcf)	Atterberg Limits LL-PL-PI	Percent Fines
▨	**LEAN CLAY (CL)**, trace sand, brown									
▨	stiff			✋ ☒	3-5-7 N=12					
▨		5		✋ ⧗	4-7-8		27.7	92		
▨	medium stiff to stiff			☒	3-4-4 N=8					
▨	white veins, stiff	10		⧗	4-6-10		29.2	91	48-21-27	92
▨	medium stiff	15	▽	☒	4-3-3 N=6					
▨	soft	20		☒	1-1-2 N=3					
	21.5 ***Boring Terminated at 21.5 Feet***									

See Exploration and Testing Procedures for a description of field and laboratory procedures used and additional data (If any).

See Supporting Information for explanation of symbols and abbreviations.

Notes

Water Level Observations
▽ While drilling

Advancement Method
Hollow Stem Auger

Abandonment Method
Boring backfilled with bentonite slurry and auger cuttings upon completion.

Drill Rig
Diedrich D-50 (track)

Hammer Type
Automatic

Driller
Terracon

Logged by
DD

Boring Started
02-15-2023

Boring Completed
02-15-2023

Darden Solar Facility
Cantua Creek | Fresno, CA
Terracon Project No. 60225172

23041 Avenida De La Carlota
Ste 350
Laguna Hills, CA

Boring Log No. B-119

Graphic Log	Location: See Exploration Plan Depth (Ft.)	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	EXPANSION INDEX	Water Content (%)	Dry Unit Weight (pcf)	Atterberg Limits LL-PL-PI	Percent Fines
▨	**LEAN CLAY (CL)**, brown									
▨	soft to medium stiff			✋ ☒	0-0-4 N=4				46-18-28	
▨	stiff	5		✋ ⧗	5-7-9		27.1	89		
▨	trace fine grained sand, soft			☒	1-1-2 N=3					
▨	10.0 **CLAYEY SAND (SC)**, brown, loose	10		⧗	2-3-7		27.1	95		26
▨			▽							
▨	15.0 **FAT CLAY (CH)**, brown, stiff	15		☒	3-4-5 N=9					
▨	20.0 **LEAN CLAY (CL)**, brown, medium stiff	20		☒	3-2-4 N=6					
▨	21.5									
	Boring Terminated at 21.5 Feet									

See Exploration and Testing Procedures for a description of field and laboratory procedures used and additional data (If any).

See Supporting Information for explanation of symbols and abbreviations.

Notes

Water Level Observations
▽ While drilling

Advancement Method
Hollow Stem Auger

Abandonment Method
Boring backfilled with bentonite slurry and auger cuttings upon completion.

Drill Rig
Diedrich D-50 (track)

Hammer Type
Automatic

Driller
Terracon

Logged by
DD

Boring Started
02-15-2023

Boring Completed
02-15-2023

Terracon
23041 Avenida De La Carlota
Ste 350
Laguna Hills, CA

Boring Log No. B-120

Graphic Log	Location: See Exploration Plan Depth (Ft.)	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	EXPANSION INDEX	Water Content (%)	Dry Unit Weight (pcf)	Atterberg Limits LL-PL-PI	Percent Fines
▨	**LEAN CLAY (CL)**, brown			✋						
	medium stiff to stiff			☒	2-3-5 N=8					
	stiff	5		✋ ⧗	5-7-9		28.9	87		
▨	7.5 **SANDY LEAN CLAY (CL)**, brown, soft to medium stiff			☒	3-2-2 N=4					61
	stiff	10		⧗	4-5-8		17.6	101		
▨	15.0 **FAT CLAY (CH)**, brown, medium stiff to stiff	15	▽	☒	3-5-3 N=8					
▨	20.0 **LEAN CLAY (CL)**, brown, medium stiff	20		☒	0-4-3 N=7					
	21.5 ***Boring Terminated at 21.5 Feet***									

See Exploration and Testing Procedures for a description of field and laboratory procedures used and additional data (If any).

See Supporting Information for explanation of symbols and abbreviations.

Notes

Water Level Observations
▽ While drilling

Advancement Method
Hollow Stem Auger

Abandonment Method
Boring backfilled with bentonite slurry and auger cuttings upon completion.

Drill Rig
Diedrich D-50 (track)

Hammer Type
Automatic

Driller
Terracon

Logged by
DD

Boring Started
02-15-2023

Boring Completed
02-15-2023

Boring Log No. B-121

Graphic Log	Location: See Exploration Plan Depth (Ft.)	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	EXPANSION INDEX	Water Content (%)	Dry Unit Weight (pcf)	Atterberg Limits LL-PL-PI	Percent Fines
▨	**FAT CLAY (CH)**, brown			✋					65-20-45	
▨	very stiff			⧗	6-8-11		24.9	83		
▨	stiff	5		✋						
▨				☒	4-4-7 N=11					
▨				⧗	4-5-5		28.3	80		
▨	10.0 **LEAN CLAY (CL)**, brown with white veins, soft to medium stiff	10		☒	0-0-4 N=4					
▨	15.0 **FAT CLAY (CH)**, brown, medium stiff	15	▽	☒	0-2-3 N=5					
▨	20.0 **LEAN CLAY (CL)**, brown, medium stiff	20		☒	3-3-3 N=6					
	21.5 ***Boring Terminated at 21.5 Feet***									

See Exploration and Testing Procedures for a description of field and laboratory procedures used and additional data (If any).

See Supporting Information for explanation of symbols and abbreviations.

Water Level Observations
▽ While drilling

Notes

Advancement Method
Hollow Stem Auger

Abandonment Method
Boring backfilled with bentonite slurry and auger cuttings upon completion.

Drill Rig
Diedrich D-50 (track)

Hammer Type
Automatic

Driller
Terracon

Logged by
DD

Boring Started
02-15-2023

Boring Completed
02-15-2023

Boring Log No. B-122

Graphic Log	Location: See Exploration Plan Depth (Ft.)	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	EXPANSION INDEX	Water Content (%)	Dry Unit Weight (pcf)	Atterberg Limits LL-PL-PI	Percent Fines
▨	**LEAN CLAY**, trace sand, brown									
				✋						
	medium stiff to stiff			☒	2-3-5 N=8					
				✋						
	stiff	5		⧗	6-7-8		22.8	92		
	white veins, medium stiff			☒	1-3-2 N=5					
	stiff	10		⧗	3-4-5		34.4	84		
		15		☒	2-4-5 N=9					
			▽							
▨ 20.0	**CLAYEY SAND**, brown, loose	20		☒	3-3-3 N=6					
21.5	***Boring Terminated at 21.5 Feet***									

See Exploration and Testing Procedures for a description of field and laboratory procedures used and additional data (If any).

See Supporting Information for explanation of symbols and abbreviations.

Water Level Observations
▽ While drilling

Drill Rig
Diedrich D-50 (track)

Hammer Type
Automatic

Driller
Terracon

Notes

Advancement Method
Hollow Stem Auger

Abandonment Method
Boring backfilled with bentonite slurry and auger cuttings upon completion.

Logged by
DD

Boring Started
02-15-2023

Boring Completed
02-15-2023

Terracon
23041 Avenida De La Carlota
Ste 350
Laguna Hills, CA

Boring Log No. B-123

Location: See Exploration Plan

Depth (Ft.)	Description	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	EXPANSION INDEX	Water Content (%)	Dry Unit Weight (pcf)	Atterberg Limits LL-PL-PI	Percent Fines
	FAT CLAY (CH), trace sand, brown									
				✋					50-25-25	86
	stiff			⧗	4-5-8		27.5	85		
		5		✋ ☒	3-4-6 N=10					
	medium stiff			⧗	3-4-5		28.3	82		
10.0	**SANDY LEAN CLAY (CL)**, brown, soft to medium stiff	10		☒	2-2-2 N=4					63
15.0	**LEAN CLAY (CL)**, brown, medium stiff	15	▽	☒	2-3-3 N=6					
		20		☒	0-3-3 N=6					
21.5	***Boring Terminated at 21.5 Feet***									

See Exploration and Testing Procedures for a description of field and laboratory procedures used and additional data (If any).

See Supporting Information for explanation of symbols and abbreviations.

Water Level Observations
▽ While drilling

Notes

Advancement Method
Hollow Stem Auger

Abandonment Method
Boring backfilled with bentonite slurry and auger cuttings upon completion.

Drill Rig
Diedrich D-50 (track)

Hammer Type
Automatic

Driller
Terracon

Logged by
DD

Boring Started
02-15-2023

Boring Completed
02-15-2023

Boring Log No. B-124

Location: See Exploration Plan

Graphic Log	Depth (Ft.)	Description	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	EXPANSION INDEX	Water Content (%)	Dry Unit Weight (pcf)	Atterberg Limits LL-PL-PI	Percent Fines
▨		**FAT CLAY (CH)**, trace sand, brown									
▨		stiff			☒	3-4-5 N=9				55-18-37	97
▨			5		⧗	4-5-6		24.9	90		
▨					☒	4-5-6 N=11					
▨			10		⧗	3-5-5		20.7	91		
▨	15.0	**POORLY GRADED SAND WITH CLAY (SP-SC)**, very loose	15		☒	0-1-2 N=3					
▨				▽							
▨	21.5	loose	20		☒	3-2-3 N=5					
		Boring Terminated at 21.5 Feet									

See Exploration and Testing Procedures for a description of field and laboratory procedures used and additional data (If any).

See Supporting Information for explanation of symbols and abbreviations.

Notes

Water Level Observations
▽ At completion of drilling

Advancement Method
Hollow Stem Auger

Abandonment Method
Boring backfilled with bentonite slurry and auger cuttings upon completion.

Drill Rig
Diedrich D-50 (track)

Hammer Type
Automatic

Driller
Terracon

Logged by
JB

Boring Started
04-14-2023

Boring Completed
04-14-2023

Boring Log No. B-125

Graphic Log	Location: See Exploration Plan Depth (Ft.)	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	EXPANSION INDEX	Water Content (%)	Dry Unit Weight (pcf)	Atterberg Limits LL-PL-PI	Percent Fines
▨	**LEAN CLAY (CL)**, trace sand, brown									
▨	stiff			⧗	5-8-9		16.4	98		97
▨	medium stiff	5		✋ ⧗	3-2-3					
▨	7.5 **SANDY LEAN CLAY (CL)**, stiff			☒	4-5-5 N=10					
▨	medium stiff	10		☒	4-3-3 N=6					
▨			▽							
▨	soft	15		☒	4-1-2 N=3					69
▨	stiff	20		☒	0-4-5 N=9					
	21.5 ***Boring Terminated at 21.5 Feet***									

See Exploration and Testing Procedures for a description of field and laboratory procedures used and additional data (If any).

See Supporting Information for explanation of symbols and abbreviations.

Notes

Water Level Observations
▽ At completion of drilling

Advancement Method
Hollow Stem Auger

Abandonment Method
Boring backfilled with bentonite slurry and auger cuttings upon completion.

Drill Rig
Diedrich D-50 (track)

Hammer Type
Automatic

Driller
Terracon

Logged by
JB

Boring Started
04-13-2023

Boring Completed
04-13-2023

Darden Solar Facility
Cantua Creek | Fresno, CA
Terracon Project No. 60225172

Terracon
23041 Avenida De La Carlota
Ste 350
Laguna Hills, CA

Boring Log No. B-126

Graphic Log	Location: See Exploration Plan Depth (Ft.)	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	EXPANSION INDEX	Water Content (%)	Dry Unit Weight (pcf)	Atterberg Limits LL-PL-PI	Percent Fines
▨	**LEAN CLAY (CL)**, trace sand, brown									
▨	stiff			☒	4-5-9 N=14					
▨	medium stiff	5		⧗	2-2-6					97
▨	soft			☒	1-1-2 N=3					
▨	stiff	10		⧗	3-3-7					
▨	15.0									
▨	**LEAN CLAY WITH SAND (CL)**, brown, soft to medium stiff	15		☒	1-1-3 N=4					
▨			▽							
▨	soft	20		☒	1-1-2 N=3					
▨	21.5									
	Boring Terminated at 21.5 Feet									

See Exploration and Testing Procedures for a description of field and laboratory procedures used and additional data (If any).

See Supporting Information for explanation of symbols and abbreviations.

Water Level Observations
▽ At completion of drilling

Notes

Advancement Method
Hollow Stem Auger

Abandonment Method
Boring backfilled with bentonite slurry and auger cuttings upon completion.

Drill Rig
Diedrich D-50 (track)

Hammer Type
Automatic

Driller
Terracon

Logged by
JB

Boring Started
04-13-2023

Boring Completed
04-13-2023

Darden Solar Facility
Cantua Creek | Fresno, CA
Terracon Project No. 60225172

23041 Avenida De La Carlota
Ste 350
Laguna Hills, CA

Boring Log No. B-127

Location: See Exploration Plan

Graphic Log	Depth (Ft.)	Description	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	EXPANSION INDEX	Water Content (%)	Dry Unit Weight (pcf)	Atterberg Limits LL-PL-PI	Percent Fines
▨		**SANDY LEAN CLAY (CL)**, brown									
▨		very stiff			⧗	10-11-12		13.1	100		
▨		medium stiff	5		☒	2-3-4 N=7					
▨		stiff			⧗	4-5-7		25.5	94		
▨	10.0	**CLAYEY SAND (SC)**, brown, loose	10		☒	2-3-3 N=6					
▨				▽							
▨	15.0	**LEAN CLAY WITH SAND (CL)**, dark brown, medium stiff	15		☒	2-3-3 N=6					
▨	20.0	**CLAYEY SAND (SC)**, dark brown, very loose	20		☒	2-1-1 N=2					
	21.5	***Boring Terminated at 21.5 Feet***									

See Exploration and Testing Procedures for a description of field and laboratory procedures used and additional data (If any).

See Supporting Information for explanation of symbols and abbreviations.

Notes

Water Level Observations
▽ At completion of drilling

Advancement Method
Hollow Stem Auger

Abandonment Method
Boring backfilled with bentonite slurry and auger cuttings upon completion.

Drill Rig
Diedrich D-50 (track)

Hammer Type
Automatic

Driller
Terracon

Logged by
JB

Boring Started
04-14-2023

Boring Completed
04-14-2023

Boring Log No. B-128

Graphic Log	Location: See Exploration Plan Depth (Ft.)	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	EXPANSION INDEX	Water Content (%)	Dry Unit Weight (pcf)	Atterberg Limits LL-PL-PI	Percent Fines
▨	**FAT CLAY (CH)**, trace sand, light brown									
▨				✋						
▨	soft			☒	2-2-1 N=3				61-28-33	96
▨				✋						
▨	medium stiff	5		⧗	2-3-4		30.2	86		
▨	soft			☒	2-1-1 N=2					
▨	medium stiff	10		⧗	2-2-4		22.4	98		
▨			▽							
▨	brown	15		☒	2-3-3 N=6					
▨	20.0									
▨	**CLAYEY SAND (SC)**, brown, very loose	20		☒	5-1-1 N=2					
	21.5									
	Boring Terminated at 21.5 Feet									

See Exploration and Testing Procedures for a description of field and laboratory procedures used and additional data (If any).

See Supporting Information for explanation of symbols and abbreviations.

Water Level Observations

▽ At completion of drilling

Notes

Advancement Method
Hollow Stem Auger

Abandonment Method
Boring backfilled with bentonite slurry and auger cuttings upon completion.

Drill Rig
Diedrich D-50 (track)

Hammer Type
Automatic

Driller
Terracon

Logged by
JB

Boring Started
04-13-2023

Boring Completed
04-13-2023

23041 Avenida De La Carlota
Ste 350
Laguna Hills, CA

Boring Log No. B-129

Graphic Log	Location: See Exploration Plan Depth (Ft.)	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	EXPANSION INDEX	Water Content (%)	Dry Unit Weight (pcf)	Atterberg Limits LL-PL-PI	Percent Fines
▨	**LEAN CLAY (CL)**, trace sand and gravel, brown									
▨				✋						94
▨	stiff			⧗	2-4-5		24.4	87		
▨				✋						
▨	soft to medium stiff	5		☒	1-2-2 N=4					
▨	stiff			⧗	2-4-7		26.0	93		
▨	10.0									
▩	**CLAYEY SAND (SC)**, very loose	10		☒	0-1-1 N=2					
▩			▽							
▩		15		☒	2-1-1 N=2					
▩		20		☒	0-1-1 N=2					
▩	21.5									
	Boring Terminated at 21.5 Feet									

See Exploration and Testing Procedures for a description of field and laboratory procedures used and additional data (If any).

See Supporting Information for explanation of symbols and abbreviations.

Notes

Water Level Observations
▽ At completion of drilling

Advancement Method
Hollow Stem Auger

Abandonment Method
Boring backfilled with bentonite slurry and auger cuttings upon completion.

Drill Rig
Diedrich D-50 (track)

Hammer Type
Automatic

Driller
Terracon

Logged by
JB

Boring Started
04-13-2023

Boring Completed
04-13-2023

Darden Solar Facility
Cantua Creek | Fresno, CA
Terracon Project No. 60225172

23041 Avenida De La Carlota
Ste 350
Laguna Hills, CA

Boring Log No. B-130

Graphic Log	Location: See Exploration Plan Depth (Ft.)	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	EXPANSION INDEX	Water Content (%)	Dry Unit Weight (pcf)	Atterberg Limits LL-PL-PI	Percent Fines
▨	**LEAN CLAY WITH SAND (CL)**, light brown									
	soft			✋						
				☒	2-1-2 N=3					81
	medium stiff	5		✋ ⧗	2-3-5		27.0	85		
	soft to medium stiff			☒	2-2-2 N=4					
	stiff	10		⧗	3-6-7		31.0	88		
	medium stiff to stiff	15		☒	2-4-4 N=8					
	20.0									
▨	**CLAYEY SAND (SC)**, brown, medium dense	20		☒	8-8-10 N=18					
	21.5									
	Boring Terminated at 21.5 Feet									

See Exploration and Testing Procedures for a description of field and laboratory procedures used and additional data (If any).

See Supporting Information for explanation of symbols and abbreviations.

Notes

Water Level Observations

Advancement Method
Hollow Stem Auger

Abandonment Method
Boring backfilled with bentonite slurry and auger cuttings upon completion.

Drill Rig
Diedrich D-50 (track)

Hammer Type
Automatic

Driller
Terracon

Logged by
JB

Boring Started
04-13-2023

Boring Completed
04-13-2023

Terracon
23041 Avenida De La Carlota
Ste 350
Laguna Hills, CA

Boring Log No. B-131

Graphic Log	Location: See Exploration Plan Depth (Ft.)	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	EXPANSION INDEX	Water Content (%)	Dry Unit Weight (pcf)	Atterberg Limits LL-PL-PI	Percent Fines
▨	**LEAN CLAY WITH SAND (CL)**, light brown									
				✋						
	stiff			⧗	3-9-8		21.1	96		
	very stiff	5		✋ ☒	3-9-8 N=17					72
	stiff			⧗	2-4-9		31.1	82		
	medium stiff	10		☒	2-2-4 N=6					
		15		☒	2-2-5 N=7					
		20		☒	3-2-3 N=5					
	21.5									
	Boring Terminated at 21.5 Feet									

See Exploration and Testing Procedures for a description of field and laboratory procedures used and additional data (If any).

See Supporting Information for explanation of symbols and abbreviations.

Notes

Water Level Observations

Advancement Method
Hollow Stem Auger

Abandonment Method
Boring backfilled with bentonite slurry and auger cuttings upon completion.

Drill Rig
Diedrich D-50 (track)

Hammer Type
Automatic

Driller
Terracon

Logged by
JB

Boring Started
04-13-2023

Boring Completed
04-13-2023

Darden Solar Facility
Cantua Creek | Fresno, CA
Terracon Project No. 60225172

Terracon
23041 Avenida De La Carlota
Ste 350
Laguna Hills, CA

Boring Log No. B-132

Graphic Log	Location: See Exploration Plan Depth (Ft.)	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	EXPANSION INDEX	Water Content (%)	Dry Unit Weight (pcf)	Atterberg Limits LL-PL-PI	Percent Fines
	LEAN CLAY WITH SAND (CL), light brown									87
	medium stiff				2-3-3 N=6					
		5			1-2-4		31.0	88		
	dark brown, soft to medium stiff				3-2-2 N=4					
	medium stiff	10			2-2-6		25.3	93		
			▽							
	15.0 **CLAYEY SAND (SC)**, dark brown, loose	15			2-4-4 N=8					39
	20.0 **LEAN CLAY (CL)**, trace sand, light brown, medium stiff	20			2-3-2 N=5					
	21.5 ***Boring Terminated at 21.5 Feet***									

See Exploration and Testing Procedures for a description of field and laboratory procedures used and additional data (If any).

See Supporting Information for explanation of symbols and abbreviations.

Water Level Observations
▽ At completion of drilling

Notes

Advancement Method
Hollow Stem Auger

Abandonment Method
Boring backfilled with bentonite slurry and auger cuttings upon completion.

Drill Rig
Diedrich D-50 (track)

Hammer Type
Automatic

Driller
Terracon

Logged by
JB

Boring Started
04-11-2023

Boring Completed
04-11-2023

Darden Solar Facility
Cantua Creek | Fresno, CA
Terracon Project No. 60225172

Terracon
23041 Avenida De La Carlota
Ste 350
Laguna Hills, CA

Boring Log No. B-133

Graphic Log	Location: See Exploration Plan Depth (Ft.)	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	EXPANSION INDEX	Water Content (%)	Dry Unit Weight (pcf)	Atterberg Limits LL-PL-PI	Percent Fines
	SANDY LEAN CLAY (CL), brown									
	medium dense				5-10-11		19.6	98		
	loose	5			3-4-2 N=6					
					2-4-6		28.1	89		
	10.0 **CLAYEY SAND (SC)**, brown, loose	10			2-2-3 N=5					
	15.0 **LEAN CLAY (CL)**, trace sand, light brown, soft to medium stiff	15	▽		1-1-3 N=4					
	soft	20			1-1-1 N=2					
	21.5 ***Boring Terminated at 21.5 Feet***									

See Exploration and Testing Procedures for a description of field and laboratory procedures used and additional data (If any).

See Supporting Information for explanation of symbols and abbreviations.

Water Level Observations
▽ At completion of drilling

Notes

Advancement Method
Hollow Stem Auger

Abandonment Method
Boring backfilled with bentonite slurry and auger cuttings upon completion.

Drill Rig
Diedrich D-50 (track)

Hammer Type
Automatic

Driller
Terracon

Logged by
JB

Boring Started
04-11-2023

Boring Completed
04-11-2023

Darden Solar Facility
Cantua Creek | Fresno, CA
Terracon Project No. 60225172

23041 Avenida De La Carlota
Ste 350
Laguna Hills, CA

Boring Log No. B-134

Location: See Exploration Plan

Graphic Log	Depth (Ft.)	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	EXPANSION INDEX	Water Content (%)	Dry Unit Weight (pcf)	Atterberg Limits LL-PL-PI	Percent Fines
	LEAN CLAY WITH SAND (CL), brown									
	soft to medium stiff				2-2-2 N=4					79
	medium stiff	5			2-3-4		28.5	86		
	soft to medium stiff				1-2-2 N=4					
	medium stiff	10			2-3-3		27.4	95		
	15.0									
	POORLY GRADED SAND WITH CLAY (SP-SC), brown, very loose	15	▽		1-1-2 N=3					
	20.0									
	CLAYEY SAND (SC), light brown, very loose	20			0-1-2 N=3					
	21.5									
	Boring Terminated at 21.5 Feet									

See Exploration and Testing Procedures for a description of field and laboratory procedures used and additional data (If any).

See Supporting Information for explanation of symbols and abbreviations.

Water Level Observations
▽ At completion of drilling

Notes

Advancement Method
Hollow Stem Auger

Abandonment Method
Boring backfilled with bentonite slurry and auger cuttings upon completion.

Drill Rig
Diedrich D-50 (track)

Hammer Type
Automatic

Driller
Terracon

Logged by
JB

Boring Started
04-13-2023

Boring Completed
04-13-2023

Boring Log No. B-135

Graphic Log	Location: See Exploration Plan Depth (Ft.)	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	EXPANSION INDEX	Water Content (%)	Dry Unit Weight (pcf)	Atterberg Limits LL-PL-PI	Percent Fines
▨	**SANDY LEAN CLAY (CL)**, brown			✋						
▨	medium stiff			⧗	2-2-3		24.6	85		
▨		5		✋						
▨				☒	1-2-3 N=5					
▨				⧗	1-2-4		25.7	92		
▨	10.0									
▨	**LEAN CLAY (CL)**, trace sand, light brown, soft	10		☒	1-1-1 N=2					
▨		15	▽	☒	1-2-1 N=3					
▨		20		☒	2-1-1 N=2					
▨	21.5									
	Boring Terminated at 21.5 Feet									

See Exploration and Testing Procedures for a description of field and laboratory procedures used and additional data (If any).

See Supporting Information for explanation of symbols and abbreviations.

Notes

Water Level Observations
▽ At completion of drilling

Advancement Method
Hollow Stem Auger

Abandonment Method
Boring backfilled with bentonite slurry and auger cuttings upon completion.

Drill Rig
Diedrich D-50 (track)

Hammer Type
Automatic

Driller
Terracon

Logged by
JB

Boring Started
04-13-2023

Boring Completed
04-13-2023

Darden Solar Facility
Cantua Creek | Fresno, CA
Terracon Project No. 60225172

23041 Avenida De La Carlota
Ste 350
Laguna Hills, CA

Boring Log No. B-136

Graphic Log	Location: See Exploration Plan Depth (Ft.)	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	EXPANSION INDEX	Water Content (%)	Dry Unit Weight (pcf)	Atterberg Limits LL-PL-PI	Percent Fines
▨	**LEAN CLAY (CL)**, trace sand, brown									
	medium stiff			⧗	2-2-3					
		5		✋ X	3-3-4 N=7		28.7	88		86
	light brown			⧗	1-2-4		23.0	100		
▨	10.0 **POORLY GRADED SAND WITH CLAY (SP-SC)**, brown, loose	10		X	3-4-4 N=8					
			▽							
▨	15.0 **LEAN CLAY WITH SAND (CL)**, light brown, soft to medium stiff	15		X	1-1-3 N=4					
	stiff	20		X	4-4-5 N=9					
	21.5 ***Boring Terminated at 21.5 Feet***									

See Exploration and Testing Procedures for a description of field and laboratory procedures used and additional data (If any).

See Supporting Information for explanation of symbols and abbreviations.

Water Level Observations
▽ At completion of drilling

Notes

Advancement Method
Hollow Stem Auger

Abandonment Method
Boring backfilled with bentonite slurry and auger cuttings upon completion.

Drill Rig
Diedrich D-50 (track)

Hammer Type
Automatic

Driller
Terracon

Logged by
JB

Boring Started
04-15-2023

Boring Completed
04-15-2023

Boring Log No. B-137

Graphic Log	Location: See Exploration Plan Depth (Ft.)	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	EXPANSION INDEX	Water Content (%)	Dry Unit Weight (pcf)	Atterberg Limits LL-PL-PI	Percent Fines
▨	**LEAN CLAY (CL)**, trace sand, brown									
▨				✋						98
▨	very stiff			⧗	15-13-14		15.0	105		
▨	tannish brown	5		✋						
▨				⊠	6-8-10 N=18					
▨	stiff			⧗	6-7-9		19.3	89		
▨	brown	10		⊠	4-6-6 N=12					
▨		15		⊠	5-6-6 N=12					
▨	medium stiff to stiff	20		⊠	3-4-4 N=8					
▨	21.5									
	Boring Terminated at 21.5 Feet									

See Exploration and Testing Procedures for a description of field and laboratory procedures used and additional data (If any).

See Supporting Information for explanation of symbols and abbreviations.

Water Level Observations
Groundwater not encountered

Drill Rig
CME 75 (track)

Hammer Type
Automatic

Driller
2R Drilling

Notes

Advancement Method
Hollow Stem Auger

Abandonment Method
Boring backfilled with bentonite slurry and auger cuttings upon completion.

Logged by
CR

Boring Started
06-05-2023

Boring Completed
06-05-2023

Boring Log No. B-138

Graphic Log	Location: See Exploration Plan Depth (Ft.)	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	EXPANSION INDEX	Water Content (%)	Dry Unit Weight (pcf)	Atterberg Limits LL-PL-PI	Percent Fines
▨	**LEAN CLAY (CL)**, trace sand, brown			✋						98
▨	medium stiff to stiff			☒	3-3-5 N=8					
▨	very stiff	5		✋ ⧗	6-11-17		26.0	93		
▨				☒	4-8-10 N=18					
▨		10		⧗	7-16-16		18.2	102		
▨	medium stiff	15		☒	3-3-4 N=7					
▨	very stiff	20		☒	7-10-10 N=20					
	21.5 ***Boring Terminated at 21.5 Feet***									

See Exploration and Testing Procedures for a description of field and laboratory procedures used and additional data (If any).

See Supporting Information for explanation of symbols and abbreviations.

Water Level Observations
Groundwater not encountered

Notes

Advancement Method
Hollow Stem Auger

Abandonment Method
Boring backfilled with bentonite slurry and auger cuttings upon completion.

Drill Rig
CME 75 (track)

Hammer Type
Automatic

Driller
2R Drilling

Logged by
CR

Boring Started
06-06-2023

Boring Completed
06-06-2023

Darden Solar Facility
Cantua Creek | Fresno, CA
Terracon Project No. 60225172

23041 Avenida De La Carlota
Ste 350
Laguna Hills, CA

Boring Log No. B-139

Graphic Log	Location: See Exploration Plan Depth (Ft.)	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	EXPANSION INDEX	Water Content (%)	Dry Unit Weight (pcf)	Atterberg Limits LL-PL-PI	Percent Fines
▨	**LEAN CLAY WITH SAND (CL)**, brown			✋						79
▨	stiff			⧗	6-7-10		24.1	93		
▨	medium stiff to stiff	5		✋ ☒	4-3-5 N=8					
▨	hard			⧗	18-24-32		21.3	98		
▨	very stiff	10		☒	5-7-9 N=16					
▨	medium stiff	15		☒	3-4-3 N=7					
▨	medium stiff to stiff 21.5	20		☒	2-3-5 N=8					
	Boring Terminated at 21.5 Feet									

See Exploration and Testing Procedures for a description of field and laboratory procedures used and additional data (If any).

See Supporting Information for explanation of symbols and abbreviations.

Notes

Water Level Observations
Groundwater not encountered

Advancement Method
Hollow Stem Auger

Abandonment Method
Boring backfilled with bentonite slurry and auger cuttings upon completion.

Drill Rig
CME 75 (track)

Hammer Type
Automatic

Driller
2R Drilling

Logged by
CR

Boring Started
06-08-2023

Boring Completed
06-08-2023

Boring Log No. B-140

Graphic Log	Location: See Exploration Plan Depth (Ft.)	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	EXPANSION INDEX	Water Content (%)	Dry Unit Weight (pcf)	Atterberg Limits LL-PL-PI	Percent Fines
▨	**LEAN CLAY WITH SAND (CL)**, brown			✋						82
▨	very stiff			☒	8-9-11 N=20					
▨	5.0			✋						
▨	**LEAN CLAY (CL)**, trace sand, brown, very stiff	5		⧗	6-10-13					
▨	stiff			☒	4-5-8 N=13					
▨	very stiff	10		⧗	7-10-10		27.4	89		
▨	medium stiff	15		☒	3-2-3 N=5					
▨	20.0		▽							
▨	**CLAYEY SAND (SC)**, brown, medium dense	20		☒	2-4-6 N=10					
▨	21.5									
	Boring Terminated at 21.5 Feet									

See Exploration and Testing Procedures for a description of field and laboratory procedures used and additional data (If any).

See Supporting Information for explanation of symbols and abbreviations.

Water Level Observations
▽ At completion of drilling

Drill Rig
CME 75 (track)

Hammer Type
Automatic

Driller
2R Drilling

Logged by
CR

Boring Started
06-07-2023

Boring Completed
06-07-2023

Notes

Advancement Method
Hollow Stem Auger

Abandonment Method
Boring backfilled with bentonite slurry and auger cuttings upon completion.

Boring Log No. E-1

Graphic Log	Location: See Exploration Plan Depth (Ft.)	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	EXPANSION INDEX	Water Content (%)	Dry Unit Weight (pcf)	Atterberg Limits LL-PL-PI	Percent Fines
▨	**CLAYEY SAND (SC)**, light brown									
▨	loose			⧗	3-5-7		16.9	92		
				✋						
▨	5.0 **LEAN CLAY (CL)**, trace sand, light brown, medium stiff	5		⧗	2-3-5		23.2	94		
▨	7.5 **CLAYEY SAND (SC)**, light brown, loose			⧗	2-3-6		26.6	94		
▨	10.0 **LEAN CLAY (CL)**, trace sand, light brown, stiff	10		⧗	4-5-5		33.6	86		
▨		15	▽	☒	4-4-6 N=10					
▨	soft	20		⧗	1-2-2		31.4	89		
▨	25.0	25								

See Exploration and Testing Procedures for a description of field and laboratory procedures used and additional data (If any).

See Supporting Information for explanation of symbols and abbreviations.

Water Level Observations
▽ At completion of drilling

Drill Rig
Diedrich D-50 (track)

Hammer Type
Automatic

Driller
Terracon

Notes

Advancement Method
Hollow Stem Auger

Abandonment Method
Boring backfilled with bentonite slurry and auger cuttings upon completion.

Logged by
JB

Boring Started
04-11-2023

Boring Completed
04-11-2023

23041 Avenida De La Carlota
Ste 350
Laguna Hills, CA

Boring Log No. E-1

Graphic Log	Location: See Exploration Plan Depth (Ft.)	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	EXPANSION INDEX	Water Content (%)	Dry Unit Weight (pcf)	Atterberg Limits LL-PL-PI	Percent Fines
	SANDY LEAN CLAY (CL), brown, medium stiff			☒	1-3-4 N=7					66
	30.0 **LEAN CLAY WITH SAND (CL)**, brown, soft	30		⧗	1-2-1		24.9	99		
	stiff	35		☒	3-4-7 N=11					83
	40.0 **CLAYEY SAND (SC)**, brown, loose	40		⧗	2-4-6		22.1			
	45.0 **SANDY LEAN CLAY (CL)**, light brown stiff	45		☒	3-4-7 N=11					
		50								

See Exploration and Testing Procedures for a description of field and laboratory procedures used and additional data (If any).

See Supporting Information for explanation of symbols and abbreviations.

Notes

Water Level Observations
▽ At completion of drilling

Advancement Method
Hollow Stem Auger

Abandonment Method
Boring backfilled with bentonite slurry and auger cuttings upon completion.

Drill Rig
Diedrich D-50 (track)

Hammer Type
Automatic

Driller
Terracon

Logged by
JB

Boring Started
04-11-2023

Boring Completed
04-11-2023

Boring Log No. E-1

Graphic Log	Location: See Exploration Plan Depth (Ft.)	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	EXPANSION INDEX	Water Content (%)	Dry Unit Weight (pcf)	Atterberg Limits LL-PL-PI	Percent Fines
	SANDY LEAN CLAY (CL), light brown *(continued)* very stiff 51.5				3-8-19		24.9	97		
	Boring Terminated at 51.5 Feet									

See Exploration and Testing Procedures for a description of field and laboratory procedures used and additional data (If any).

See Supporting Information for explanation of symbols and abbreviations.

Water Level Observations
▽ At completion of drilling

Drill Rig
Diedrich D-50 (track)

Hammer Type
Automatic

Driller
Terracon

Logged by
JB

Boring Started
04-11-2023

Boring Completed
04-11-2023

Notes

Advancement Method
Hollow Stem Auger

Abandonment Method
Boring backfilled with bentonite slurry and auger cuttings upon completion.

Boring Log No. SUB-1

Graphic Log	Location: See Exploration Plan Depth (Ft.)	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	EXPANSION INDEX	Water Content (%)	Dry Unit Weight (pcf)	Atterberg Limits LL-PL-PI	Percent Fines
▨	**LEAN CLAY WITH SAND (CL)**, brown			┃		102			48-22-26	79
▨	stiff			⧗	3-5-7		22.3	96		
▨	soft to medium stiff	5		✋ ✕	1-1-3 N=4					
▨	7.5 **CLAYEY SAND (SC)**, dark brown, loose			⧗	2-2-7		28.2	87		
▨	medium dense	10		⧗	2-4-6		20.5	93		
▨	15.0 **SANDY LEAN CLAY (CL)**, light brown stiff	15	▽	✕	1-4-5 N=9					
▨		20		⧗	1-5-6		29.5	91		
		25								

See Exploration and Testing Procedures for a description of field and laboratory procedures used and additional data (If any).

See Supporting Information for explanation of symbols and abbreviations.

Notes

Water Level Observations
▽ At completion of drilling

Advancement Method
Hollow Stem Auger

Abandonment Method
Boring backfilled with bentonite slurry and auger cuttings upon completion.

Drill Rig
Diedrich D-50 (track)

Hammer Type
Automatic

Driller
Terracon

Logged by
JB

Boring Started
04-11-2023

Boring Completed
04-11-2023

Boring Log No. SUB-1

Graphic Log	Location: See Exploration Plan Depth (Ft.)	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	EXPANSION INDEX	Water Content (%)	Dry Unit Weight (pcf)	Atterberg Limits LL-PL-PI	Percent Fines
▨	**SANDY LEAN CLAY (CL)**, light brown *(continued)* stiff			☒	2-4-6 N=10					62
▨	soft	30		⧗	2-2-1		23.2	104		
▨	35.0 **CLAYEY SAND (SC)**, dark brown, very loose	35		☒	0-0-1 N=1					
▨	40.0 **SANDY LEAN CLAY (CL)**, dark brown, stiff	40		⧗	2-5-6		34.1	86		
▨	soft	45		☒	2-1-1 N=2					68
	50.0	50								

See Exploration and Testing Procedures for a description of field and laboratory procedures used and additional data (If any).

See Supporting Information for explanation of symbols and abbreviations.

Water Level Observations
▽ At completion of drilling

Drill Rig
Diedrich D-50 (track)

Hammer Type
Automatic

Driller
Terracon

Logged by
JB

Boring Started
04-11-2023

Boring Completed
04-11-2023

Notes

Advancement Method
Hollow Stem Auger

Abandonment Method
Boring backfilled with bentonite slurry and auger cuttings upon completion.

Terracon
23041 Avenida De La Carlota
Ste 350
Laguna Hills, CA

Boring Log No. SUB-1

Graphic Log	Location: See Exploration Plan Depth (Ft.)	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	EXPANSION INDEX	Water Content (%)	Dry Unit Weight (pcf)	Atterberg Limits LL-PL-PI	Percent Fines
🟨	**CLAYEY SAND (SC)**, very loose 51.5			⧗	2-2-1		15.9	109		
	Boring Terminated at 51.5 Feet									

See Exploration and Testing Procedures for a description of field and laboratory procedures used and additional data (If any).

See Supporting Information for explanation of symbols and abbreviations.

Water Level Observations

▽ At completion of drilling

Notes

Advancement Method
Hollow Stem Auger

Abandonment Method
Boring backfilled with bentonite slurry and auger cuttings upon completion.

Drill Rig
Diedrich D-50 (track)

Hammer Type
Automatic

Driller
Terracon

Logged by
JB

Boring Started
04-11-2023

Boring Completed
04-11-2023

Darden Solar Facility
Cantua Creek | Fresno, CA
Terracon Project No. 60225172

23041 Avenida De La Carlota
Ste 350
Laguna Hills, CA

Boring Log No. BESS-1

Location: See Exploration Plan

Depth (Ft.)	Description	Depth (Ft.)	Water Level Observations	Field Test Results	EXPANSION INDEX	Water Content (%)	Dry Unit Weight (pcf)	Atterberg Limits LL-PL-PI	Percent Fines
	SANDY LEAN CLAY (CL), brown				92				67
	stiff			7-8-6		16.1	94		
		5		3-4-6		20.3	85		
7.5	**CLAYEY SAND (SC)**, brown, loose			3-10-8		18.3	87		
10.0	**LEAN CLAY WITH SAND (CL)**, brown soft	10		1-2-2		34.5	84		
	medium stiff	15		1-2-4 N=6					
	stiff	20		1-4-6		20.3	103		
		25	▽						

See Exploration and Testing Procedures for a description of field and laboratory procedures used and additional data (If any).

See Supporting Information for explanation of symbols and abbreviations.

Notes

Water Level Observations
▽ At completion of drilling

Advancement Method
Hollow Stem Auger

Abandonment Method
Boring backfilled with bentonite slurry and auger cuttings upon completion.

Drill Rig
Diedrich D-50 (track)

Hammer Type
Automatic

Driller
Terracon

Logged by
JB

Boring Started
04-10-2023

Boring Completed
04-10-2023

Boring Log No. BESS-1

Graphic Log	Location: See Exploration Plan Depth (Ft.)	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	EXPANSION INDEX	Water Content (%)	Dry Unit Weight (pcf)	Atterberg Limits LL-PL-PI	Percent Fines
▨	**LEAN CLAY WITH SAND (CL)**, brown *(continued)* soft			☒	1-1-2 N=3					
▨	medium stiff	30		⧗	1-3-2		22.6	102		
▨	soft	35		☒	1-1-2 N=3					
▨	40.0 **CLAYEY SAND (SC)** medium dense	40		⧗	3-6-6		22.1	103		
▨	loose	45		☒	1-2-3 N=5					
		50								

See Exploration and Testing Procedures for a description of field and laboratory procedures used and additional data (If any).

See Supporting Information for explanation of symbols and abbreviations.

Water Level Observations
▽ At completion of drilling

Drill Rig
Diedrich D-50 (track)

Hammer Type
Automatic

Driller
Terracon

Logged by
JB

Boring Started
04-10-2023

Boring Completed
04-10-2023

Notes

Advancement Method
Hollow Stem Auger

Abandonment Method
Boring backfilled with bentonite slurry and auger cuttings upon completion.

Boring Log No. BESS-1

Graphic Log	Location: See Exploration Plan Depth (Ft.)	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	EXPANSION INDEX	Water Content (%)	Dry Unit Weight (pcf)	Atterberg Limits LL-PL-PI	Percent Fines
▨	**CLAYEY SAND (SC)** *(continued)* medium dense 51.5	—		☒	4-6-9 N=15					
	Boring Terminated at 51.5 Feet									

See Exploration and Testing Procedures for a description of field and laboratory procedures used and additional data (If any).

See Supporting Information for explanation of symbols and abbreviations.

Notes

Water Level Observations
▽ At completion of drilling

Advancement Method
Hollow Stem Auger

Abandonment Method
Boring backfilled with bentonite slurry and auger cuttings upon completion.

Drill Rig
Diedrich D-50 (track)

Hammer Type
Automatic

Driller
Terracon

Logged by
JB

Boring Started
04-10-2023

Boring Completed
04-10-2023

Darden Solar Facility
Cantua Creek | Fresno, CA
Terracon Project No. 60225172

Terracon
23041 Avenida De La Carlota
Ste 350
Laguna Hills, CA

Boring Log No. SUB-2

Graphic Log	Location: See Exploration Plan Depth (Ft.)	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	EXPANSION INDEX	Water Content (%)	Dry Unit Weight (pcf)	Atterberg Limits LL-PL-PI	Percent Fines
▨	**CLAYEY SAND (SC)**, brown			│		29			32-17-15	42
▨	light brown, medium dense			⧗	4-6-13		14.2	103		
▨		5		☒	7-9-14 N=23					
▨	brown			⧗	3-13-24		11.7	107		
▨		10		☒	8-10-12 N=22				41-19-22	39
▨		15		☒	4-5-7 N=12					
▨		20		☒	3-5-8 N=13					
▨	25.0	25								

See Exploration and Testing Procedures for a description of field and laboratory procedures used and additional data (If any).

See Supporting Information for explanation of symbols and abbreviations.

Notes

Water Level Observations
Groundwater not encountered

Advancement Method
Hollow Stem Auger

Abandonment Method
Boring backfilled with bentonite chips upon completion.

Drill Rig
Diedrich D-50 (track)

Hammer Type
Automatic

Driller
Terracon

Logged by
AC

Boring Started
08-01-2023

Boring Completed
08-01-2023

23041 Avenida De La Carlota
Ste 350
Laguna Hills, CA

Boring Log No. SUB-2

Graphic Log	Location: See Exploration Plan Depth (Ft.)	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	EXPANSION INDEX	Water Content (%)	Dry Unit Weight (pcf)	Atterberg Limits LL-PL-PI	Percent Fines
▨	**SANDY LEAN CLAY (CL)**, brown, medium stiff to stiff			☒	3-3-5 N=8				30-18-12	67
▨	30.0 **CLAYEY SAND (SC)**, light brown, dense	30		☒	4-18-28 N=46					13
▨	35.0 **POORLY GRADED SAND WITH CLAY (SP-SC)**, brown, very dense	35		☒	16-41-37 N=78					
▨	medium dense	40		☒	14-12-6 N=18					
▨		45		☒	4-5-8 N=13					
	50.0 ***Auger Refusal at 50 Feet***	50								

See Exploration and Testing Procedures for a description of field and laboratory procedures used and additional data (If any).

See Supporting Information for explanation of symbols and abbreviations.

Notes

Water Level Observations
Groundwater not encountered

Advancement Method
Hollow Stem Auger

Abandonment Method
Boring backfilled with bentonite chips upon completion.

Drill Rig
Diedrich D-50 (track)

Hammer Type
Automatic

Driller
Terracon

Logged by
AC

Boring Started
08-01-2023

Boring Completed
08-01-2023

Boring Log No. SW-1

Graphic Log	Location: See Exploration Plan Depth (Ft.)	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	EXPANSION INDEX	Water Content (%)	Dry Unit Weight (pcf)	Atterberg Limits LL-PL-PI	Percent Fines
	CLAYEY SAND (SC), tan								30-20-10	26
	light brown, medium dense				3-23-31		11.9	93		
	dense	5			9-11-31 N=42				33-19-14	
	tan, medium dense				7-17-23					33
	10.0 **SILTY CLAYEY SAND (SC-SM)**, light brown, medium dense	10			7-7-9 N=16				24-20-4	
	loose	15			5-4-5 N=9					
	trace gravel, medium dense	20			5-12-16 N=28					
	25.0	25								

See Exploration and Testing Procedures for a description of field and laboratory procedures used and additional data (If any).

See Supporting Information for explanation of symbols and abbreviations.

Notes

Water Level Observations
Groundwater not encountered

Advancement Method
Hollow Stem Auger

Abandonment Method
Boring backfilled with cement grout slurry upon completion

Drill Rig
Diedrich D-50 (track)

Hammer Type
Automatic

Driller
Terracon

Logged by
AC

Boring Started
08-01-2023

Boring Completed
08-01-2023

Darden Solar Facility
Cantua Creek | Fresno, CA
Terracon Project No. 60225172

23041 Avenida De La Carlota
Ste 350
Laguna Hills, CA

Boring Log No. SW-1

Graphic Log	Location: See Exploration Plan Depth (Ft.)	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	EXPANSION INDEX	Water Content (%)	Dry Unit Weight (pcf)	Atterberg Limits LL-PL-PI	Percent Fines
▨	**CLAYEY SAND (SC)**, light brown, medium dense			☒	8-7-7 N=14					41
		30		☒	4-5-8 N=13					
		35		☒	6-6-7 N=13					
	40.0									
▨	**POORLY GRADED SAND WITH CLAY (SP-SC)**, tan, medium dense	40		☒	14-14-14 N=28					
	45.0									
▨	**CLAYEY SAND (SC)**, brown medium dense	45		☒	6-7-11 N=18				33-17-16	
		50								

See Exploration and Testing Procedures for a description of field and laboratory procedures used and additional data (If any).

See Supporting Information for explanation of symbols and abbreviations.

Water Level Observations
Groundwater not encountered

Drill Rig
Diedrich D-50 (track)

Hammer Type
Automatic

Driller
Terracon

Logged by
AC

Boring Started
08-01-2023

Boring Completed
08-01-2023

Notes

Advancement Method
Hollow Stem Auger

Abandonment Method
Boring backfilled with cement grout slurry upon completion

Boring Log No. SW-1

Graphic Log	Location: See Exploration Plan Depth (Ft.)	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	EXPANSION INDEX	Water Content (%)	Dry Unit Weight (pcf)	Atterberg Limits LL-PL-PI	Percent Fines
▨	**CLAYEY SAND (SC)**, brown *(continued)* dense 51.5	—		☒	9-12-25 N=37					
	Boring Terminated at 51.5 Feet									

See Exploration and Testing Procedures for a description of field and laboratory procedures used and additional data (If any).

See Supporting Information for explanation of symbols and abbreviations.

Water Level Observations
Groundwater not encountered

Notes

Advancement Method
Hollow Stem Auger

Abandonment Method
Boring backfilled with cement grout slurry upon completion

Drill Rig
Diedrich D-50 (track)

Hammer Type
Automatic

Driller
Terracon

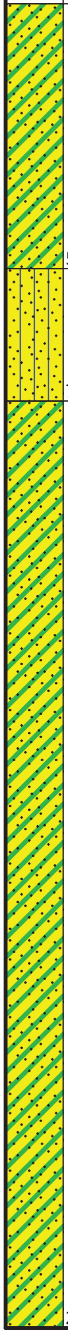
Logged by
AC

Boring Started
08-01-2023

Boring Completed
08-01-2023

Boring Log No. E-2

Location: See Exploration Plan



Graphic Log Depth (Ft.)	Description	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	EXPANSION INDEX	Water Content (%)	Dry Unit Weight (pcf)	Atterberg Limits LL-PL-PI	Percent Fines
	CLAYEY SAND (SC), brown									
				✋		38			32-17-15	38
	medium dense			⧗	7-17-24		10.7	103		
5.0	**SILTY SAND (SM)**, brown, dense	5		✋ ⧖	7-17-19 N=36				NP	
7.5	**CLAYEY SAND (SC)**, brown, medium dense			⧖	5-7-9 N=16				35-18-17	43
	tan, dense	10		⧗	9-29-32		10.8	113		
	medium dense	15		⧖	5-8-7 N=15					
	tannish brown, dense	20		⧖	11-20-20 N=40					
25.0		25								

See Exploration and Testing Procedures for a description of field and laboratory procedures used and additional data (If any).

See Supporting Information for explanation of symbols and abbreviations.

Notes

Water Level Observations
Groundwater not encountered

Advancement Method
Hollow Stem Auger

Abandonment Method
Boring backfilled with cement grout slurry upon completion

Drill Rig
Diedrich D-50 (track)

Hammer Type
Automatic

Driller
Terracon

Logged by
AC

Boring Started
08-02-2023

Boring Completed
08-02-2023

Terracon
23041 Avenida De La Carlota
Ste 350
Laguna Hills, CA

Boring Log No. E-2

Graphic Log	Location: See Exploration Plan Depth (Ft.)	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	EXPANSION INDEX	Water Content (%)	Dry Unit Weight (pcf)	Atterberg Limits LL-PL-PI	Percent Fines
▨	**CLAYEY SAND (SC)**, brown, medium dense			☒	6-6-7 N=13					
▨	30.0 **SILTY CLAYEY SAND (SC-SM)**, brown, medium dense	30		☒	7-7-7 N=14				26-20-6	
▨		35		☒	5-6-8 N=14					
▨	tan, dense	40		☒	13-20-17 N=37					
▨	45.0 **CLAYEY SAND (SC)**, brown medium dense	45		☒	9-12-13 N=25					
		50								

See Exploration and Testing Procedures for a description of field and laboratory procedures used and additional data (If any).

See Supporting Information for explanation of symbols and abbreviations.

Notes

Water Level Observations
Groundwater not encountered

Advancement Method
Hollow Stem Auger

Abandonment Method
Boring backfilled with cement grout slurry upon completion

Drill Rig
Diedrich D-50 (track)

Hammer Type
Automatic

Driller
Terracon

Logged by
AC

Boring Started
08-02-2023

Boring Completed
08-02-2023

23041 Avenida De La Carlota
Ste 350
Laguna Hills, CA

Boring Log No. E-2

Graphic Log	Location: See Exploration Plan Depth (Ft.)	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	EXPANSION INDEX	Water Content (%)	Dry Unit Weight (pcf)	Atterberg Limits LL-PL-PI	Percent Fines
▨	**CLAYEY SAND (SC)**, brown *(continued)* dense 51.5			☒	13-24-20 N=44					
	Boring Terminated at 51.5 Feet									

See Exploration and Testing Procedures for a description of field and laboratory procedures used and additional data (If any).

See Supporting Information for explanation of symbols and abbreviations.

Water Level Observations
Groundwater not encountered

Notes

Advancement Method
Hollow Stem Auger

Abandonment Method
Boring backfilled with cement grout slurry upon completion

Drill Rig
Diedrich D-50 (track)

Hammer Type
Automatic

Driller
Terracon

Logged by
AC

Boring Started
08-02-2023

Boring Completed
08-02-2023

Boring Log No. T-1

Graphic Log	Location: See Exploration Plan Depth (Ft.)	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	EXPANSION INDEX	Water Content (%)	Dry Unit Weight (pcf)	Atterberg Limits LL-PL-PI	Percent Fines
	SANDY FAT CLAY (CH), brown			✋					54-18-36	
	medium stiff			⧗	2-4-5		20.4	77		
	soft to medium stiff	5		✋ ⊠	2-2-2 N=4					
	stiff			⧗	3-5-11		31.9	81		
	10.0 **SANDY LEAN CLAY (CL)** dark brown, soft to medium stiff	10		⊠	2-2-2 N=4					
	brown, stiff	15		⊠	2-5-6 N=11					62
		20	▽	⊠	3-5-6 N=11					
		25								

See Exploration and Testing Procedures for a description of field and laboratory procedures used and additional data (If any).

See Supporting Information for explanation of symbols and abbreviations.

Notes

Water Level Observations
▽ At completion of drilling

Advancement Method
Hollow Stem Auger

Abandonment Method
Boring backfilled with cement grout slurry upon completion

Drill Rig
Diedrich D-50 (track)

Hammer Type
Automatic

Driller
Terracon

Logged by
AH

Boring Started
08-10-2023

Boring Completed
08-10-2023

Terracon
23041 Avenida De La Carlota
Ste 350
Laguna Hills, CA

Boring Log No. T-1

Graphic Log	Location: See Exploration Plan Depth (Ft.)	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	EXPANSION INDEX	Water Content (%)	Dry Unit Weight (pcf)	Atterberg Limits LL-PL-PI	Percent Fines
▨	**SANDY LEAN CLAY (CL)** *(continued)* brown, medium stiff to stiff			☒	2-3-5 N=8					
▨	30.0 **CLAYEY SAND (SC)**, brown, loose	30		☒	2-2-3 N=5					
▨	35.0 **SANDY LEAN CLAY (CL)**, light brown, soft	35		☒	1-2-1 N=3					57
▨	brown, medium stiff	40		☒	2-3-4 N=7					
	41.5 ***Boring Terminated at 41.5 Feet***									

See Exploration and Testing Procedures for a description of field and laboratory procedures used and additional data (If any).

See Supporting Information for explanation of symbols and abbreviations.

Notes

Water Level Observations
▽ At completion of drilling

Advancement Method
Hollow Stem Auger

Abandonment Method
Boring backfilled with cement grout slurry upon completion

Drill Rig
Diedrich D-50 (track)

Hammer Type
Automatic

Driller
Terracon

Logged by
AH

Boring Started
08-10-2023

Boring Completed
08-10-2023

Terracon
23041 Avenida De La Carlota
Ste 350
Laguna Hills, CA

Boring Log No. T-2

Location: See Exploration Plan

Graphic Log	Depth (Ft.)	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	EXPANSION INDEX	Water Content (%)	Dry Unit Weight (pcf)	Atterberg Limits LL-PL-PI	Percent Fines
▨	**LEAN CLAY WITH SAND (CL)**, brown									
				✋					42-17-25	71
	soft			⧗	2-2-1		19.0	84		
	medium stiff	5		✋						
				☒	2-2-3 N=5					
				⧗	4-4-5		24.9	82		
		10		☒	2-3-4 N=7					
	medium stiff to stiff	15		☒	2-3-5 N=8					
	stiff	20		☒	4-6-8 N=14					84
	25.0	25								

See Exploration and Testing Procedures for a description of field and laboratory procedures used and additional data (If any).

See Supporting Information for explanation of symbols and abbreviations.

Water Level Observations
▽ At completion of drilling

Notes

Advancement Method
Hollow Stem Auger

Abandonment Method
Boring backfilled with cement grout slurry upon completion

Drill Rig
Diedrich D-50 (track)

Hammer Type
Automatic

Driller
Terracon

Logged by
AH

Boring Started
08-10-2023

Boring Completed
08-10-2023

Terracon
23041 Avenida De La Carlota
Ste 350
Laguna Hills, CA

Boring Log No. T-2

Graphic Log	Location: See Exploration Plan Depth (Ft.)	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	EXPANSION INDEX	Water Content (%)	Dry Unit Weight (pcf)	Atterberg Limits LL-PL-PI	Percent Fines
▨	**CLAYEY SAND (SC)**, brown, loose			☒	4-4-5 N=9					47
	30.0		▽							
▨	**SANDY LEAN CLAY (CL)**, light brown, medium stiff to stiff	30		☒	2-3-5 N=8					
		35		☒	2-3-5 N=8					
	40.0									
▨	**CLAYEY SAND (SC)**, gray, medium dense	40		☒	8-9-13 N=22					
	brown	45		☒	4-8-9 N=17					43
		50								

See Exploration and Testing Procedures for a description of field and laboratory procedures used and additional data (If any).

See Supporting Information for explanation of symbols and abbreviations.

Notes

Water Level Observations
▽ At completion of drilling

Advancement Method
Hollow Stem Auger

Abandonment Method
Boring backfilled with cement grout slurry upon completion

Drill Rig
Diedrich D-50 (track)

Hammer Type
Automatic

Driller
Terracon

Logged by
AH

Boring Started
08-10-2023

Boring Completed
08-10-2023

Boring Log No. T-2

Graphic Log	Location: See Exploration Plan Depth (Ft.)	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	EXPANSION INDEX	Water Content (%)	Dry Unit Weight (pcf)	Atterberg Limits LL-PL-PI	Percent Fines
▨	**CLAYEY SAND (SC)**, gray, medium dense *(continued)* 51.5			☒	4-8-12 N=20					
	Boring Terminated at 51.5 Feet									

See Exploration and Testing Procedures for a description of field and laboratory procedures used and additional data (If any).

See Supporting Information for explanation of symbols and abbreviations.

Water Level Observations
▽ At completion of drilling

Notes

Advancement Method
Hollow Stem Auger

Abandonment Method
Boring backfilled with cement grout slurry upon completion

Drill Rig
Diedrich D-50 (track)

Hammer Type
Automatic

Driller
Terracon

Logged by
AH

Boring Started
08-10-2023

Boring Completed
08-10-2023

Terracon
23041 Avenida De La Carlota
Ste 350
Laguna Hills, CA

Boring Log No. T-3

Graphic Log	Location: See Exploration Plan Depth (Ft.)	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	EXPANSION INDEX	Water Content (%)	Dry Unit Weight (pcf)	Atterberg Limits LL-PL-PI	Percent Fines
▨	**SANDY LEAN CLAY (CL)**, brown			✋					39-14-25	
	medium stiff			⧗	2-2-3		15.5	85		
▨	5.0 **CLAYEY SAND (SC)**, brown, very loose	5		✋ ⊠	2-2-1 N=3					36
	loose			⧗	2-3-5		14.2	88		
	light brown	10		⊠	3-2-3 N=5					
▨	15.0 **SANDY LEAN CLAY (CL)**, dark brown, soft	15		⊠	2-1-2 N=3					72
▨	20.0 **CLAYEY SAND (SC)**, light brown, medium dense	20		⊠	2-4-6 N=10					38
	25.0	25								

See Exploration and Testing Procedures for a description of field and laboratory procedures used and additional data (If any).

See Supporting Information for explanation of symbols and abbreviations.

Notes

Water Level Observations
Groundwater not encountered

Advancement Method
Hollow Stem Auger

Abandonment Method
Boring backfilled with cement grout slurry upon completion

Drill Rig
Diedrich D-50 (track)

Hammer Type
Automatic

Driller
Terracon

Logged by
AH

Boring Started
08-09-2023

Boring Completed
08-10-2023

Darden Solar Facility
Cantua Creek | Fresno, CA
Terracon Project No. 60225172

Terracon
23041 Avenida De La Carlota
Ste 350
Laguna Hills, CA

Boring Log No. T-3

Graphic Log	Location: See Exploration Plan Depth (Ft.)	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	EXPANSION INDEX	Water Content (%)	Dry Unit Weight (pcf)	Atterberg Limits LL-PL-PI	Percent Fines
▨	**LEAN CLAY (CL)**, trace sand dark brown, very stiff			☒	3-6-11 N=17					
▨	brown, stiff	30		☒	3-6-7 N=13					90
▨	brown, stiff	35		☒	4-6-7 N=13					
▨	medium stiff	40		☒	3-3-4 N=7					
	41.5 ***Boring Terminated at 41.5 Feet***									

See Exploration and Testing Procedures for a description of field and laboratory procedures used and additional data (If any).

See Supporting Information for explanation of symbols and abbreviations.

Water Level Observations
Groundwater not encountered

Drill Rig
Diedrich D-50 (track)

Hammer Type
Automatic

Driller
Terracon

Logged by
AH

Boring Started
08-09-2023

Boring Completed
08-10-2023

Notes

Advancement Method
Hollow Stem Auger

Abandonment Method
Boring backfilled with cement grout slurry upon completion

Boring Log No. T-4

Graphic Log	Location: See Exploration Plan Depth (Ft.)	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	EXPANSION INDEX	Water Content (%)	Dry Unit Weight (pcf)	Atterberg Limits LL-PL-PI	Percent Fines
▨	**SANDY LEAN CLAY (CL)** light brown									
				✋					40-16-24	67
	medium stiff			⧗	2-3-5		18.3	71		
		5		✋						
	dark brown, soft to medium stiff			☒	2-2-2 N=4					
	light brown, medium stiff			⧗	2-3-4					
		10		☒	2-2-5 N=7					
	brown	15		☒	3-3-3 N=6					61
		20		☒	2-3-4 N=7					
		25								

See Exploration and Testing Procedures for a description of field and laboratory procedures used and additional data (If any).

See Supporting Information for explanation of symbols and abbreviations.

Notes

Water Level Observations
Groundwater not encountered

Advancement Method
Hollow Stem Auger

Abandonment Method
Boring backfilled with cement grout slurry upon completion

Drill Rig
Diedrich D-50 (track)

Hammer Type
Automatic

Driller
Terracon

Logged by
AH

Boring Started
08-09-2023

Boring Completed
08-09-2023

Darden Solar Facility
Cantua Creek | Fresno, CA
Terracon Project No. 60225172

Terracon
23041 Avenida De La Carlota
Ste 350
Laguna Hills, CA

Boring Log No. T-4

Graphic Log	Location: See Exploration Plan Depth (Ft.)	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	EXPANSION INDEX	Water Content (%)	Dry Unit Weight (pcf)	Atterberg Limits LL-PL-PI	Percent Fines
▨	**SANDY LEAN CLAY (CL)** *(continued)* light brown, medium stiff to stiff			☒	2-3-5 N=8					
▨	brown, very stiff	30		⧗	3-6-13		15.4	96		
	31.5									
	Boring Terminated at 31.5 Feet									

See Exploration and Testing Procedures for a description of field and laboratory procedures used and additional data (If any).

See Supporting Information for explanation of symbols and abbreviations.

Notes

Water Level Observations
Groundwater not encountered

Advancement Method
Hollow Stem Auger

Abandonment Method
Boring backfilled with cement grout slurry upon completion

Drill Rig
Diedrich D-50 (track)

Hammer Type
Automatic

Driller
Terracon

Logged by
AH

Boring Started
08-09-2023

Boring Completed
08-09-2023

Boring Log No. T-5

Graphic Log	Location: See Exploration Plan Depth (Ft.)	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	EXPANSION INDEX	Water Content (%)	Dry Unit Weight (pcf)	Atterberg Limits LL-PL-PI	Percent Fines
▨	**SANDY LEAN CLAY (CL)**, brown			✋						66
▨	medium stiff			⧗	3-3-3		11.6	71		
▨		5		✋ ☒	2-2-3 N=5					
▨	7.5 **CLAYEY SAND (SC)**, light brown, loose			⧗	3-4-7		9.3	80		
▨	medium dense	10		☒	4-3-6 N=9					
▨	15.0 **LEAN CLAY WITH SAND (CL)**, dark brown, stiff	15		☒	3-4-5 N=9					83
▨	20.0 **CLAYEY SAND (SC)** brown, loose	20		☒	3-2-3 N=5					45
		25								

See Exploration and Testing Procedures for a description of field and laboratory procedures used and additional data (If any).

See Supporting Information for explanation of symbols and abbreviations.

Notes

Water Level Observations
Groundwater not encountered

Advancement Method
Hollow Stem Auger

Abandonment Method
Boring backfilled with cement grout slurry upon completion

Drill Rig
Diedrich D-50 (track)

Hammer Type
Automatic

Driller
Terracon

Logged by
AH

Boring Started
08-09-2023

Boring Completed
08-09-2023

Terracon
23041 Avenida De La Carlota
Ste 350
Laguna Hills, CA

Boring Log No. T-5

Graphic Log	Location: See Exploration Plan Depth (Ft.)	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	EXPANSION INDEX	Water Content (%)	Dry Unit Weight (pcf)	Atterberg Limits LL-PL-PI	Percent Fines
▨	**CLAYEY SAND (SC)** *(continued)* light brown, medium dense			☒	4-5-6 N=11					
▨	loose	30		☒	4-4-4 N=8					
▨	light brown, medium dense	35		☒	7-8-9 N=17					
▨	sample disturbed	40		⧗	10-14-16		3.7			
	41.5 ***Boring Terminated at 41.5 Feet***									

See Exploration and Testing Procedures for a description of field and laboratory procedures used and additional data (If any).

See Supporting Information for explanation of symbols and abbreviations.

Notes

Water Level Observations
Groundwater not encountered

Advancement Method
Hollow Stem Auger

Abandonment Method
Boring backfilled with cement grout slurry upon completion

Drill Rig
Diedrich D-50 (track)

Hammer Type
Automatic

Driller
Terracon

Logged by
AH

Boring Started
08-09-2023

Boring Completed
08-09-2023

Darden Solar Facility
Cantua Creek | Fresno, CA
Terracon Project No. 60225172

23041 Avenida De La Carlota
Ste 350
Laguna Hills, CA

Boring Log No. T-6

Graphic Log	Location: See Exploration Plan Depth (Ft.)	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	EXPANSION INDEX	Water Content (%)	Dry Unit Weight (pcf)	Atterberg Limits LL-PL-PI	Percent Fines
▨	**LEAN CLAY WITH SAND (CL)**, dark brown			✋						71
▨	medium stiff			⧗	2-4-4		24.7	76		
▨	soft	5		✋ ⊠	2-1-2 N=3					
▨	medium stiff			⧗	1-4-4		28.5	76		
▨		10		⊠	1-2-3 N=5					
▨	soft	15		⊠	1-2-1 N=3					
▨	20.0 **SANDY LEAN CLAY (CL)**, brown, stiff	20		⧗	3-4-6		20.6	87		61
▨	25.0	25								

See Exploration and Testing Procedures for a description of field and laboratory procedures used and additional data (If any).

See Supporting Information for explanation of symbols and abbreviations.

Water Level Observations
Groundwater not encountered

Drill Rig
Diedrich D-50 (track)

Hammer Type
Automatic

Driller
Terracon

Logged by
AH

Boring Started
08-08-2023

Boring Completed
08-08-2023

Notes

Advancement Method
Hollow Stem Auger

Abandonment Method
Boring backfilled with cement grout slurry upon completion

23041 Avenida De La Carlota
Ste 350
Laguna Hills, CA

Boring Log No. T-6

Graphic Log	Location: See Exploration Plan Depth (Ft.)	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	EXPANSION INDEX	Water Content (%)	Dry Unit Weight (pcf)	Atterberg Limits LL-PL-PI	Percent Fines
▨	**CLAYEY SAND (SC)**, light brown, medium dense			☒	4-7-4 N=11					
▨	loose	30		☒	2-3-4 N=7					
▨	light brown, medium dense	35		☒	7-6-6 N=12					
▨	brown, loose	40		☒	3-3-3 N=6					
▨	trace gravel, light brown, medium dense	45		☒	10-15-7 N=22					
▨	50.0	50								

See Exploration and Testing Procedures for a description of field and laboratory procedures used and additional data (If any).

See Supporting Information for explanation of symbols and abbreviations.

Notes

Water Level Observations
Groundwater not encountered

Advancement Method
Hollow Stem Auger

Abandonment Method
Boring backfilled with cement grout slurry upon completion

Drill Rig
Diedrich D-50 (track)

Hammer Type
Automatic

Driller
Terracon

Logged by
AH

Boring Started
08-08-2023

Boring Completed
08-08-2023

Boring Log No. T-6

Graphic Log	Location: See Exploration Plan Depth (Ft.)	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	EXPANSION INDEX	Water Content (%)	Dry Unit Weight (pcf)	Atterberg Limits LL-PL-PI	Percent Fines
▨	**LEAN CLAY WITH SAND (CL)**, brown, medium stiff 51.5			☒	4-2-5 N=7					
	Boring Terminated at 51.5 Feet									

See Exploration and Testing Procedures for a description of field and laboratory procedures used and additional data (If any).

See Supporting Information for explanation of symbols and abbreviations.

Water Level Observations
Groundwater not encountered

Notes

Advancement Method
Hollow Stem Auger

Abandonment Method
Boring backfilled with cement grout slurry upon completion

Drill Rig
Diedrich D-50 (track)

Hammer Type
Automatic

Driller
Terracon

Logged by
AH

Boring Started
08-08-2023

Boring Completed
08-08-2023

Terracon
23041 Avenida De La Carlota
Ste 350
Laguna Hills, CA

Boring Log No. T-7

Location: See Exploration Plan

Graphic Log	Depth (Ft.)	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	EXPANSION INDEX	Water Content (%)	Dry Unit Weight (pcf)	Atterberg Limits LL-PL-PI	Percent Fines
▨	**LEAN CLAY (CL)**, dark brown			✋						
	stiff			⧗	3-4-7		31.3	68		
	5.0	5								
▨	**LEAN CLAY WITH SAND (CL)**, dark brown, soft			✋ ⊠	2-1-2 N=3					85
				⧗	2-2-2		20.0	82		
	10.0	10								
▨	**CLAYEY SAND (SC)**, dark brown, loose			⊠	1-2-2 N=4					
	medium dense	15		⊠	3-5-7 N=12					
		20		⊠	4-5-6 N=11					
	25.0	25								

See Exploration and Testing Procedures for a description of field and laboratory procedures used and additional data (If any).

See Supporting Information for explanation of symbols and abbreviations.

Notes

Water Level Observations
Groundwater not encountered

Advancement Method
Hollow Stem Auger

Abandonment Method
Boring backfilled with cement grout slurry upon completion

Drill Rig
Diedrich D-50 (track)

Hammer Type
Automatic

Driller
Terracon

Logged by
AH

Boring Started
08-08-2023

Boring Completed
08-08-2023

Boring Log No. T-7

Graphic Log	Location: See Exploration Plan Depth (Ft.)	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	EXPANSION INDEX	Water Content (%)	Dry Unit Weight (pcf)	Atterberg Limits LL-PL-PI	Percent Fines
▨	**SANDY LEAN CLAY (CL)**, dark brown, medium stiff			☒	3-3-4 N=7					70
▨	stiff	30		☒	3-4-5 N=9					
	31.5 ***Boring Terminated at 31.5 Feet***									

See Exploration and Testing Procedures for a description of field and laboratory procedures used and additional data (If any).

See Supporting Information for explanation of symbols and abbreviations.

Notes

Water Level Observations
Groundwater not encountered

Advancement Method
Hollow Stem Auger

Abandonment Method
Boring backfilled with cement grout slurry upon completion

Drill Rig
Diedrich D-50 (track)

Hammer Type
Automatic

Driller
Terracon

Logged by
AH

Boring Started
08-08-2023

Boring Completed
08-08-2023

Terracon
23041 Avenida De La Carlota
Ste 350
Laguna Hills, CA

Boring Log No. T-8

Location: See Exploration Plan

Depth (Ft.)	Description	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	EXPANSION INDEX	Water Content (%)	Dry Unit Weight (pcf)	Atterberg Limits LL-PL-PI	Percent Fines
	SANDY LEAN CLAY (CL), brown									
	medium stiff				1-3-4		21.4	84		
	soft to medium stiff	5			1-2-2 N=4					
	medium stiff				2-2-4					
10.0	**SANDY SILT (ML)**, brown, stiff	10			3-4-5 N=9				NP	54
	medium stiff	15			3-3-3 N=6					
20.0	**SILTY SAND (SM)** light brown, loose	20			5-4-5 N=9					43
		25								

See Exploration and Testing Procedures for a description of field and laboratory procedures used and additional data (If any).

See Supporting Information for explanation of symbols and abbreviations.

Notes

Water Level Observations
Groundwater not encountered

Advancement Method
Hollow Stem Auger

Abandonment Method
Boring backfilled with cement grout slurry upon completion

Drill Rig
Diedrich D-50 (track)

Hammer Type
Automatic

Driller
Terracon

Logged by
AC

Boring Started
07-31-2023

Boring Completed
07-31-2023

Boring Log No. T-8

Graphic Log	Location: See Exploration Plan Depth (Ft.)	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	EXPANSION INDEX	Water Content (%)	Dry Unit Weight (pcf)	Atterberg Limits LL-PL-PI	Percent Fines
	SILTY SAND (SM) *(continued)* brown, medium dense			☒	3-5-7 N=12				NP	39
	30.0 **SANDY LEAN CLAY (CL)**, brown, medium stiff to stiff	30		☒	2-3-5 N=8					
	35.0 **CLAYEY SAND (SC)**, brown, medium dense	35		☒	4-6-6 N=12					29
	40.0 **SANDY LEAN CLAY (CL)**, brown, stiff	40		☒	5-5-6 N=11					
	45.0 **CLAYEY SAND (SC)**, brown, very dense	45		☒	3-15-37 N=52					
		50								

See Exploration and Testing Procedures for a description of field and laboratory procedures used and additional data (If any).

See Supporting Information for explanation of symbols and abbreviations.

Notes

Water Level Observations
Groundwater not encountered

Advancement Method
Hollow Stem Auger

Abandonment Method
Boring backfilled with cement grout slurry upon completion

Drill Rig
Diedrich D-50 (track)

Hammer Type
Automatic

Driller
Terracon

Logged by
AC

Boring Started
07-31-2023

Boring Completed
07-31-2023

Boring Log No. T-8

Graphic Log	Location: See Exploration Plan Depth (Ft.)	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	EXPANSION INDEX	Water Content (%)	Dry Unit Weight (pcf)	Atterberg Limits LL-PL-PI	Percent Fines
▨	**CLAYEY SAND (SC)**, brown, very dense *(continued)* 51.5			☒	21-25-27 N=52					
	Boring Terminated at 51.5 Feet									

See Exploration and Testing Procedures for a description of field and laboratory procedures used and additional data (If any).

See Supporting Information for explanation of symbols and abbreviations.

Water Level Observations
Groundwater not encountered

Notes

Advancement Method
Hollow Stem Auger

Abandonment Method
Boring backfilled with cement grout slurry upon completion

Drill Rig
Diedrich D-50 (track)

Hammer Type
Automatic

Driller
Terracon

Logged by
AC

Boring Started
07-31-2023

Boring Completed
07-31-2023

Terracon
23041 Avenida De La Carlota
Ste 350
Laguna Hills, CA

Boring Log No. T-9

Graphic Log	Location: See Exploration Plan Depth (Ft.)	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	EXPANSION INDEX	Water Content (%)	Dry Unit Weight (pcf)	Atterberg Limits LL-PL-PI	Percent Fines
▨	**SANDY LEAN CLAY (CL)**, dark brown			|					38-16-22	61
▨	brown, stiff			⧗	2-3-7		31.5	78		
▨	medium stiff	5		✋ ☒	2-2-3 N=5					
▨	brown			⧗	1-2-3					52
▨	brown, stiff	10		☒	2-6-8 N=14					
▨	15.0									
▨	**CLAYEY SAND (SC)**, light brown, medium dense	15		☒	7-5-5 N=10					
▨		20		☒	8-9-7 N=16					
▨	25.0	25								

See Exploration and Testing Procedures for a description of field and laboratory procedures used and additional data (If any).

See Supporting Information for explanation of symbols and abbreviations.

Notes

Water Level Observations
Groundwater not encountered

Advancement Method
Hollow Stem Auger

Abandonment Method
Boring backfilled with cement grout slurry upon completion

Drill Rig
Diedrich D-50 (track)

Hammer Type
Automatic

Driller
Terracon

Logged by
AC

Boring Started
07-31-2023

Boring Completed
07-31-2023

Boring Log No. T-9

Graphic Log	Location: See Exploration Plan Depth (Ft.)	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	EXPANSION INDEX	Water Content (%)	Dry Unit Weight (pcf)	Atterberg Limits LL-PL-PI	Percent Fines
▨	**SANDY SILTY CLAY (CL-ML)**, dark brown, stiff			☒	3-5-5 N=10				29-22-7	
▨		30		☒	4-5-6 N=11					
▨	brown	35		☒	2-5-5 N=10					
▨		40		☒	4-5-7 N=12					
	41.5 ***Boring Terminated at 41.5 Feet***									

See Exploration and Testing Procedures for a description of field and laboratory procedures used and additional data (If any).

See Supporting Information for explanation of symbols and abbreviations.

Notes

Water Level Observations
Groundwater not encountered

Advancement Method
Hollow Stem Auger

Abandonment Method
Boring backfilled with cement grout slurry upon completion

Drill Rig
Diedrich D-50 (track)

Hammer Type
Automatic

Driller
Terracon

Logged by
AC

Boring Started
07-31-2023

Boring Completed
07-31-2023

Darden Solar Facility
Cantua Creek | Fresno, CA
Terracon Project No. 60225172

Terracon
23041 Avenida De La Carlota
Ste 350
Laguna Hills, CA

Boring Log No. T-10

Graphic Log	Location: See Exploration Plan Depth (Ft.)	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	EXPANSION INDEX	Water Content (%)	Dry Unit Weight (pcf)	Atterberg Limits LL-PL-PI	Percent Fines
	LEAN CLAY WITH SAND (CL), brown									74
	stiff				5-5-9		11.9	82		
	5.0 **SANDY LEAN CLAY (CL)**, brown, very stiff	5			7-8-10 N=18					
					9-13-23		9.1	101		
	light brown	10			7-9-11 N=20				41-21-20	
	15.0 **CLAYEY SAND (SC)**, brown loose	15			4-4-5 N=9					34
	trace gravel, brown, dense	20			12-18-19 N=37					
		25								

See Exploration and Testing Procedures for a description of field and laboratory procedures used and additional data (If any).

See Supporting Information for explanation of symbols and abbreviations.

Notes

Water Level Observations
Groundwater not encountered

Advancement Method
Hollow Stem Auger

Abandonment Method
Boring backfilled with cement grout slurry upon completion

Drill Rig
Diedrich D-50 (track)

Hammer Type
Automatic

Driller
Terracon

Logged by
AC

Boring Started
07-31-2023

Boring Completed
07-31-2023

Boring Log No. T-10

Graphic Log	Location: See Exploration Plan Depth (Ft.)	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	EXPANSION INDEX	Water Content (%)	Dry Unit Weight (pcf)	Atterberg Limits LL-PL-PI	Percent Fines
▨	**CLAYEY SAND (SC)**, brown *(continued)* dense			☒	8-10-23 N=33					
▨	very dense	30		☒	16-27-47 N=74					
	31.5									
	Boring Terminated at 31.5 Feet									

See Exploration and Testing Procedures for a description of field and laboratory procedures used and additional data (If any).

See Supporting Information for explanation of symbols and abbreviations.

Notes

Water Level Observations
Groundwater not encountered

Advancement Method
Hollow Stem Auger

Abandonment Method
Boring backfilled with cement grout slurry upon completion

Drill Rig
Diedrich D-50 (track)

Hammer Type
Automatic

Driller
Terracon

Logged by
AC

Boring Started
07-31-2023

Boring Completed
07-31-2023

SUMMARY

OF

CONE PENETRATION TEST DATA

Project:

Darden Solar
Westside, CA
April 3-7, 2023

Prepared for:

Mr. Victor Nguyen
Terracon Consultants, Inc.
23041 Avenida De La Carlota, Ste 350
Laguna Hills, CA 92653
Office (949) 261-0051 / Fax (949) 261-6110

Prepared by:

KEHOE TESTING & ENGINEERING
5415 Industrial Drive
Huntington Beach, CA 92649-1518
Office (714) 901-7270 / Fax (714) 901-7289
www.kehoetesting.com

TABLE OF CONTENTS

SUMMARY

OF

CONE PENETRATION TEST DATA

1. INTRODUCTION

This report presents the results of a Cone Penetration Test (CPT) program carried out for the Darden Solar project located in Westside, California. The work was performed by Kehoe Testing & Engineering (KTE) on April 3-7, 2023. The scope of work was performed as directed by Terracon Consultants, Inc. personnel.

2. SUMMARY OF FIELD WORK

The fieldwork consisted of performing CPT soundings at 39 locations to determine the soil lithology. A summary is provided in **TABLE 2.1**.

LOCATION	DEPTH OF CPT (ft)	COMMENTS/NOTES:
CPT-1	20	
CPT-2	21	
CPT-3	20	
CPT-6	20	
CPT-7	20	
CPT-8	20	
CPT-10	20	
CPT-11	20	
CPT-12	20	
CPT-14	20	
CPT-15	20	
CPT-18	20	
CPT-19	20	
CPT-20	20	
CPT-21	20	
CPT-22	20	
CPT-23	20	
CPT-24	20	
CPT-25	20	
CPT-26	20	
CPT-27	20	
CPT-28	20	
CPT-29	20	
CPT-30	20	
CPT-31	20	
CPT-32	20	

LOCATION	DEPTH OF CPT (ft)	COMMENTS/NOTES:
CPT-33	20	
CPT-34	20	
CPT-35	20	
CPT-36	20	
CPT-37	20	
CPT-38	20	
CPT-39	20	
CPT-40	20	
CPT-41	20	
CPT-42	20	
CPT-43	20	
CPT-44	20	
CPT-45	20	

TABLE 2.1 - Summary of CPT Soundings

3. FIELD EQUIPMENT & PROCEDURES

The CPT soundings were carried out by **KTE** using an integrated electronic cone system manufactured by Vertek. The CPT soundings were performed in accordance with ASTM standards (D5778). The cone penetrometers were pushed using a direct push rig anchored with an eight-inch diameter ground anchor. This rig has a pushing capacity of approximately 15 tons. The cone used during the program was a 10 cm^2 cone with a cone net area ratio of 0.83. The following parameters were recorded at approximately 2.5 cm depth intervals:

- Cone Resistance (qc)
- Sleeve Friction (fs)
- Dynamic Pore Pressure (u)
- Inclination
- Penetration Speed

The above parameters were recorded and viewed in real time using a laptop computer. Data is stored at the KTE office for up to 2 years for future analysis and reference. A complete set of baseline readings was taken prior to each sounding to determine temperature shifts and any zero load offsets. Monitoring base line readings ensures that the cone electronics are operating properly.

4. CONE PENETRATION TEST DATA & INTERPRETATION

The Cone Penetration Test data is presented in graphical form in the attached Appendix. These plots were generated using the CPeT-IT program. Penetration depths are referenced to ground surface. The soil behavior type on the CPT plots is derived from the attached CPT SBT plot (Robertson, “Interpretation of Cone Penetration Test…”, 2009) and presents major soil lithologic changes. The stratigraphic interpretation is based on relationships between cone resistance (qc), sleeve friction (fs), and penetration pore pressure (u). The friction ratio (Rf), which is sleeve friction divided by cone resistance, is a calculated parameter that is used along with cone resistance to infer soil behavior type. Generally, cohesive soils (clays) have high friction ratios, low cone resistance and generate excess pore water pressures. Cohesionless soils (sands) have lower friction ratios, high cone bearing and generate little (or negative) excess pore water pressures.

The CPT data files have also been provided. These files can be imported in CPeT-IT (software by GeoLogismiki) and other programs to calculate various geotechnical parameters.

It should be noted that it is not always possible to clearly identify a soil type based on qc, fs and u. In these situations, experience, judgement and an assessment of the pore pressure data should be used to infer the soil behavior type.

If you have any questions regarding this information, please do not hesitate to call our office at (714) 901-7270.

Sincerely,

KEHOE TESTING & ENGINEERING

Steven P. Kehoe
President

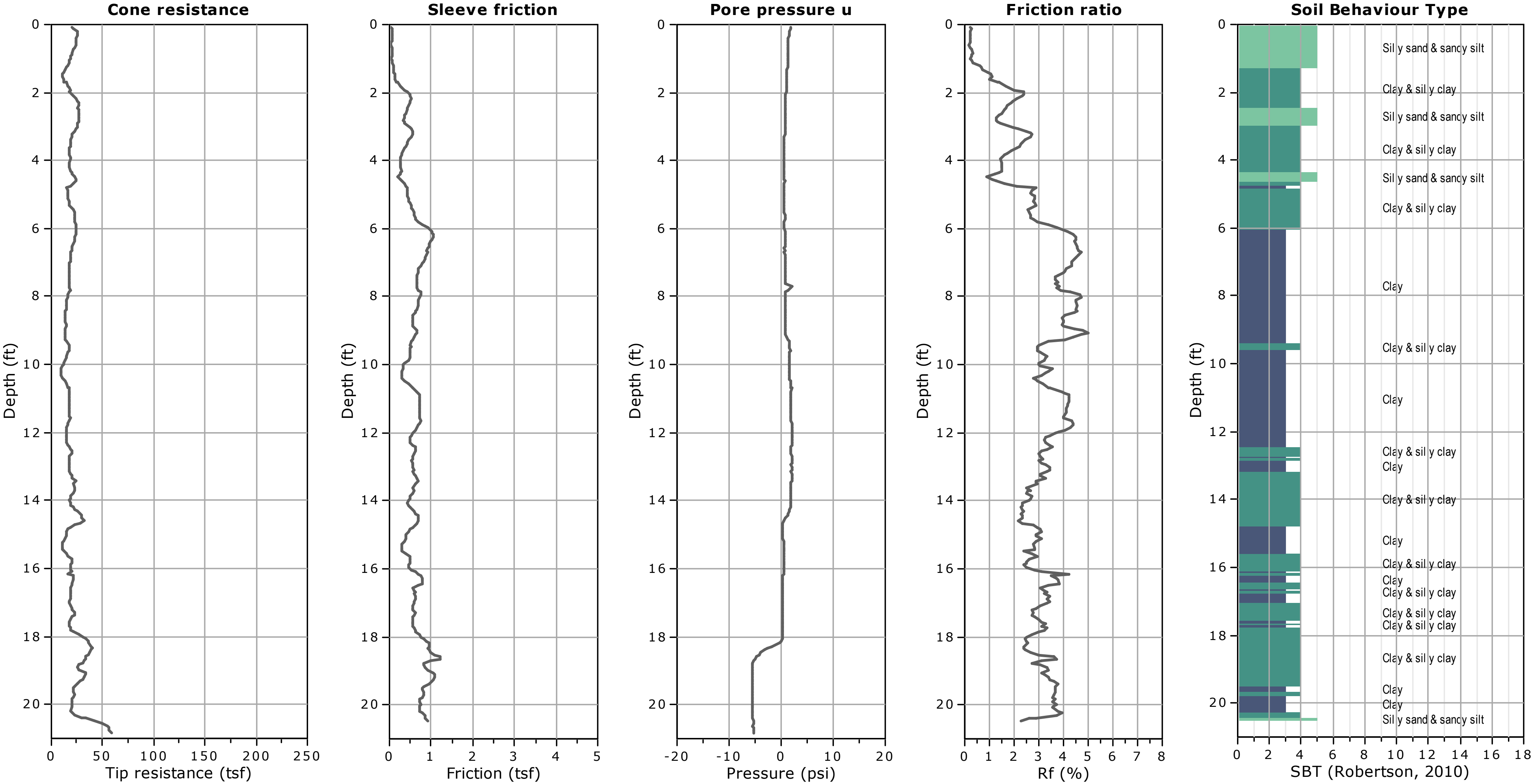
04/13/23-aa-5298

APPENDIX

Kehoe Testing and Engineering
714-901-7270
steve@kehoetesting.com
www.kehoetesting.com

Project: **Terracon Consultants / Darden Solar**
Location: **Westside, CA**

CPT-1
Total depth: 20.82 ft, Date: 4/4/2023



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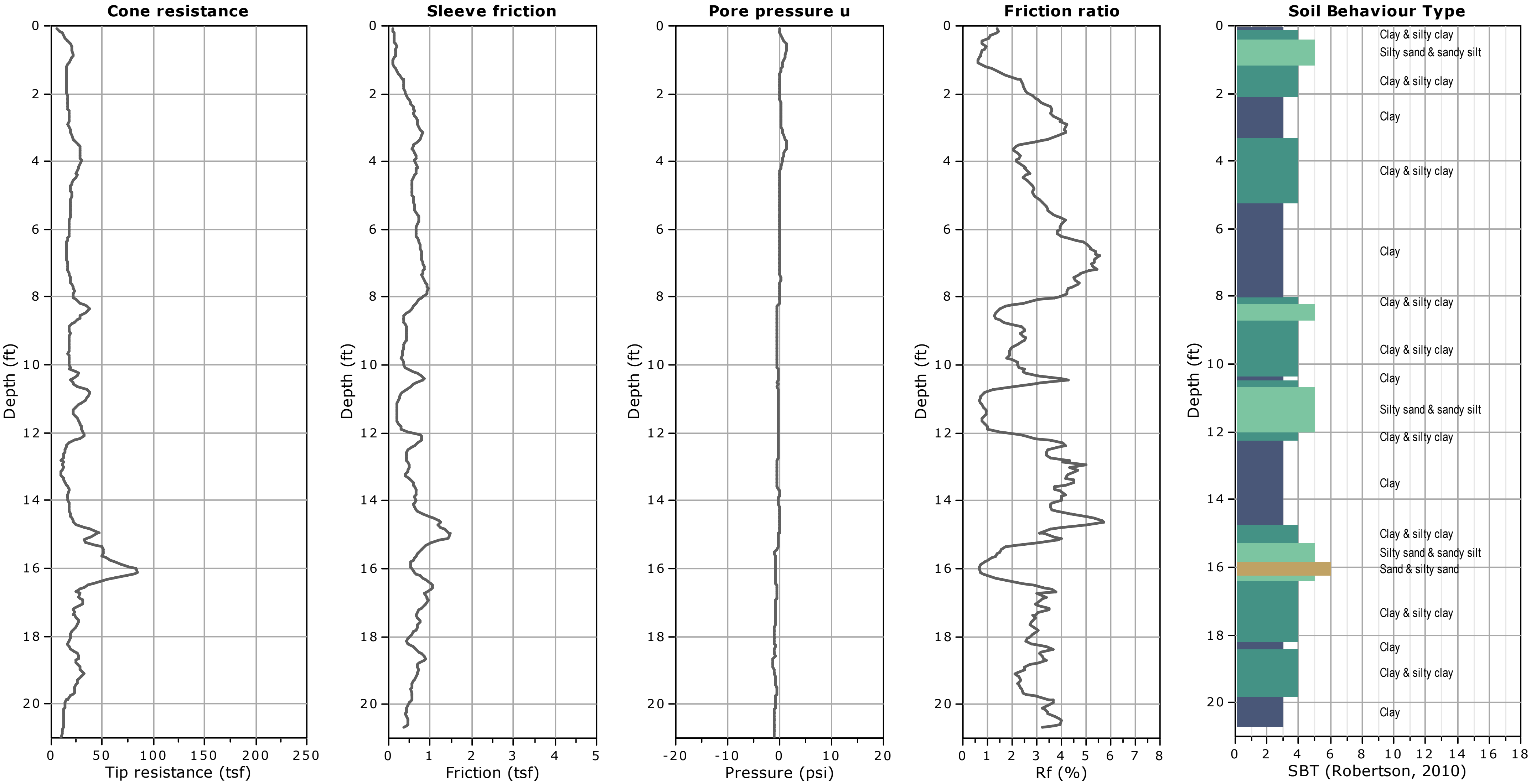
Project: **Terracon Consultants / Darden Solar**
Location: **Westside, CA**

CPT-2
Total depth: 21.00 ft, Date: 4/3/2023



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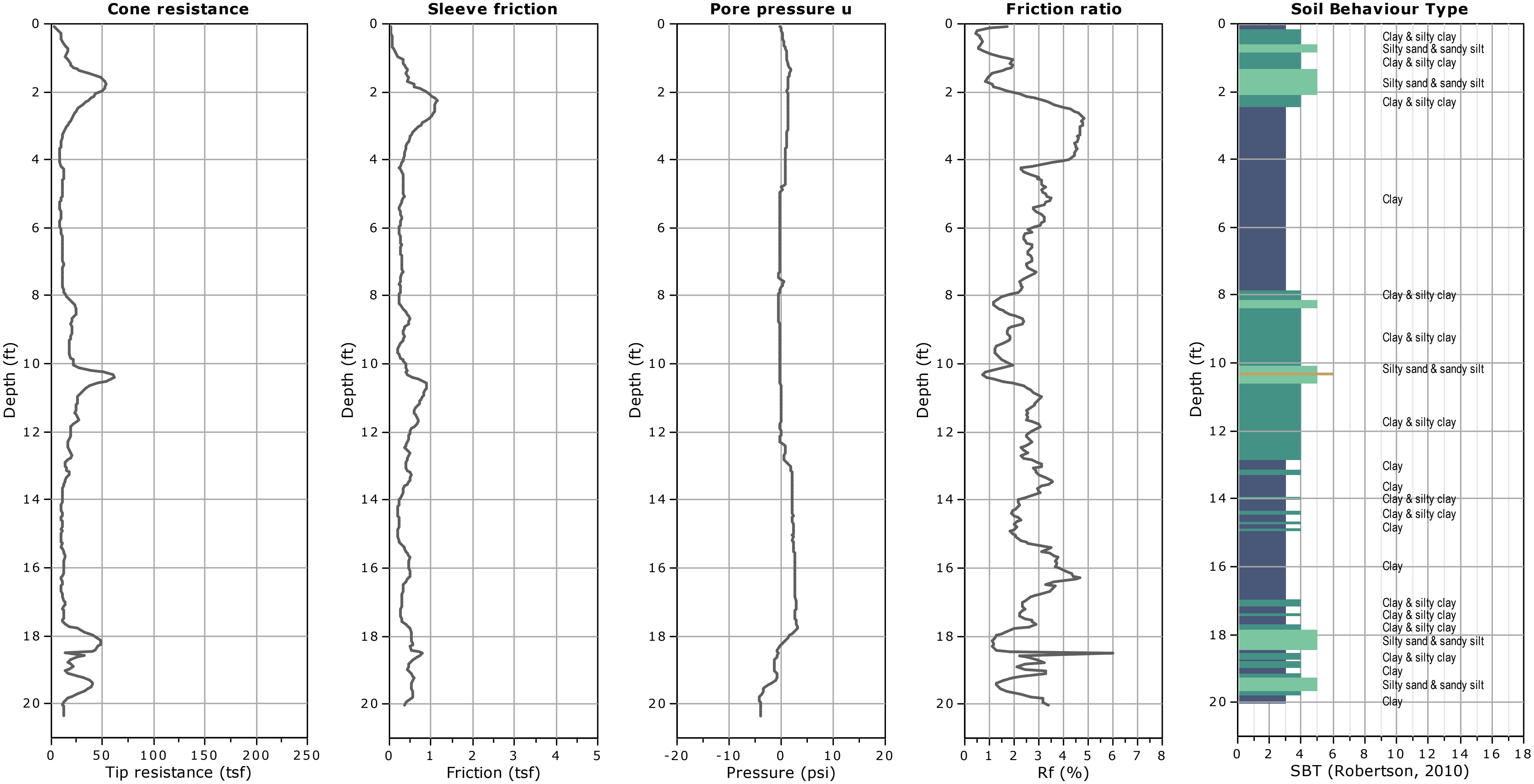
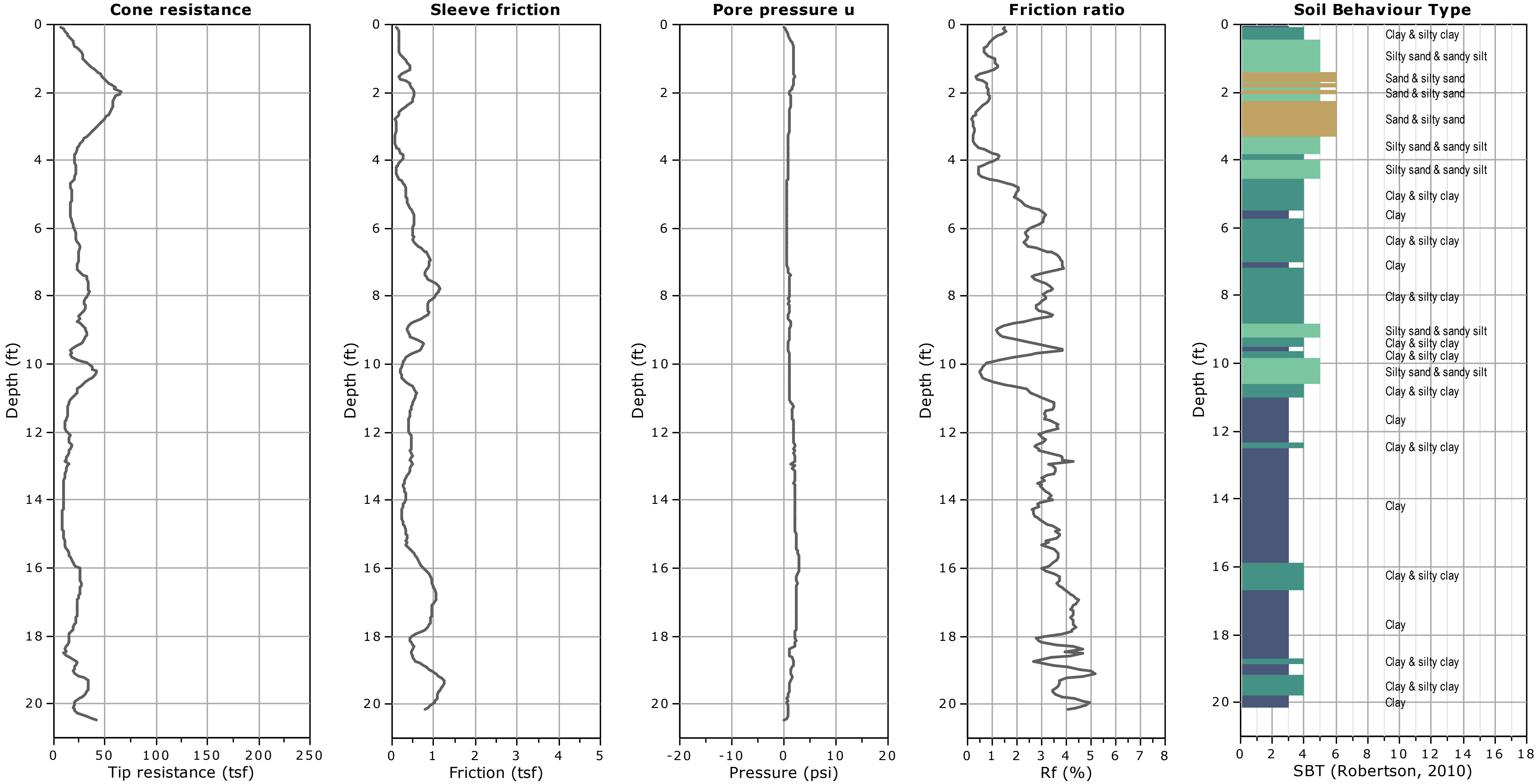
Project: **Terracon Consultants / Darden Solar**
Location: **Westside, CA**

CPT-3
Total depth: 20.35 ft, Date: 4/4/2023



Project: **Terracon Consultants / Darden Solar**
Location: **Westside, CA**

CPT-6
Total depth: 20.49 ft, Date: 4/4/2023



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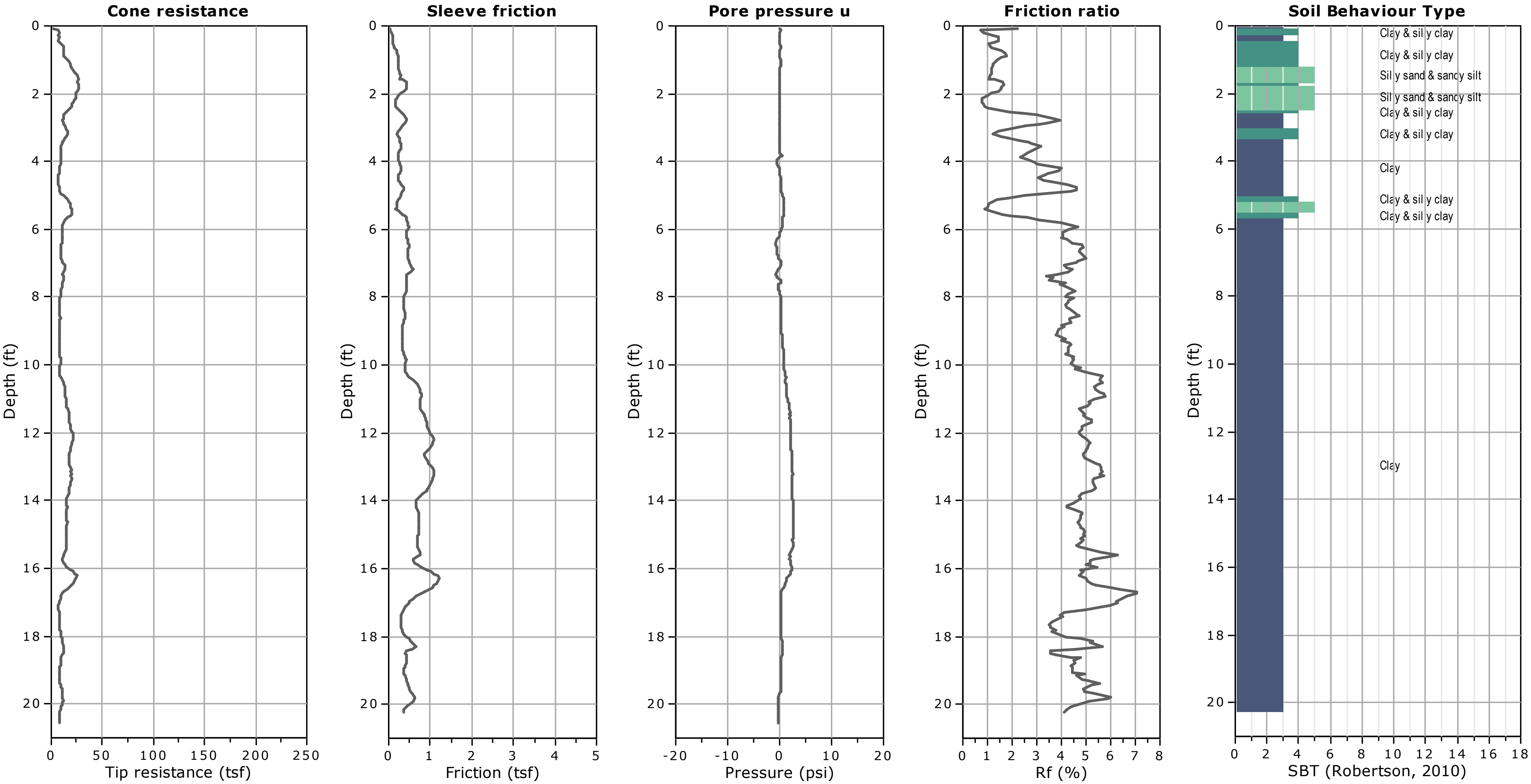
www.kehoetesting.com

Project: **Terracon Consultants / Darden Solar**
Location: **Westside, CA**

CPT-7
Total depth: 20.55 ft, Date: 4/3/2023



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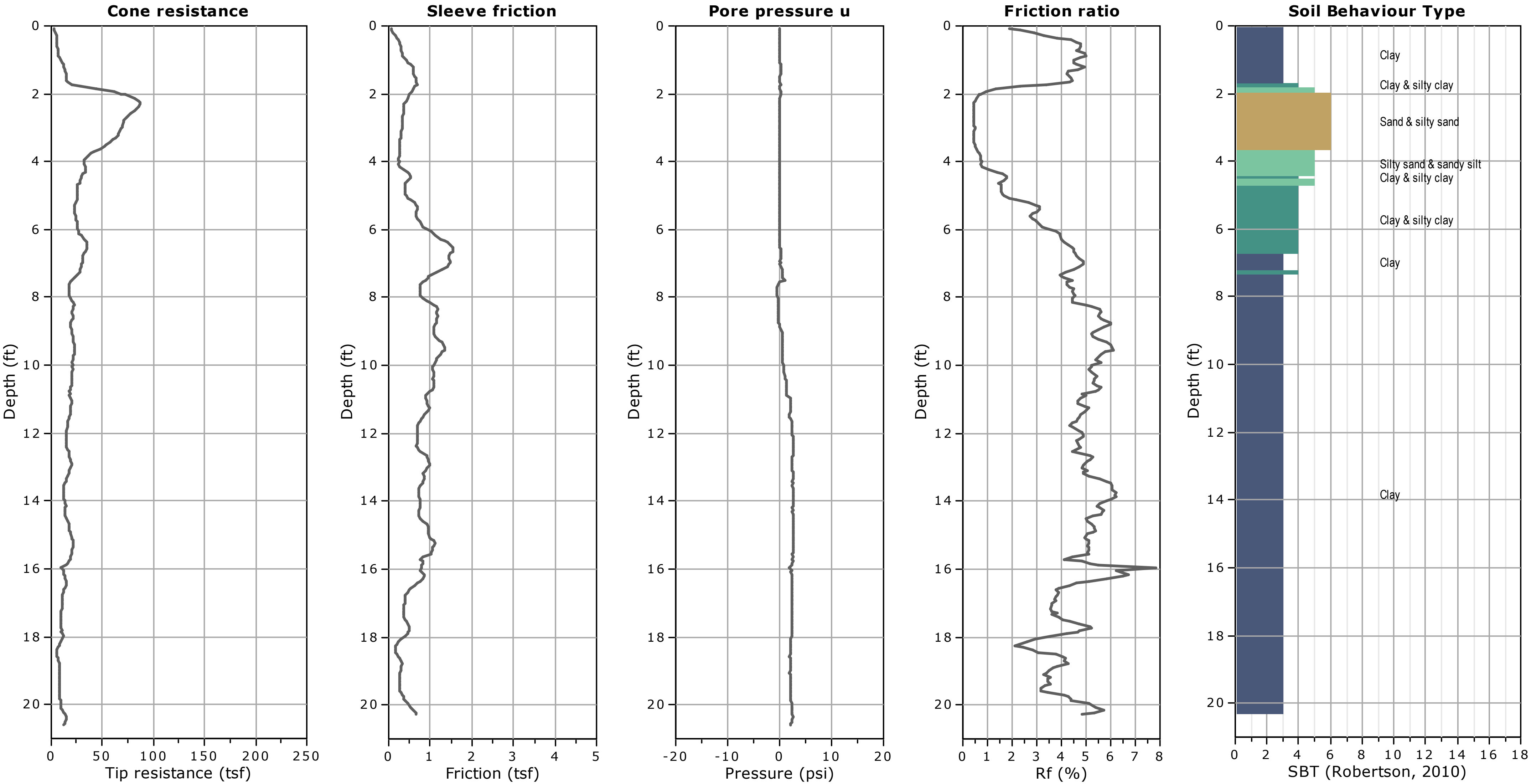
www.kehoetesting.com

Project: **Terracon Consultants / Darden Solar**
Location: **Westside, CA**

CPT-8
Total depth: 20.61 ft, Date: 4/3/2023



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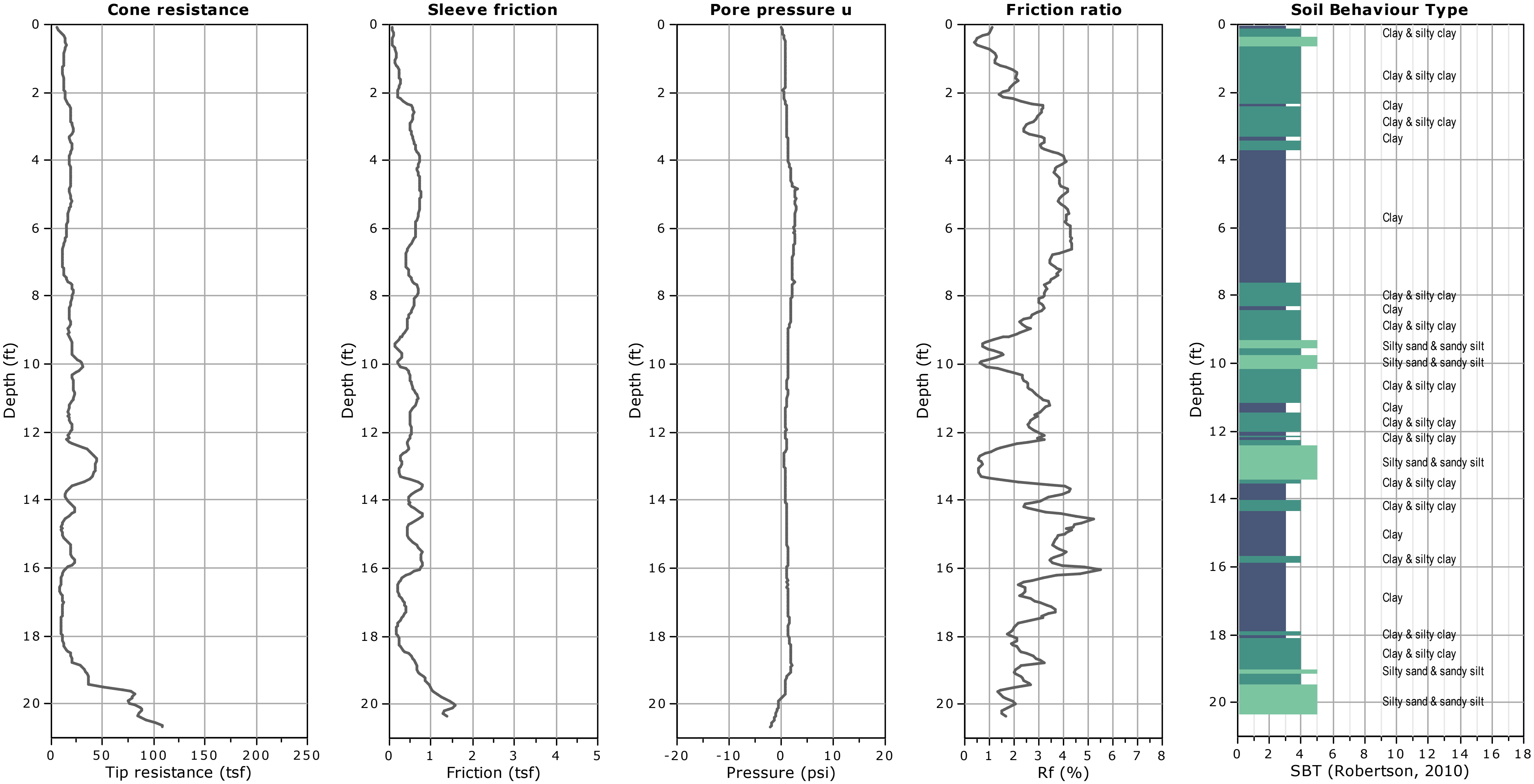
steve@kehoetesting.com
www.kehoetesting.com

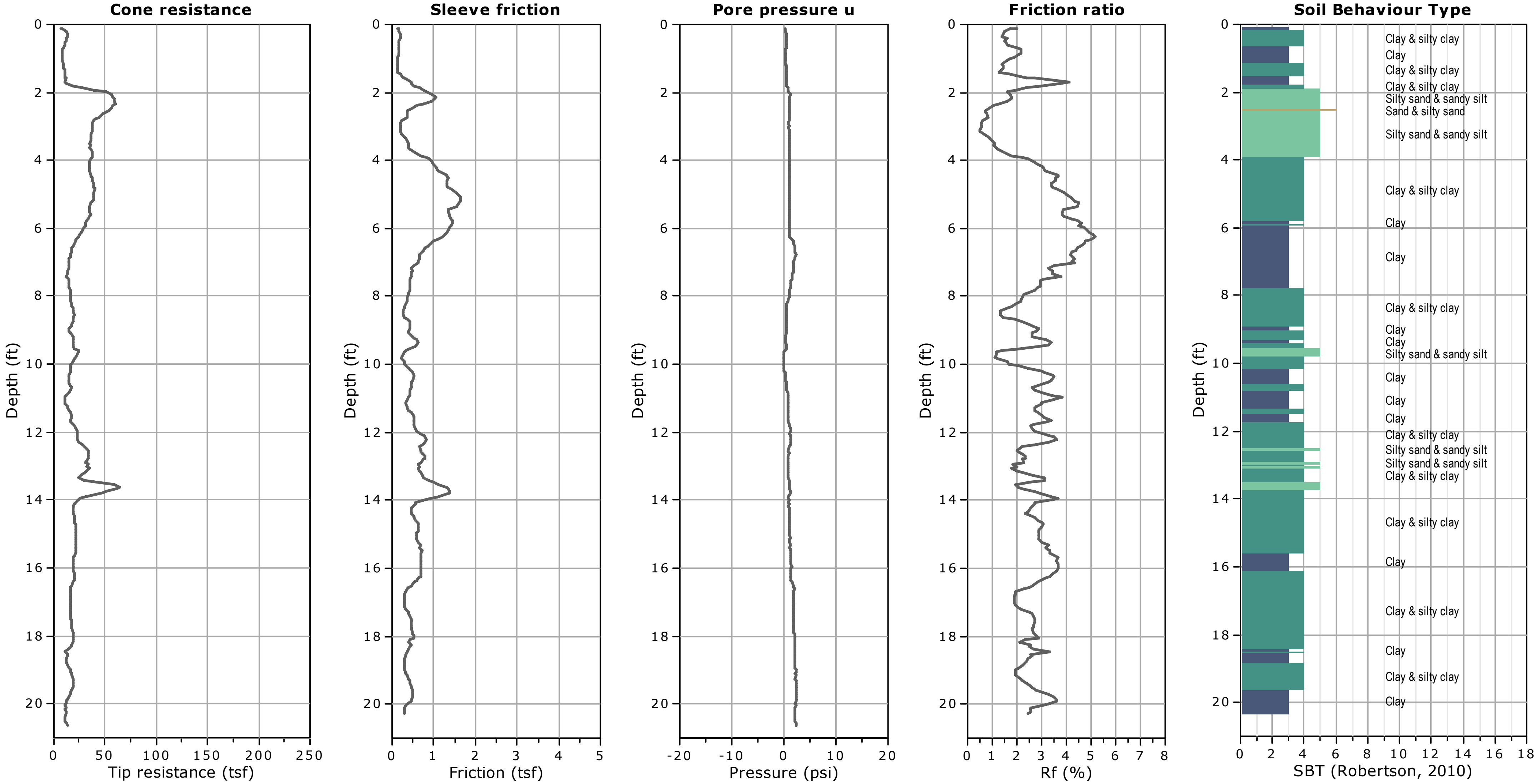
Project: **Terracon Consultants / Darden Solar**
Location: **Westside, CA**

CPT-10
Total depth: 20.69 ft, Date: 4/4/2023



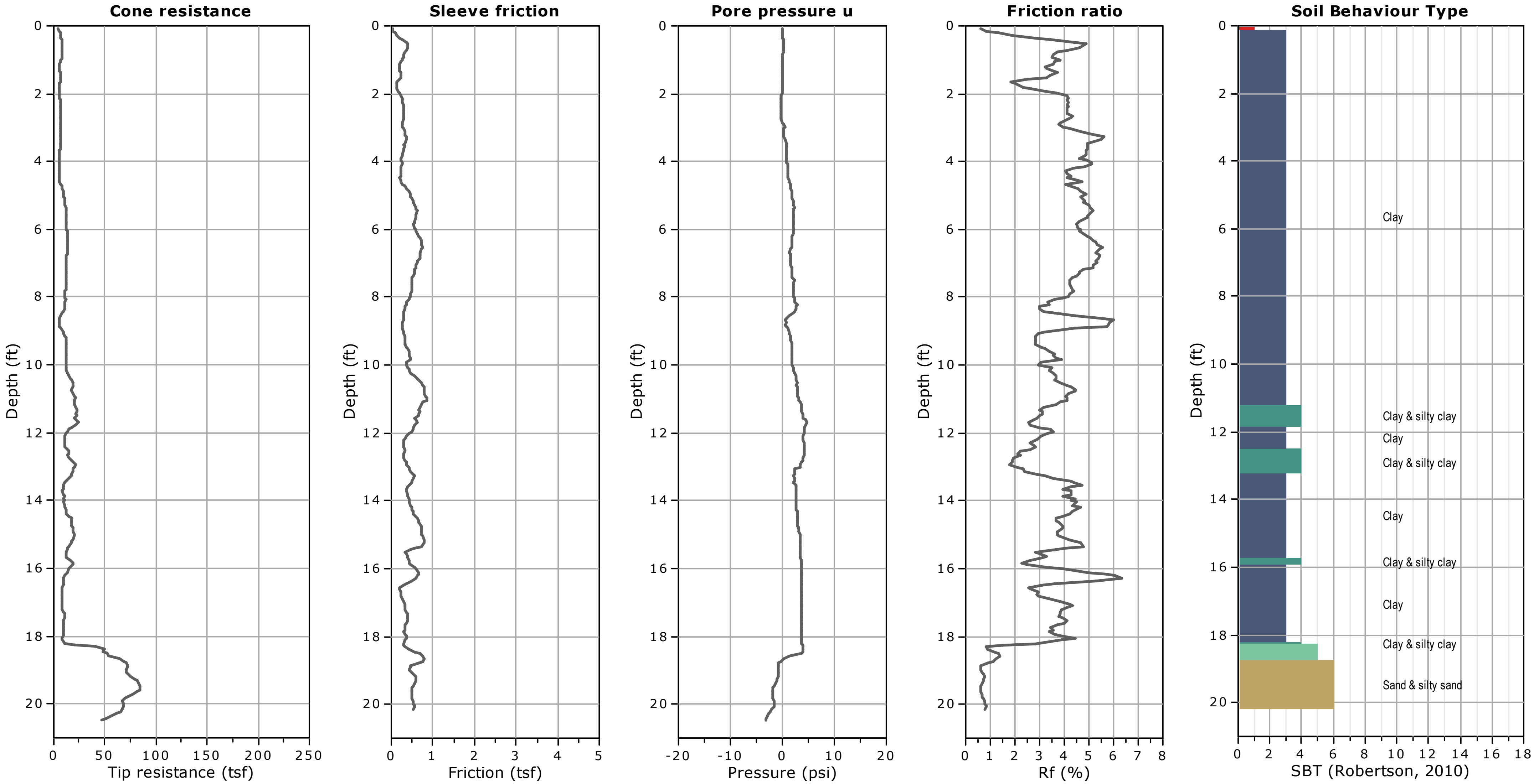
Project: **Terracon Consultants / Darden Solar**
Location: **Westside, CA**

CPT-11
Total depth: 20.63 ft, Date: 4/4/2023



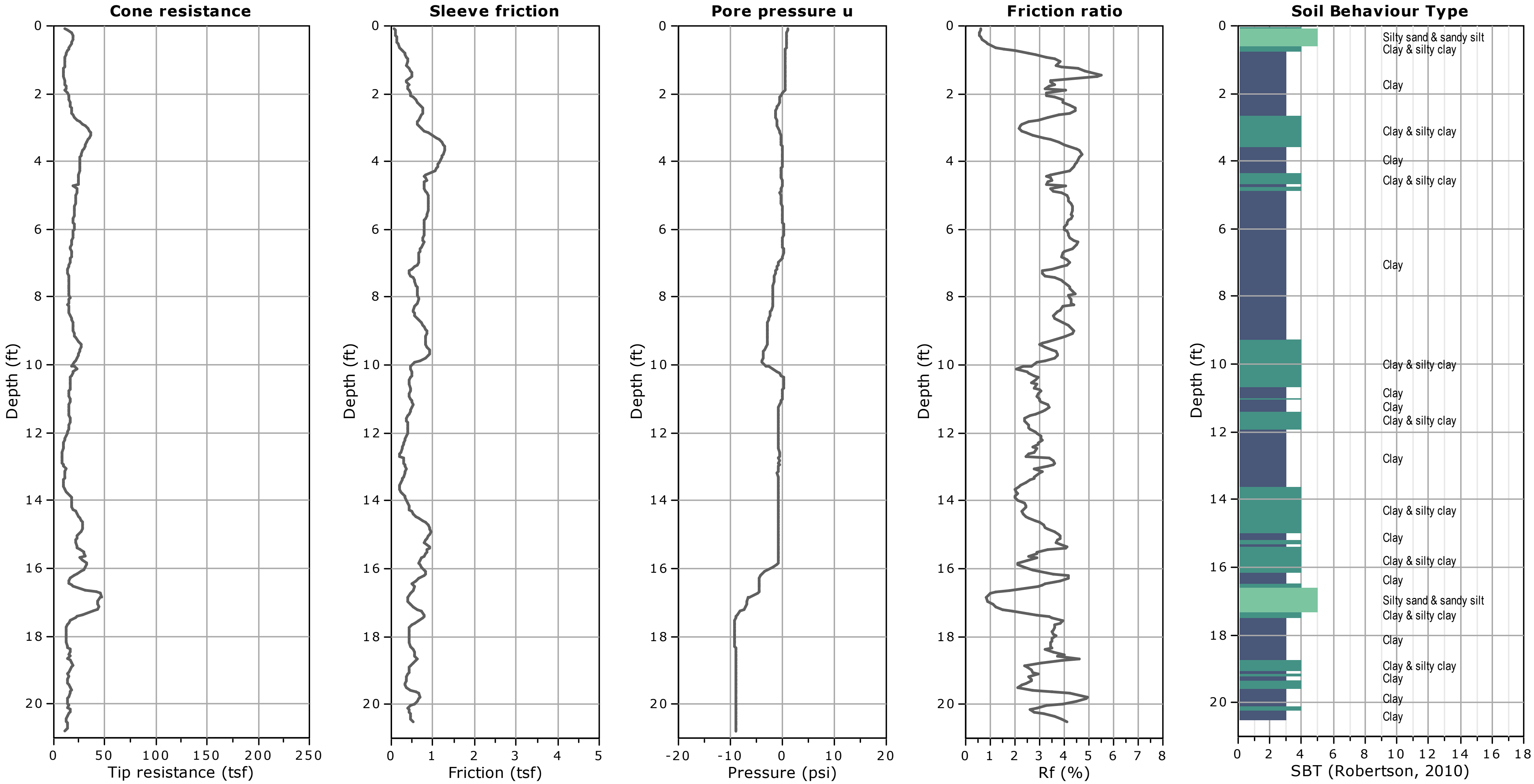
Project: **Terracon Consultants / Darden Solar**
Location: **Westside, CA**

CPT-12
Total depth: 20.48 ft, Date: 4/4/2023



Project: **Terracon Consultants / Darden Solar**
Location: **Westside, CA**

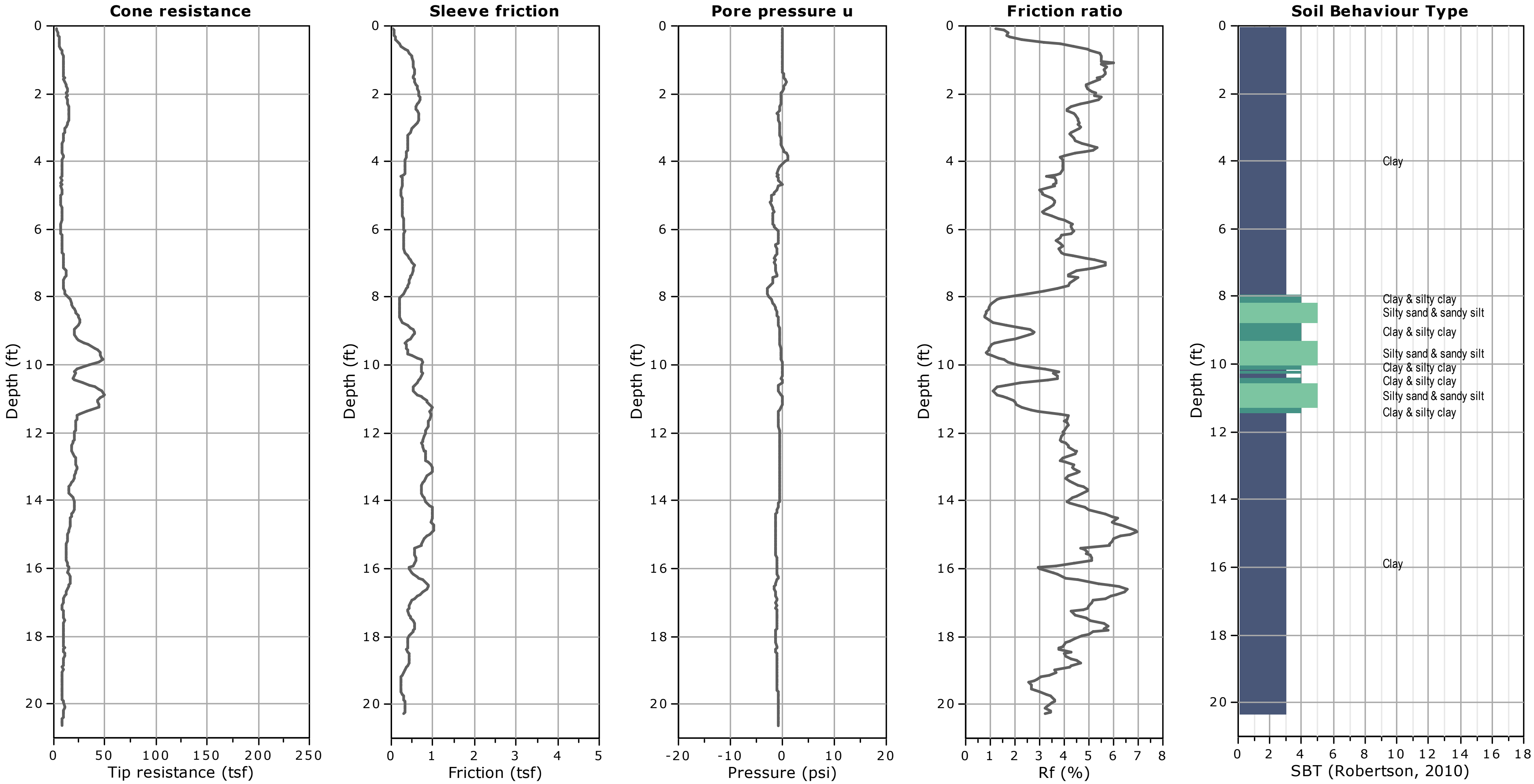
CPT-14
Total depth: 20.81 ft, Date: 4/3/2023



]

Project: **Terracon Consultants / Darden Solar**
Location: **Westside, CA**

CPT-15
Total depth: 20.63 ft, Date: 4/3/2023



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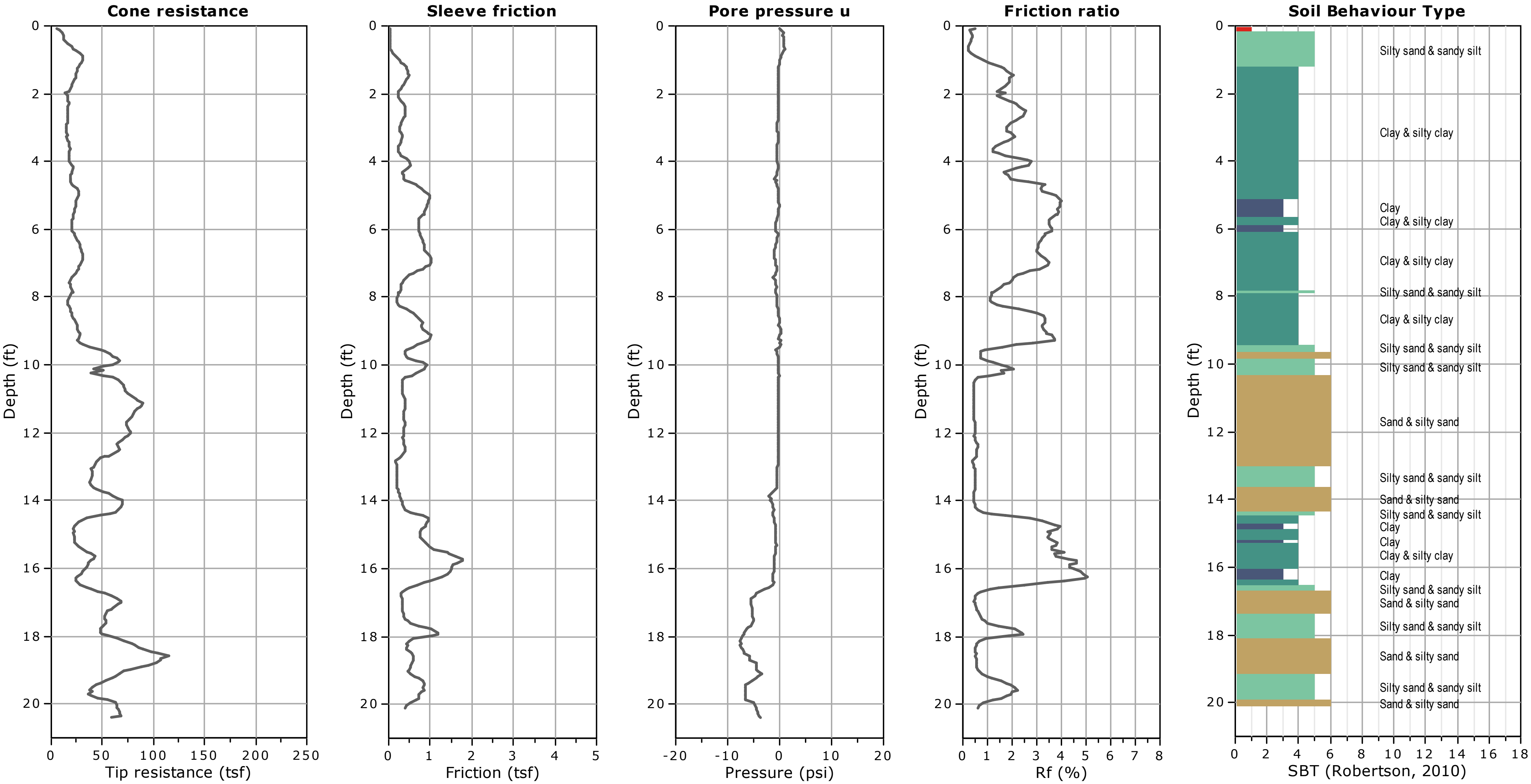
Project: **Terracon Consultants / Darden Solar**
Location: **Westside, CA**

CPT-18
Total depth: 20.41 ft, Date: 4/6/2023



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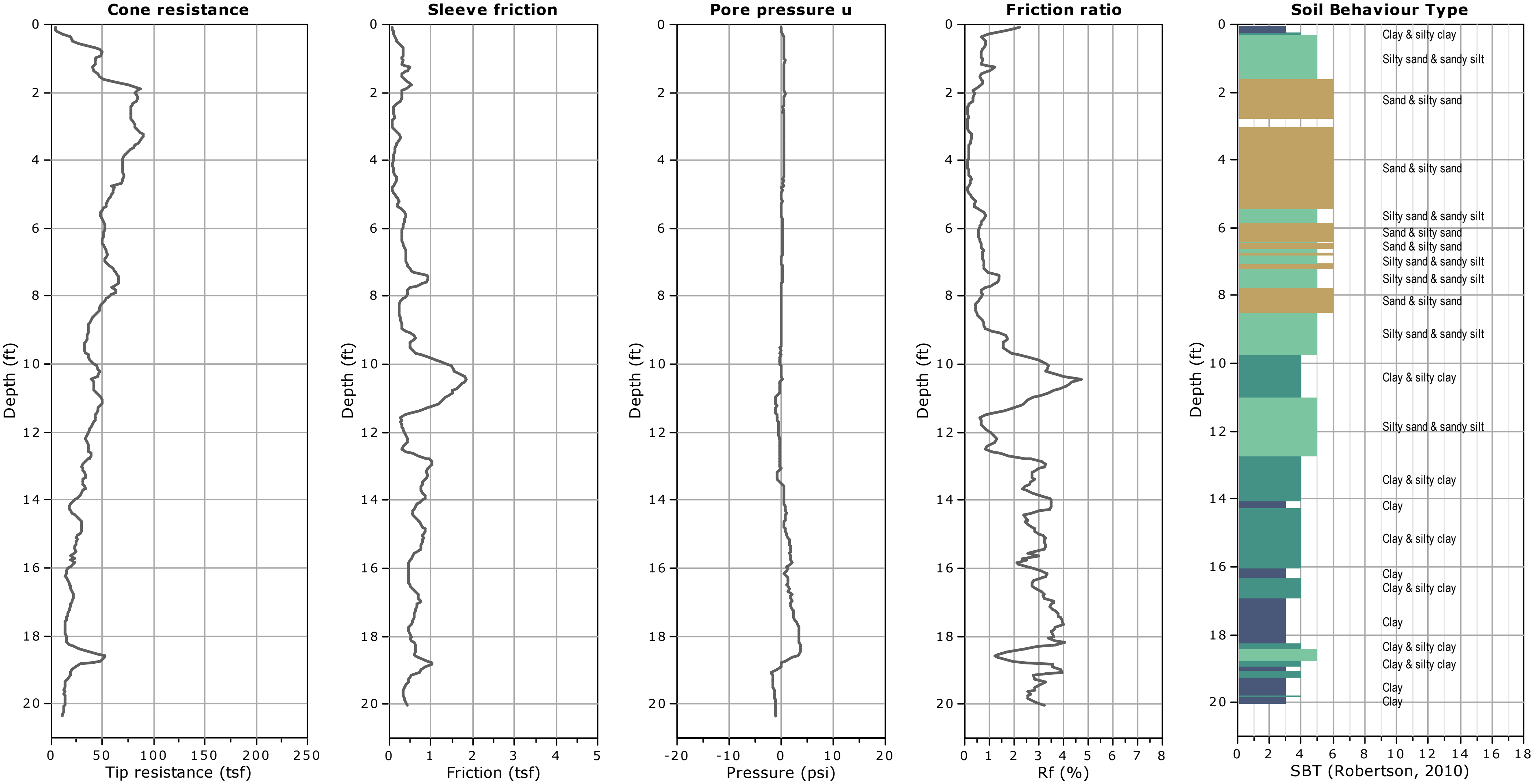
Project: **Terracon Consultants / Darden Solar**
Location: **Westside, CA**

CPT-19
Total depth: 20.35 ft, Date: 4/4/2023



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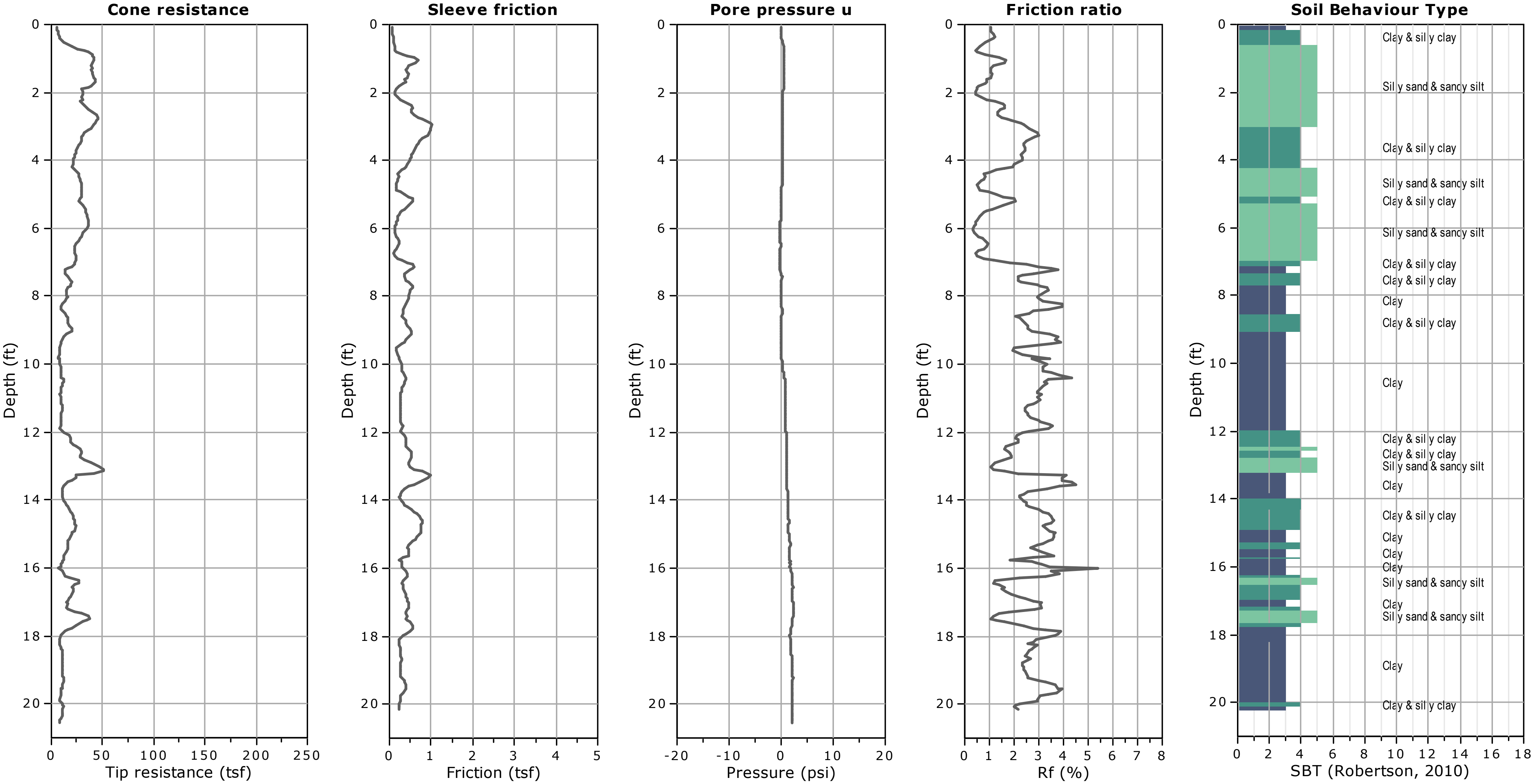
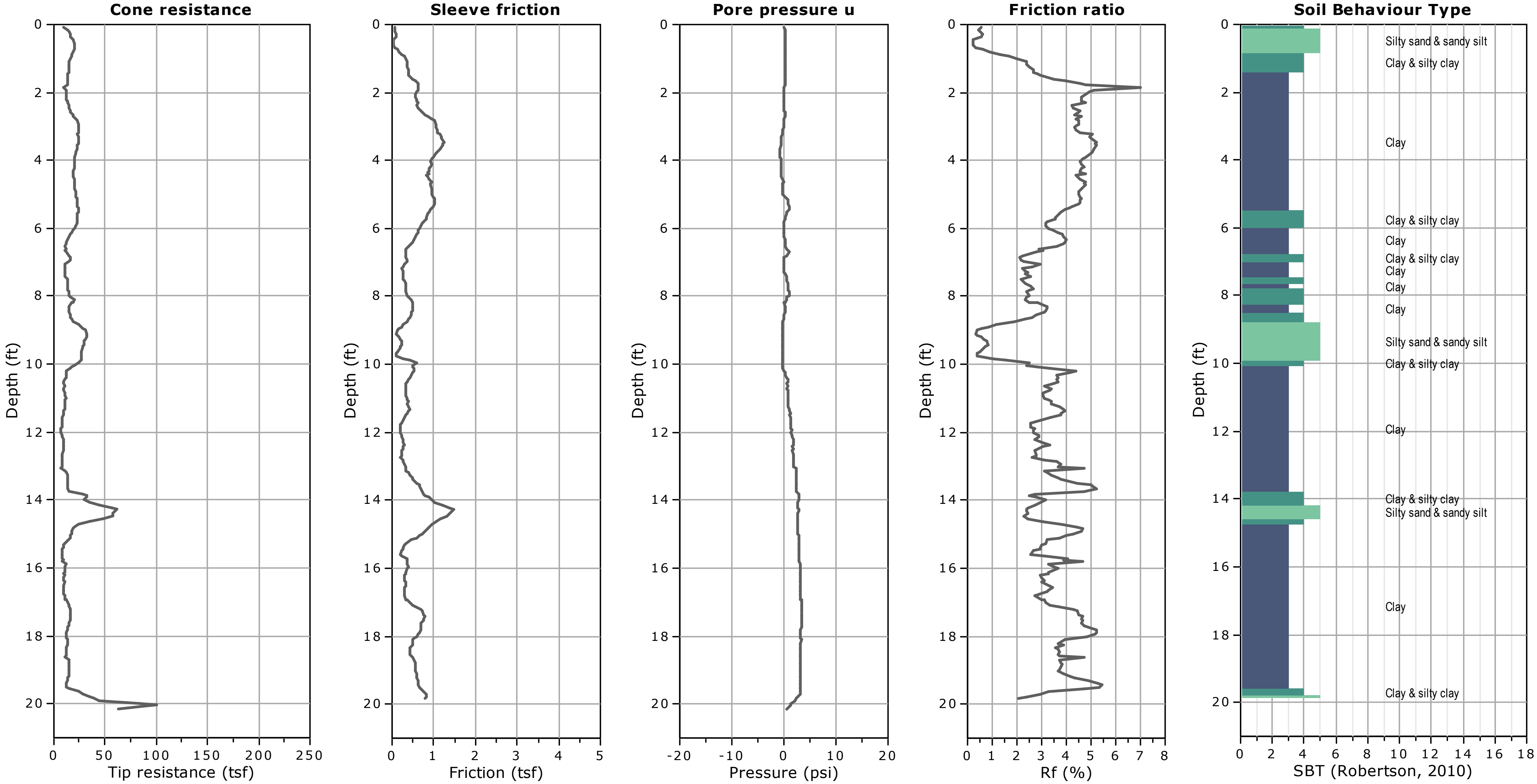
Project: **Terracon Consultants / Darden Solar**
Location: **Westside, CA**

CPT-20
Total depth: 20.54 ft, Date: 4/4/2023



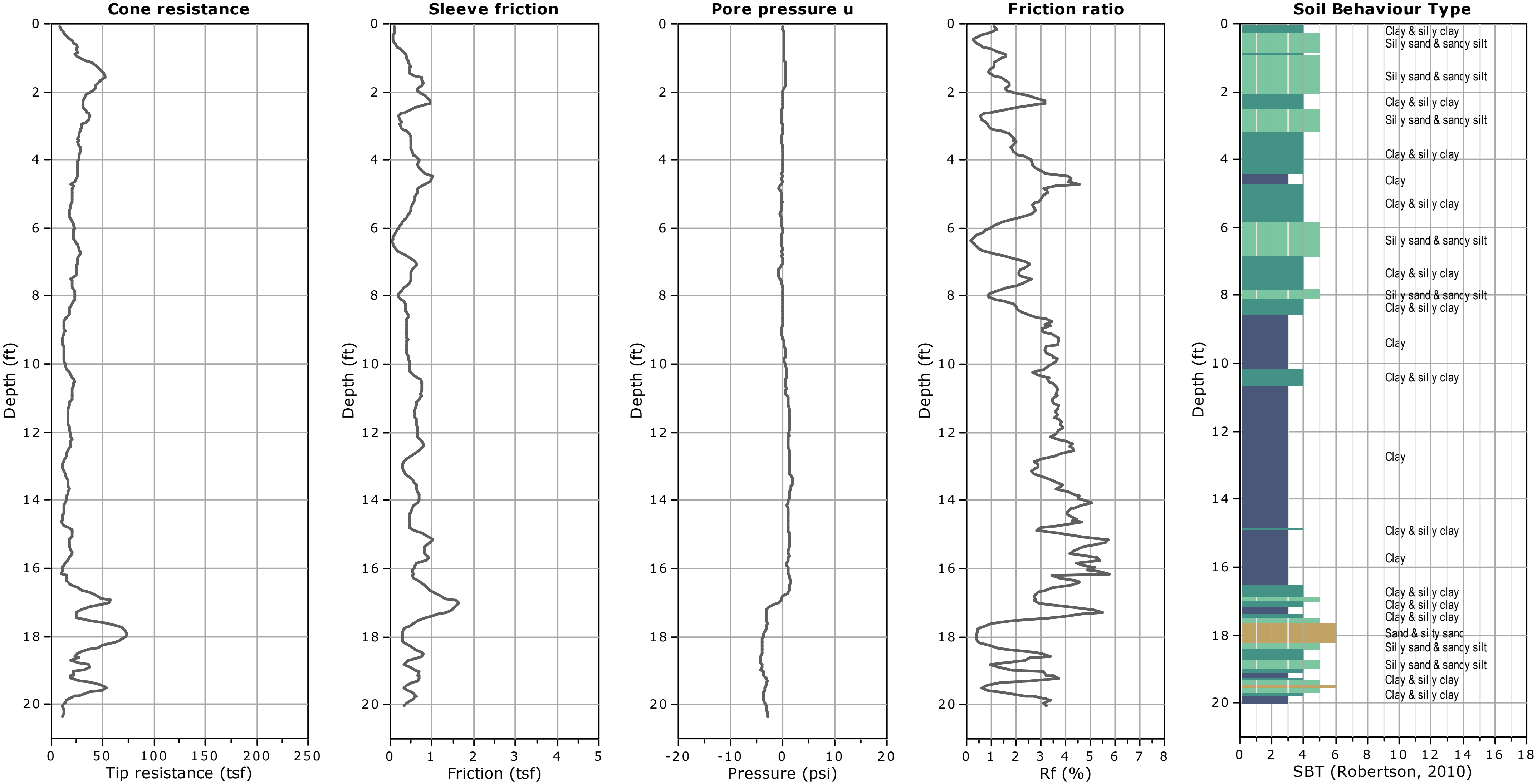
Project: **Terracon Consultants / Darden Solar**
Location: **Westside, CA**

CPT-21
Total depth: 20.16 ft, Date: 4/4/2023



Project: **Terracon Consultants / Darden Solar**
Location: **Westside, CA**

CPT-22
Total depth: 20.36 ft, Date: 4/4/2023



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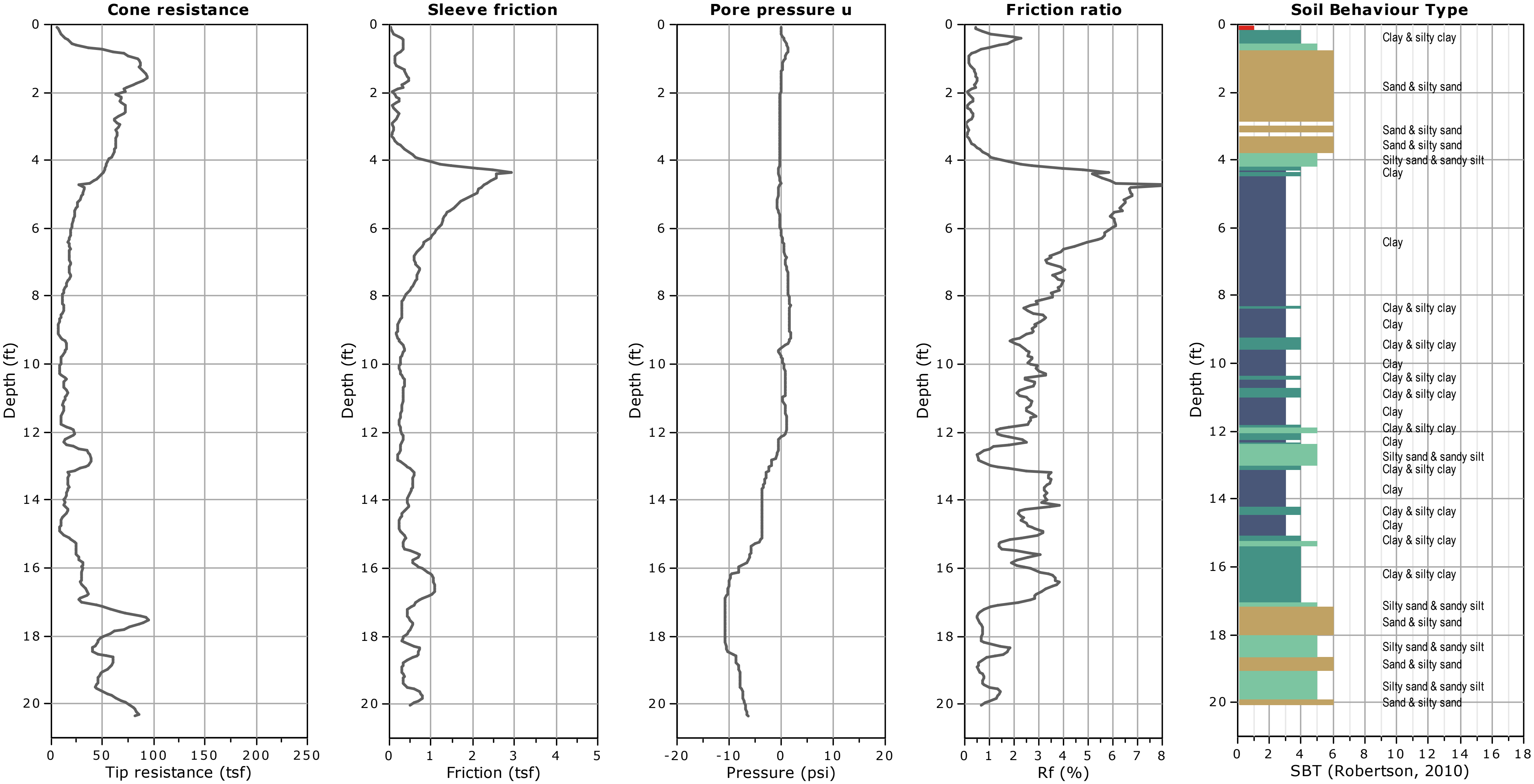
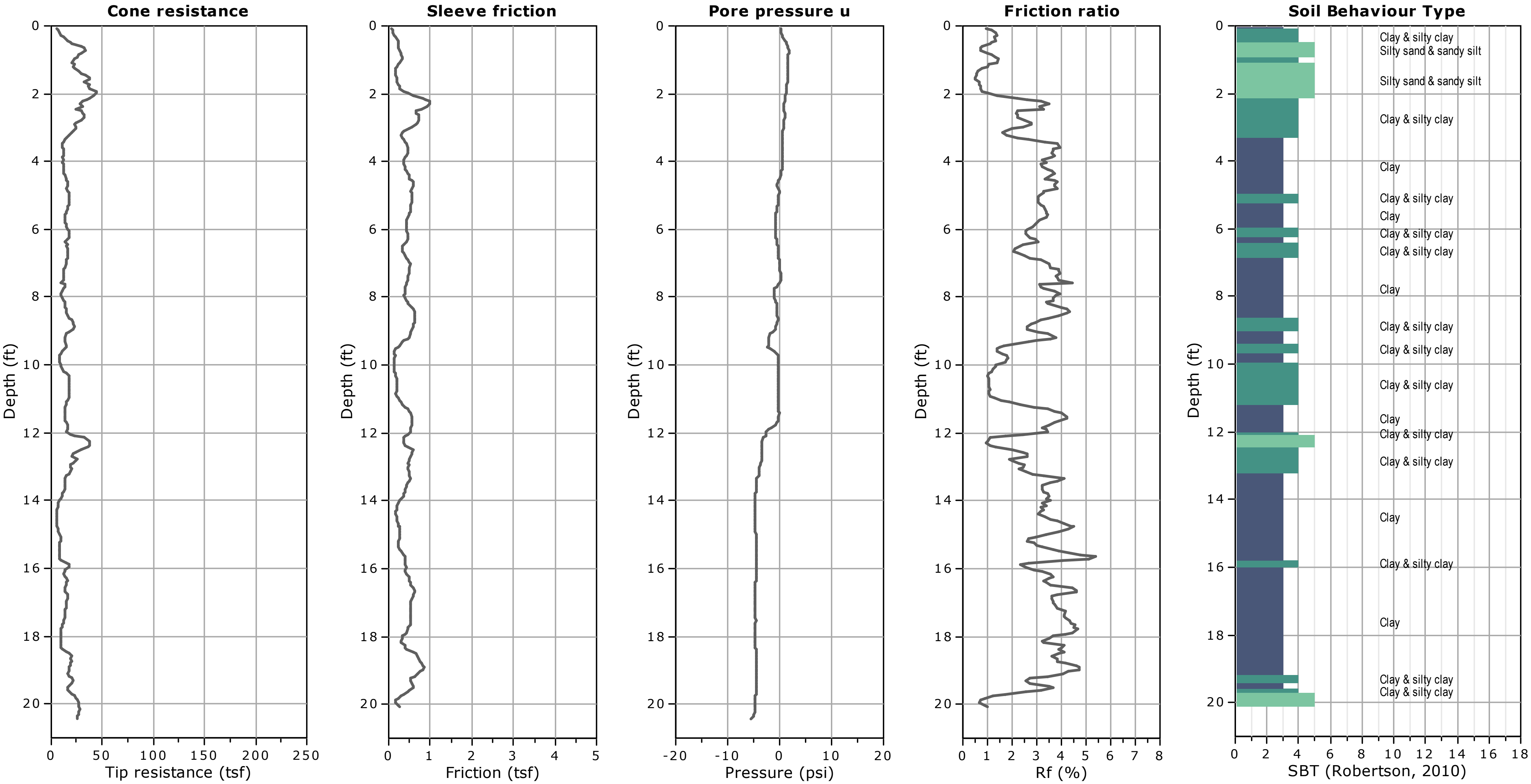
Project: **Terracon Consultants / Darden Solar**
Location: **Westside, CA**

CPT-23
Total depth: 20.35 ft, Date: 4/5/2023



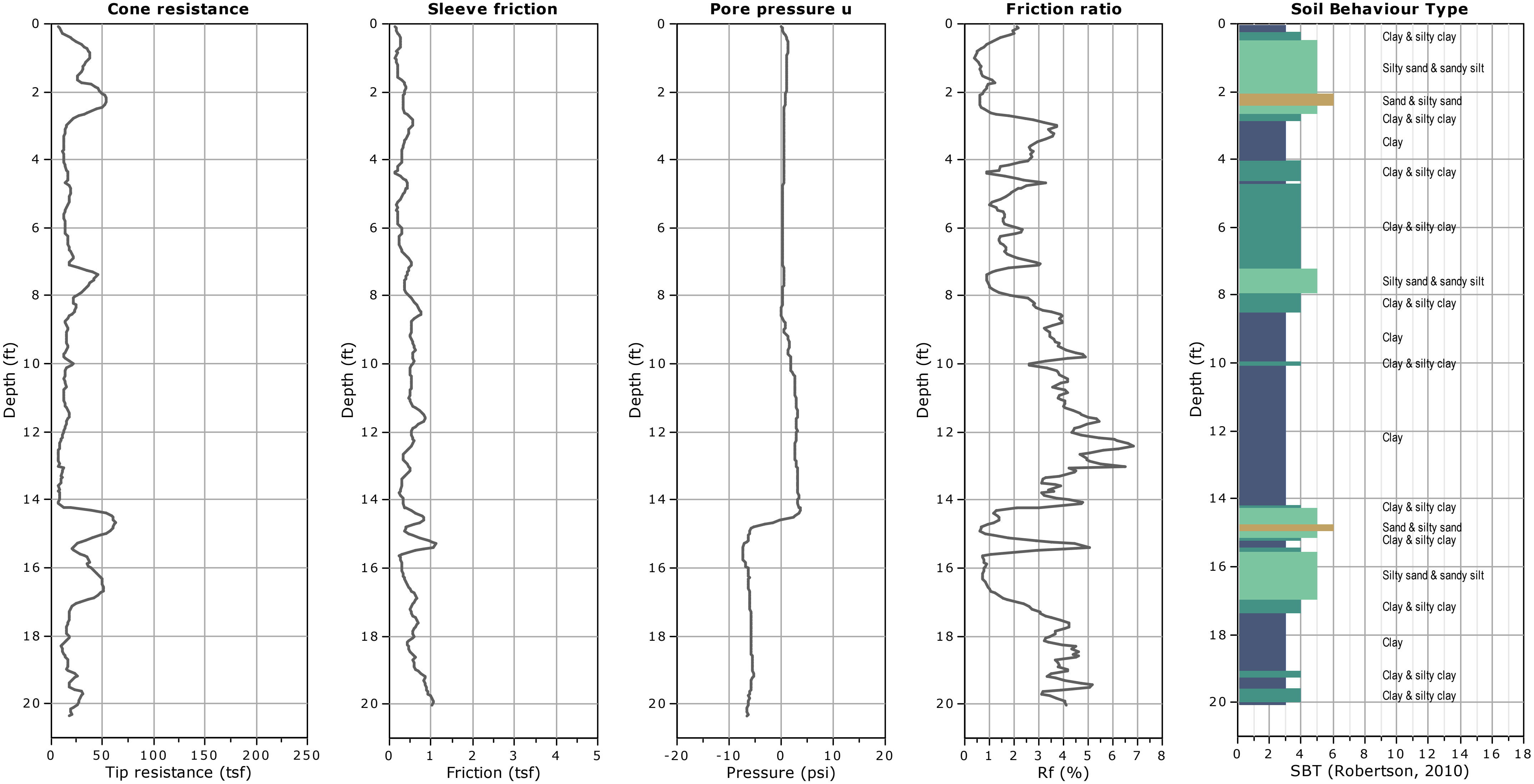
Project: **Terracon Consultants / Darden Solar**
Location: **Westside, CA**

CPT-24
Total depth: 20.43 ft, Date: 4/5/2023



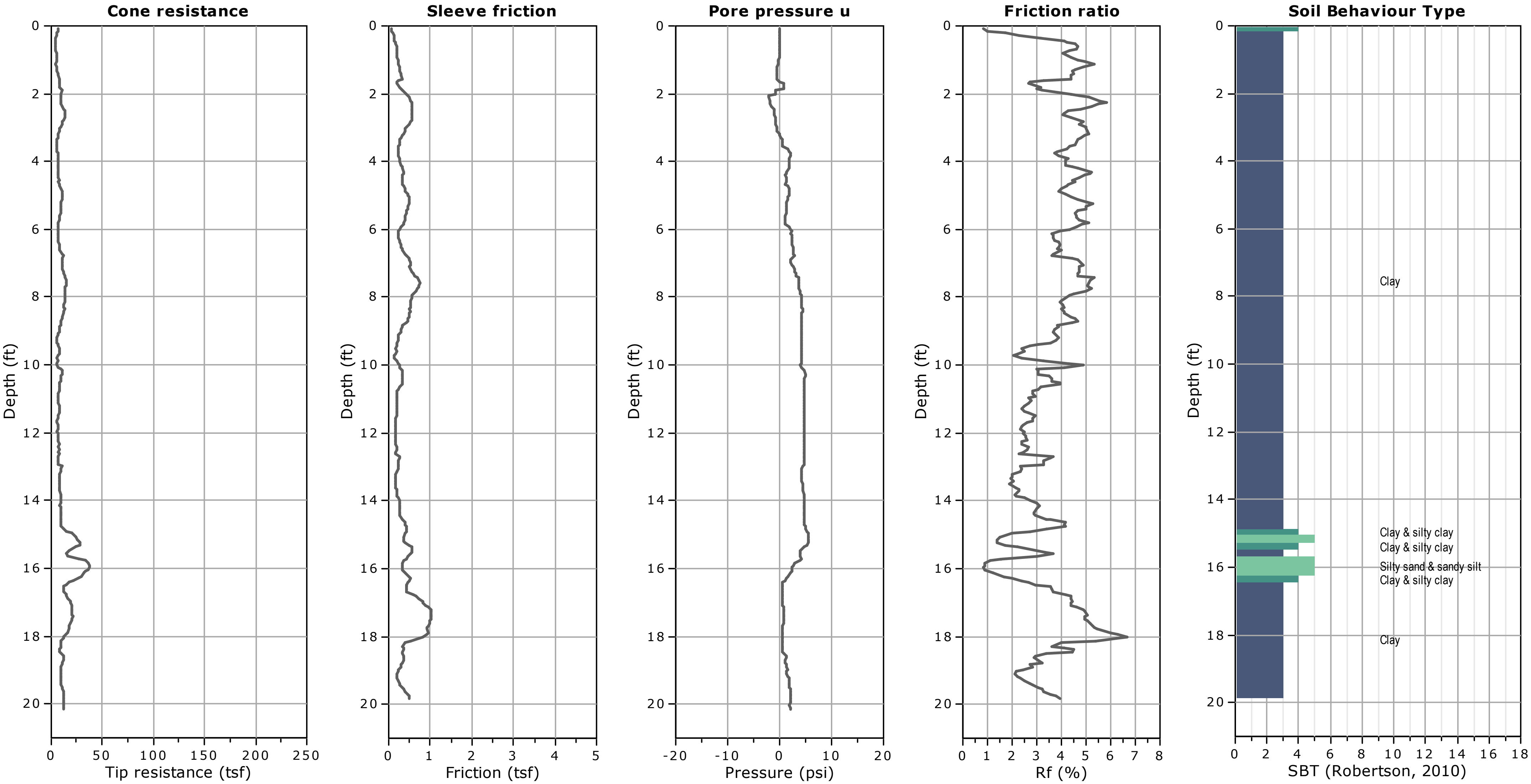
Project: **Terracon Consultants / Darden Solar**
Location: **Westside, CA**

CPT-25
Total depth: 20.34 ft, Date: 4/5/2023



Project: **Terracon Consultants / Darden Solar**
Location: **Westside, CA**

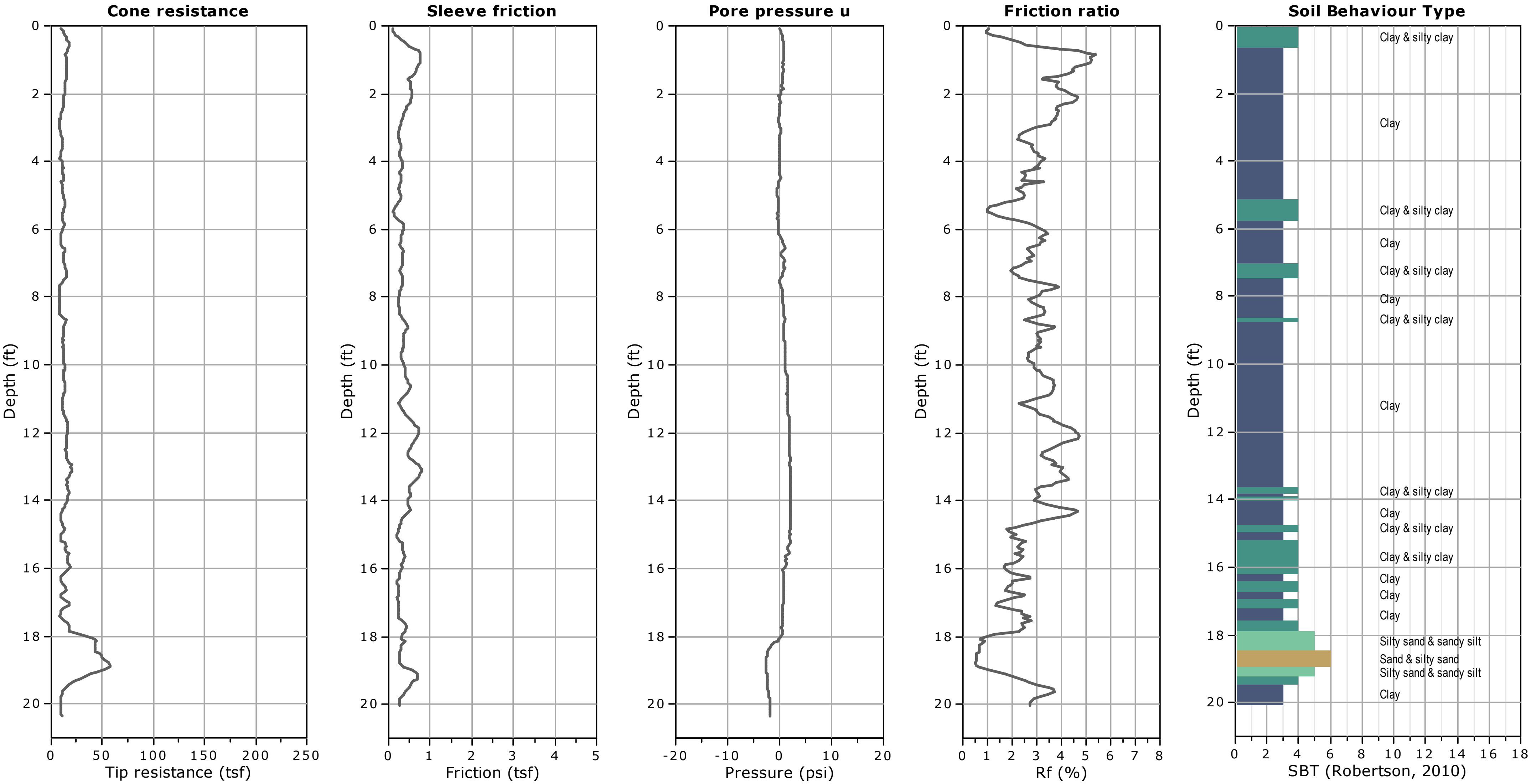
CPT-26
Total depth: 20.15 ft, Date: 4/5/2023



Project: **Terracon Consultants / Darden Solar**
Location: **Westside, CA**

CPT-27

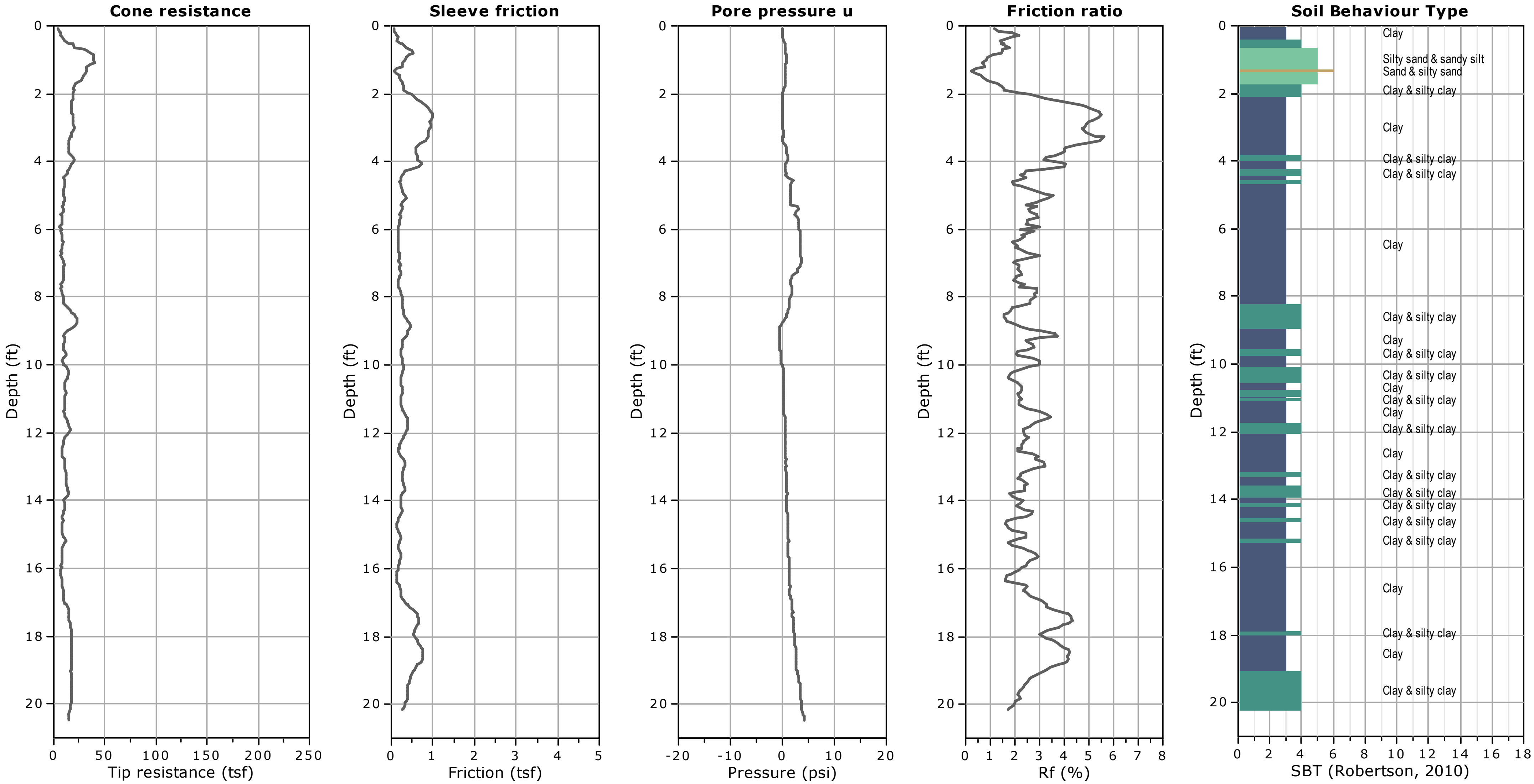
Total depth: 20.36 ft, Date: 4/5/2023



Project: **Terracon Consultants / Darden Solar**
Location: **Westside, CA**

CPT-28

Total depth: 20.48 ft, Date: 4/5/2023



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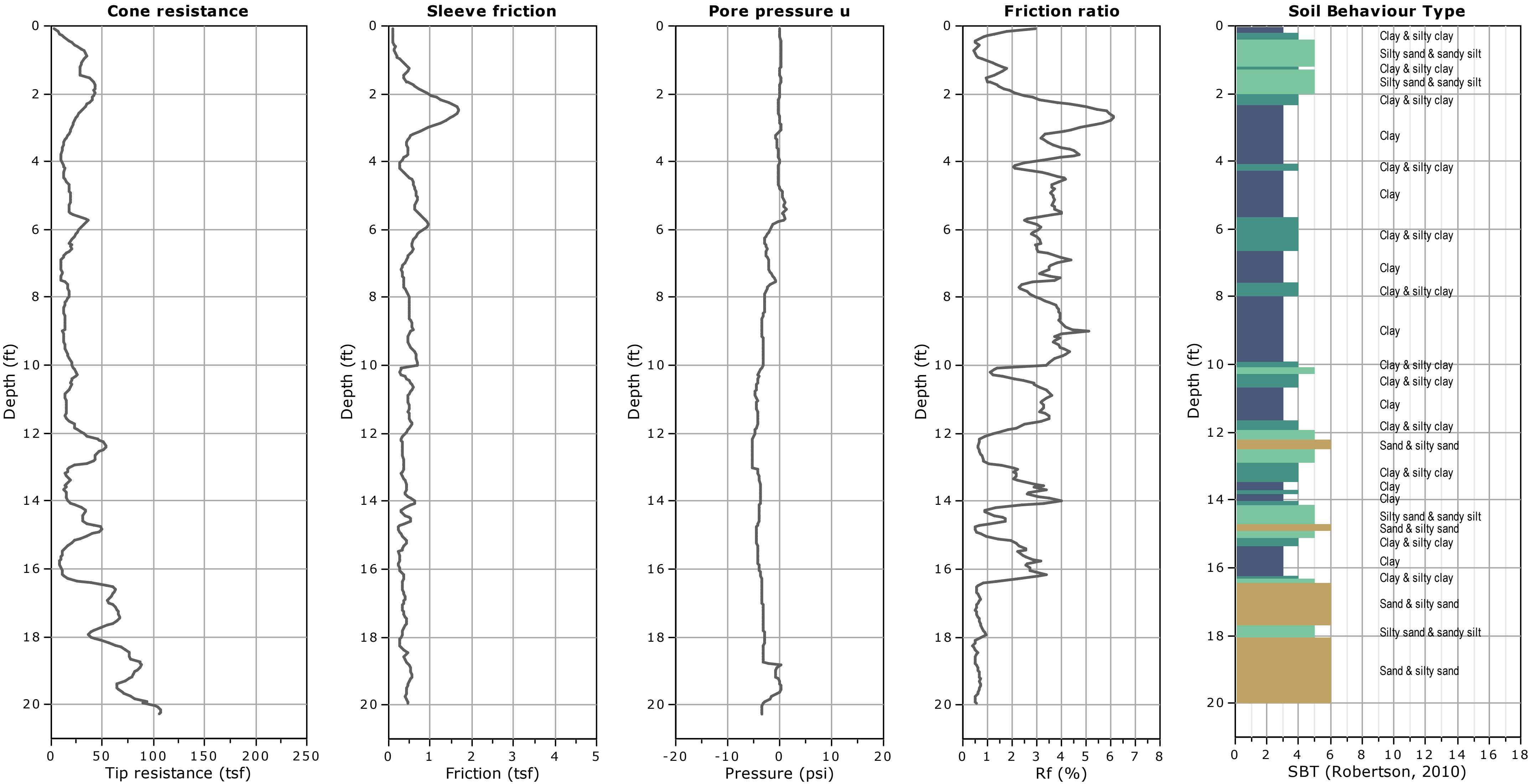
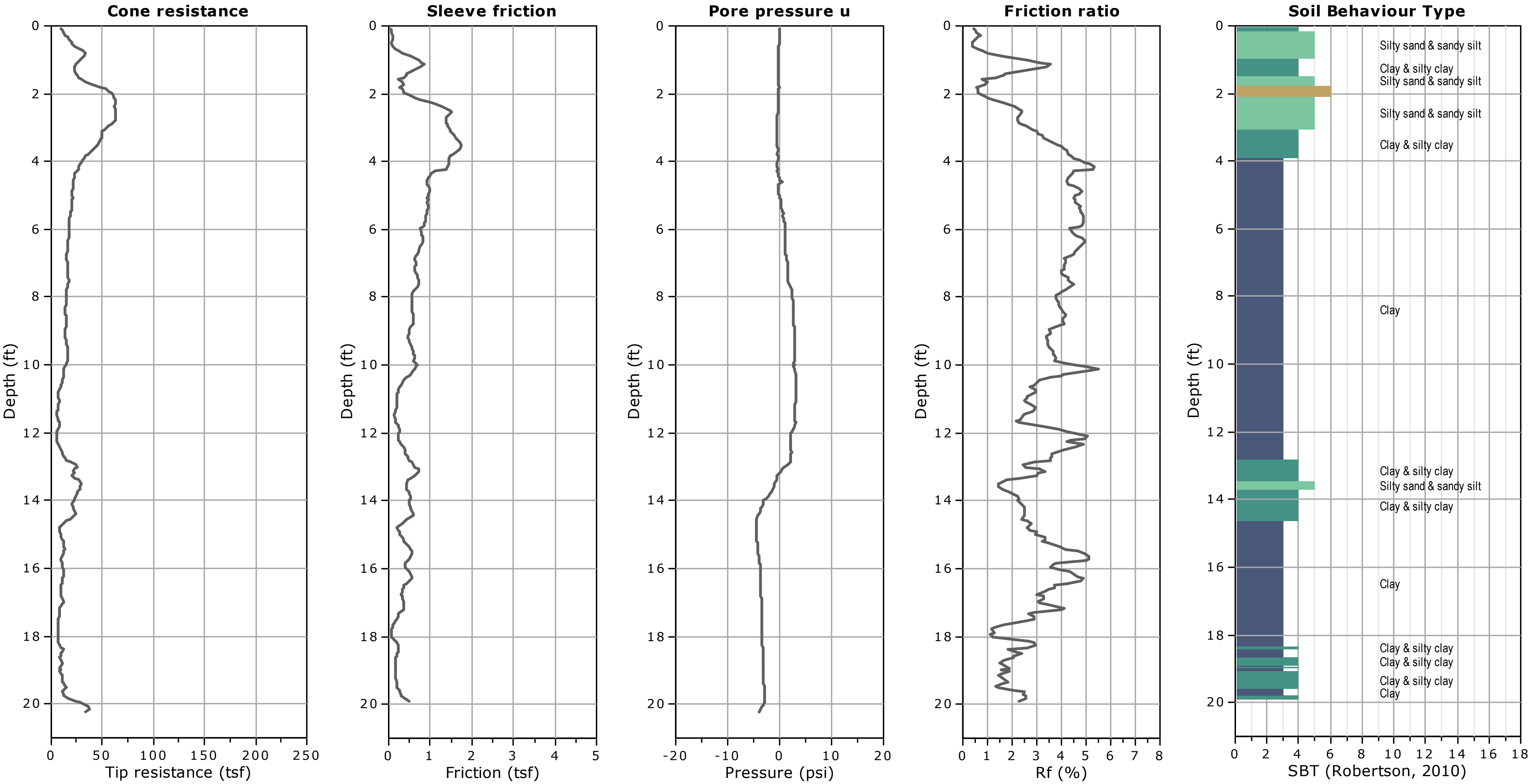
Project: **Terracon Consultants / Darden Solar**
Location: **Westside, CA**

CPT-29
Total depth: 20.28 ft, Date: 4/5/2023



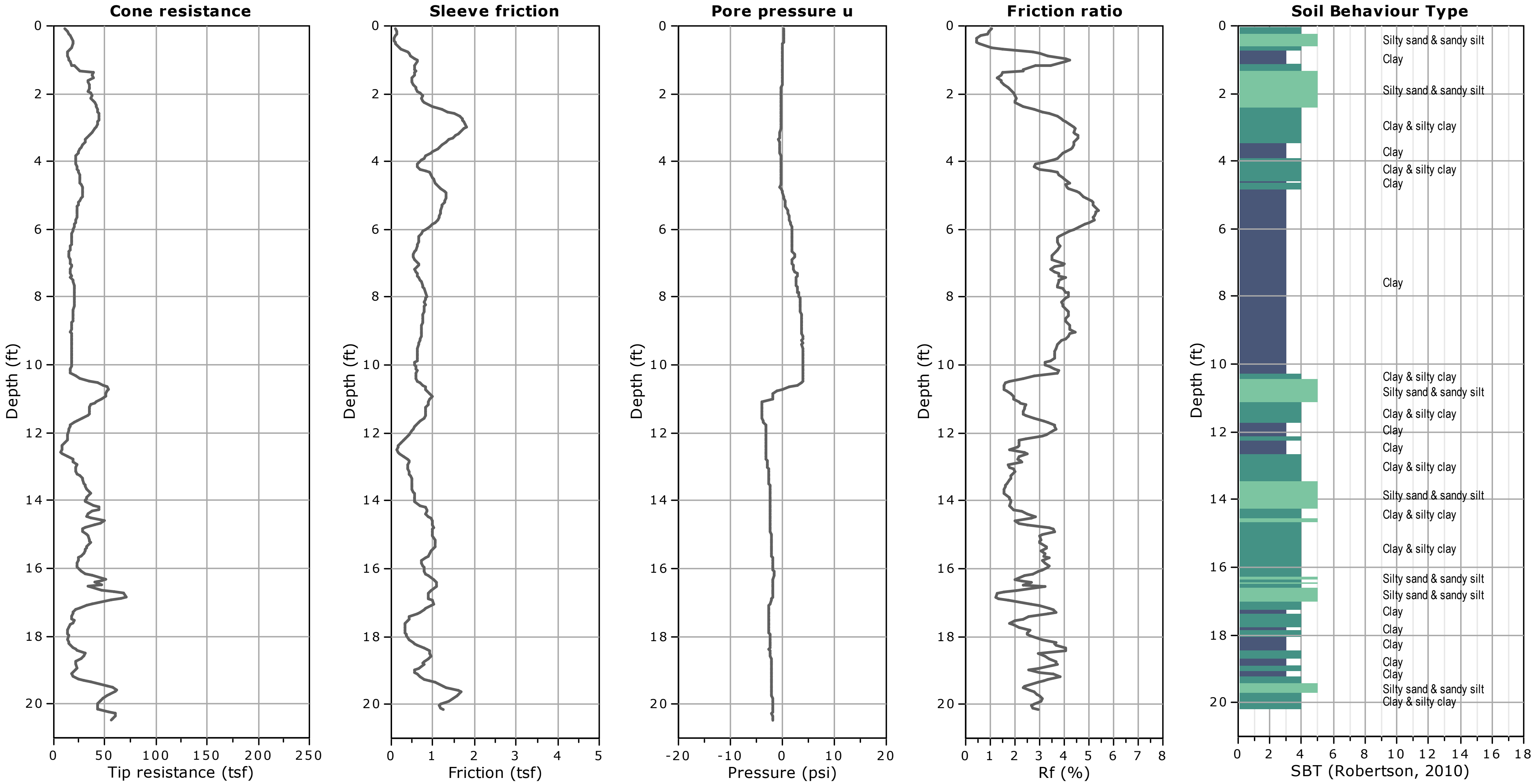
Project: **Terracon Consultants / Darden Solar**
Location: **Westside, CA**

CPT-30
Total depth: 20.24 ft, Date: 4/5/2023



Project: **Terracon Consultants / Darden Solar**
Location: **Westside, CA**

CPT-31
Total depth: 20.49 ft, Date: 4/5/2023



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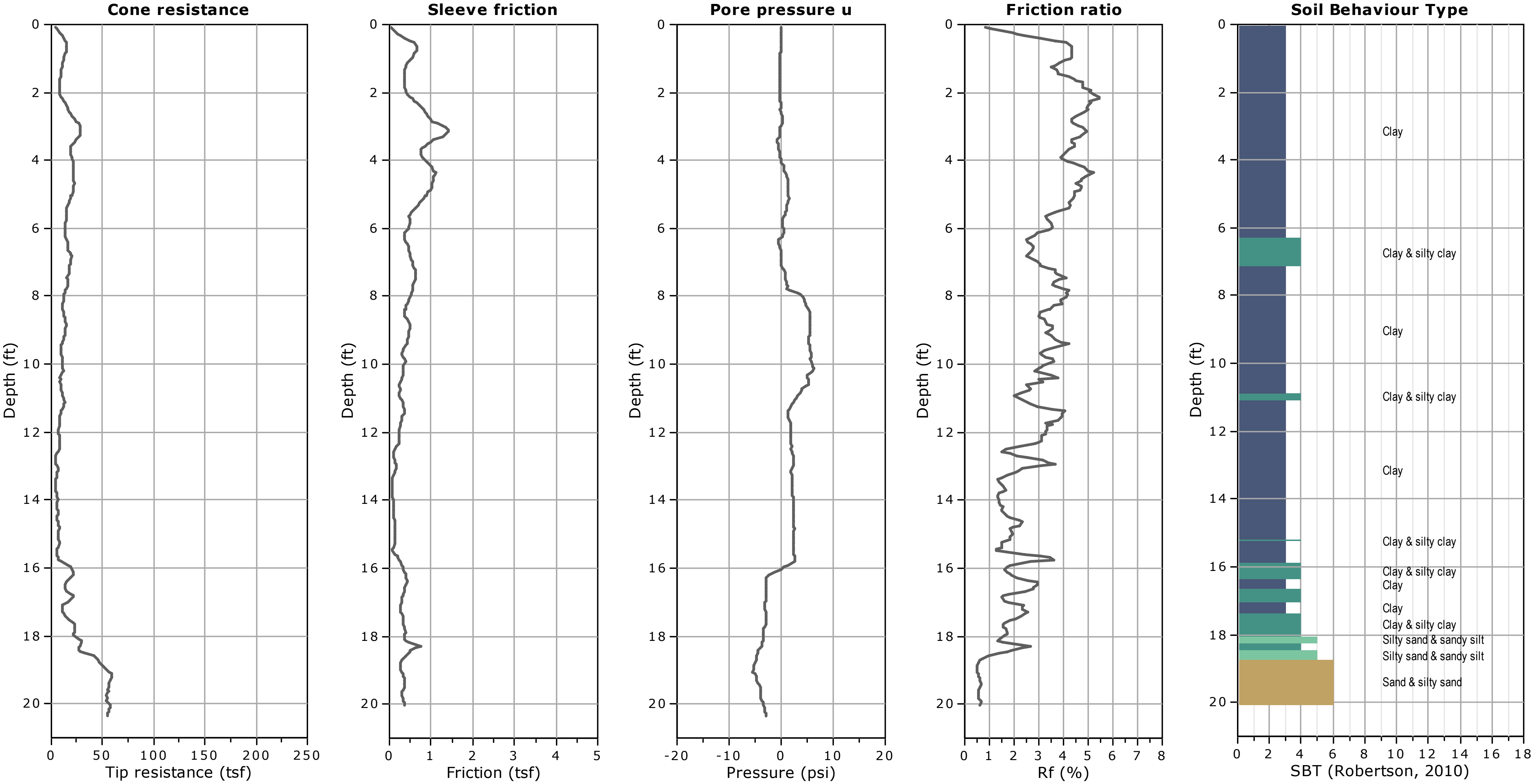
Project: **Terracon Consultants / Darden Solar**
Location: **Westside, CA**

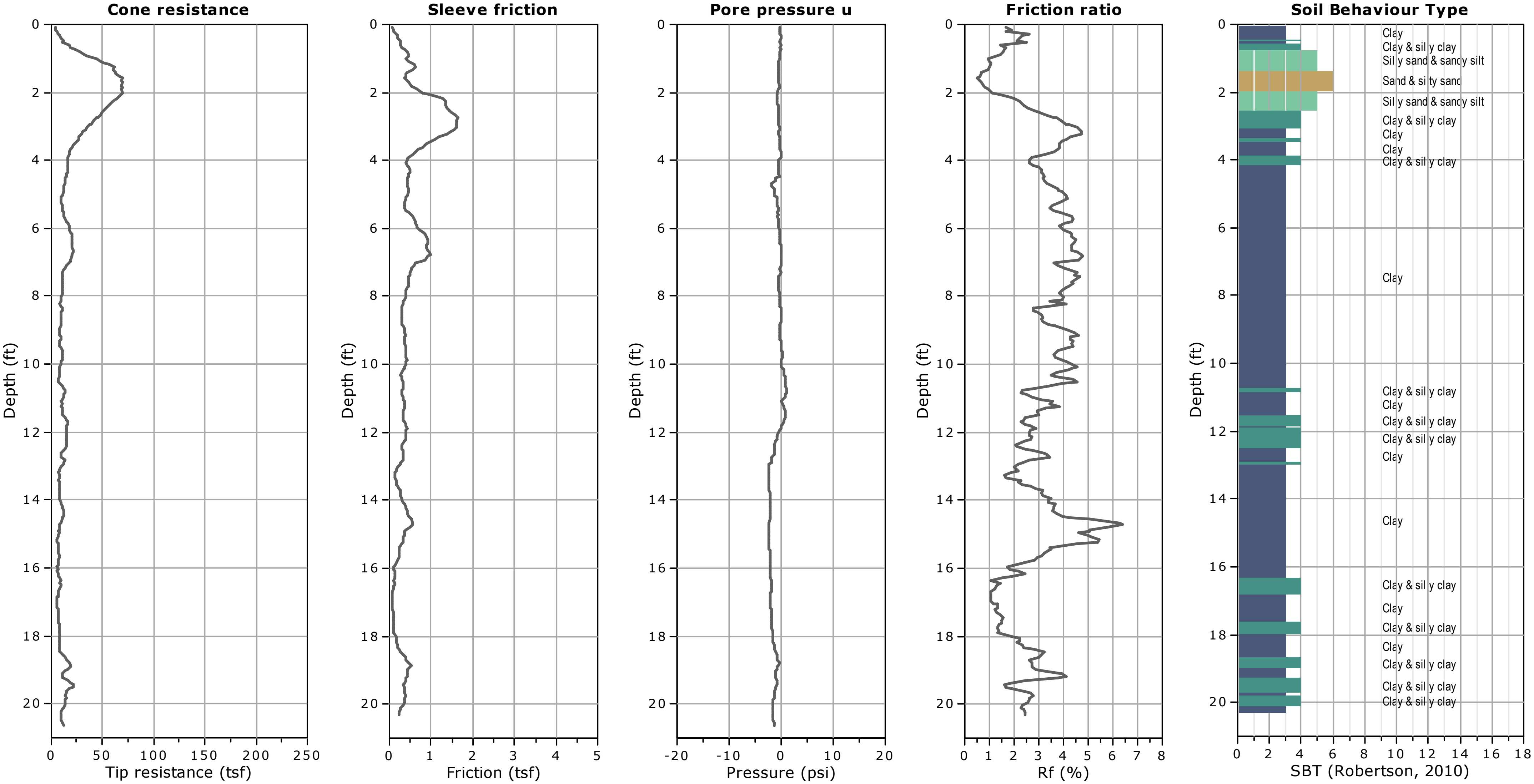
CPT-32

Total depth: 20.35 ft, Date: 4/5/2023



Project: **Terracon Consultants / Darden Solar**
Location: **Westside, CA**

CPT-33
Total depth: 20.62 ft, Date: 4/6/2023



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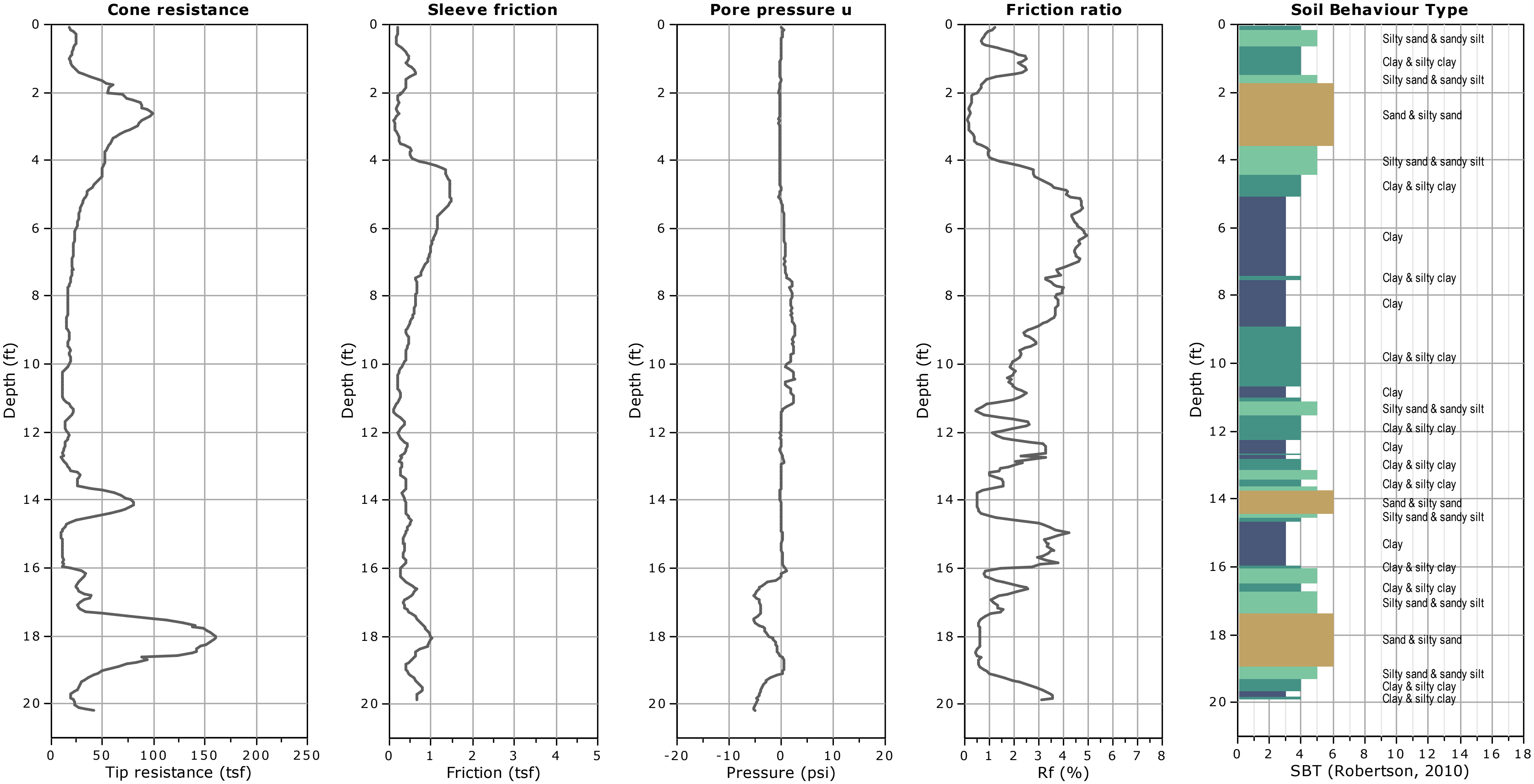
Project: **Terracon Consultants / Darden Solar**
Location: **Westside, CA**

CPT-34

Total depth: 20.21 ft, Date: 4/6/2023



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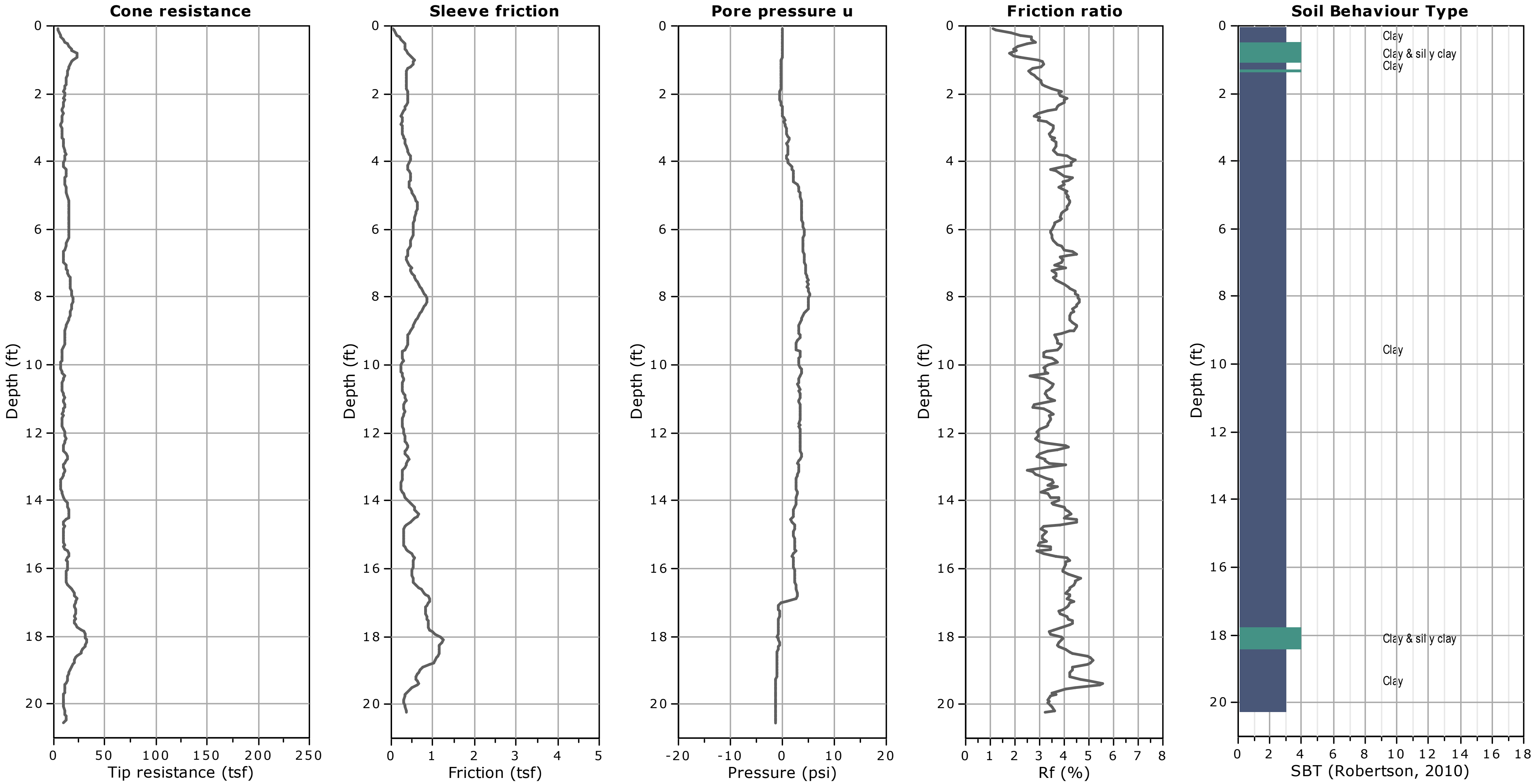
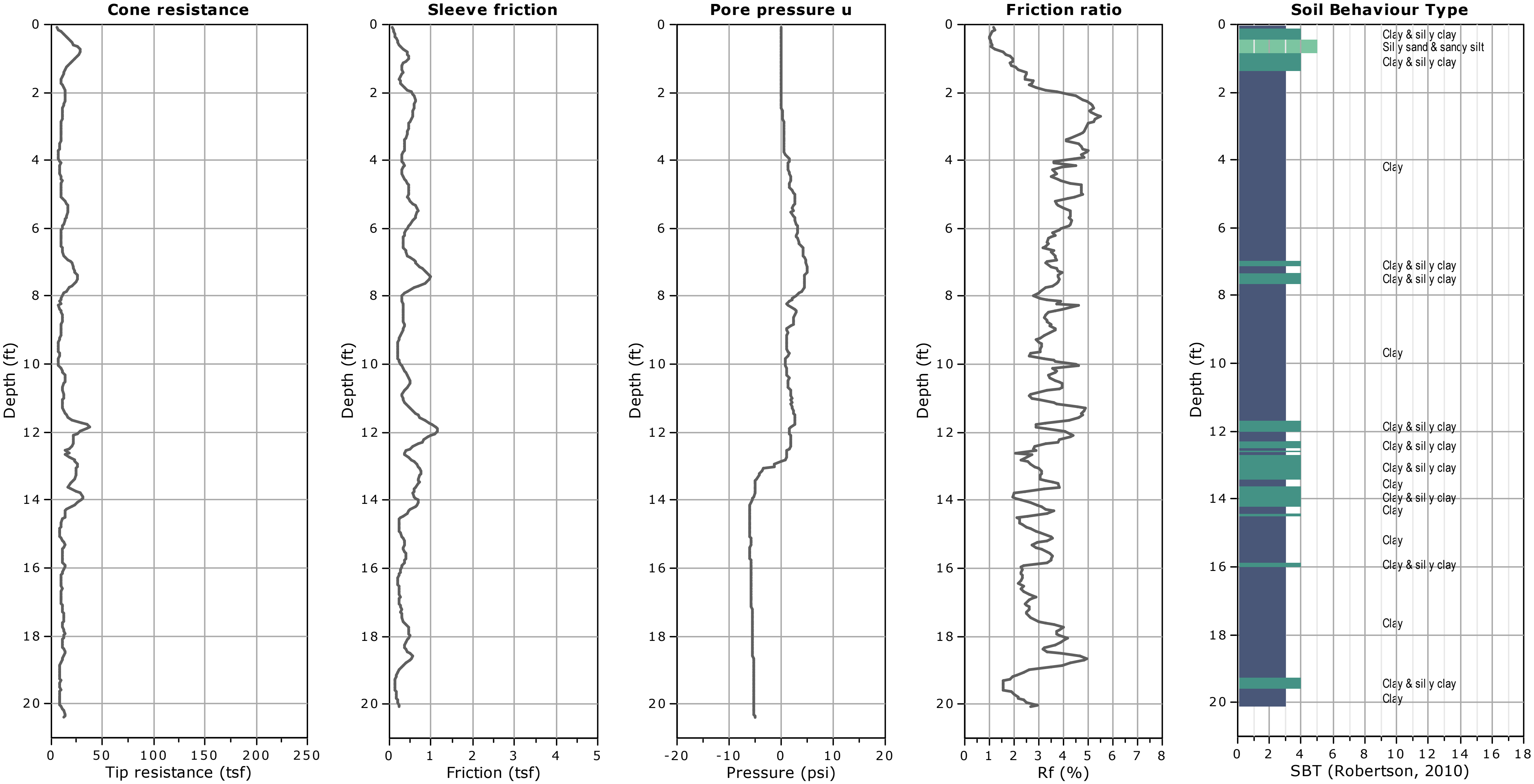
Project: **Terracon Consultants / Darden Solar**
Location: **Westside, CA**

CPT-35
Total depth: 20.54 ft, Date: 4/6/2023



Project: **Terracon Consultants / Darden Solar**
Location: **Westside, CA**

CPT-36
Total depth: 20.41 ft, Date: 4/6/2023



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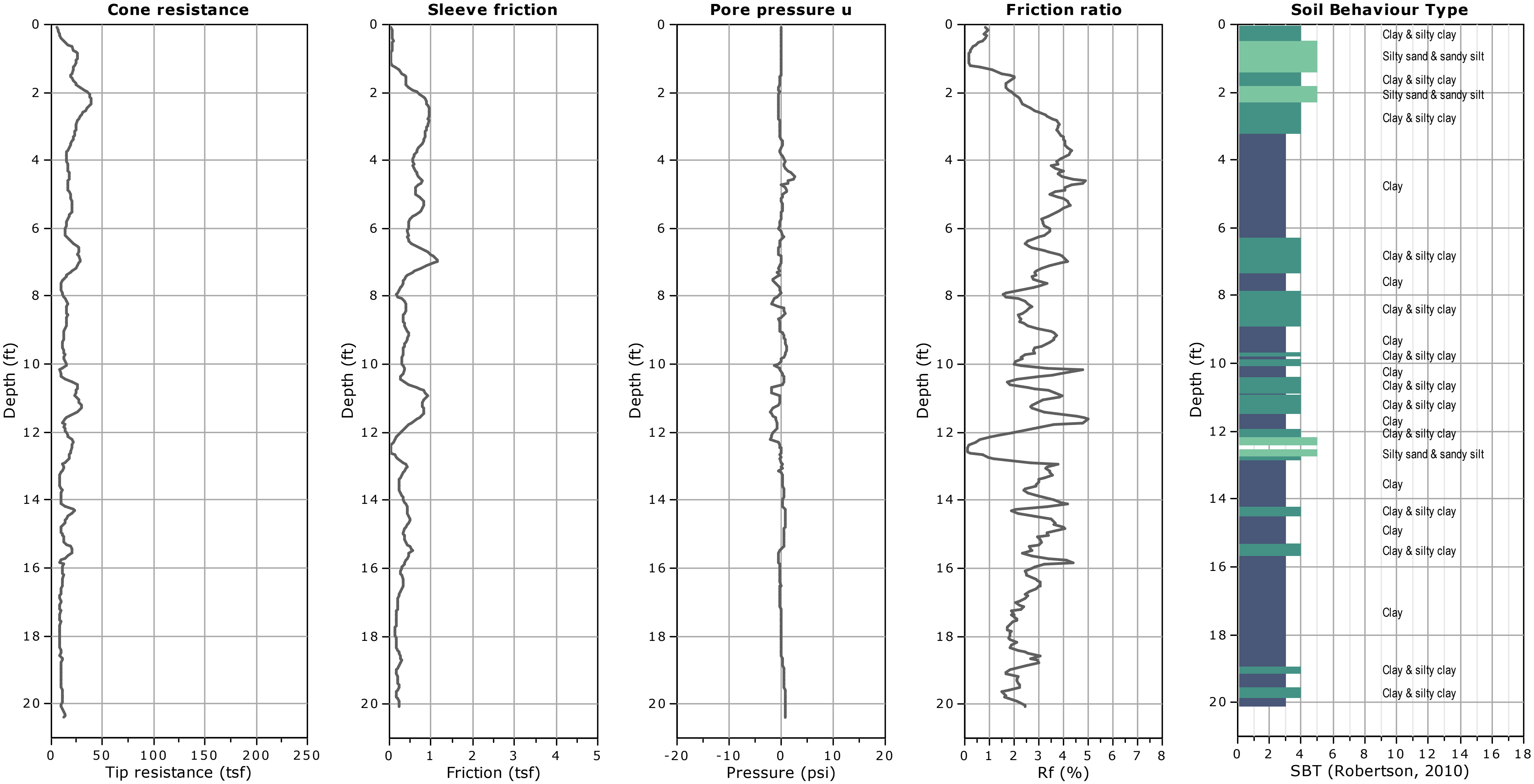
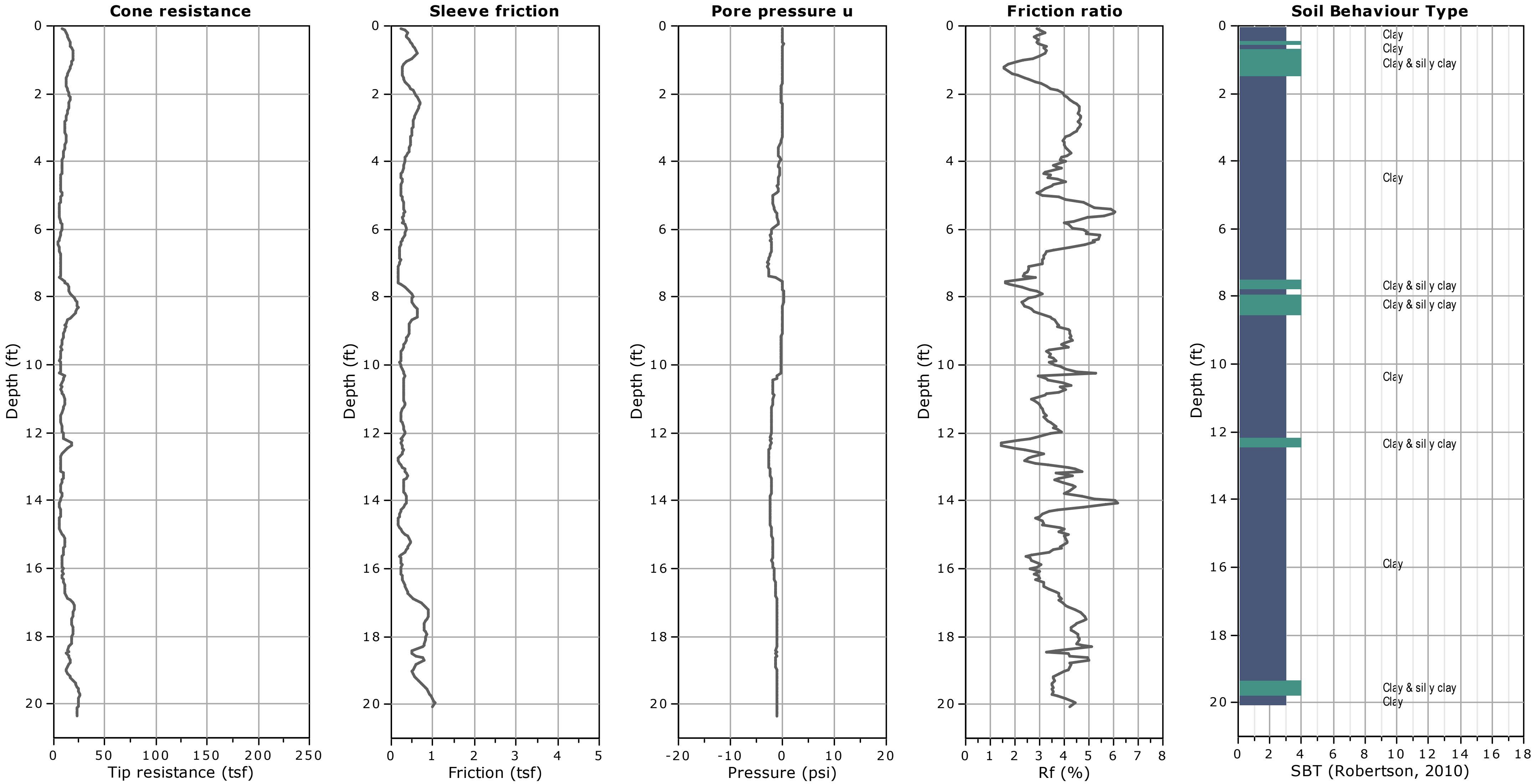
Project: **Terracon Consultants / Darden Solar**
Location: **Westside, CA**

CPT-37
Total depth: 20.41 ft, Date: 4/6/2023



Project: **Terracon Consultants / Darden Solar**
Location: **Westside, CA**

CPT-38
Total depth: 20.35 ft, Date: 4/6/2023



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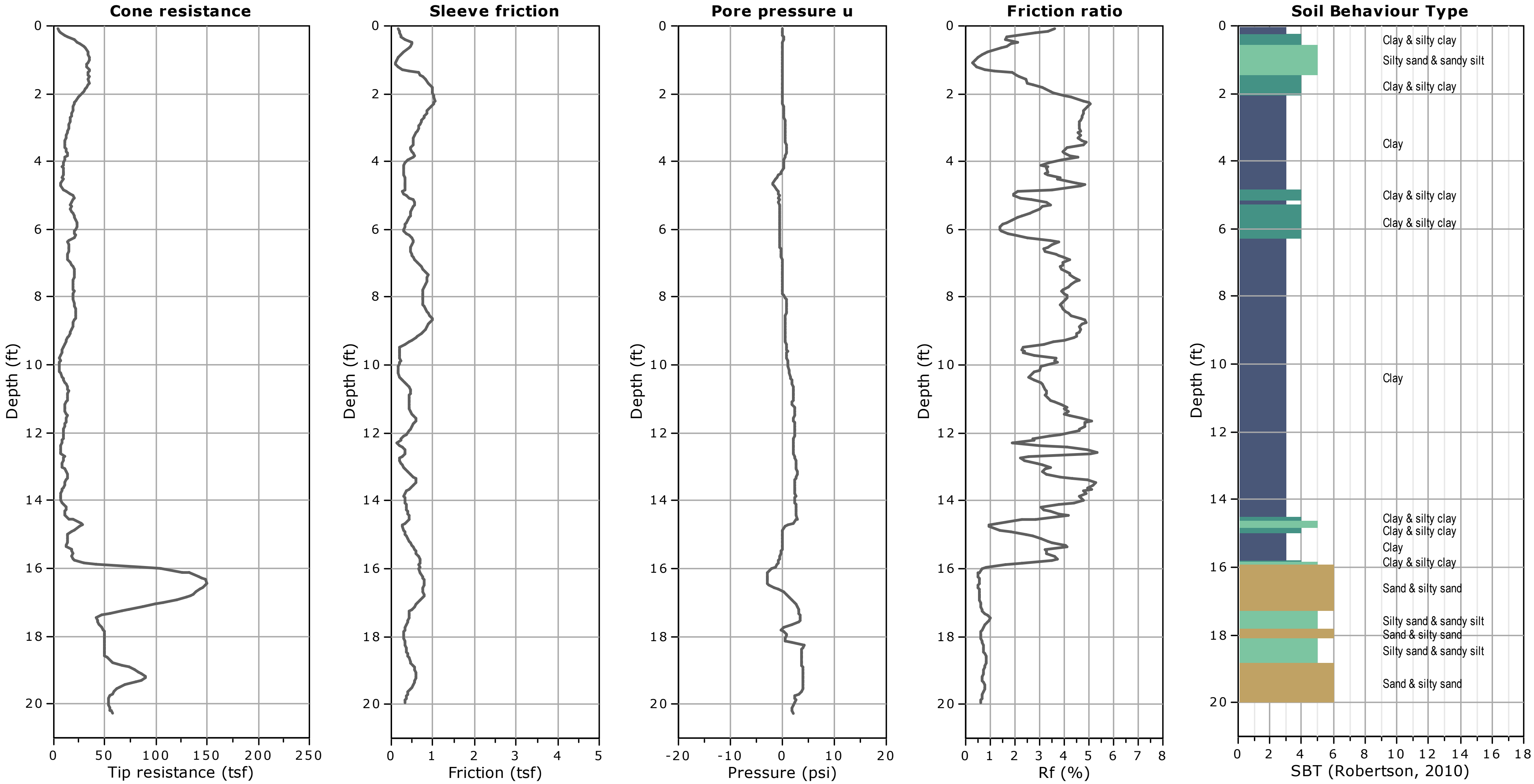
Project: Terracon Consultants / Darden Solar
Location: Westside, CA

CPT-39
Total depth: 20.29 ft, Date: 4/6/2023



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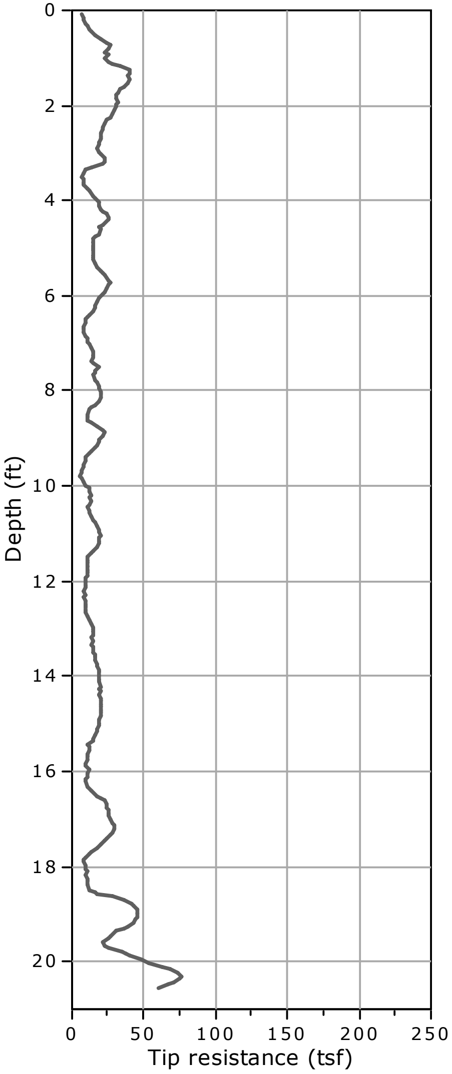
Project: **Terracon Consultants / Darden Solar**
Location: **Westside, CA**

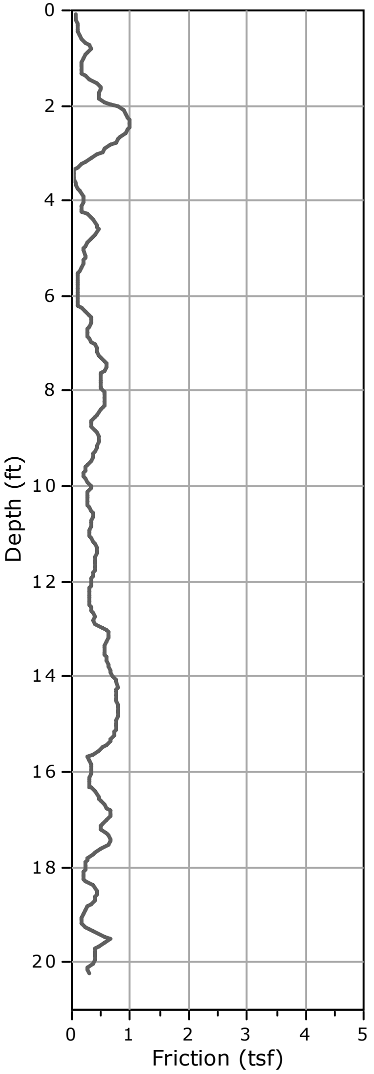
CPT-40

Total depth: 20.54 ft, Date: 4/6/2023

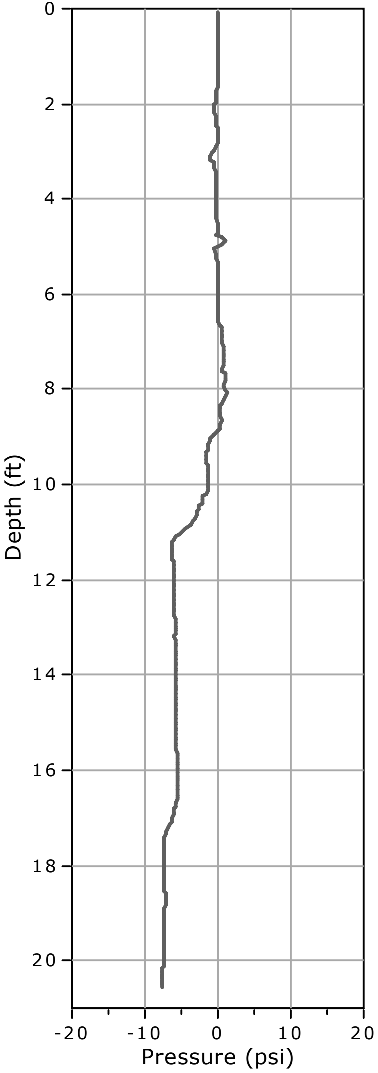
Cone resistance



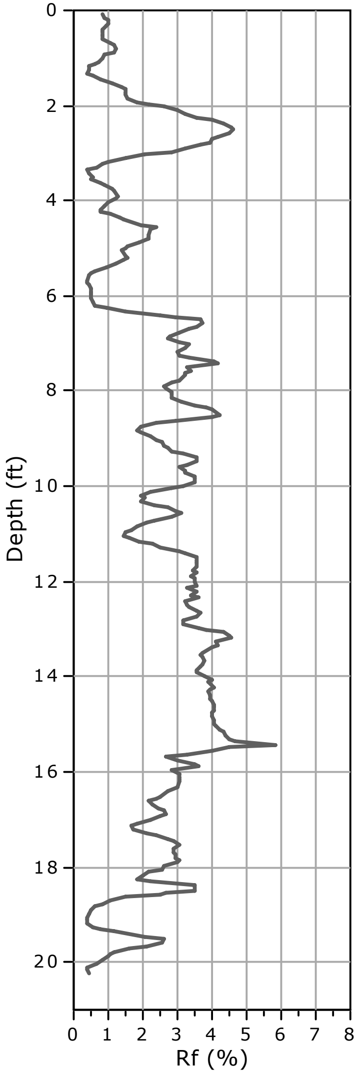
Sleeve friction



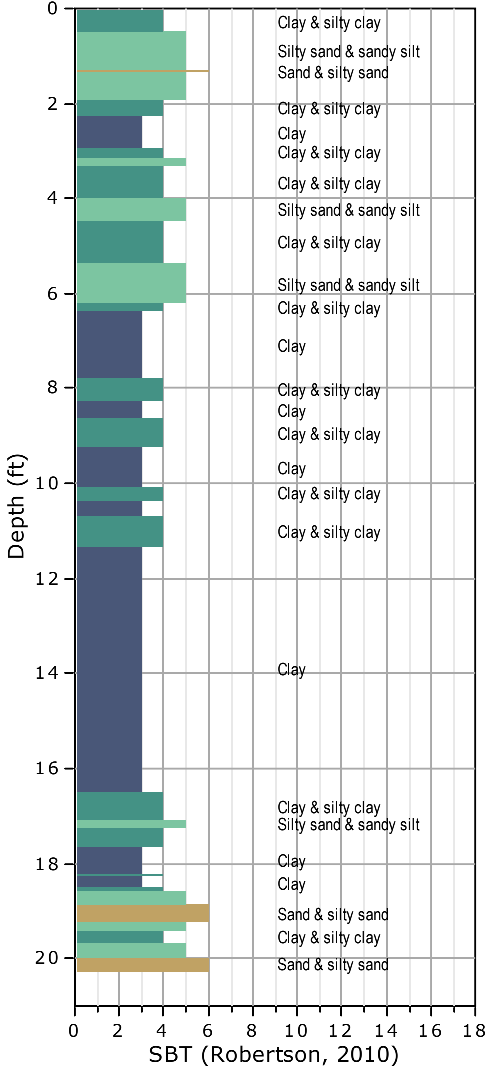
Pore pressure u



Friction ratio



Soil Behaviour Type



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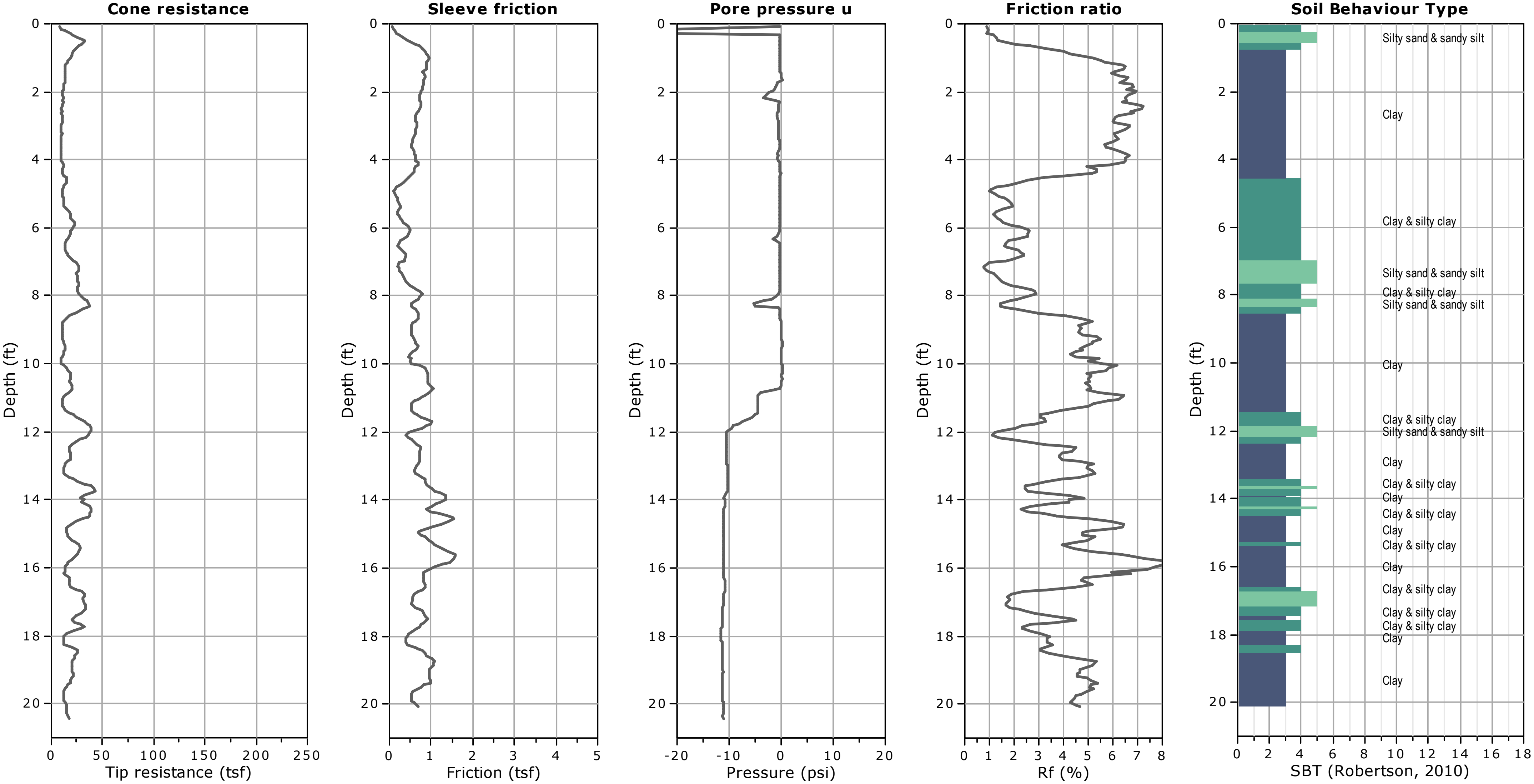
Project: **Terracon Consultants / Darden Solar**

Location: **Westside, CA**

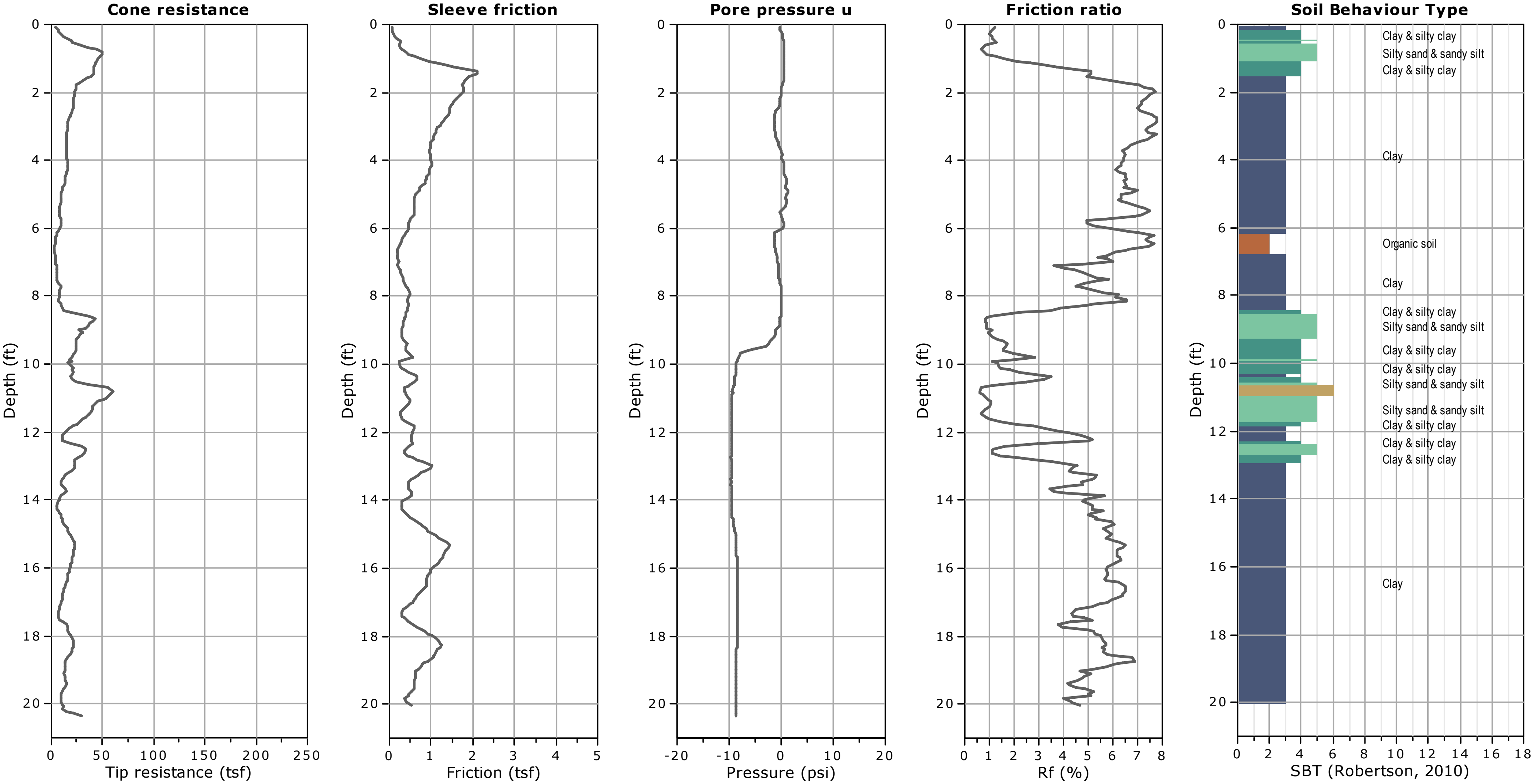
CPT-41

Total depth: 20.43 ft, Date: 4/7/2023



Project: **Terracon Consultants / Darden Solar**
Location: **Westside, CA**

CPT-42
Total depth: 20.36 ft, Date: 4/7/2023



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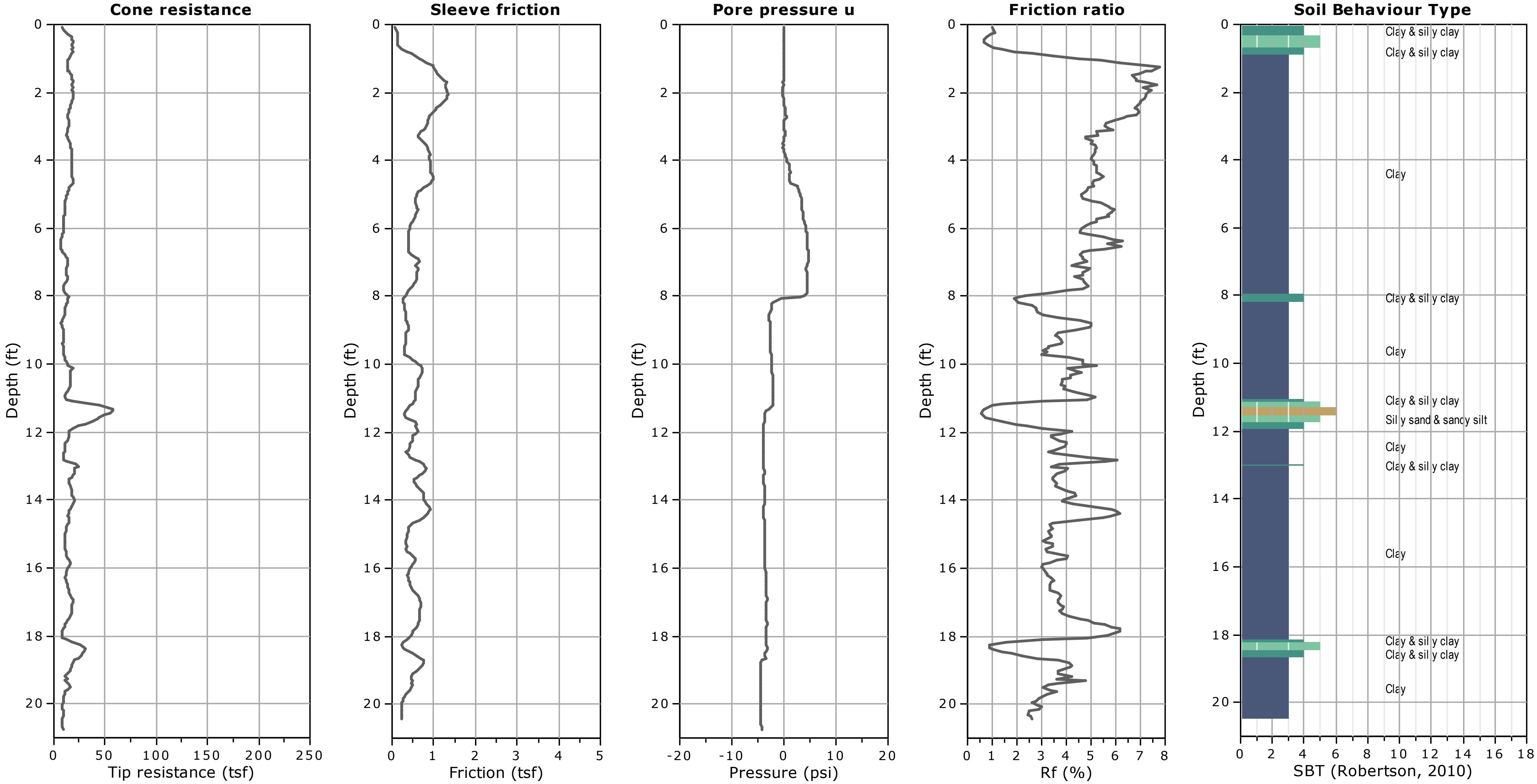
Project: **Terracon Consultants / Darden Solar**
Location: **Westside, CA**

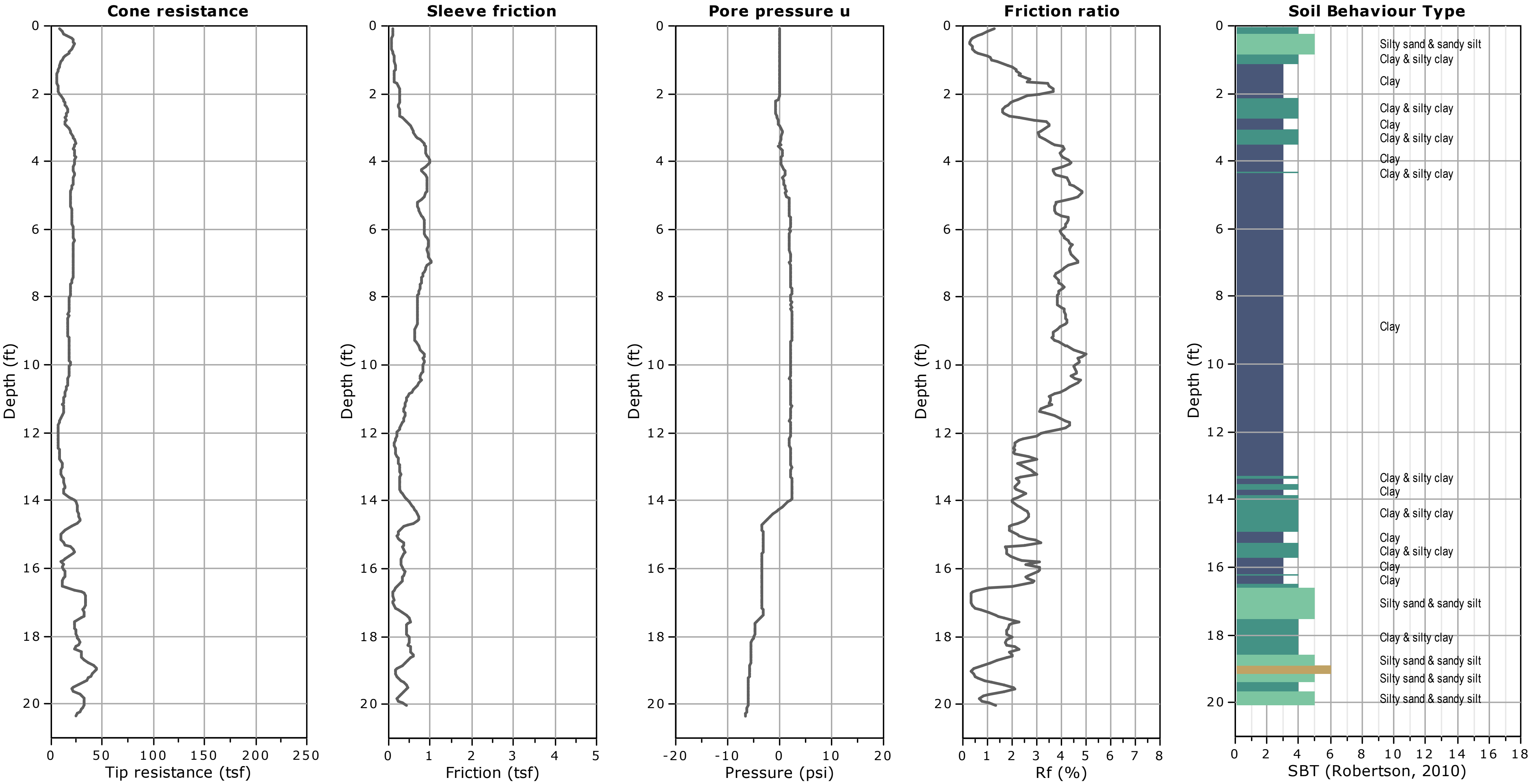
CPT-43
Total depth: 20.74 ft, Date: 4/7/2023



Project: **Terracon Consultants / Darden Solar**
Location: **Westside, CA**

CPT-44

Total depth: 20.35 ft, Date: 4/6/2023



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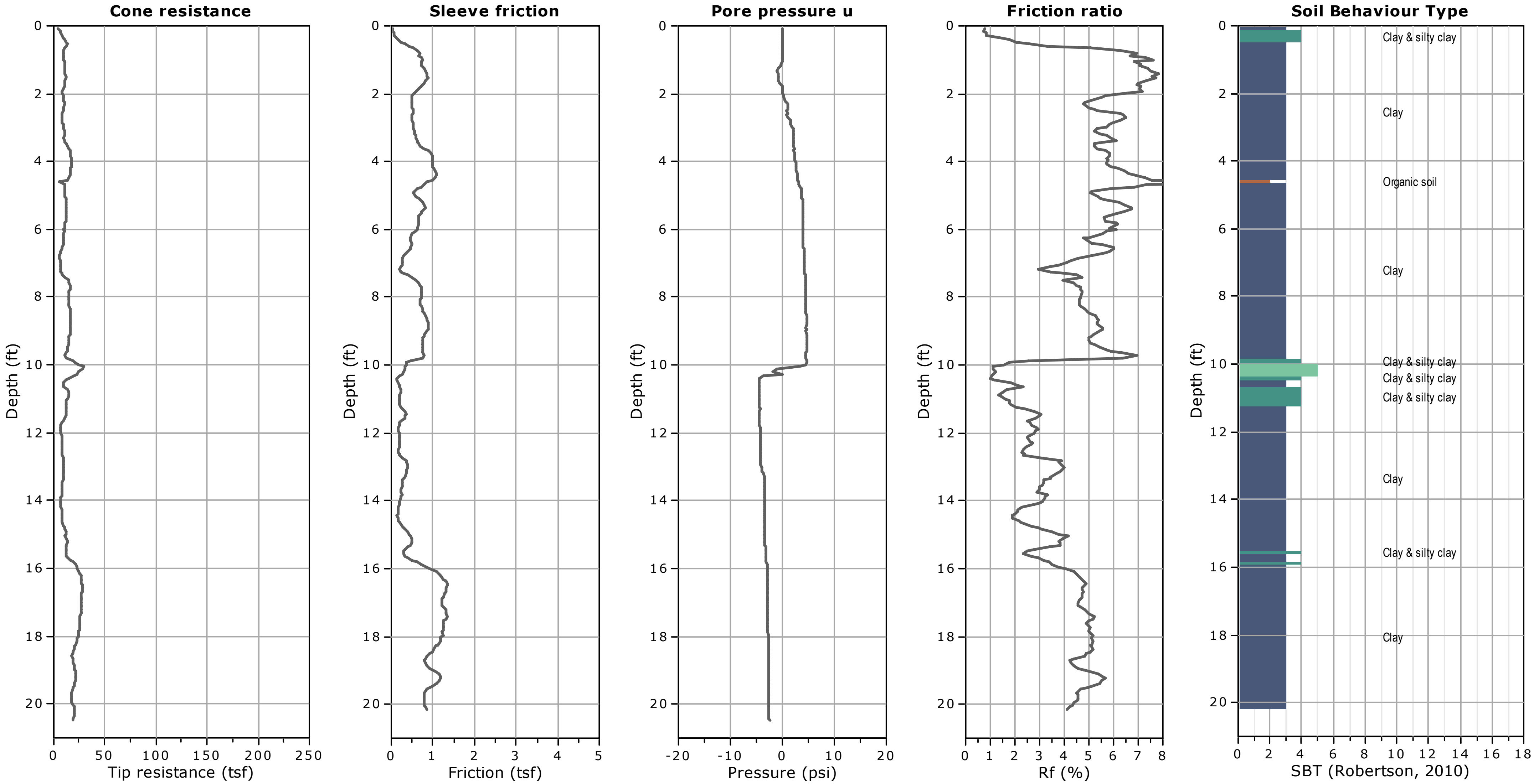
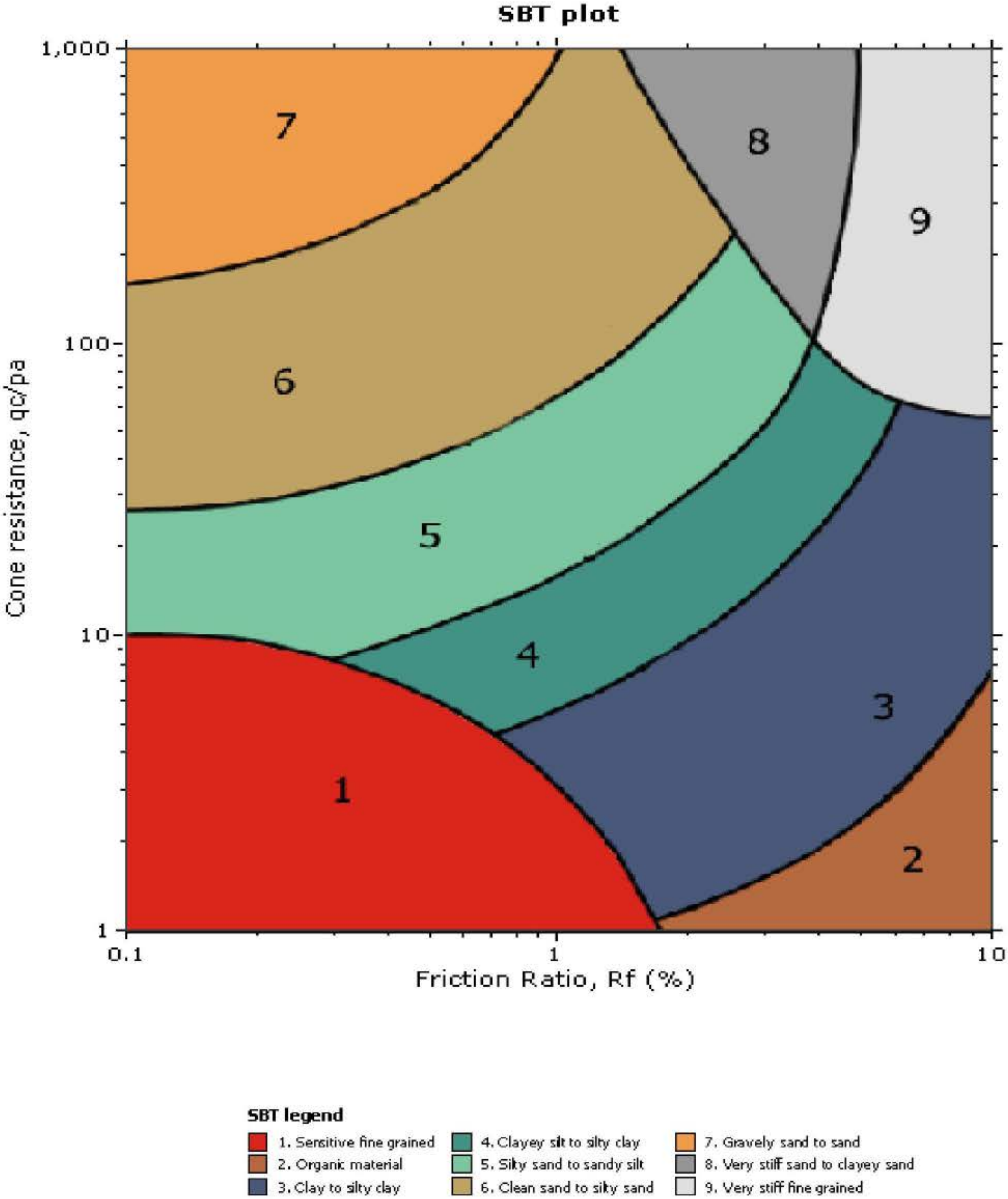
Project: **Terracon Consultants / Darden Solar**
Location: **Westside, CA**

CPT-45
Total depth: 20.49 ft, Date: 4/7/2023




SBT plot
1,000
100
10
1
Cone resistance, qc/pa
0.1
1
10
Friction Ratio, Rf (%)
7
8
9
6
5
4
3
1
2
SBT legend
1. Sensitive fine grained
2. Organic material
3. Clay to silty clay
4. Clayey silt to silty clay
5. Silty sand to sandy silt
6. Clean sand to silty sand
7. Gravely sand to sand
8. Very stiff sand to clayey sand
9. Very stiff fine grained

Laboratory Test Results

Contents:

Laboratory Testing Procedures

The project engineer reviewed the field data and assigned laboratory tests. The laboratory testing program included the following types of tests:

- ASTM D2216 Standard Test Methods for Laboratory Determination of Water (Moisture) Content of Soil and Rock by Mass
- ASTM D7263 Standard Test Methods for Laboratory Determination of Dry Density (Unit Weight) of Soil Specimens
- ASTM D4318 Standard Test Methods for Liquid Limit, Plastic Limit, and Plasticity Index of Soils
- ASTM D1140 Standard Test Methods for Determining the Amount of Material Finer than 75-µm (No. 200) Sieve in Soils by Washing
- ASTM D1557 Standard Test Methods for Laboratory Compaction Characteristics of Soil Using Modified Effort
- ASTM D4829 Standard Test Method for Expansion Index of Soils
- ASTM D1883 Standard Test Method for California Bearing Ratio (CBR) of Laboratory-Compacted Soils
- ASTM D2166 Standard Test Method for Unconfined Compressive Strength of Cohesive Soil
- ASTM D4546 Standard Test Methods for One-Dimensional Consolidation Properties of Soils Using Incremental Loading

The laboratory testing program also included review of soil samples by an engineer. Based on the results of our field and laboratory programs, we described and classified the soil samples in accordance with the Unified Soil Classification System.

Thermal Resistivity: Thermal resistivity tests were analyzed by Geotherm USA. Terracon collected bulk samples of subsurface materials obtained within proposed array and substation/BESS areas. Each bulk sample had a Modified Proctor test performed, and each bulk sample was tested for thermal resistivity tests on samples remolded to 85% in the array areas or 90% in the substation/BESS location. The percent compaction is based on comparing to the material’s maximum dry density as determined by test method ASTM D1557 (Modified Proctor). Tests included a minimum of 4 readings, including optimum moisture content or as-received moisture (whichever is higher), totally dry condition, and 2 intermediate moisture contents.

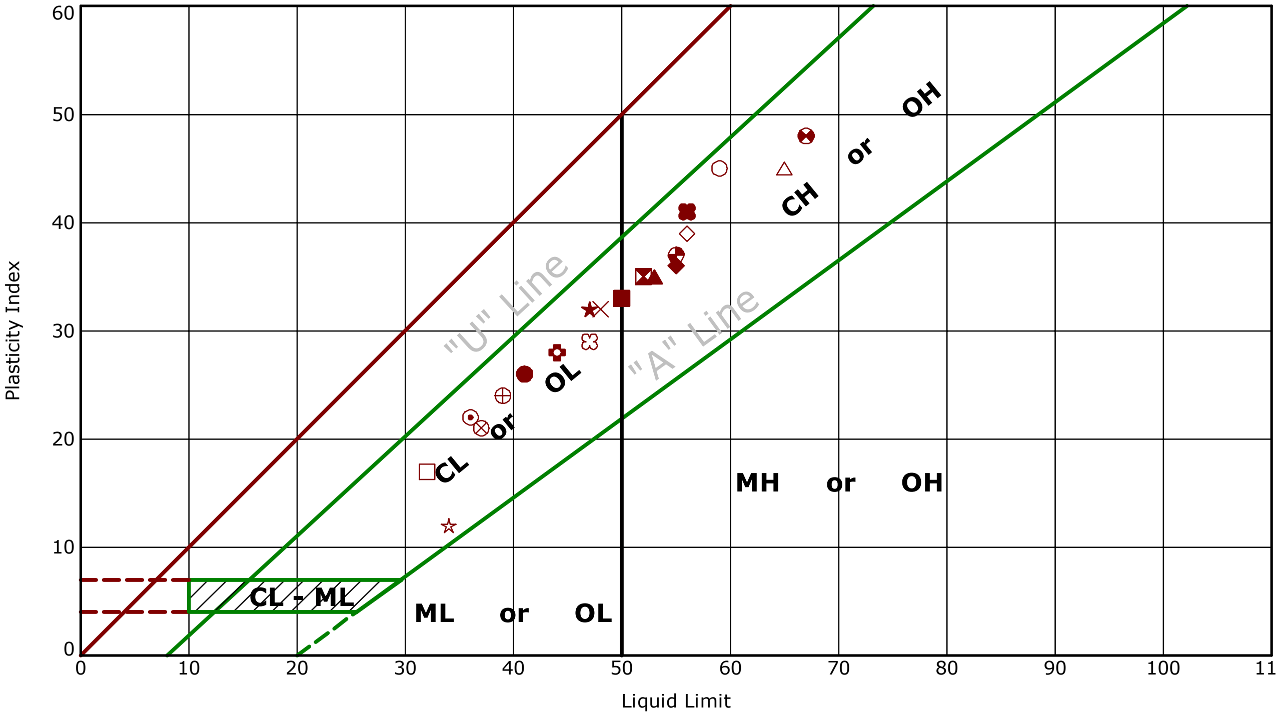
Corrosivity Testing: Bulk samples of near surface soils were tested in the laboratory for the following properties in general accordance with the corresponding standards:

- pH Analysis (ASTM G51)
- Chloride (ASTM D512)
- Sulfate (ASTM C1580)
- Sulfide Content (AWWA 4500-S D)
- Oxidation-Reduction Potential (ASTM G200)

- Electrical Resistivity Testing (ASTM G187)

Atterberg Limit Results

ASTM D4318



	Boring ID	Depth (Ft)	LL	PL	PI	Fines	USCS	Description
●	B-1	0 - 4	41	15	26	62.1	CL	SANDY LEAN CLAY
⊠	B-3	0 - 4	52	17	35		CH	FAT CLAY
▲	B-3	10 - 11.5	53	18	35	89.7	CH	FAT CLAY
★	B-6	15 - 16.5	47	15	32	88.5	CL	LEAN CLAY
⊙	B-10	1 - 4	36	14	22	63.4	CL	SANDY LEAN CLAY
✚	B-11	0 - 4	44	16	28	77.2	CL	LEAN CLAY with SAND
○	B-12	0 - 4	59	14	45	83.2	CH	FAT CLAY with SAND
△	B-17	0 - 4	65	20	45	95.2	CH	FAT CLAY
⊗	B-20	0 - 4	37	16	21	66.3	CL	SANDY LEAN CLAY
⊕	B-21	0 - 4	39	15	24	68.6	CL	SANDY LEAN CLAY
□	B-22	0 - 4	32	15	17	60.1	CL	SANDY LEAN CLAY
⨂	B-24	0 - 4	67	19	48		CH	FAT CLAY
◕	B-29	0 - 4	55	18	37	86.2	CH	FAT CLAY
☆	B-36	7.5 - 9	34	22	12	63.7	CL	SANDY LEAN CLAY
✥	B-38	0 - 4	47	18	29	71.5	CL	LEAN CLAY with SAND
■	B-40	0 - 4	50	17	33		CH	FAT CLAY
◆	B-41	0 - 4	55	19	36		CH	FAT CLAY
◇	B-42	1 - 5	56	17	39		CH	SANDY FAT CLAY
✕	B-49	1 - 5	48	16	32		CL	LEAN CLAY
✤	B-50	0 - 4	56	15	41	81.1	CH	FAT CLAY with SAND

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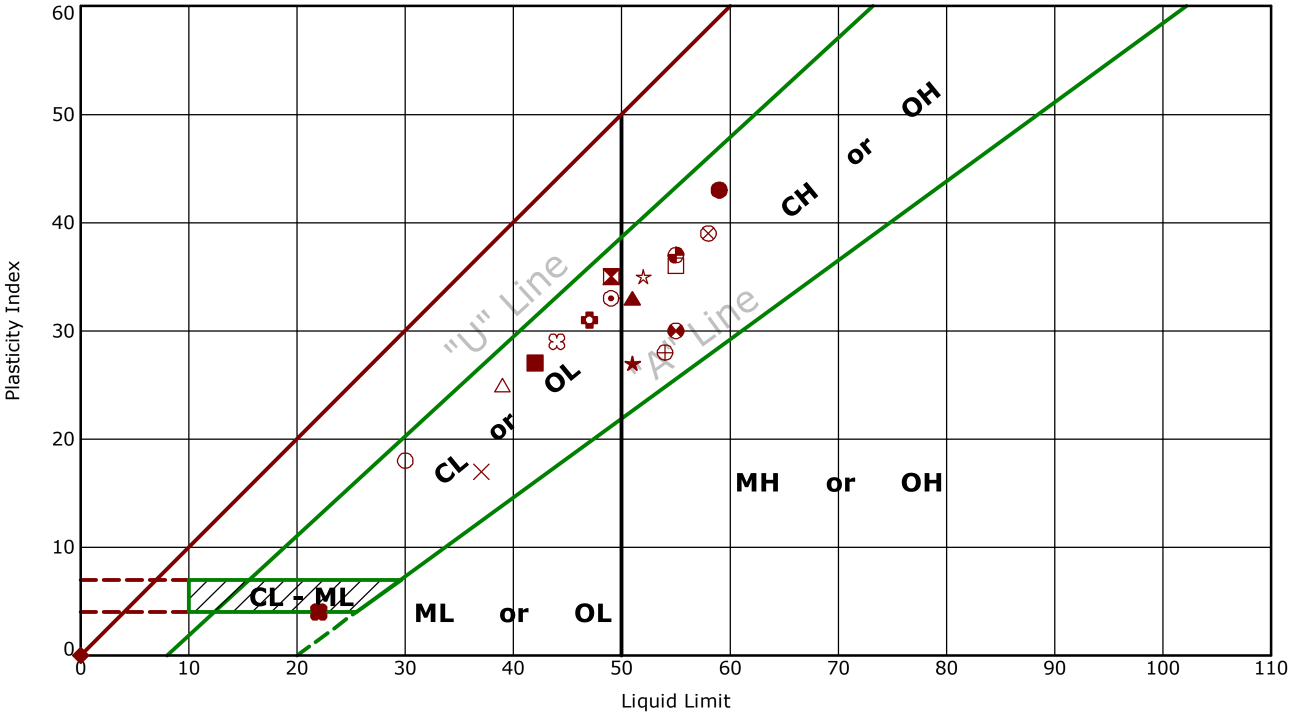
Ste 350
Laguna Hills, CA

Atterberg Limit Results

ASTM D4318



	Boring ID	Depth (Ft)	LL	PL	PI	Fines	USCS	Description
●	B-51	0 - 4	59	16	43	84.3	CH	FAT CLAY with SAND
▲	B-63	0 - 4	51	18	33	77.7	CH	FAT CLAY with SAND
★	B-65	0 - 4	51	24	27	76.3	CH	FAT CLAY with SAND
⊙	B-66	1 - 4	49	16	33	73.7	CL	LEAN CLAY with SAND
○	B-69	0 - 4	30	12	18	46.9	SC	CLAYEY SAND
⊗	B-79	0 - 4	58	19	39		CH	FAT CLAY
☐	B-84	0 - 4	55	19	36	78.0	CH	FAT CLAY with SAND
◕	B-90	0 - 4	55	18	37		CH	FAT CLAY
✿	B-106	0 - 4	44	15	29	88.7	CL	LEAN CLAY
■	B-107	0 - 4	42	15	27	56.6	CL	SANDY LEAN CLAY
◆	B-111	0 - 4	NP	NP	NP		ML	SANDY SILT
◇	B-113	0 - 4	42	15	27	65.9	CL	SANDY LEAN CLAY
×	B-115	2.5 - 4	37	20	17	26.7	SC	CLAYEY SAND
✤	B-116	15 - 16.5	22	18	4	16.4	SC-SM	SILTY, CLAYEY SAND

Laboratory tests are not valid if separated from original report.

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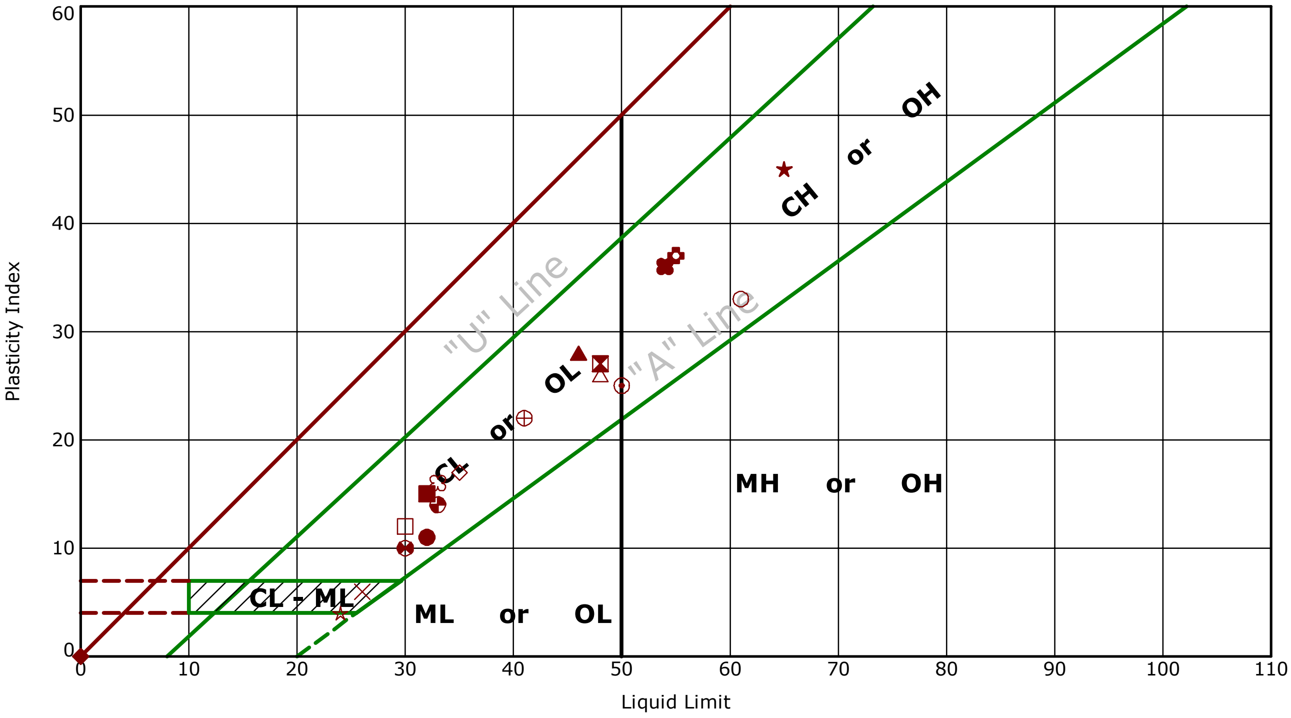
Ste 350
Laguna Hills, CA

Atterberg Limit Results

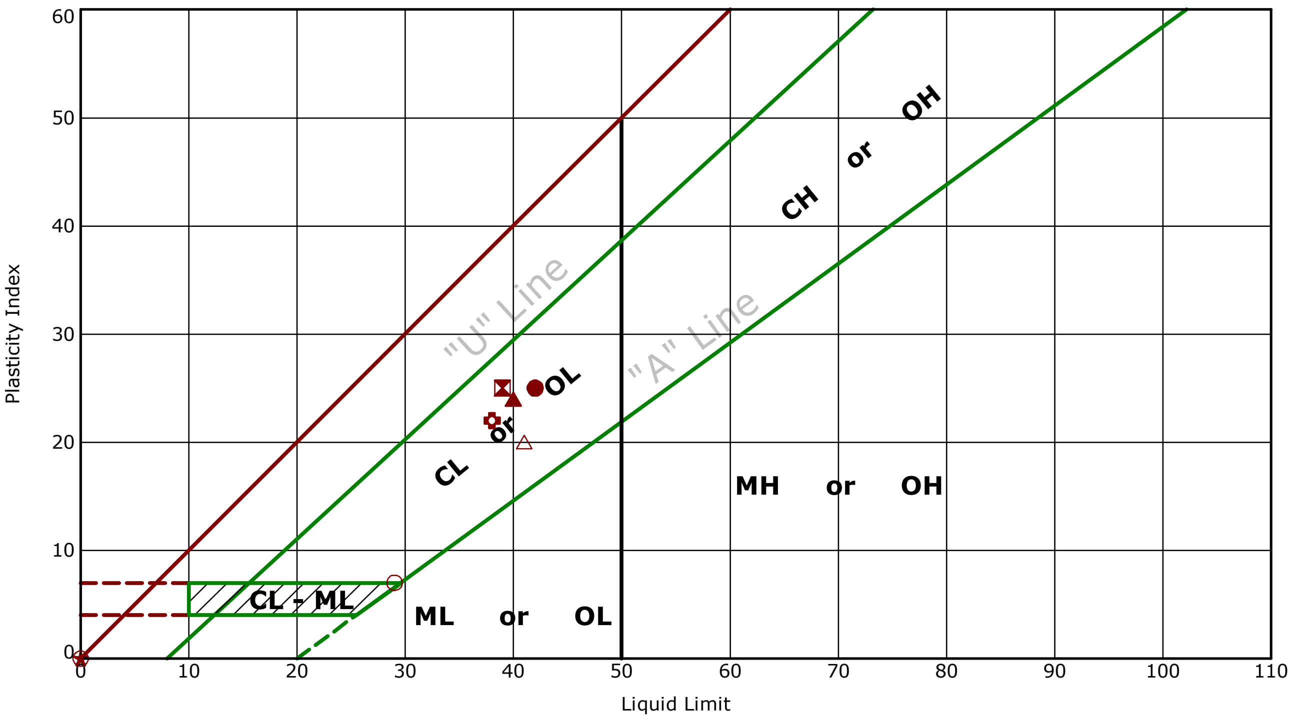
ASTM D4318



	Boring ID	Depth (Ft)	LL	PL	PI	Fines	USCS	Description
●	B-117	10 - 11.5	32	21	11	61.7	CL	SANDY LEAN CLAY
▲	B-119	0 - 4	46	18	28		CL	LEAN CLAY
★	B-121	0 - 4	65	20	45		CH	FAT CLAY
⊙	B-123	0 - 4	50	25	25	85.6	CH	FAT CLAY
○	B-128	2.5 - 4	61	28	33	96.2	CH	FAT CLAY
⊗	SUB-2	0 - 4	32	17	15	41.6	SC	CLAYEY SAND
□	SUB-2	25 - 26.5	30	18	12	67.2	CL	SANDY LEAN CLAY
◕	SW-1	5 - 6.5	33	19	14		SC	CLAYEY SAND
✿	SW-1	45 - 46.5	33	17	16		SC	CLAYEY SAND
■	E-2	0 - 4	32	17	15	38.5	SC	CLAYEY SAND
◆	E-2	5 - 6.5	NP	NP	NP		SM	SILTY SAND
◇	E-2	7.5 - 9	35	18	17	43.0	SC	CLAYEY SAND
×	E-2	30 - 31.5	26	20	6		SC-SM	SILTY, CLAYEY SAND
✤	T-1	0 - 4	54	18	36		CH	SANDY FAT CLAY

Atterberg Limit Results

ASTM D4318

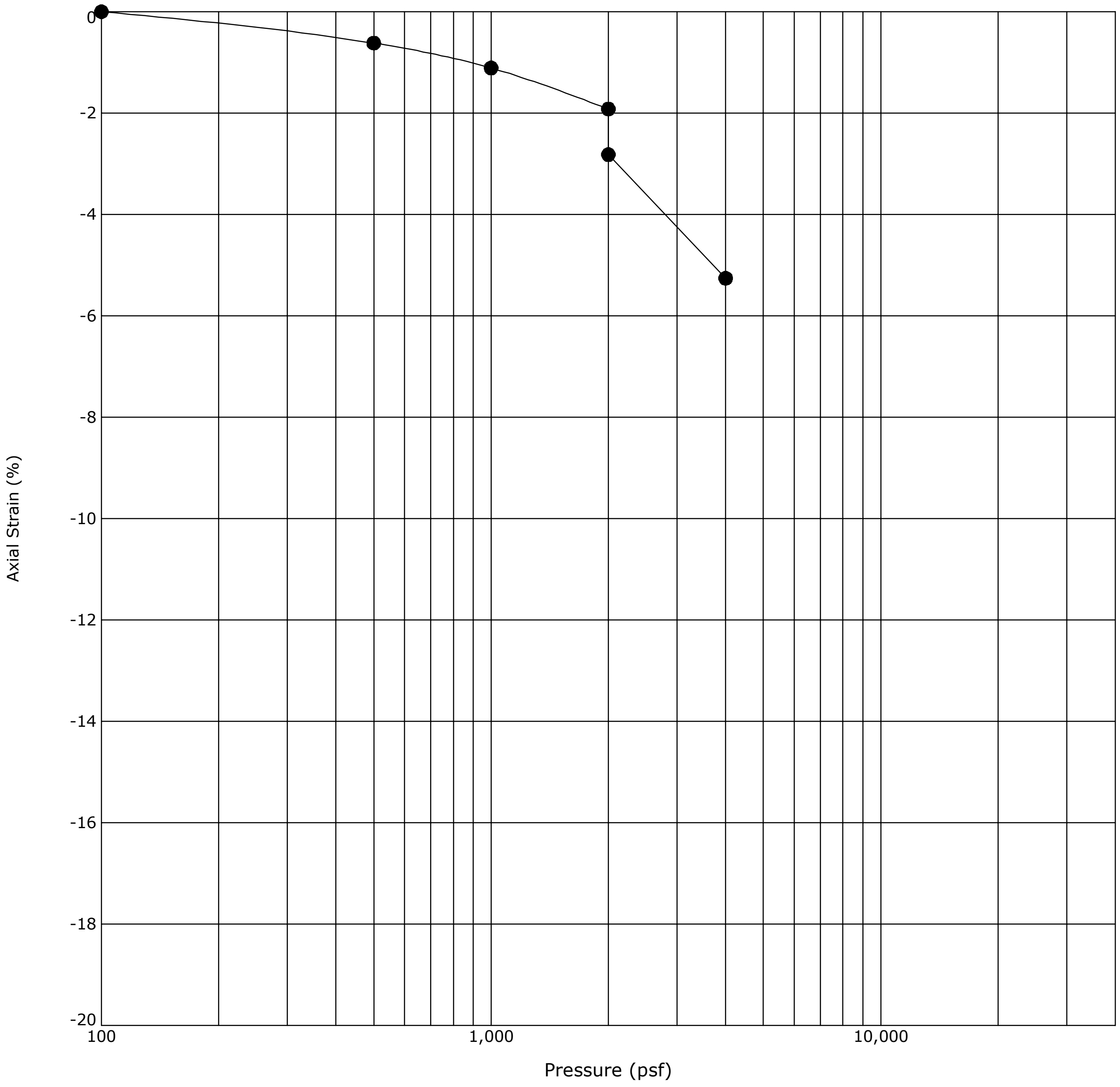


	Boring ID	Depth (Ft)	LL	PL	PI	Fines	USCS	Description
●	T-2	0 - 4	42	17	25	70.9	CL	LEAN CLAY with SAND
▲	T-4	0 - 4	40	16	24	67.0	CL	SANDY LEAN CLAY
★	T-8	10 - 11.5	NP	NP	NP	53.7	ML	SANDY SILT
⊙	T-8	25 - 26.5	NP	NP	NP	38.5	SM	SILTY SAND
○	T-9	25 - 26.5	29	22	7		CL-ML	SANDY, SILTY CLAY

23041 Avenida De La Carlota
Ste 350
Laguna Hills, CA

Swell Consolidation Test

ASTM D4546



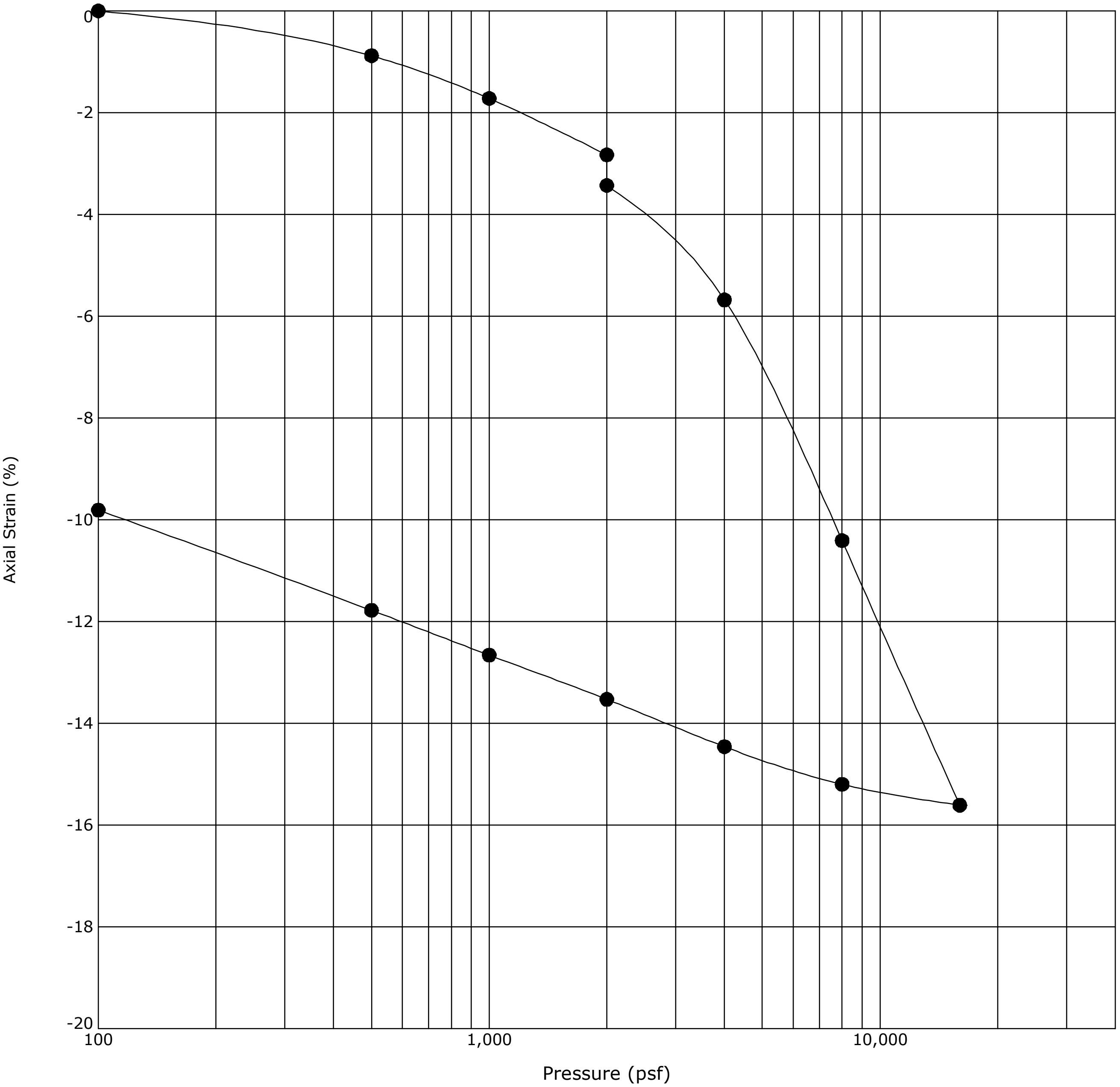
	Boring ID	Depth (Ft)	Description	USCS	γ_d(pcf)	WC (%)
●	E-1	2.5 - 4	CLAYEY SAND	SC	92	16.9

Notes: Water added at 2,000 psf

23041 Avenida De La Carlota
Ste 350
Laguna Hills, CA

Swell Consolidation Test

ASTM D2435



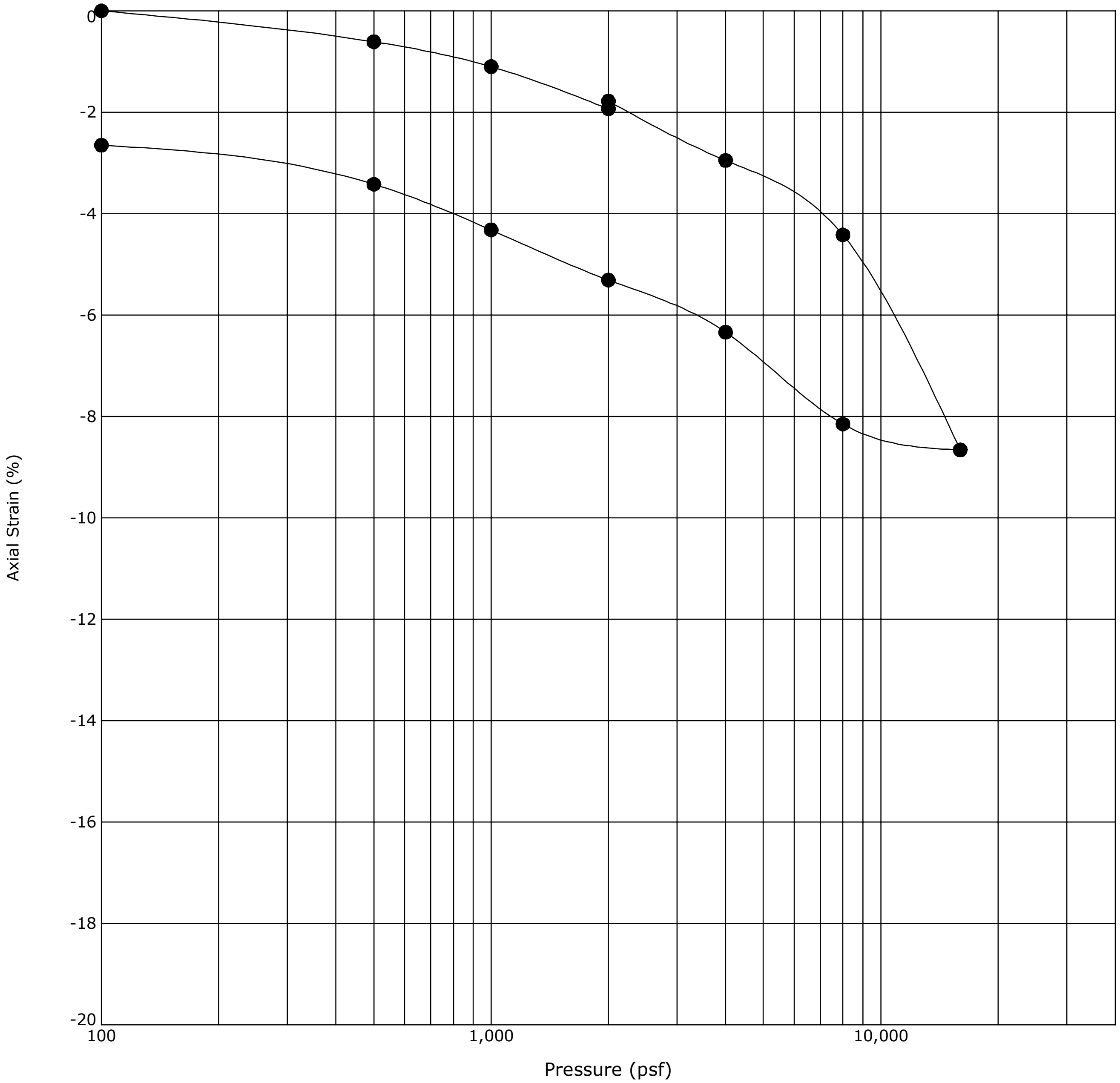
Boring ID		Depth (Ft)	Description	USCS	γ_d(pcf)	WC (%)
●	SUB-1	2.5 - 4	LEAN CLAY with SAND	CL	96	22.3

Notes: Water added at 2,000 psf

23041 Avenida De La Carlota
Ste 350
Laguna Hills, CA

Swell Consolidation Test

ASTM D2435



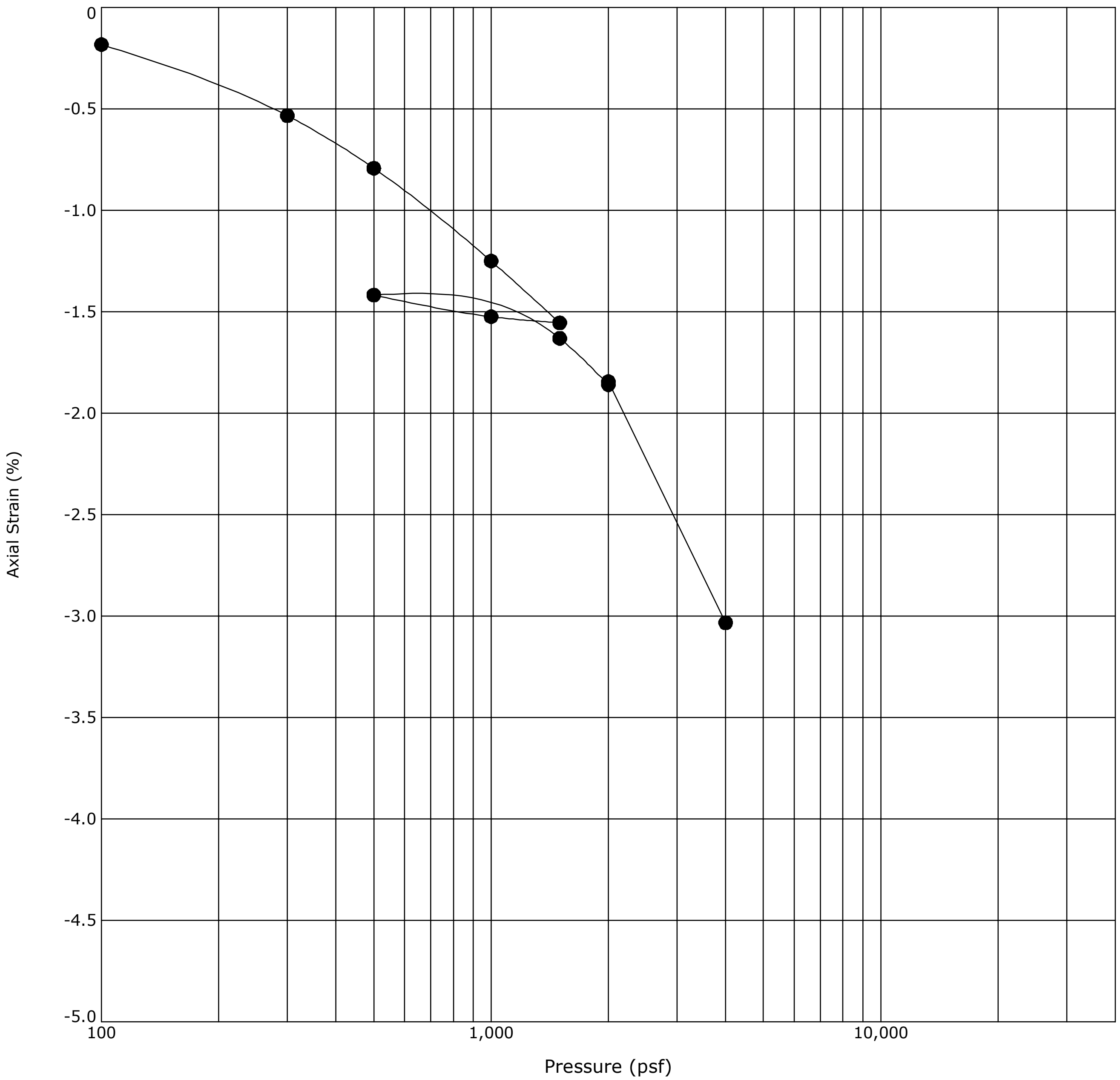
Boring ID		Depth (Ft)	Description	USCS	γ_d(pcf)	WC (%)
●	BESS-1	2.5 - 4	SANDY LEAN CLAY	CL	94	16.1

Notes: Water added at 2,000 psf

23041 Avenida De La Carlota
Ste 350
Laguna Hills, CA

Swell Consolidation Test

ASTM D4546



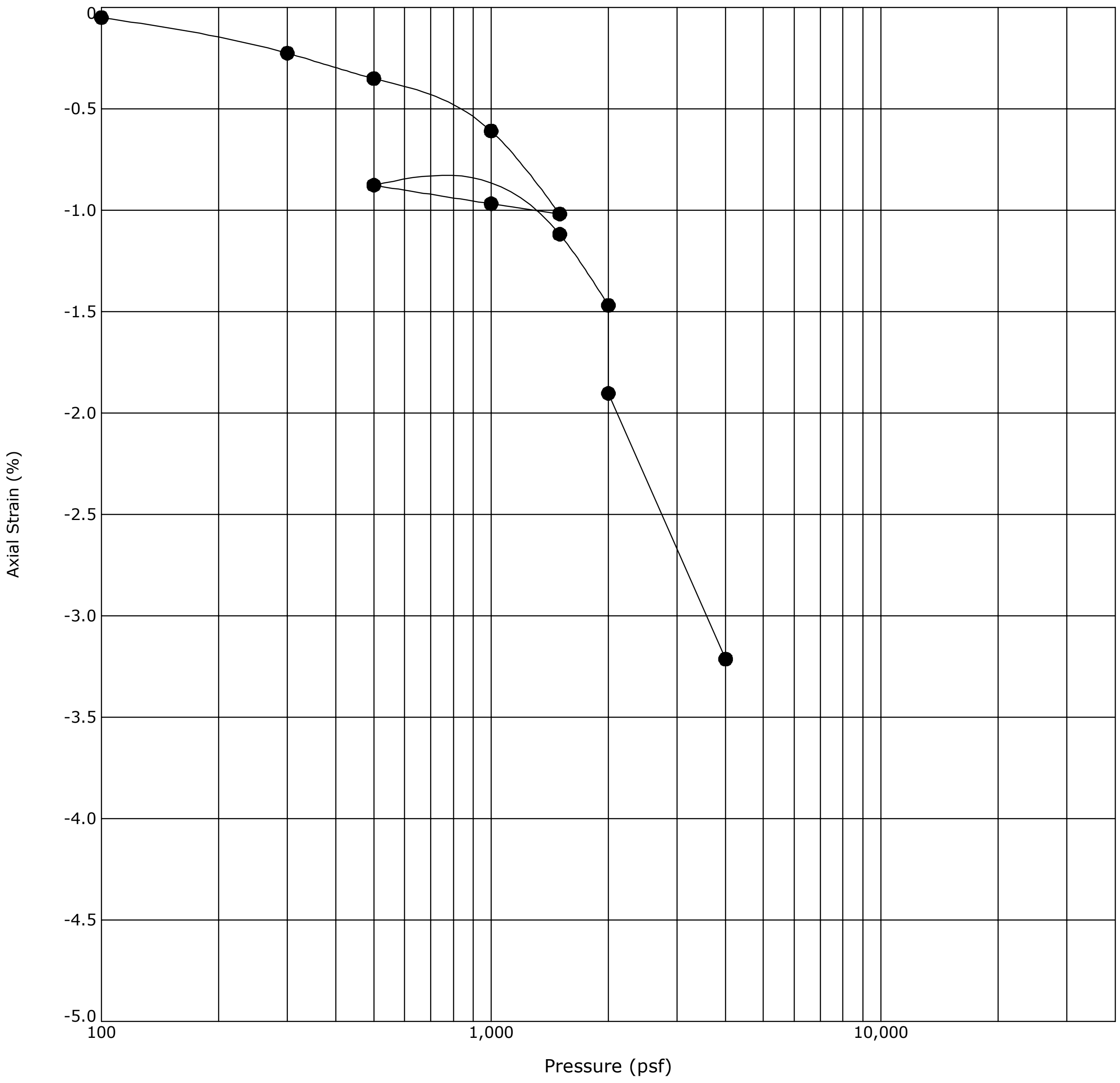
Boring ID		Depth (Ft)	Description	USCS	γ_d(pcf)	WC (%)
●	SUB-2	2.5 - 4	CLAYEY SAND	SC	103	14.2

Notes: Water added at 2,000 psf

23041 Avenida De La Carlota
Ste 350
Laguna Hills, CA

Swell Consolidation Test

ASTM D4546



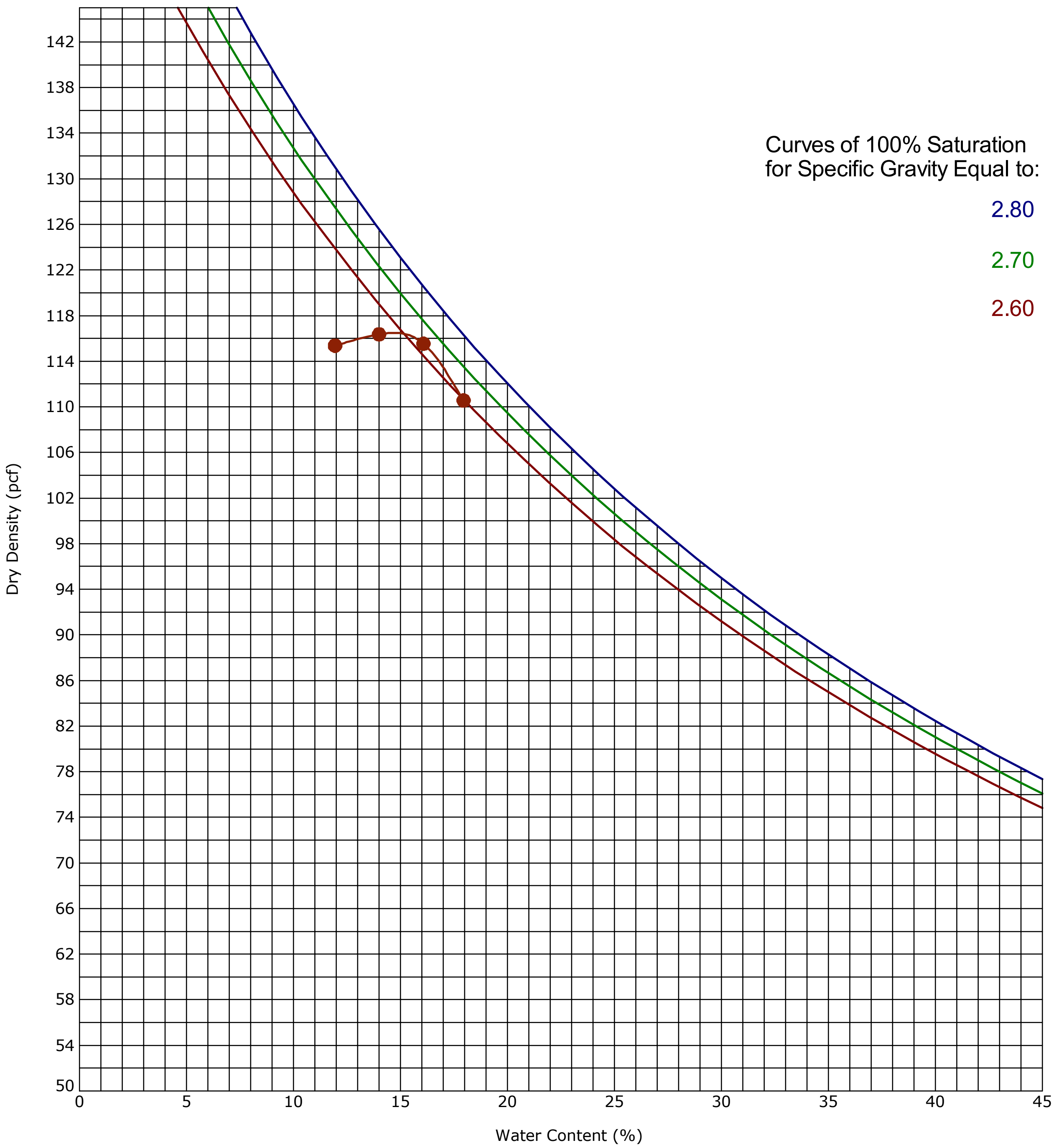
Boring ID		Depth (Ft)	Description	USCS	γ_d(pcf)	WC (%)
●	E-2	2.5 - 4	CLAYEY SAND	SC	103	10.7

Notes: Water added at 2,000 psf

23041 Avenida De La Carlota
Ste 350
Laguna Hills, CA

Moisture-Density Relationship

ASTM D698/D1557



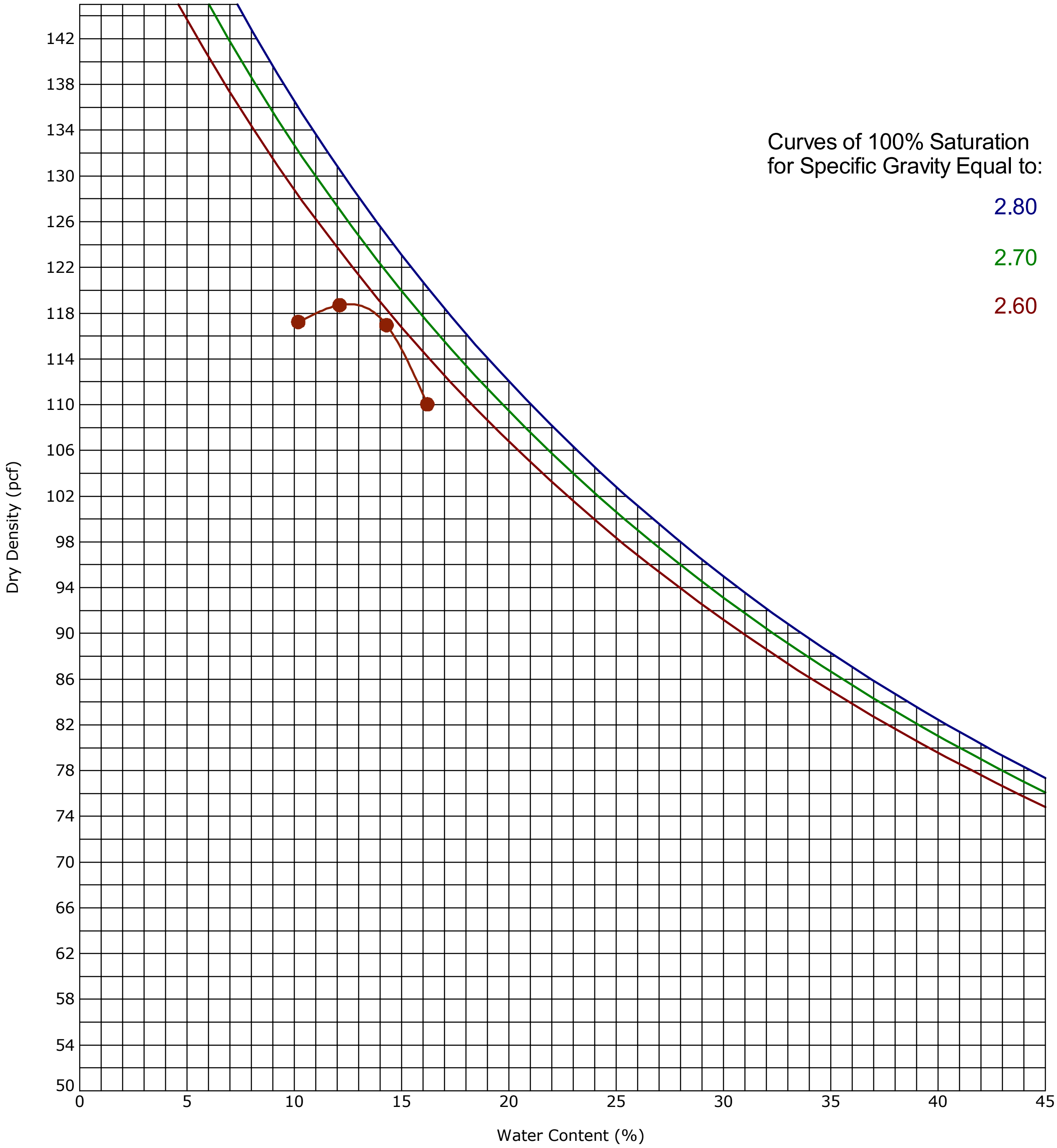
Boring ID	Depth (Ft)	Description of Materials
B-2	0 - 4	LEAN CLAY

Fines (%)	Fraction >19mm size (%)	LL	PL	PI	Test Method	Maximum Dry Density (pcf)	Optimum Water Content (%)
					ASTM D1557 Method A	116.5	14.7

23041 Avenida De La Carlota
Ste 350
Laguna Hills, CA

Moisture-Density Relationship

ASTM D698/D1557



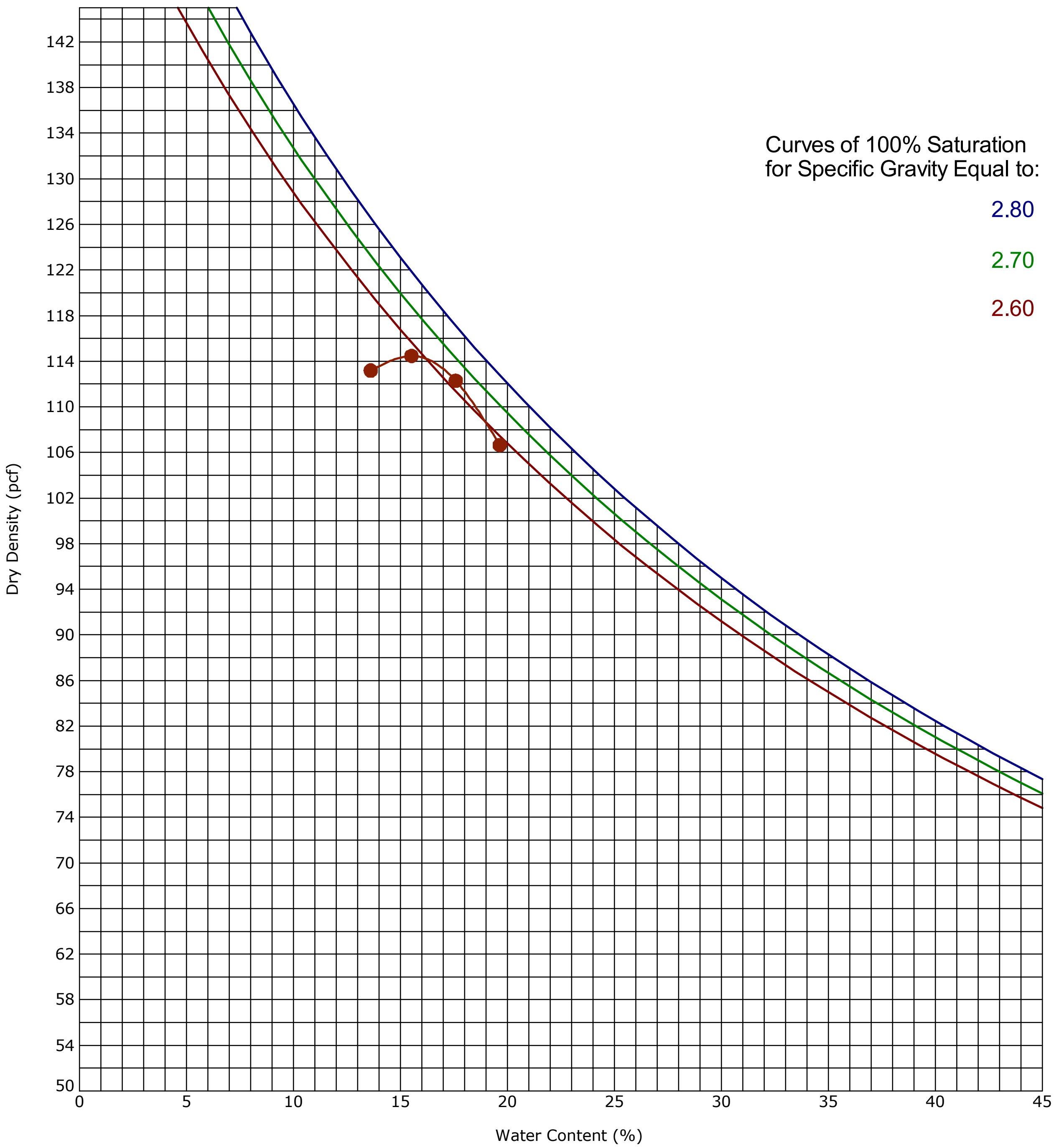
Boring ID	Depth (Ft)	Description of Materials
B-10	1 - 4	SANDY LEAN CLAY

Fines (%)	Fraction >19mm size (%)	LL	PL	PI	Test Method	Maximum Dry Density (pcf)	Optimum Water Content (%)
63		36	14	22	ASTM D1557 Method A	118.8	12.6

23041 Avenida De La Carlota
Ste 350
Laguna Hills, CA

Moisture-Density Relationship

ASTM D698/D1557



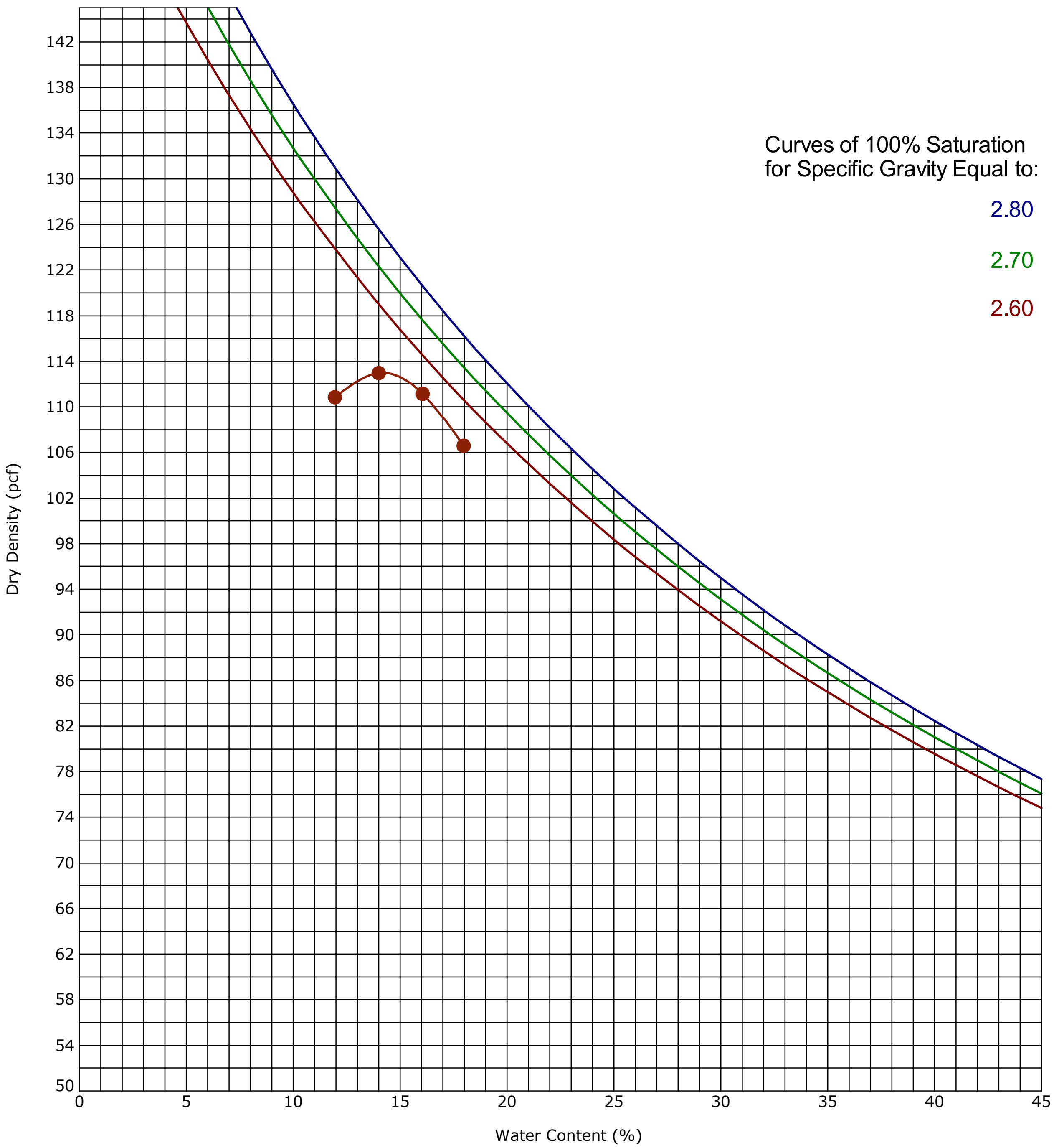
Boring ID	Depth (Ft)	Description of Materials
B-12	0 - 4	FAT CLAY with SAND

Fines (%)	Fraction >19mm size (%)	LL	PL	PI	Test Method	Maximum Dry Density (pcf)	Optimum Water Content (%)
83		59	14	45	ASTM D1557 Method B	114.5	15.5

23041 Avenida De La Carlota
Ste 350
Laguna Hills, CA

Moisture-Density Relationship

ASTM D698/D1557



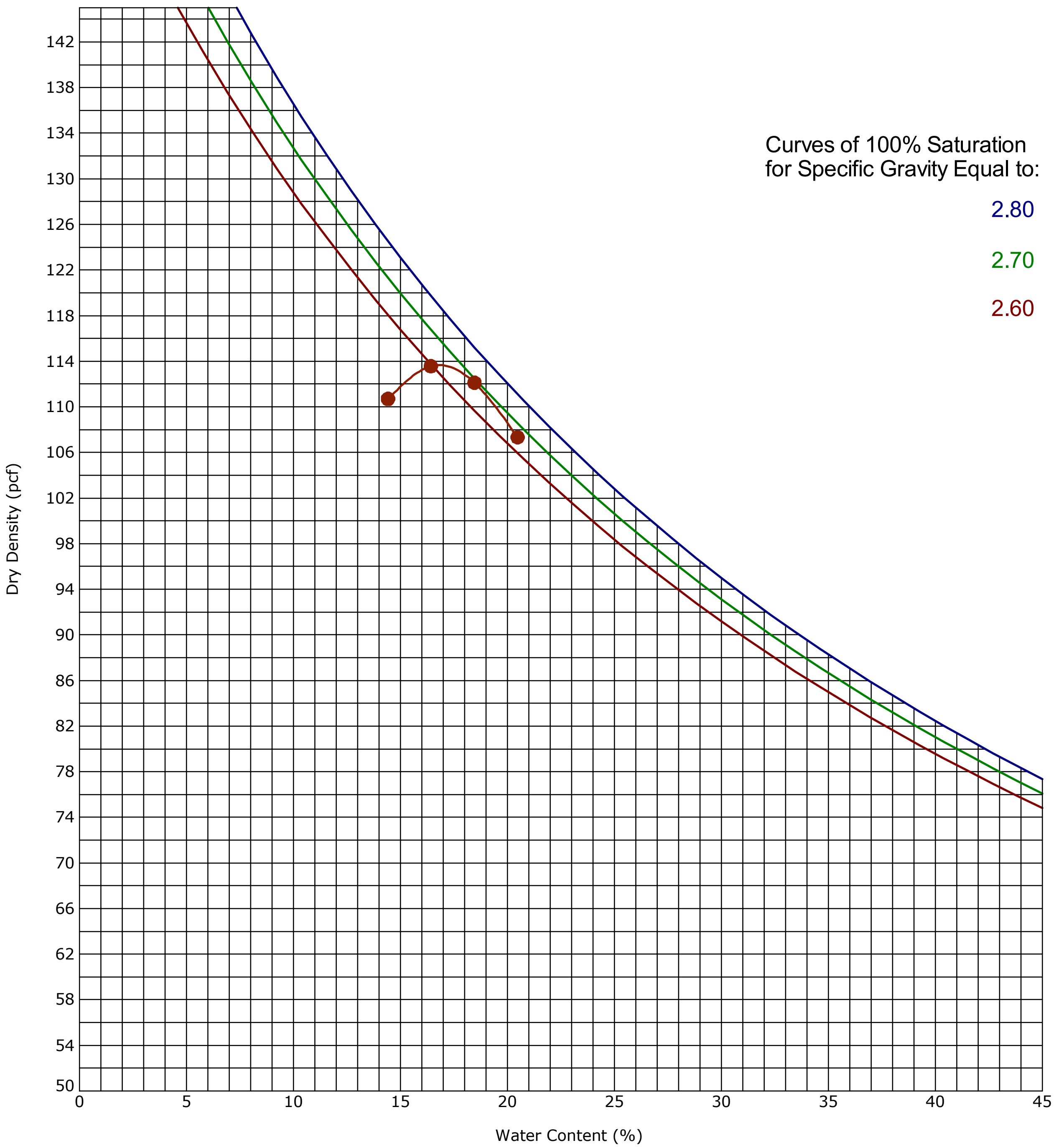
Boring ID	Depth (Ft)	Description of Materials
B-25	1 - 5	SANDY LEAN CLAY

Fines (%)	Fraction >19mm size (%)	LL	PL	PI	Test Method	Maximum Dry Density (pcf)	Optimum Water Content (%)
					ASTM D1557 Method A	113.0	14.2

Terracon
23041 Avenida De La Carlota
Ste 350
Laguna Hills, CA

Moisture-Density Relationship

ASTM D698/D1557



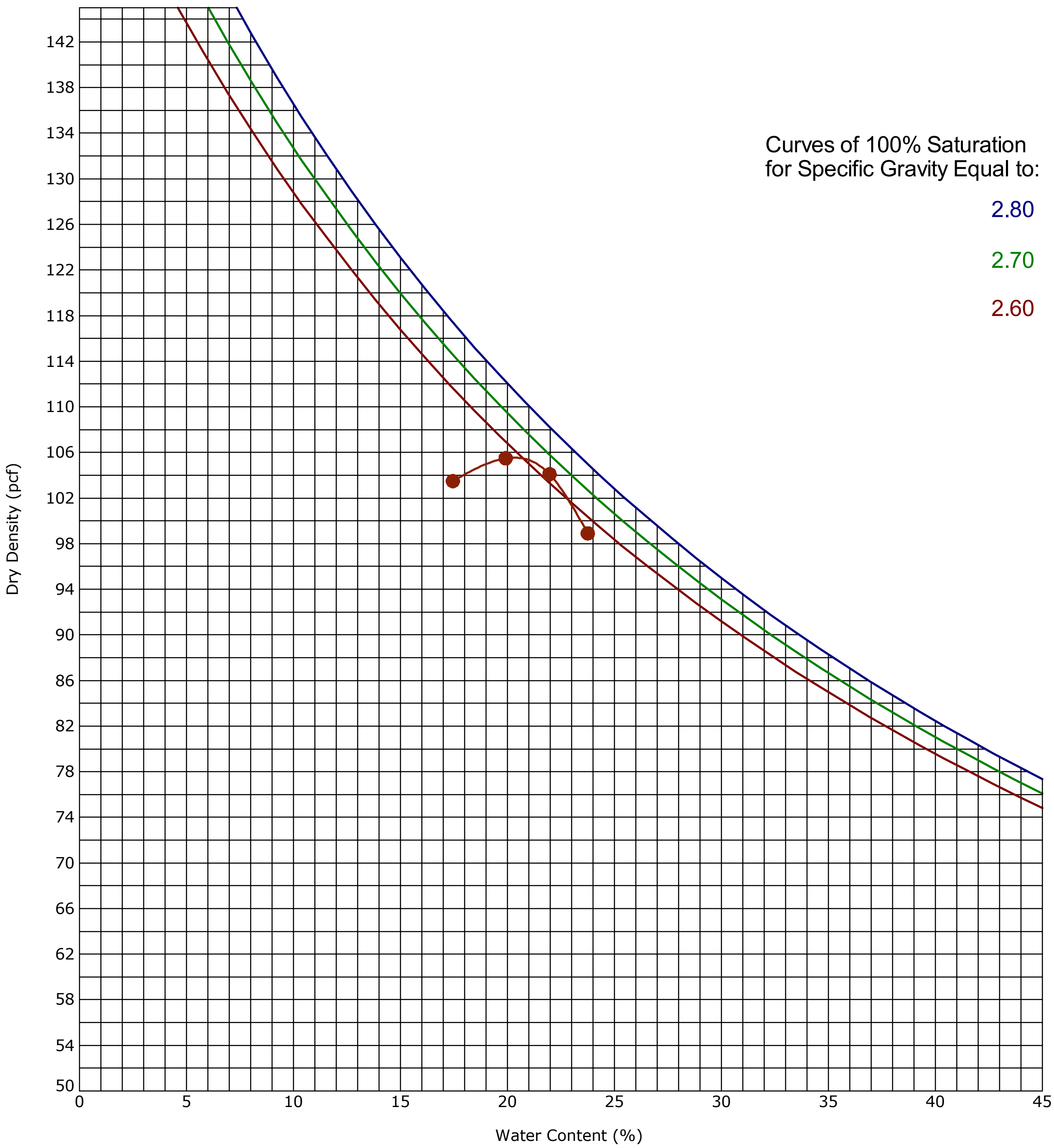
Boring ID	Depth (Ft)	Description of Materials
B-34	0 - 4	SANDY LEAN CLAY

Fines (%)	Fraction >19mm size (%)	LL	PL	PI	Test Method	Maximum Dry Density (pcf)	Optimum Water Content (%)
					ASTM D1557 Method B	113.7	16.9

23041 Avenida De La Carlota
Ste 350
Laguna Hills, CA

Moisture-Density Relationship

ASTM D698/D1557

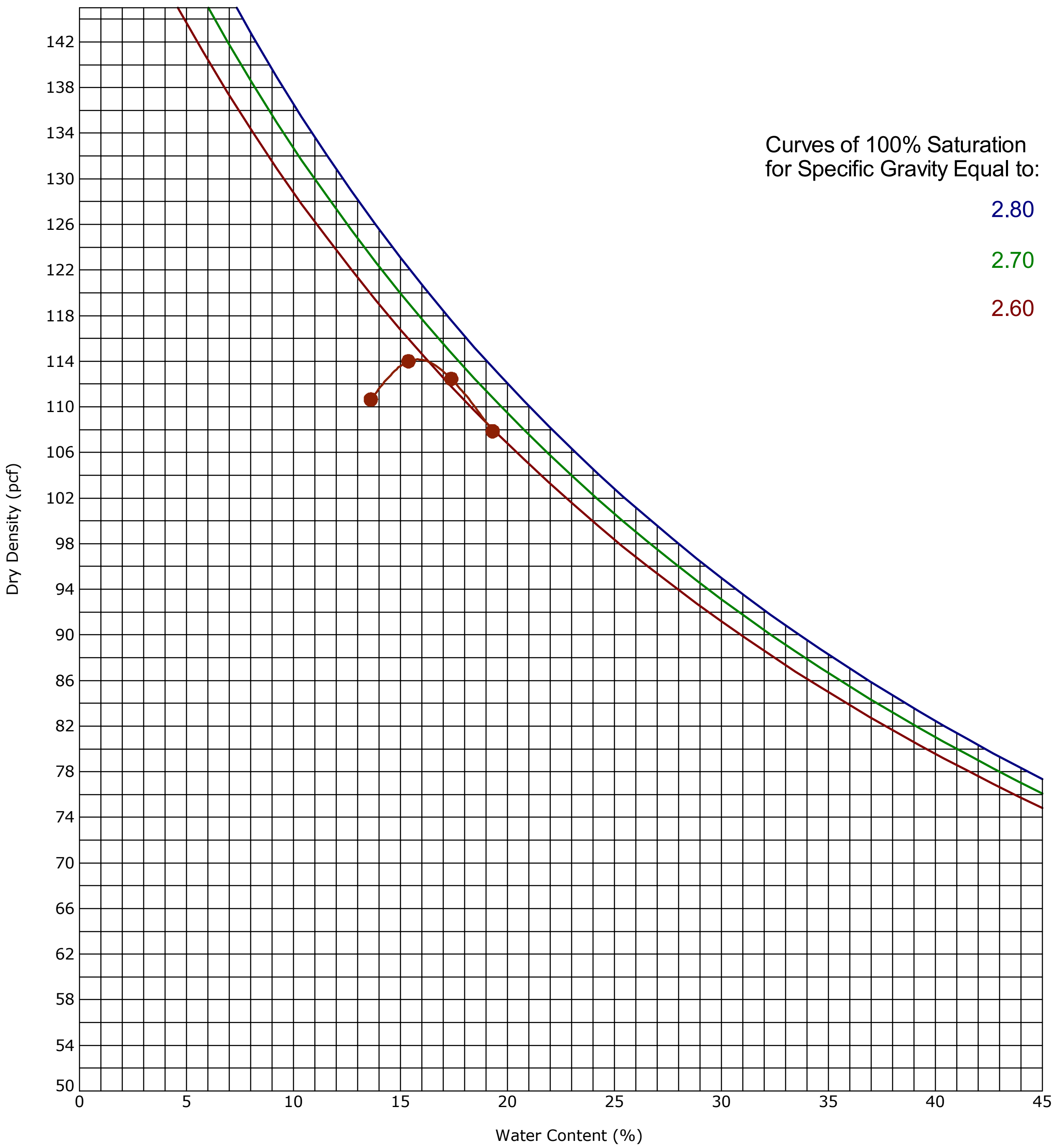


Boring ID	Depth (Ft)	Description of Materials
B-35	0 - 4	FAT CLAY

Fines (%)	Fraction >19mm size (%)	LL	PL	PI	Test Method	Maximum Dry Density (pcf)	Optimum Water Content (%)
					ASTM D1557 Method A	105.5	20.3

Moisture-Density Relationship

ASTM D698/D1557



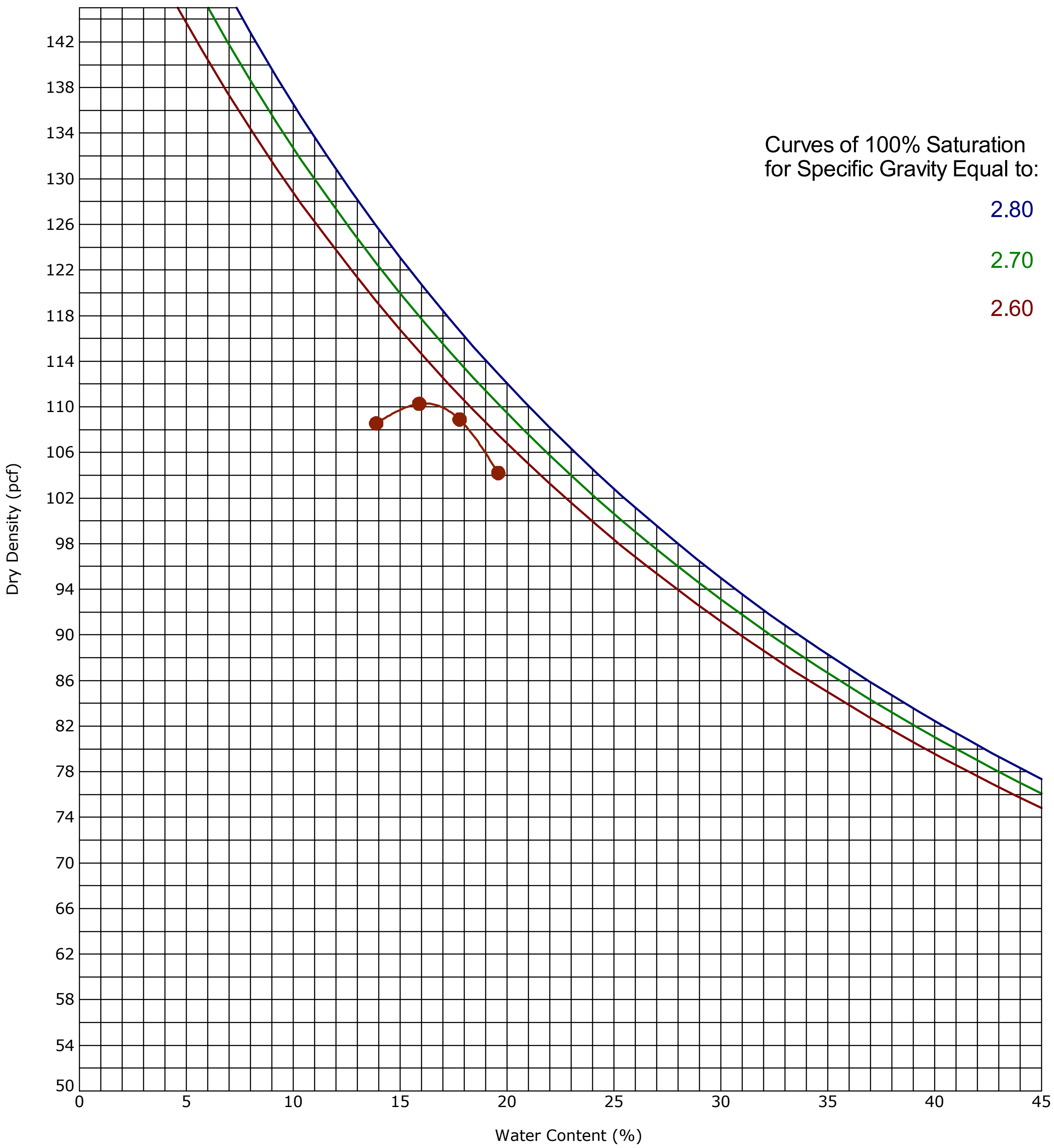
Boring ID	Depth (Ft)	Description of Materials
B-37	0 - 4	LEAN CLAY

Fines (%)	Fraction >19mm size (%)	LL	PL	PI	Test Method	Maximum Dry Density (pcf)	Optimum Water Content (%)
					ASTM D1557 Method A	114.2	15.8

23041 Avenida De La Carlota
Ste 350
Laguna Hills, CA

Moisture-Density Relationship

ASTM D698/D1557



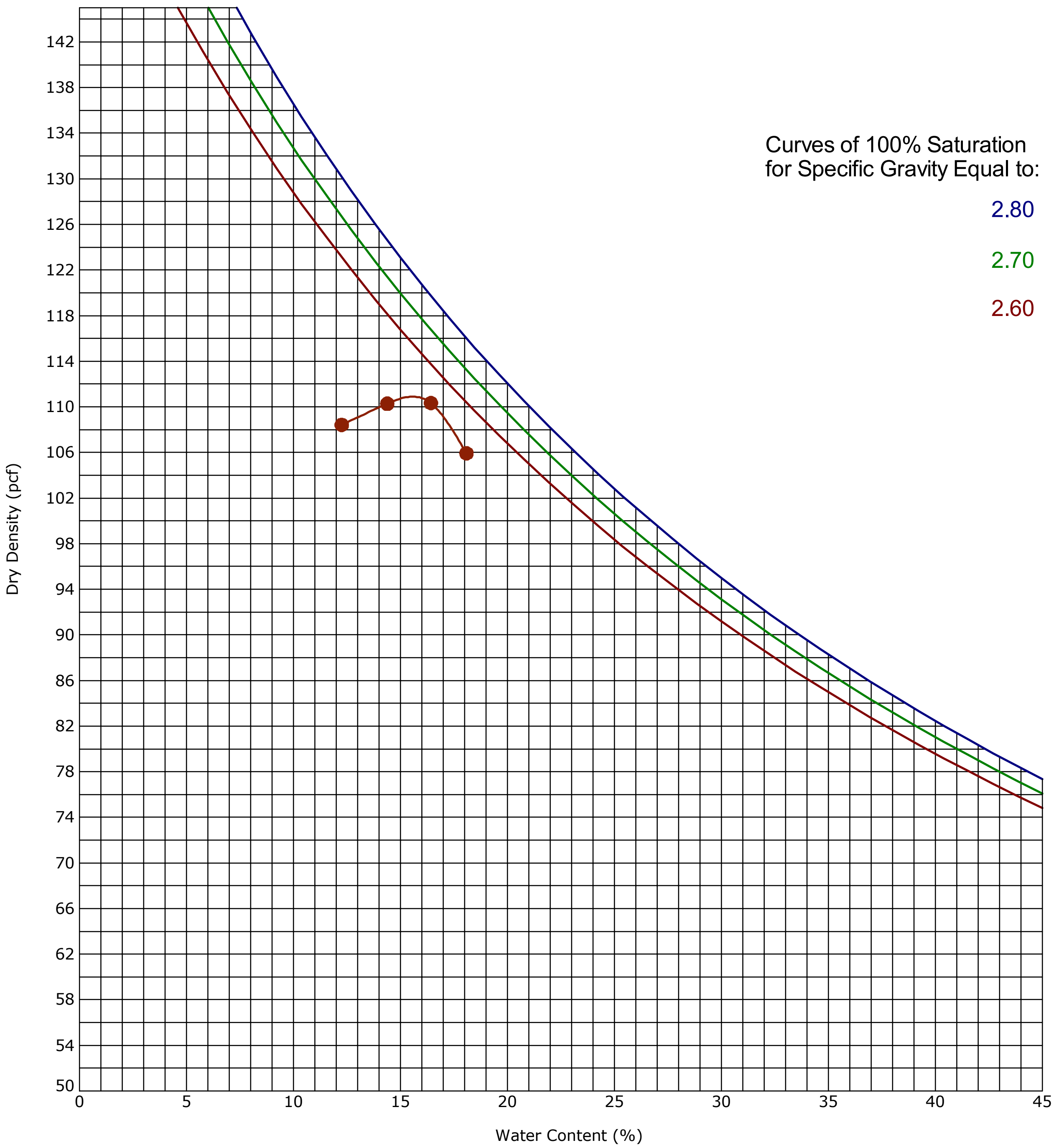
Boring ID	Depth (Ft)	Description of Materials
B-46	1 - 4	LEAN CLAY

Fines (%)	Fraction >19mm size (%)	LL	PL	PI	Test Method	Maximum Dry Density (pcf)	Optimum Water Content (%)
					ASTM D1557 Method A	110.3	16.2

Terracon
23041 Avenida De La Carlota
Ste 350
Laguna Hills, CA

Moisture-Density Relationship

ASTM D698/D1557



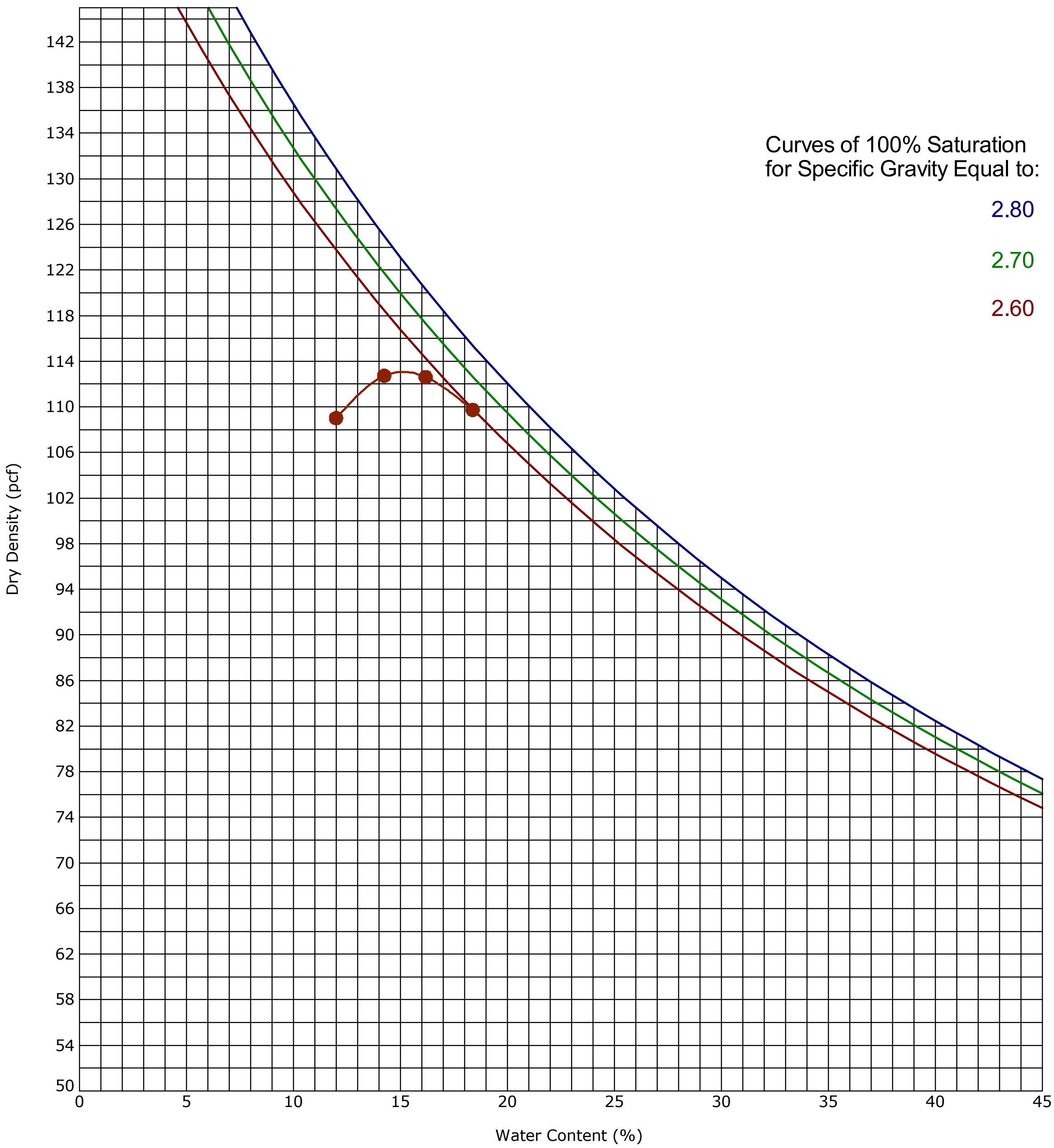
Boring ID	Depth (Ft)	Description of Materials
B-49	1 - 5	LEAN CLAY

Fines (%)	Fraction >19mm size (%)	LL	PL	PI	Test Method	Maximum Dry Density (pcf)	Optimum Water Content (%)
		48	16	32	ASTM D1557 Method A	110.9	15.6

23041 Avenida De La Carlota
Ste 350
Laguna Hills, CA

Moisture-Density Relationship

ASTM D698/D1557



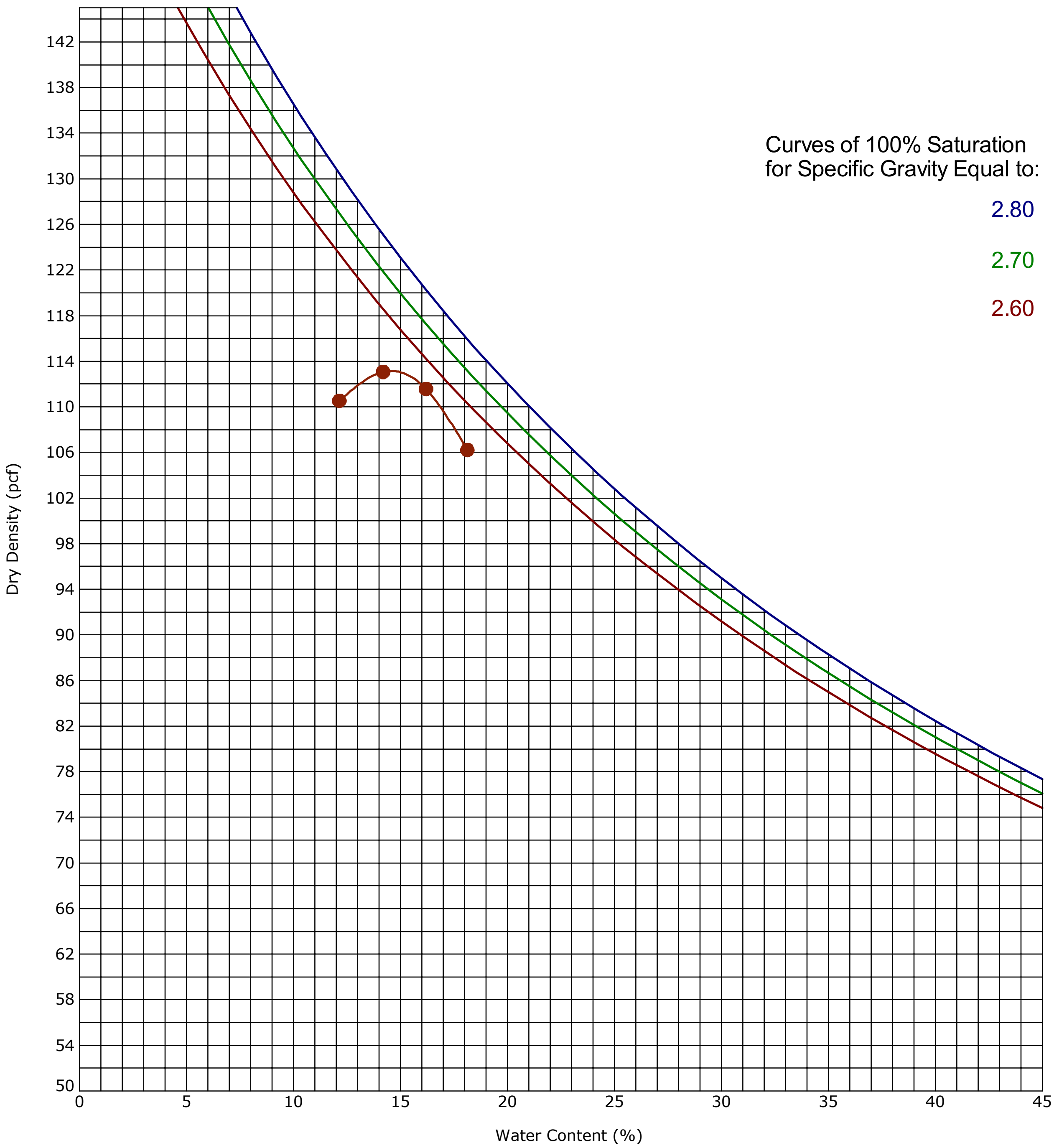
Boring ID	Depth (Ft)	Description of Materials
B-53	0 - 4	LEAN CLAY with SAND

Fines (%)	Fraction >19mm size (%)	LL	PL	PI	Test Method	Maximum Dry Density (pcf)	Optimum Water Content (%)
84	16	49	14	35	ASTM D1557 Method B	113.1	15.1

23041 Avenida De La Carlota
Ste 350
Laguna Hills, CA

Moisture-Density Relationship

ASTM D698/D1557



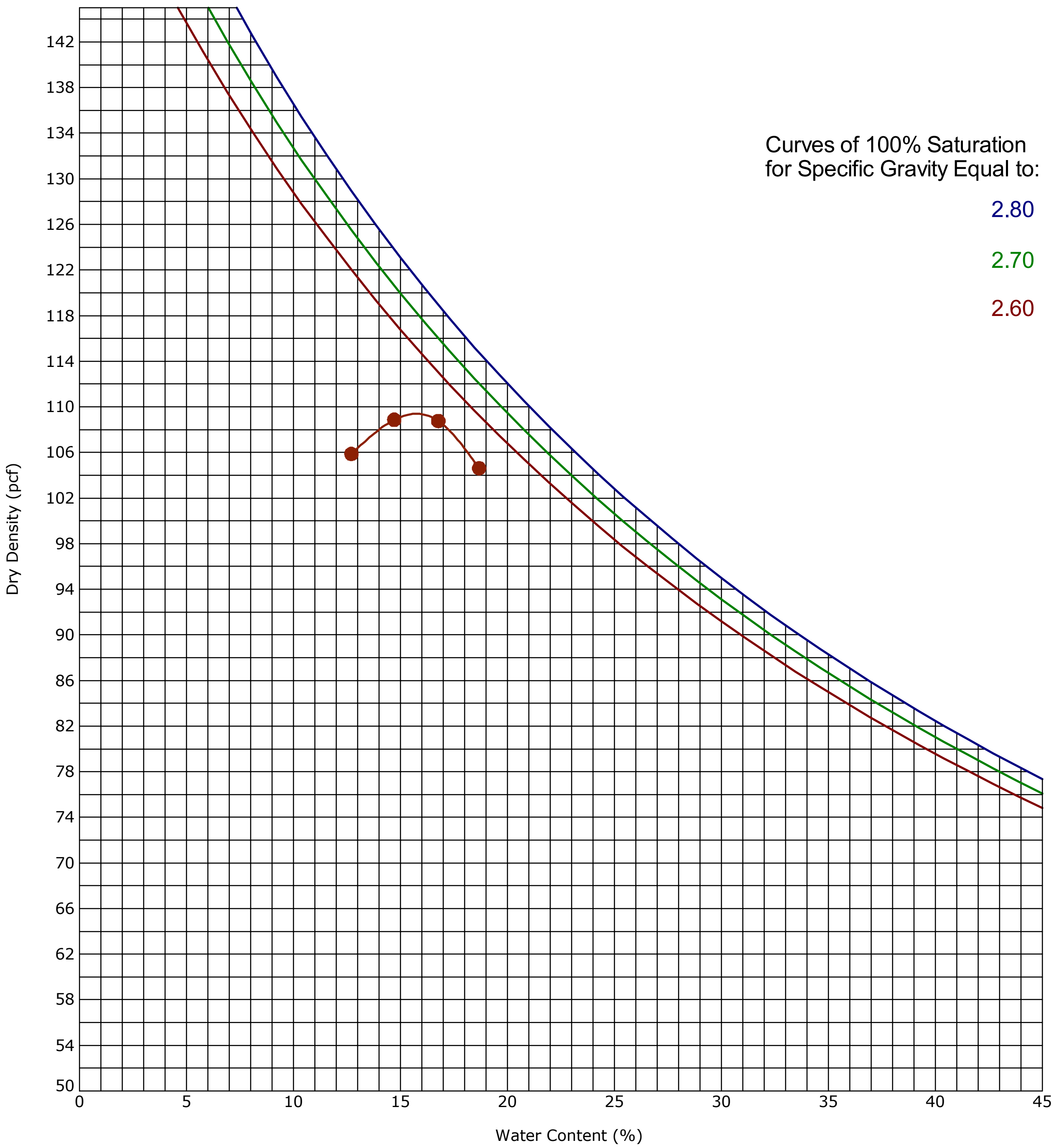
Boring ID	Depth (Ft)	Description of Materials
B-71	0 - 4	LEAN CLAY

Fines (%)	Fraction >19mm size (%)	LL	PL	PI	Test Method	Maximum Dry Density (pcf)	Optimum Water Content (%)
		39	14	25	ASTM D1557 Method A	113.2	14.6

23041 Avenida De La Carlota
Ste 350
Laguna Hills, CA

Moisture-Density Relationship

ASTM D698/D1557



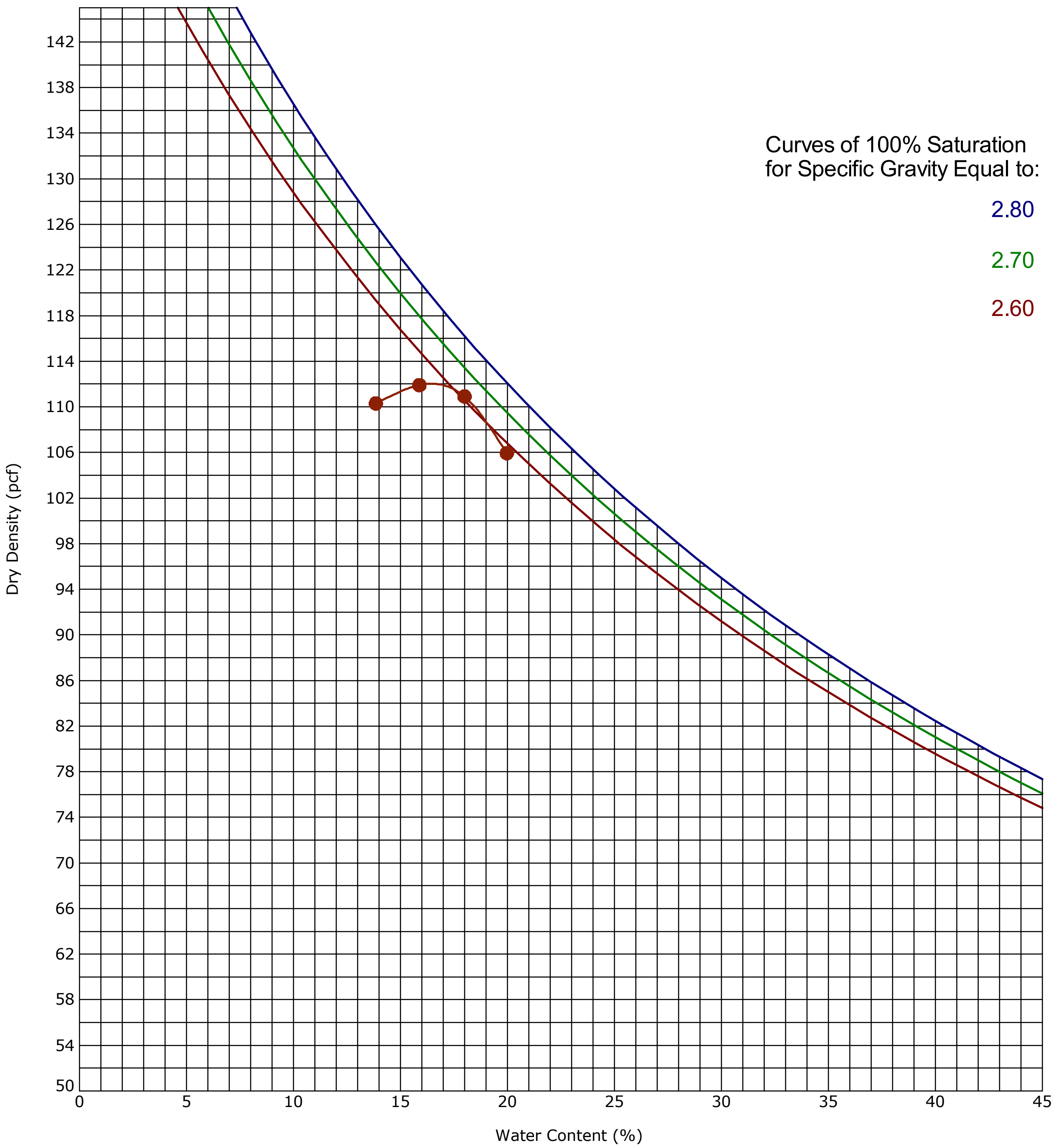
Boring ID	Depth (Ft)	Description of Materials
B-76	0 - 4	FAT CLAY

Fines (%)	Fraction >19mm size (%)	LL	PL	PI	Test Method	Maximum Dry Density (pcf)	Optimum Water Content (%)
					ASTM D1557 Method A	109.4	15.8

23041 Avenida De La Carlota
Ste 350
Laguna Hills, CA

Moisture-Density Relationship

ASTM D698/D1557



Boring ID	Depth (Ft)	Description of Materials
B-83	0 - 4	LEAN CLAY

Fines (%)	Fraction >19mm size (%)	LL	PL	PI	Test Method	Maximum Dry Density (pcf)	Optimum Water Content (%)
					ASTM D1557 Method A	112.0	16.4

LABORATORY COMPACTION CHARACTERISTICS OF SOIL REPORT

Report Number: 92091210.0405
Service Date: 08/22/23
Report Date: 09/06/23 Revision 1 -

Terracon
11555 Clay Rd, Ste 100
Houston, TX 77043-1239
713-690-8989 Reg No: F-3272

Client

Terracon Consultants, Inc.
Attn: Sean Barber
11555 Clay Road
Suite 100
Houston, TX 77043

Project

Houston In-House Quality Control
11555 Clay Rd Ste 100
Houston, TX 77043

Project Number: 92091210

Material Information

Source of Material: Darden Solar (60225172)
Proposed Use: Thermal Resistivity Testing

Sample Information

Sample Date:
Sampled By:
Sample Location: B-93

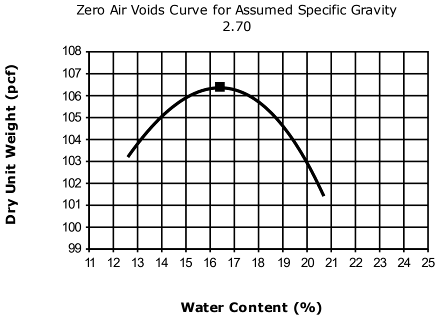
Sample Description: Brown Sandy Clay

Laboratory Test Data

Test Procedure: ASTM D1557
Test Method: Method A
Sample Preparation: Wet
Rammer Type: Mechanical
Maximum Dry Unit Weight (pcf): **106.4**
Optimum Water Content (%): **16.4**

	Result	Specifications
Liquid Limit:		
Plastic Limit:		
Plasticity Index:		
In-Place Moisture (%):		

USCS:



Comments:

Services: Obtain sample at project site in accordance with Terracon QMS Procedure 2.2-1 and return it to the laboratory. Prepare and test the sample in accordance with test methods referenced on this report.

Terracon Rep.:
Reported To:
Contractor:
Report Distribution:

Reviewed By:
Sean Barber
Project Manager

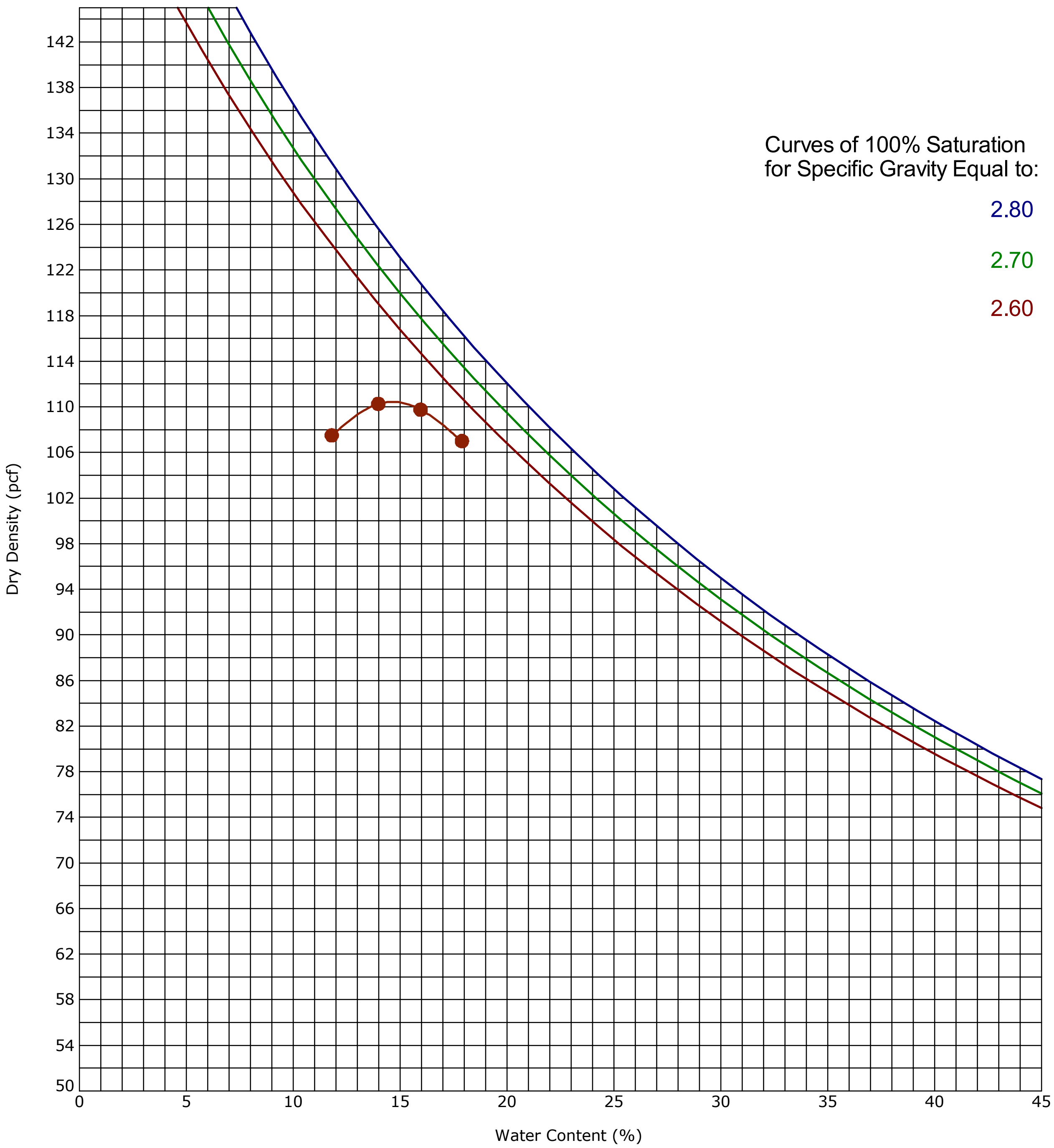
Test Methods: ASTM D1557

The tests were performed in general accordance with applicable ASTM, AASHTO, or DOT test methods. This report is exclusively for the use of the client indicated above and shall not be reproduced except in full without the written consent of our company. Test results transmitted herein are only applicable to the actual samples tested at the location(s) referenced and are not necessarily indicative of the properties of other apparently similar or identical materials.

23041 Avenida De La Carlota
Ste 350
Laguna Hills, CA

Moisture-Density Relationship

ASTM D698/D1557

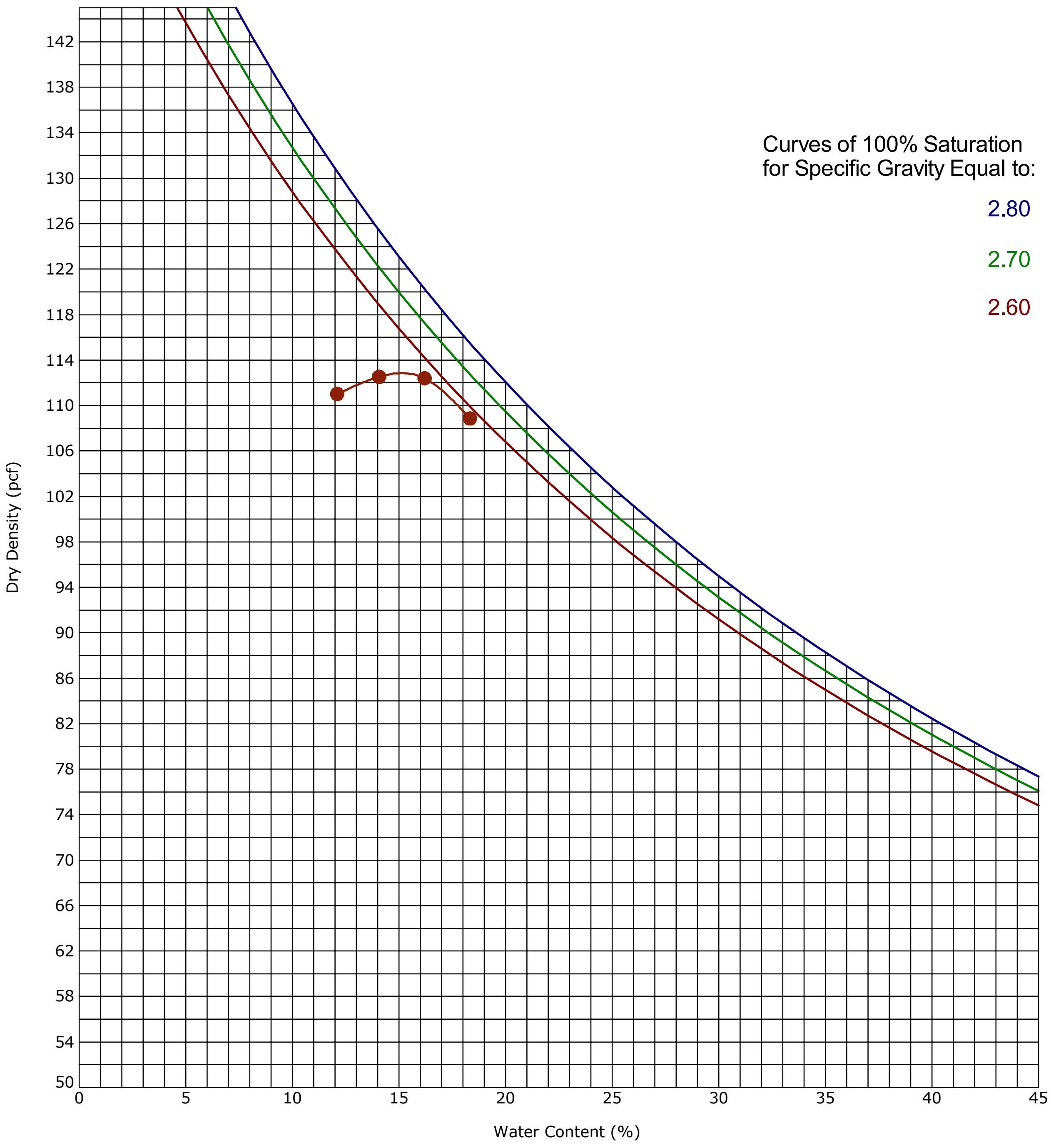


Boring ID	Depth (Ft)	Description of Materials
B-102	0 - 4	LEAN CLAY with SAND

Fines (%)	Fraction >19mm size (%)	LL	PL	PI	Test Method	Maximum Dry Density (pcf)	Optimum Water Content (%)
					ASTM D1557 Method A	110.4	14.6

Moisture-Density Relationship

ASTM D698/D1557



Boring ID	Depth (Ft)	Description of Materials
B-104	0 - 4	LEAN CLAY with SAND

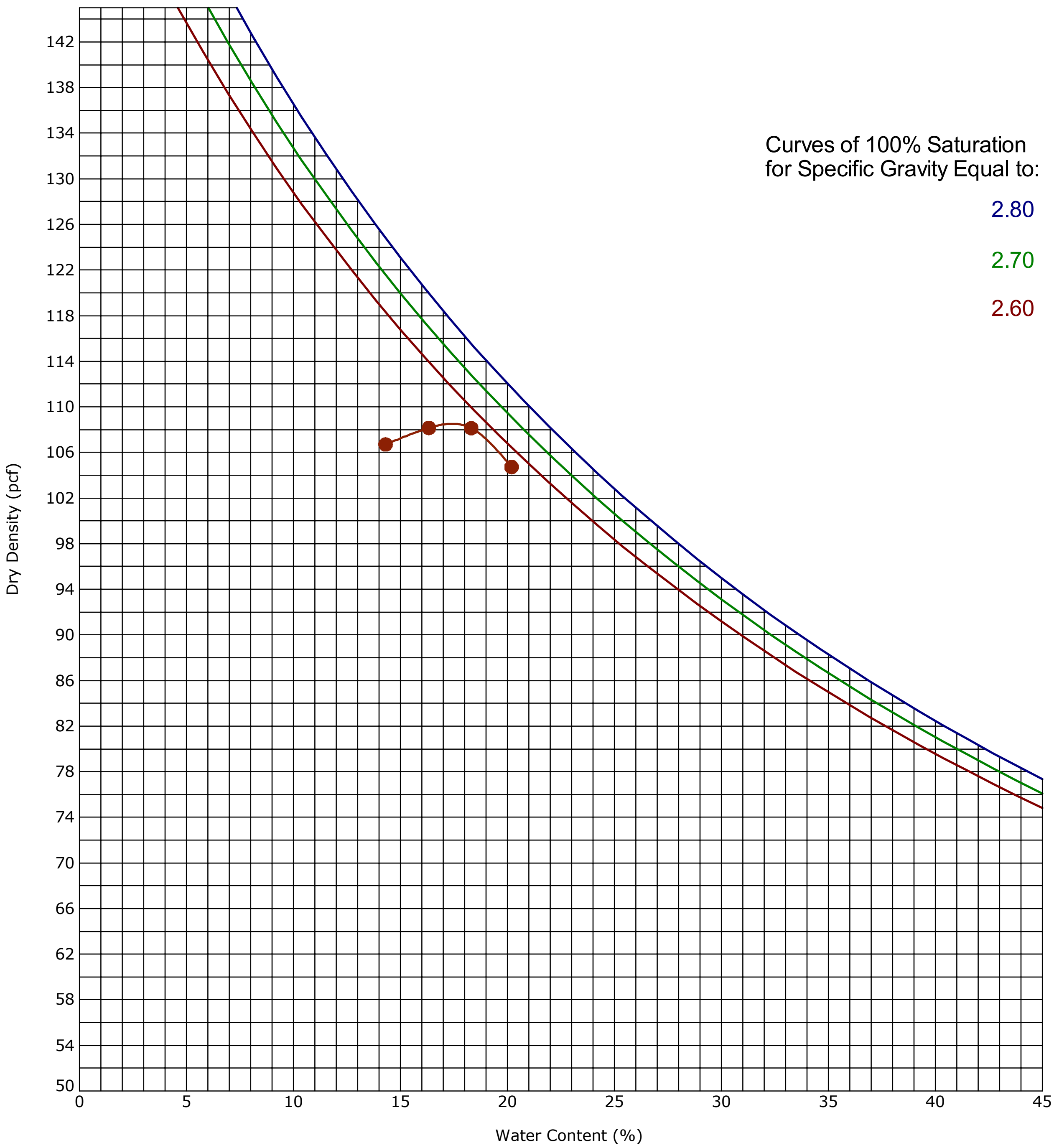
Fines (%)	Fraction >19mm size (%)	LL	PL	PI	Test Method	Maximum Dry Density (pcf)	Optimum Water Content (%)
81					ASTM D1557 Method A	112.8	15.2

Darden Solar
Cantua Creek | Fresno, CA
Terracon Project No. 60225172

23041 Avenida De La Carlota
Ste 350
Laguna Hills, CA

Moisture-Density Relationship

ASTM D698/D1557



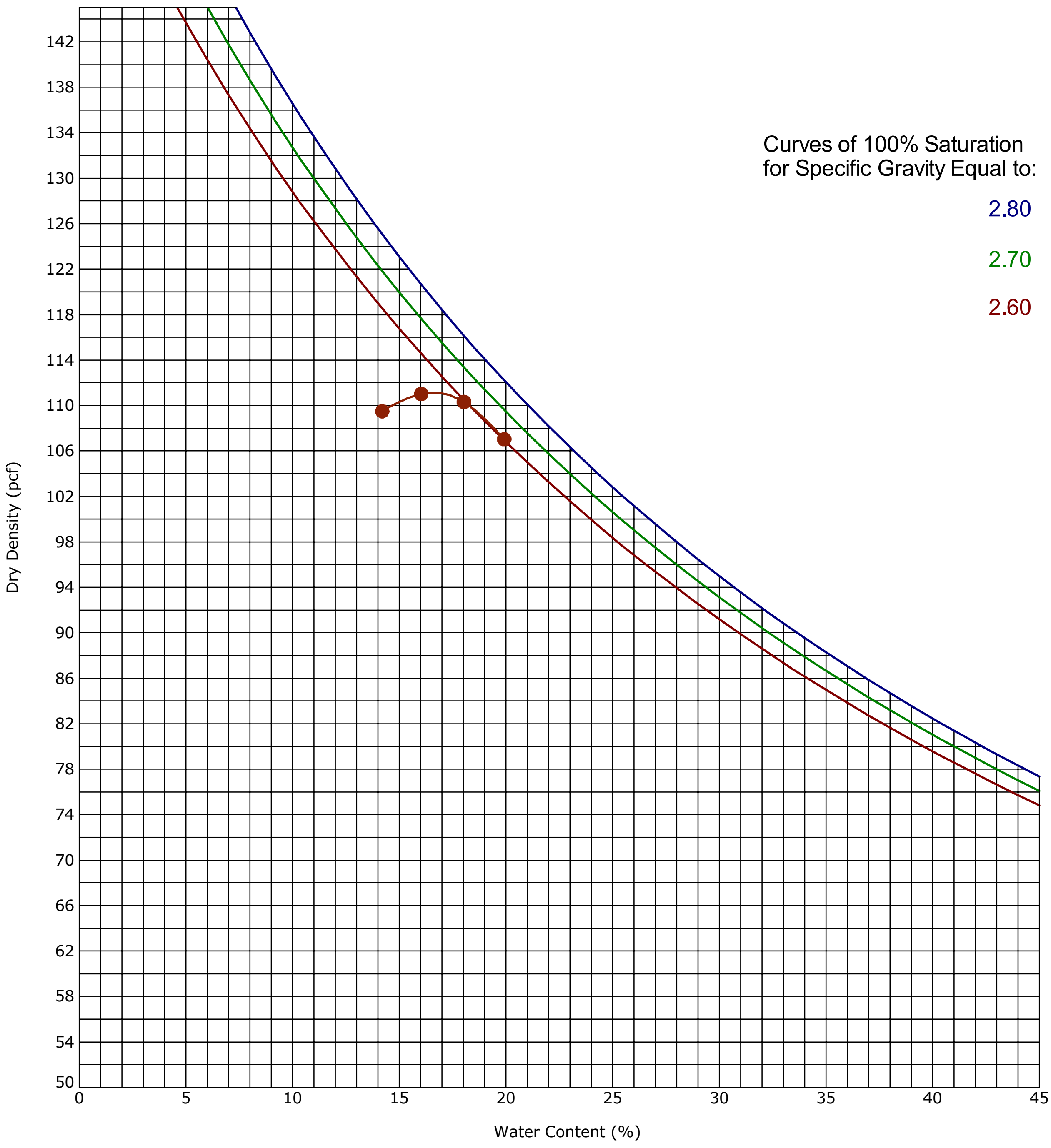
Boring ID	Depth (Ft)	Description of Materials
B-106	0 - 4	LEAN CLAY(CL)

Fines (%)	Fraction >19mm size (%)	LL	PL	PI	Test Method	Maximum Dry Density (pcf)	Optimum Water Content (%)
89		44	15	29	ASTM D1557 Method A	108.5	17.4

23041 Avenida De La Carlota
Ste 350
Laguna Hills, CA

Moisture-Density Relationship

ASTM D698/D1557



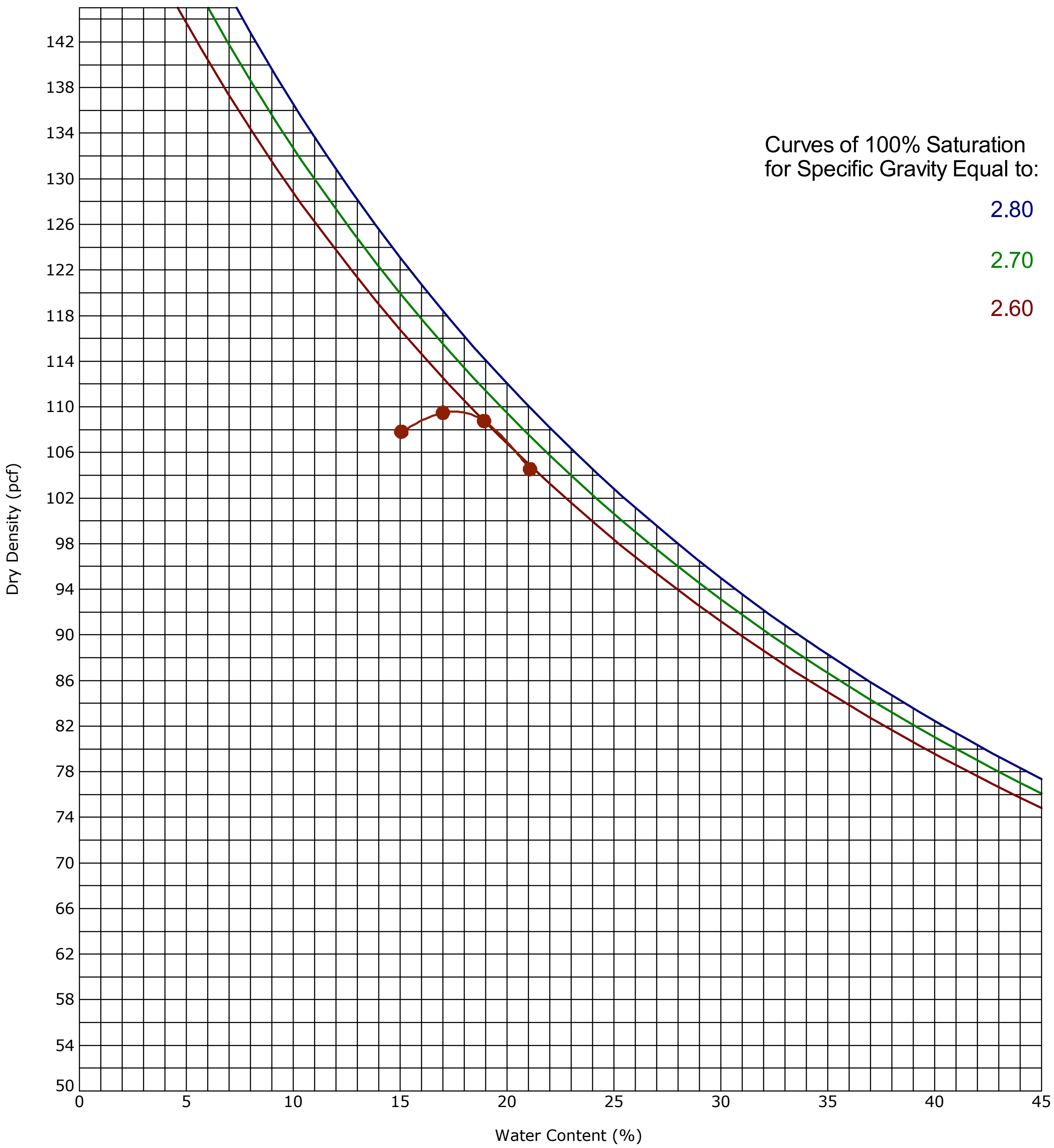
Boring ID	**Depth (Ft)**	**Description of Materials**
B-116	0 - 4	FAT CLAY

Fines (%)	**Fraction >19mm size (%)**	**LL**	**PL**	**PI**	**Test Method**	**Maximum Dry Density (pcf)**	**Optimum Water Content (%)**
					ASTM D1557 Method A	111.1	16.6

Terracon
23041 Avenida De La Carlota
Ste 350
Laguna Hills, CA

Moisture-Density Relationship

ASTM D698/D1557



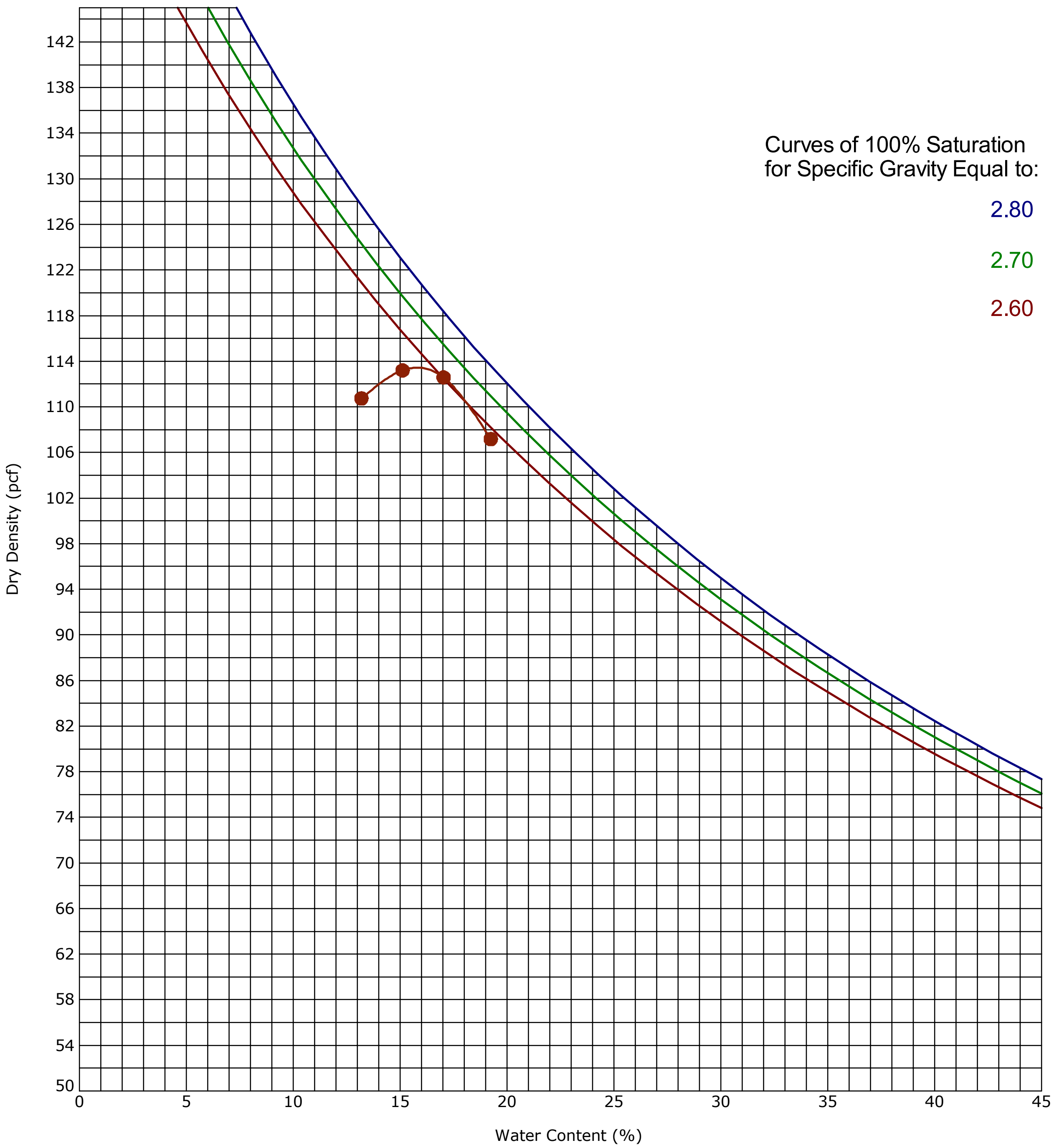
Boring ID	Depth (Ft)	Description of Materials
B-121	0 - 4	FAT CLAY

Fines (%)	Fraction >19mm size (%)	LL	PL	PI	Test Method	Maximum Dry Density (pcf)	Optimum Water Content (%)
		65	20	45	ASTM D1557 Method A	109.6	17.5

23041 Avenida De La Carlota
Ste 350
Laguna Hills, CA

Moisture-Density Relationship

ASTM D698/D1557



Boring ID	Depth (Ft)	Description of Materials
B-127	0 - 4	SANDY LEAN CLAY

Fines (%)	Fraction >19mm size (%)	LL	PL	PI	Test Method	Maximum Dry Density (pcf)	Optimum Water Content (%)
					ASTM D1557 Method A	113.4	15.8

LABORATORY COMPACTION CHARACTERISTICS OF SOIL REPORT

Report Number: 92091210.0407
Service Date: 08/22/23
Report Date: 09/06/23 Revision 1 -

Terracon
11555 Clay Rd, Ste 100
Houston, TX 77043-1239
713-690-8989 Reg No: F-3272

Client

Terracon Consultants, Inc.
Attn: Sean Barber
11555 Clay Road
Suite 100
Houston, TX 77043

Project

Houston In-House Quality Control
11555 Clay Rd Ste 100
Houston, TX 77043

Project Number: 92091210

Material Information

Source of Material: Darden Solar (60225172)
Proposed Use: Thermal Resistivity Testing

Sample Information

Sample Date:
Sampled By:
Sample Location: B-130

Sample Description: Brown Sandy Clay

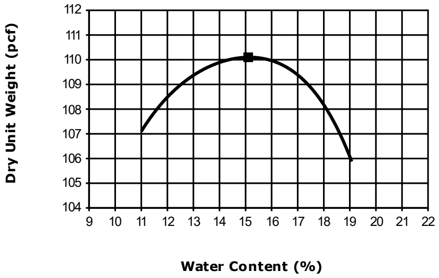
Laboratory Test Data

Test Procedure: ASTM D1557
Test Method: Method A
Sample Preparation: Wet
Rammer Type: Mechanical
Maximum Dry Unit Weight (pcf): **110.1**
Optimum Water Content (%): **15.1**

	Result	Specifications
Liquid Limit:		
Plastic Limit:		
Plasticity Index:		
In-Place Moisture (%):		

USCS: CL

Zero Air Voids Curve for Assumed Specific Gravity
2.70



Comments:

Services: Obtain sample at project site in accordance with Terracon QMS Procedure 2.2-1 and return it to the laboratory. Prepare and test the sample in accordance with test methods referenced on this report.

Terracon Rep.: **
Reported To:
Contractor:
Report Distribution:

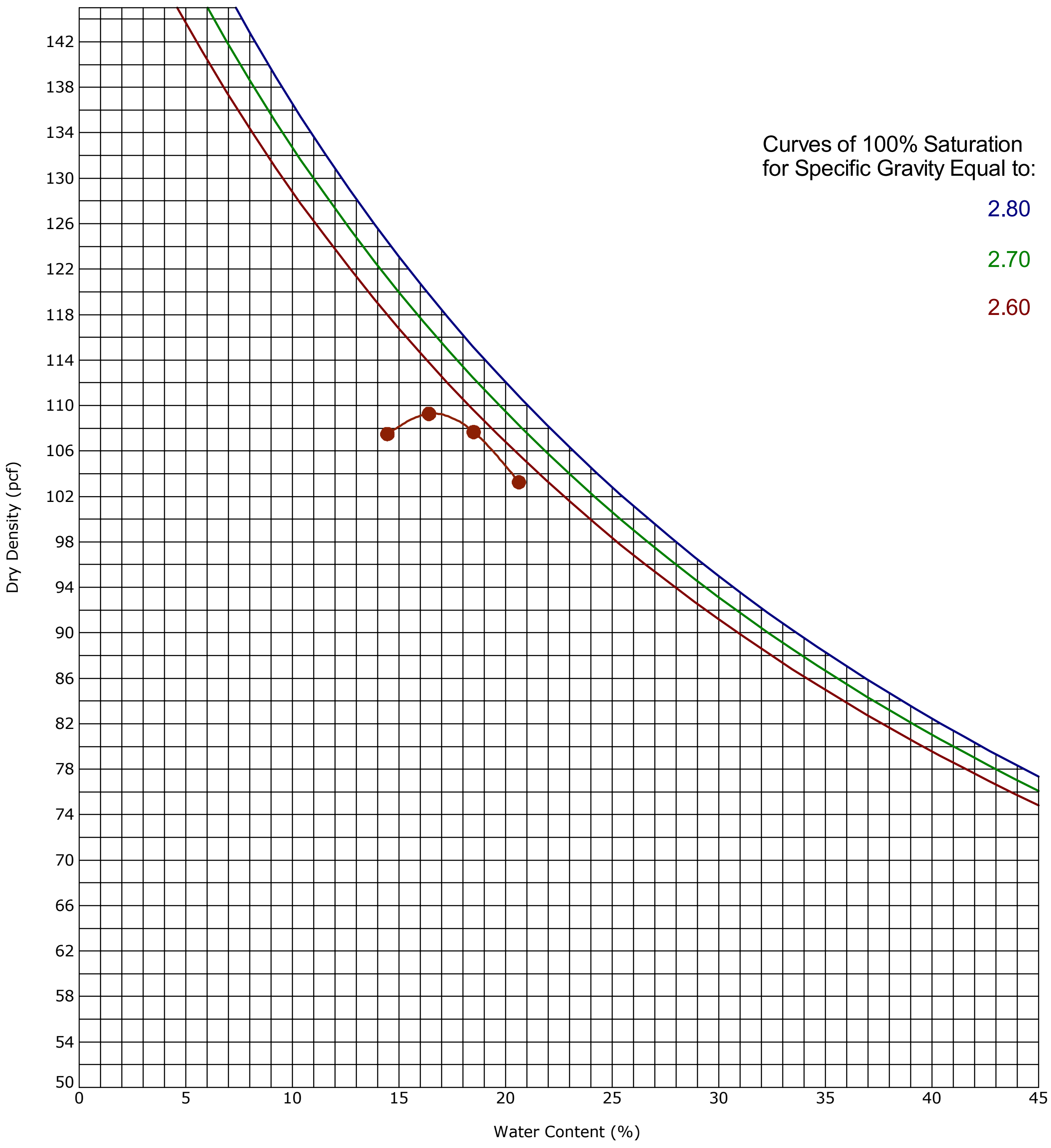
Reviewed By: Sean Barber
Sean Barber
Project Manager

Test Methods: ASTM D1557

Terracon
23041 Avenida De La Carlota
Ste 350
Laguna Hills, CA

Moisture-Density Relationship

ASTM D698/D1557



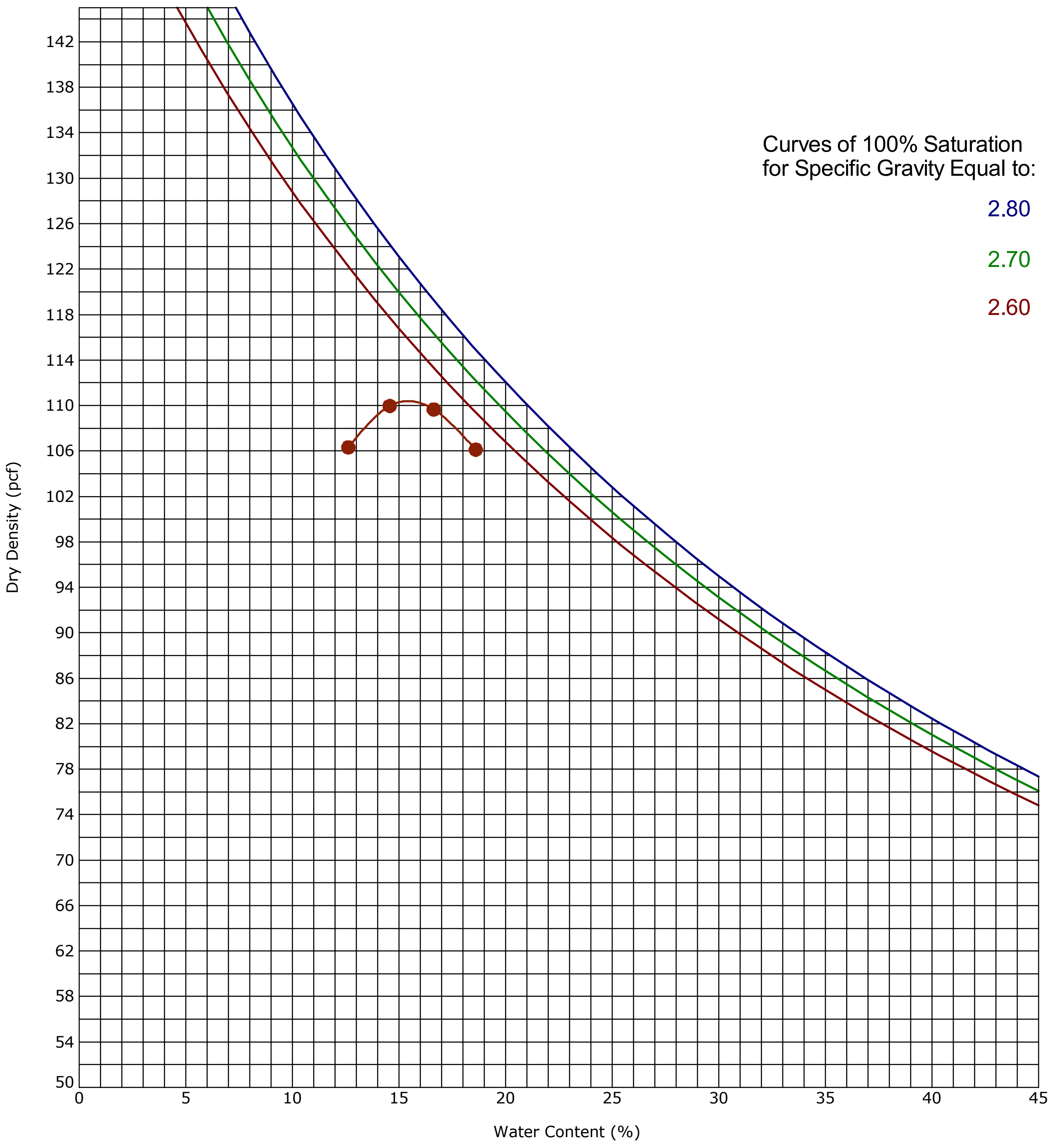
Boring ID	Depth (Ft)	Description of Materials
B-132	0 - 4	LEAN CLAY WITH SAND

Fines (%)	Fraction >19mm size (%)	LL	PL	PI	Test Method	Maximum Dry Density (pcf)	Optimum Water Content (%)
87					ASTM D1557 Method A	109.3	16.6

23041 Avenida De La Carlota
Ste 350
Laguna Hills, CA

Moisture-Density Relationship

ASTM D698/D1557



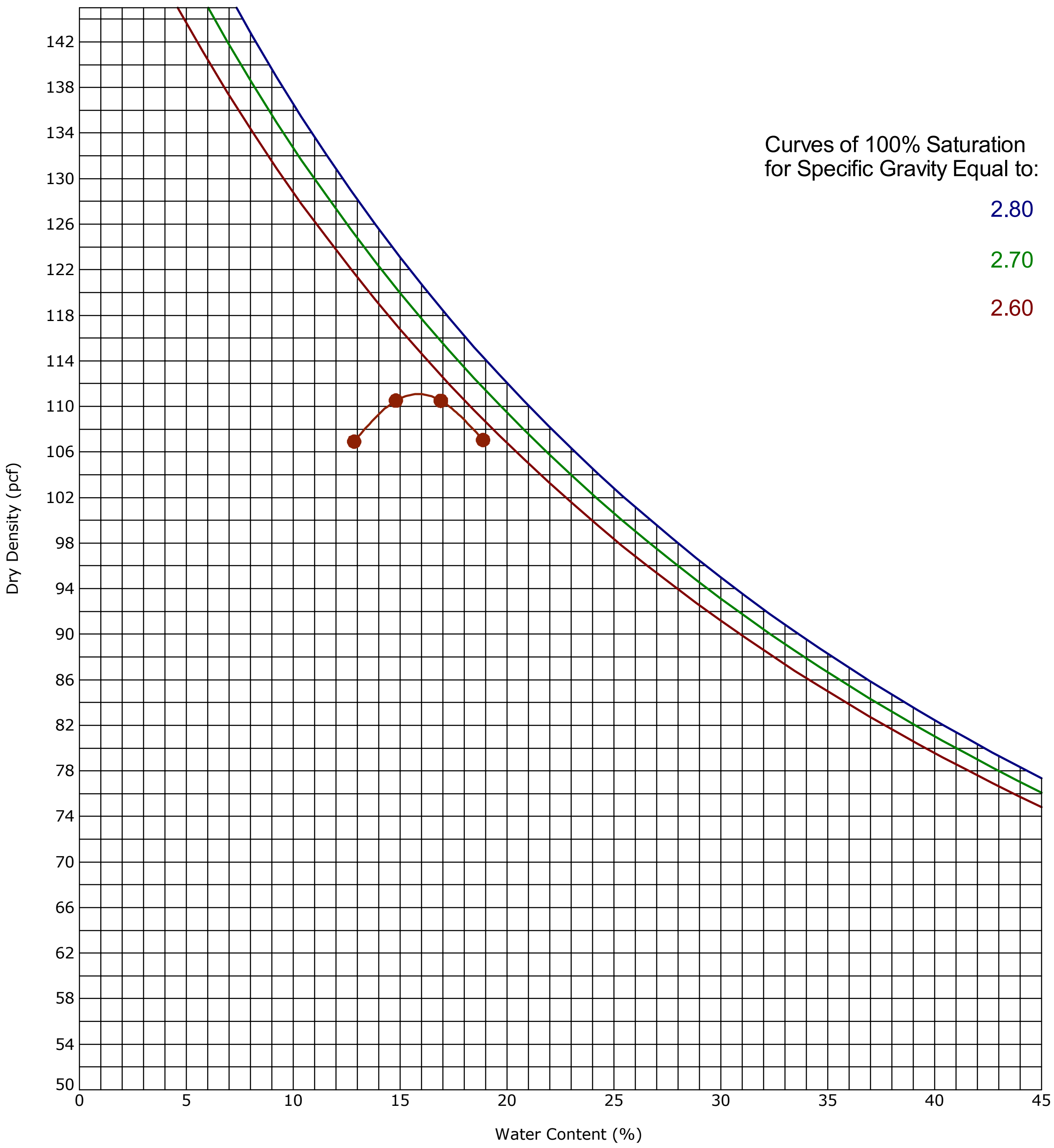
Boring ID	Depth (Ft)	Description of Materials
B-133	0 - 4	SANDY LEAN CLAY

Fines (%)	Fraction >19mm size (%)	LL	PL	PI	Test Method	Maximum Dry Density (pcf)	Optimum Water Content (%)
					ASTM D1557 Method C	110.4	15.4

23041 Avenida De La Carlota
Ste 350
Laguna Hills, CA

Moisture-Density Relationship

ASTM D698/D1557

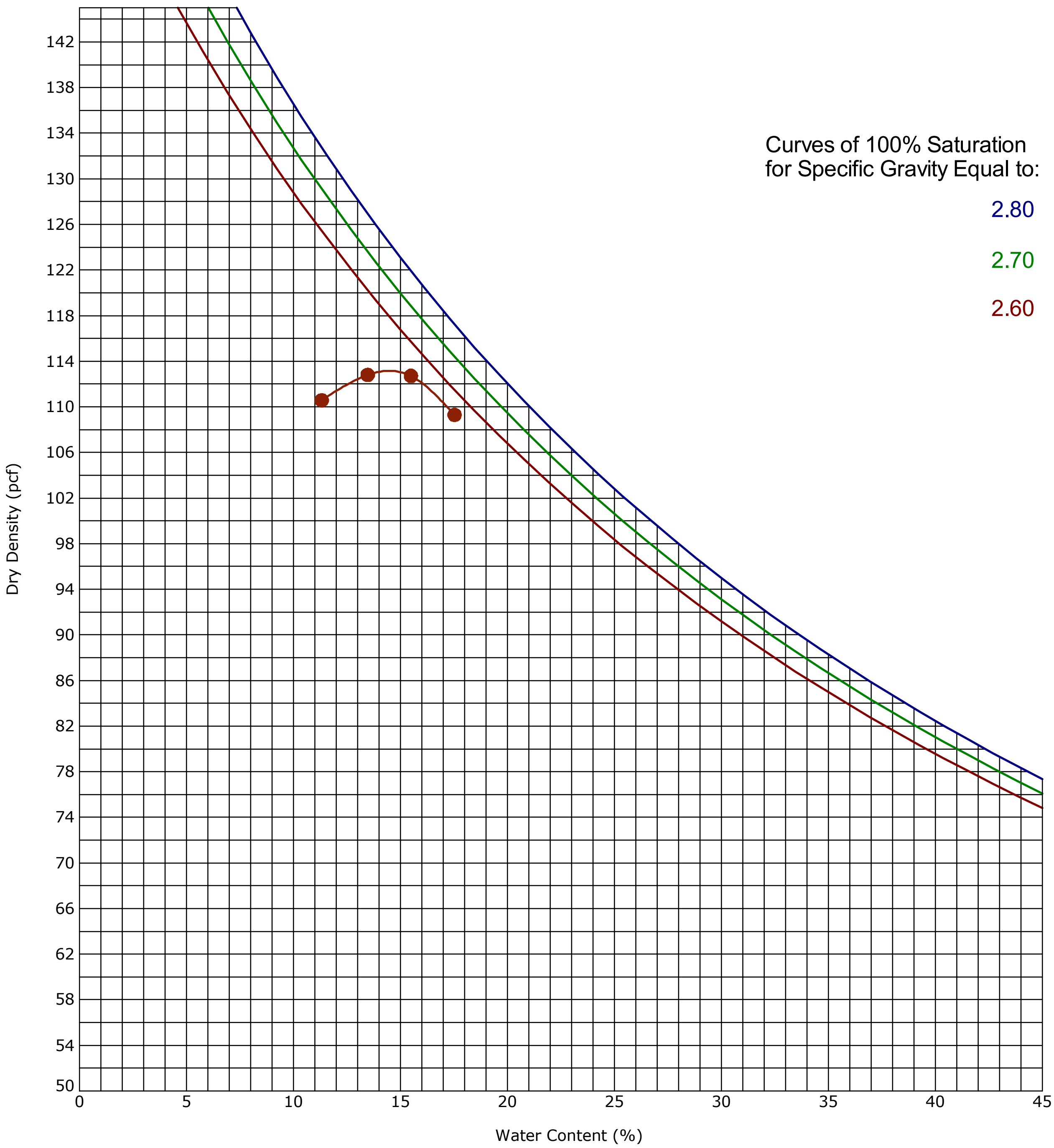


Boring ID	Depth (Ft)	Description of Materials
SUB-1	0 - 4	LEAN CLAY with SAND

Fines (%)	Fraction >19mm size (%)	LL	PL	PI	Test Method	Maximum Dry Density (pcf)	Optimum Water Content (%)
79		48	22	26	ASTM D1557 Method A	111.1	15.8

Moisture-Density Relationship

ASTM D698/D1557



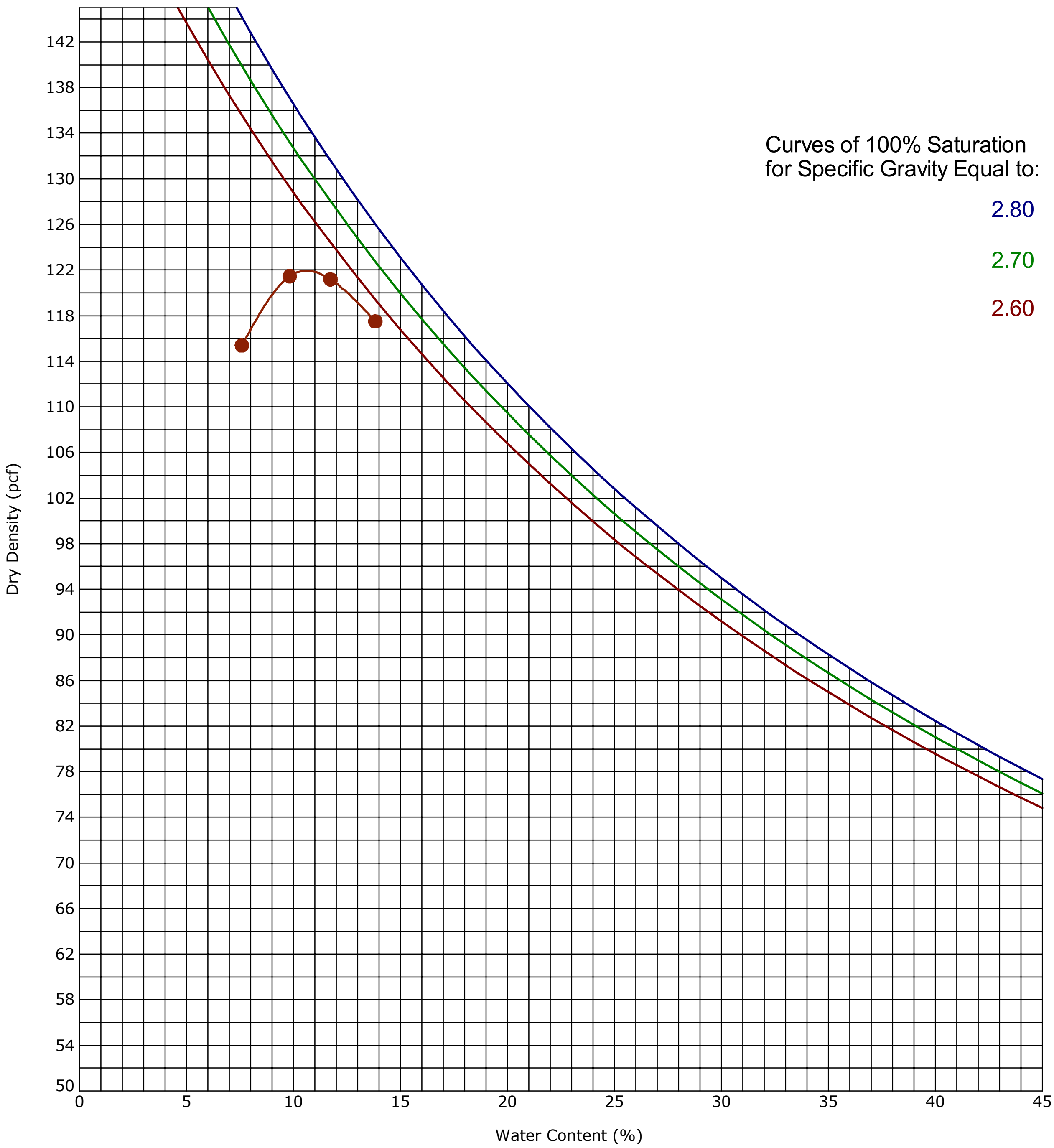
Boring ID	Depth (Ft)	Description of Materials
BESS-1	0 - 4	SANDY LEAN CLAY

Fines (%)	Fraction >19mm size (%)	LL	PL	PI	Test Method	Maximum Dry Density (pcf)	Optimum Water Content (%)
67					ASTM D1557 Method A	113.2	14.5

23041 Avenida De La Carlota
Ste 350
Laguna Hills, CA

Moisture-Density Relationship

ASTM D698/D1557



Boring ID	Depth (Ft)	Description of Materials
SUB-2	0 - 4	CLAYEY SAND

Fines (%)	Fraction >19mm size (%)	LL	PL	PI	Test Method	Maximum Dry Density (pcf)	Optimum Water Content (%)
42	58	32	17	15	ASTM D1557 Method D	121.9	10.6

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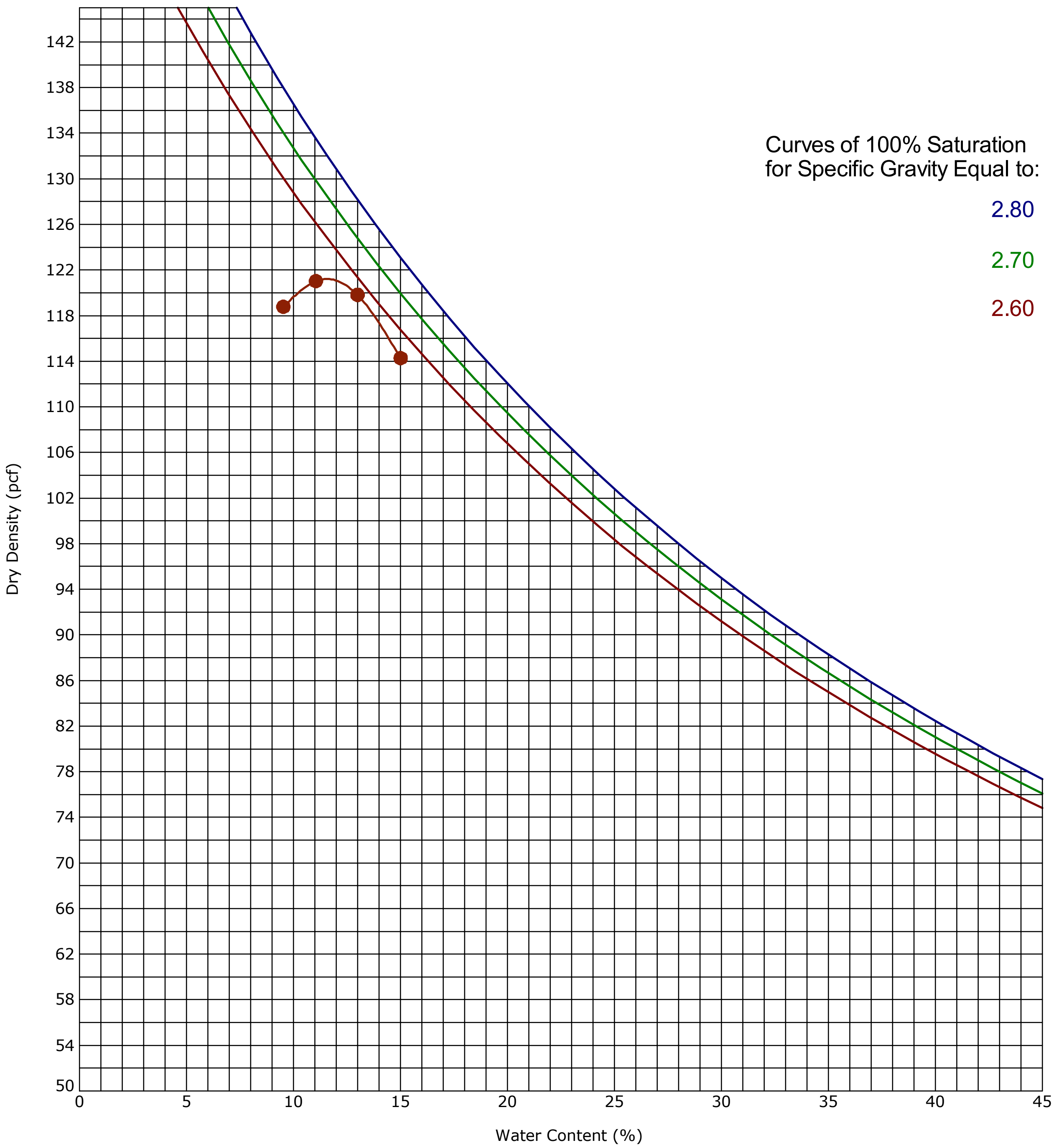
Moisture-Density Relationship

ASTM D698/D1557



Boring ID	Depth (Ft)	Description of Materials
SW-1	0 - 4	CLAYEY SAND

Fines (%)	Fraction >19mm size (%)	LL	PL	PI	Test Method	Maximum Dry Density (pcf)	Optimum Water Content (%)
26	74	30	20	10	ASTM D1557 Method D	121.2	11.6

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IP Darden I LLC

Project
Darden Solar

Sample Submitted By: Terracon (60)   **Date Received:** 3/13/2023   **Lab No.: 23-0159**

Results of Corrosion Analysis

Sample Number	--	--	--	--
Sample Location	B-2	B-7	B-9	B-22
Sample Depth (ft.)	4.0-6.0	4.0-6.0	4.0-6.0	4.0-6.0
pH Analysis, ASTM G51	8.02	8.35	8.10	8.18
Water Soluble Sulfate (SO4), ASTM C 15806 (Percent %)	0.09	0.16	1.81	0.42
Sulfides, AWWA 4500-S D, (mg/Kg)	Nil	Nil	Nil	Nil
Chlorides, ASTM D512, (mg/kg)	53	255	800	420
Red-Ox, ASTM G200, (mV)	+720	+694	+683	+676
Total Salts, AWWA 2540, (mg/Kg)	1411	4205	24528	8831
Saturated Minimum Resistivity, ASTM G-187, (ohm-cm)	281	408	107	261

Analyzed By N. Campo
Nathan Campo
Engineering Technician II

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IP Darden I LLC

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Sample Submitted By: Terracon (60)   **Date Received:** 6/12/2023   **Lab No.: 23-0343**

Results of Corrosion Analysis

Sample Number	--	--	--	--
Sample Location	B-4	B-5	B-6	B-8
Sample Depth (ft.)	4.0-6.0	4.0-6.0	4.0-6.0	4.0-6.0
pH Analysis, ASTM G51	8.21	8.61	8.45	8.51
Water Soluble Sulfate (SO4), ASTM C 1580 (Percent %)	0.01	0.08	0.02	<0.01
Sulfides, AWWA 4500-S D, (mg/Kg)	Nil	Nil	Nil	Nil
Chlorides, ASTM D512, (mg/kg)	75	95	55	55
Red-Ox, ASTM G200, (mV)	+720	+705	+720	+728
Total Salts, AWWA 2540, (mg/Kg)	1349	3214	1338	683
Saturated Minimum Resistivity, ASTM G-187, (ohm-cm)	301	308	348	469

Analyzed By N. Campo
Nathan Campo
Engineering Technician III

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Darden Solar

Sample Submitted By: Terracon (60) **Date Received:** 8/10/2023 **Lab No.: 23-0450**

Results of Corrosion Analysis

Sample Number	--	--	--	--
Sample Location	B-11	B-14	B-15	B-16
Sample Depth (ft.)	4.0-6.0	4.0-6.0	4.0-6.0	4.0-6.0
pH Analysis, ASTM G51	8.77	8.27	8.38	8.55
Water Soluble Sulfate (SO4), ASTM C 15806 (Percent %)	0.02	0.08	0.03	0.14
Sulfides, AWWA 4500-S D, (mg/Kg)	Nil	Nil	Nil	Nil
Chlorides, ASTM D512, (mg/kg)	325	527	80	267
Red-Ox, ASTM G200, (mV)	+722	+705	+714	+692
Total Salts, AWWA 2520 B, (mg/Kg)	1075	3287	1887	4345
Saturated Minimum Resistivity, ASTM G-187, (ohm-cm)	214	187	154	174

N. Campo

Analyzed By__________________________
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Engineering Technician III

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Sample Submitted By: Terracon (60)   **Date Received:** 8/10/2023   **Lab No.: 23-0450**

Results of Corrosion Analysis

Sample Number	--	--	--	--
Sample Location	B-18	B-19	B-31	B-32
Sample Depth (ft.)	4.0-6.0	4.0-6.0	4.0-6.0	4.0-6.0
pH Analysis, ASTM G51	9.18	8.28	8.76	8.04
Water Soluble Sulfate (SO4), ASTM C 15806 (Percent %)	0.01	0.04	0.04	0.16
Sulfides, AWWA 4500-S D, (mg/Kg)	Nil	Nil	Nil	Nil
Chlorides, ASTM D512, (mg/kg)	172	102	65	130
Red-Ox, ASTM G200, (mV)	+715	+712	+718	+693
Total Salts, AWWA 2520 B, (mg/Kg)	1674	2587	1668	4513
Saturated Minimum Resistivity, ASTM G-187, (ohm-cm)	288	194	247	314

Analyzed By N. Campo
Nathan Campo
Engineering Technician III

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Sample Submitted By: Terracon (60) **Date Received:** 6/12/2023 **Lab No.: 23-0343**

Results of Corrosion Analysis

Sample Number	--	--	--	--
Sample Location	B-10	B-25	B-26	B-27
Sample Depth (ft.)	5.0-6.5	5.0-6.5	4.0-6.0	4.0-6.0
pH Analysis, ASTM G51	8.79	8.22	8.27	8.36
Water Soluble Sulfate (SO4), ASTM C 1580 (Percent %)	<0.01	0.17	0.01	0.07
Sulfides, AWWA 4500-S D, (mg/Kg)	Nil	Nil	Nil	Nil
Chlorides, ASTM D512, (mg/kg)	57	152	72	320
Red-Ox, ASTM G200, (mV)	+721	+691	+72	+694
Total Salts, AWWA 2540, (mg/Kg)	1048	5392	1864	4306
Saturated Minimum Resistivity, ASTM G-187, (ohm-cm)	415	100	207	288

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Sample Submitted By: Terracon (60)   **Date Received:** 3/13/2023   **Lab No.: 23-0159**

Results of Corrosion Analysis

Sample Number	--	--	--	--
Sample Location	B-24	B-28	B-37	B-57
Sample Depth (ft.)	4.0-6.0	4.0-6.0	4.0-6.0	4.0-6.0
pH Analysis, ASTM G51	8.27	8.21	7.84	7.95
Water Soluble Sulfate (SO4), ASTM C 15806 (Percent %)	1.84	1.83	0.41	1.37
Sulfides, AWWA 4500-S D, (mg/Kg)	Nil	Nil	Nil	Nil
Chlorides, ASTM D512, (mg/kg)	927	667	170	162
Red-Ox, ASTM G200, (mV)	+671	+675	+688	+685
Total Salts, AWWA 2540, (mg/Kg)	28336	25704	7655	19096
Saturated Minimum Resistivity, ASTM G-187, (ohm-cm)	127	134	328	174

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Analyzed By
Nathan Campo
Engineering Technician II

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Sample Submitted By: Terracon (60) **Date Received:** 8/10/2023 **Lab No.: 23-0450**

Results of Corrosion Analysis

Sample Number	--	--	--
Sample Location	B-33	B-51	B-53
Sample Depth (ft.)	4.0-6.0	4.0-6.0	4.0-6.0
pH Analysis, ASTM G51	8.92	8.52	8.58
Water Soluble Sulfate (SO4), ASTM C 15806 (Percent %)	<0.01	0.03	0.04
Sulfides, AWWA 4500-S D, (mg/Kg)	Nil	Nil	Nil
Chlorides, ASTM D512, (mg/kg)	205	182	155
Red-Ox, ASTM G200, (mV)	+714	+712	+710
Total Salts, AWWA 2520 B, (mg/Kg)	1808	2682	2784
Saturated Minimum Resistivity, ASTM G-187, (ohm-cm)	328	174	254

N. Campo

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Sample Submitted By: Terracon (60) **Date Received:** 6/12/2023 **Lab No.: 23-0343**

Results of Corrosion Analysis

Sample Number	--	--	--	--
Sample Location	B-42	B-43	B-44	B-45
Sample Depth (ft.)	5.0-6.5	4.0-6.0	4.0-6.0	4.0-6.0
pH Analysis, ASTM G51	8.17	8.40	8.08	8.08
Water Soluble Sulfate (SO4), ASTM C 1580 (Percent %)	0.04	0.24	0.02	0.03
Sulfides, AWWA 4500-S D, (mg/Kg)	Nil	Nil	Nil	Nil
Chlorides, ASTM D512, (mg/kg)	300	147	452	55
Red-Ox, ASTM G200, (mV)	+714	+704	+720	+715
Total Salts, AWWA 2540, (mg/Kg)	2452	3326	1355	1736
Saturated Minimum Resistivity, ASTM G-187, (ohm-cm)	140	174	268	361

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Results of Corrosion Analysis

Sample Number	--	--	--	--
Sample Location	B-38	B-60	B-61	B-63
Sample Depth (ft.)	4.0-6.0	4.0-6.0	4.0-6.0	4.0-6.0
pH Analysis, ASTM G51	8.14	8.53	8.36	8.48
Water Soluble Sulfate (SO4), ASTM C 15806 (Percent %)	<0.01	0.13	0.40	0.21
Sulfides, AWWA 4500-S D, (mg/Kg)	Nil	Nil	Nil	Nil
Chlorides, ASTM D512, (mg/kg)	520	187	350	247
Red-Ox, ASTM G200, (mV)	+688	+697	+688	+693
Total Salts, AWWA 2540, (mg/Kg)	7352	3908	8148	4704
Saturated Minimum Resistivity, ASTM G-187, (ohm-cm)	234	335	268	335

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Results of Corrosion Analysis

Sample Number	--	--	--	--
Sample Location	B-46	B-47	B-48	B-49
Sample Depth (ft.)	5.0-6.5	4.0-6.0	4.0-6.0	5.0-6.5
pH Analysis, ASTM G51	8.41	8.25	7.92	8.31
Water Soluble Sulfate (SO4), ASTM C 1580 (Percent %)	0.11	0.02	0.09	0.07
Sulfides, AWWA 4500-S D, (mg/Kg)	Nil	Nil	Nil	Nil
Chlorides, ASTM D512, (mg/kg)	77	75	70	572
Red-Ox, ASTM G200, (mV)	+714	+722	+707	+712
Total Salts, AWWA 2540, (mg/Kg)	2021	1084	2900	2704
Saturated Minimum Resistivity, ASTM G-187, (ohm-cm)	207	167	214	180

Analyzed By N. Campo
Nathan Campo
Engineering Technician III

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Results of Corrosion Analysis

Sample Number	--	--	--	--
Sample Location	B-56	B-58	B-62	B-66
Sample Depth (ft.)	4.0-6.0	4.0-6.0	4.0-6.0	5.0
pH Analysis, ASTM G51	8.36	8.61	9.28	8.42
Water Soluble Sulfate (SO4), ASTM C 1580 (Percent %)	0.01	0.08	0.01	0.04
Sulfides, AWWA 4500-S D, (mg/Kg)	Nil	Nil	Nil	Nil
Chlorides, ASTM D512, (mg/kg)	225	75	100	110
Red-Ox, ASTM G200, (mV)	+716	+712	+719	+712
Total Salts, AWWA 2540, (mg/Kg)	1674	2716	1472	2587
Saturated Minimum Resistivity, ASTM G-187, (ohm-cm)	335	194	261	221

N. Campo

Analyzed By
Nathan Campo
Engineering Technician III

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Sample Submitted By: Terracon (60) **Date Received:** 3/21/2023 **Lab No.: 23-0165**

Results of Corrosion Analysis

Sample Number	--
Sample Location	B-64
Sample Depth (ft.)	4.0-6.0
pH Analysis, ASTM G51	8.23
Water Soluble Sulfate (SO4), ASTM C 15806 (Percent %)	0.68
Sulfides, AWWA 4500-S D, (mg/Kg)	Nil
Chlorides, ASTM D512, (mg/kg)	332
Red-Ox, ASTM G200, (mV)	+675
Total Salts, AWWA 2540, (mg/Kg)	11110
Saturated Minimum Resistivity, ASTM G-187, (ohm-cm)	184

Analyzed By N. Campo
Nathan Campo
Engineering Technician II

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Terracon

Client
IP Darden I LLC

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Sample Submitted By: Terracon (60)   **Date Received:** 6/12/2023   **Lab No.: 23-0343**

Results of Corrosion Analysis

Sample Number	--	--	--	--
Sample Location	B-67	B-69	B-71	B-72
Sample Depth (ft.)	4.0-6.0	4.0-6.0	4.0-6.0	4.0-6.0
pH Analysis, ASTM G51	8.57	8.64	8.39	8.60
Water Soluble Sulfate (SO4), ASTM C 1580 (Percent %)	<0.01	<0.01	0.06	0.04
Sulfides, AWWA 4500-S D, (mg/Kg)	Nil	Nil	Nil	Nil
Chlorides, ASTM D512, (mg/kg)	197	52	225	115
Red-Ox, ASTM G200, (mV)	+720	+729	+705	+715
Total Salts, AWWA 2540, (mg/Kg)	1366	515	3270	2240
Saturated Minimum Resistivity, ASTM G-187, (ohm-cm)	2144	804	201	231

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Analyzed By ______________________
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Engineering Technician III

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Sample Submitted By: Terracon (60) **Date Received:** 3/13/2023 **Lab No.: 23-0159**

Results of Corrosion Analysis

Sample Number	--	--	--	--
Sample Location	B-70	B-80	B-82	B-85
Sample Depth (ft.)	4.0-6.0	4.0-6.0	4.0-6.0	4.0-6.0
pH Analysis, ASTM G51	8.19	8.19	8.42	8.60
Water Soluble Sulfate (SO4), ASTM C 15806 (Percent %)	1.87	1.29	0.09	0.04
Sulfides, AWWA 4500-S D, (mg/Kg)	Nil	Nil	Nil	Nil
Chlorides, ASTM D512, (mg/kg)	217	247	80	100
Red-Ox, ASTM G200, (mV)	+676	+685	+705	+720
Total Salts, AWWA 2540, (mg/Kg)	24360	19712	3175	1293
Saturated Minimum Resistivity, ASTM G-187, (ohm-cm)	134	180	556	247

Analyzed By N. Campo
Nathan Campo
Engineering Technician II

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Sample Submitted By: Terracon (60) **Date Received:** 6/12/2023 **Lab No.: 23-0343**

Results of Corrosion Analysis

Sample Number	--	--	--	--
Sample Location	B-73	B-74	B-75	B-76
Sample Depth (ft.)	4.0-6.0	4.0-6.0	4.0-6.0	4.0-6.0
pH Analysis, ASTM G51	8.80	8.27	8.42	8.47
Water Soluble Sulfate (SO4), ASTM C 1580 (Percent %)	0.06	0.11	0.23	0.07
Sulfides, AWWA 4500-S D, (mg/Kg)	Nil	Nil	Nil	Nil
Chlorides, ASTM D512, (mg/kg)	307	72	157	540
Red-Ox, ASTM G200, (mV)	+714	+700	+691	+715
Total Salts, AWWA 2540, (mg/Kg)	2021	3729	5588	2368
Saturated Minimum Resistivity, ASTM G-187, (ohm-cm)	160	207	127	174

Analyzed By N. Campo

Nathan Campo
Engineering Technician III

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Terracon

Client
IP Darden I LLC

Project
Darden Solar

Sample Submitted By: Terracon (60) **Date Received:** 6/12/2023 **Lab No.: 23-0343**

Results of Corrosion Analysis

Sample Number	--	--	--	--
Sample Location	B-78	B-81	B-88	B-89
Sample Depth (ft.)	4.0-6.0	4.0-6.0	4.0-6.0	4.0-6.0
pH Analysis, ASTM G51	8.48	8.48	9.20	8.53
Water Soluble Sulfate (SO4), ASTM C 1580 (Percent %)	0.02	0.01	0.03	0.01
Sulfides, AWWA 4500-S D, (mg/Kg)	Nil	Nil	Nil	Nil
Chlorides, ASTM D512, (mg/kg)	80	292	102	75
Red-Ox, ASTM G200, (mV)	+714	+714	+715	+719
Total Salts, AWWA 2540, (mg/Kg)	2156	2458	2396	1489
Saturated Minimum Resistivity, ASTM G-187, (ohm-cm)	180	127	174	321

N. Campo

Analyzed By ____________________
Nathan Campo
Engineering Technician III

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Sample Submitted By: Terracon (60) **Date Received:** 3/13/2023 **Lab No.: 23-0159**

Results of Corrosion Analysis

Sample Number	--	--	--	--
Sample Location	B-87	B-92	B-93	B-96
Sample Depth (ft.)	4.0-6.0	4.0-6.0	4.0-6.0	4.0-6.0
pH Analysis, ASTM G51	8.45	8.33	8.52	8.19
Water Soluble Sulfate (SO4), ASTM C 15806 (Percent %)	0.01	0.10	0.02	0.05
Sulfides, AWWA 4500-S D, (mg/Kg)	Nil	Nil	Nil	Nil
Chlorides, ASTM D512, (mg/kg)	75	150	220	455
Red-Ox, ASTM G200, (mV)	+720	+715	+720	+705
Total Salts, AWWA 2540, (mg/Kg)	1411	1814	1439	3057
Saturated Minimum Resistivity, ASTM G-187, (ohm-cm)	341	241	247	120

Analyzed By N. Campo
Nathan Campo
Engineering Technician II

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Sample Submitted By: Terracon (60) **Date Received:** 6/12/2023 **Lab No.: 23-0343**

Results of Corrosion Analysis

Sample Number	--	--	--	--
Sample Location	B-97	B-102	B-103	B-105
Sample Depth (ft.)	4.0-6.0	4.0-6.0	4.0-6.0	4.0-6.0
pH Analysis, ASTM G51	7.79	8.66	8.47	8.13
Water Soluble Sulfate (SO4), ASTM C 1580 (Percent %)	0.01	<0.01	0.01	0.01
Sulfides, AWWA 4500-S D, (mg/Kg)	Nil	Nil	Nil	Nil
Chlorides, ASTM D512, (mg/kg)	53	65	58	85
Red-Ox, ASTM G200, (mV)	+721	+725	+720	+720
Total Salts, AWWA 2540, (mg/Kg)	1041	751	1338	1400
Saturated Minimum Resistivity, ASTM G-187, (ohm-cm)	415	388	335	274

N. Campo

Analyzed By ____________________
Nathan Campo
Engineering Technician III

The tests were performed in general accordance with applicable ASTM and AWWA test methods. This report is exclusively for the use of the client indicated above and shall not be reproduced except in full without the written consent of our company. Test results transmitted herein are only applicable to the actual samples tested at the location(s) referenced and are not necessarily indicative of the properties of other apparently similar or identical materials.

750 Pilot Road, Suite F
Las Vegas, Nevada 89119
(702) 597-9393

Client
IP Darden I LLC

Project
Darden Solar

Sample Submitted By: Terracon (60) **Date Received:** 3/13/2023 **Lab No.: 23-0159**

Results of Corrosion Analysis

Sample Number	--	--	--	--
Sample Location	B-99	B-100	B-107	B-110
Sample Depth (ft.)	4.0-6.0	4.0-6.0	4.0-6.0	4.0-6.0
pH Analysis, ASTM G51	8.54	8.33	8.46	8.53
Water Soluble Sulfate (SO4), ASTM C 15806 (Percent %)	0.11	0.14	0.35	0.38
Sulfides, AWWA 4500-S D, (mg/Kg)	Nil	Nil	Nil	Nil
Chlorides, ASTM D512, (mg/kg)	100	100	55	322
Red-Ox, ASTM G200, (mV)	+714	+700	+698	+691
Total Salts, AWWA 2540, (mg/Kg)	2184	3612	3796	5404
Saturated Minimum Resistivity, ASTM G-187, (ohm-cm)	221	214	147	87

N. Campo

Analyzed By ____________________
Nathan Campo
Engineering Technician II

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Client
IP Darden I LLC

Project
Darden Solar

Sample Submitted By: Terracon (60) **Date Received:** 6/12/2023 **Lab No.: 23-0343**

Results of Corrosion Analysis

Sample Number	--	--	--	--
Sample Location	B-106	B-108	B-109	B-124
Sample Depth (ft.)	5.0-6.5	4.0-6.0	4.0-6.0	4.0-6.0
pH Analysis, ASTM G51	8.45	9.28	9.14	9.63
Water Soluble Sulfate (SO4), ASTM C 1580 (Percent %)	0.34	0.01	0.01	0.05
Sulfides, AWWA 4500-S D, (mg/Kg)	Nil	Nil	Nil	Nil
Chlorides, ASTM D512, (mg/kg)	67	75	120	122
Red-Ox, ASTM G200, (mV)	+689	+722	+720	+712
Total Salts, AWWA 2540, (mg/Kg)	6294	973	1265	2699
Saturated Minimum Resistivity, ASTM G-187, (ohm-cm)	154	288	180	134

N. Campo

Analyzed By
Nathan Campo
Engineering Technician III

750 Pilot Road, Suite F
Las Vegas, Nevada 89119
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Client
IP Darden I LLC

Project
Darden Solar

Sample Submitted By: Terracon (60)   **Date Received:** 3/13/2023   **Lab No.: 23-0159**

Results of Corrosion Analysis

Sample Number	--	--	--	--
Sample Location	B-112	B-115	B-117	B-119
Sample Depth (ft.)	4.0-6.0	4.0-6.0	4.0-6.0	4.0-6.0
pH Analysis, ASTM G51	8.39	8.90	8.83	8.35
Water Soluble Sulfate (SO4), ASTM C 15806 (Percent %)	0.32	0.01	0.04	0.06
Sulfides, AWWA 4500-S D, (mg/Kg)	Nil	Nil	Nil	Nil
Chlorides, ASTM D512, (mg/kg)	195	77	77	85
Red-Ox, ASTM G200, (mV)	+676	+724	+721	+720
Total Salts, AWWA 2540, (mg/Kg)	8680	850	1136	1400
Saturated Minimum Resistivity, ASTM G-187, (ohm-cm)	140	582	274	281

Analyzed By N. Campo
Nathan Campo
Engineering Technician II

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Project
Darden Solar

Sample Submitted By: Terracon (60) **Date Received:** 6/12/2023 **Lab No.: 23-0343**

Results of Corrosion Analysis

Sample Number	--	--	--	--
Sample Location	B-126	B-128	B-129	B-130
Sample Depth (ft.)	4.0-6.0	4.0-6.0	4.0-6.0	4.0-6.0
pH Analysis, ASTM G51	9.07	8.63	9.50	9.20
Water Soluble Sulfate (SO4), ASTM C 1580 (Percent %)	<0.01	0.01	0.01	0.02
Sulfides, AWWA 4500-S D, (mg/Kg)	Nil	Nil	Nil	Nil
Chlorides, ASTM D512, (mg/kg)	57	80	55	170
Red-Ox, ASTM G200, (mV)	+730	+720	+721	+714
Total Salts, AWWA 2540, (mg/Kg)	477	1428	1181	1752
Saturated Minimum Resistivity, ASTM G-187, (ohm-cm)	509	281	214	207

N. Campo

Analyzed By ______________________
Nathan Campo
Engineering Technician III

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Client
IP Darden I LLC

Project
Darden Solar

Sample Submitted By: Terracon (60) **Date Received:** 3/13/2023 **Lab No.: 23-0159**

Results of Corrosion Analysis

Sample Number	--	--	--
Sample Location	B-120	B-122	B-123
Sample Depth (ft.)	4.0-6.0	4.0-6.0	4.0-6.0
pH Analysis, ASTM G51	8.36	8.55	8.45
Water Soluble Sulfate (SO4), ASTM C 15806 (Percent %)	0.17	0.04	0.08
Sulfides, AWWA 4500-S D, (mg/Kg)	Nil	Nil	Nil
Chlorides, ASTM D512, (mg/kg)	67	90	57
Red-Ox, ASTM G200, (mV)	+715	+720	+720
Total Salts, AWWA 2540, (mg/Kg)	1803	1383	1327
Saturated Minimum Resistivity, ASTM G-187, (ohm-cm)	268	288	348

Analyzed By N. Campo
Nathan Campo
Engineering Technician II

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Project
Darden Solar

Sample Submitted By: Terracon (60) **Date Received:** 6/12/2023 **Lab No.: 23-0343**

Results of Corrosion Analysis

Sample Number	--	--	--	--
Sample Location	B-131	B-133	B-134	B-136
Sample Depth (ft.)	4.0-6.0	4.0-6.0	4.0-6.0	4.0-6.0
pH Analysis, ASTM G51	8.50	8.84	8.25	8.75
Water Soluble Sulfate (SO4), ASTM C 1580 (Percent %)	0.03	0.02	0.02	0.01
Sulfides, AWWA 4500-S D, (mg/Kg)	Nil	Nil	Nil	Nil
Chlorides, ASTM D512, (mg/kg)	175	125	82	377
Red-Ox, ASTM G200, (mV)	+715	+714	+695	+711
Total Salts, AWWA 2540, (mg/Kg)	2251	2128	3959	2788
Saturated Minimum Resistivity, ASTM G-187, (ohm-cm)	120	247	120	140

Analyzed By N. Campo
Nathan Campo
Engineering Technician III

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Client
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Project
Darden Solar

Sample Submitted By: Terracon (60) **Date Received:** 6/12/2023 **Lab No.: 23-0343**

Results of Corrosion Analysis

Sample Number	--	--	--
Sample Location	E-1	SUB-1	BESS-1
Sample Depth (ft.)	4.0-6.0	4.0-6.0	4.0-6.0
pH Analysis, ASTM G51	8.55	8.69	8.48
Water Soluble Sulfate (SO4), ASTM C 1580 (Percent %)	0.01	0.01	0.01
Sulfides, AWWA 4500-S D, (mg/Kg)	Nil	Nil	Nil
Chlorides, ASTM D512, (mg/kg)	130	127	177
Red-Ox, ASTM G200, (mV)	+718	+724	+715
Total Salts, AWWA 2540, (mg/Kg)	1618	808	1920
Saturated Minimum Resistivity, ASTM G-187, (ohm-cm)	308	435	254

N. Campo

Analyzed By
Nathan Campo
Engineering Technician III

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CERCO
analytical
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Concord, CA 94520-1006
925 462 2771 Fax. 925 462 2775
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Client: JDH Corrosion Consultants, Inc.
Client's Project No.: 2023345 (60225172)
Client's Project Name: Darden Solar
Date Sampled: Not Indicated
Date Received: 12-Sep-23
Matrix: Soil
Authorization: Signed Chain of Custody

Date of Report: 15-Sep-2023

Job/Sample No.	Sample I.D.	Redox (mV)	pH	Resistivity (As Received) (ohms-cm)	Resistivity (100% Saturation) (ohms-cm)	Sulfide (mg/kg)*	Chloride (mg/kg)*	Sulfate (mg/kg)*
2309021-001	SUB-2 0-4'	290	8.14	58,000	1,500	-	N.D.	36
2309021-002	SW-1 0-4'	270	8.18	200,000	3,000	-	N.D.	N.D.
2309021-003	E-2 0-4'	260	8.24	17,000	1,200	-	55	33

Method:	ASTM D1498	ASTM D4972	ASTM G57	ASTM G57	ASTM D4658M	ASTM D4327	ASTM D4327
Reporting Limit:	-	-	-	-	50	15	15
Date Analyzed:	13-Sep-2023	14-Sep-2023	14-Sep-2023	14-Sep-2023	-	13-Sep-2023	13-Sep-2023

* Results Reported on "As Received" Basis

N.D. - None Detected

Julia Clauson
Chemist

Quality Control Summary - **All laboratory quality control parameters were found to be within established limits**

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CALIFORNIA BEARING RATIO (CBR)
OF LABORATORY-COMPACTED SOIL
ASTM D 1883

Project Name: Darden Solar
Project No. : 60225172
Boring No.: B-133
Sample No.: -
Depth (ft.) : 0-4
Soil Description : Fat Clay

Tested By : ALB Date 06/15/23
Input By: NN Date 06/19/23
Checked By: AP Date 06/20/23

SAMPLE DESCRIPTION BEFORE SOAKING

Mold Number	D
Blows Per Layer	10
Wt of Wet Soil & Mold (gm)	11730
Weight of Mold (gm)	7838
Weight of Wet Soil (gm)	3892
Mold Volume (cu.ft)	0.0750
Container No.	
Wet Wt. Soil + Container (gm)	664.75
Dry Wt. Soil + Container (gm)	639.95
Wt. Container (gm)	474.57
Moisture Content (%)	15.00
Wet Density (pcf)	114.4
Dry Density (pcf)	99.5

SAMPLE PREPARATION

Wt of Hammer (Lbs)	10
No. of Layers	5
No. of Blows/Layer	10
Drop Height (inches)	18
Surcharge Weight (Lbs)	10
Max. Dry Density (pcf)	110.3
Molded Relative Comp (%)	90.2
Req'd % Moisture	15.4
No. of Trials	1
% Retained 3/4" Sieve	0.00%

DEFORMATION DURING SOAKING PERIOD

Sample Length (inch) 5

DATE	TIME	Mold No.:	D
		Dial Rdgs	Swell (in)
06/15/23	16:55	0.0710	
06/16/23	08:10	0.4520	
06/19/23	08:50	0.4890	0.4180
Percent Swell/Collapse (+/-)			8.36

AFTER SOAKING

Mold Number	D
Wt. of Wet Soil + Mold (gm)	12216
Weight of Mold (gm)	7838
Weight of Wet Soil (gm)	4378
Final Sample Volume (cu.ft)	0.0813
Container No.	
Wet Wt. Soil + Container (gm)	623.23
Dry Wt. Soil + Container (gm)	499.09
Wt. Container (gm)	151.29
Mosture Content (%)	35.7
Wet Density (pcf)	118.8
After Test Dry Density (pcf)	87.5

TEST LOAD DATA

Piston Diameter (inches): 1.954

Penetration (inch)	Mold No.: D	
	LOAD (lb)	Stress (psi)
0.000	0	0.00
0.025	9	3.00
0.050	17	5.67
0.075	23	7.67
0.100	28	9.34
0.125	34	11.34
0.150	39	13.01
0.175	44	14.67
0.200	48	16.01
0.225	51	17.01
0.250	55	18.34
0.275	58	19.34
0.300	62	20.68
0.325	64	21.34
0.350	67	22.34
0.375	70	23.34
0.400	72	24.01
0.425	75	25.01
0.450	78	26.01
0.475	80	26.68
0.500	81	27.01

TEST RESULTS

CBR @ .1": 1
CBR @ .2": 1

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CALIFORNIA BEARING RATIO (CBR)
OF LABORATORY-COMPACTED SOIL
ASTM D 1883

Project Name:	Darden Solar	Tested By :	ALB	Date	06/15/23
Project No. :	60225172	Input By:	NN	Date	06/19/23
Boring No.:	B-133	Checked By:	AP	Date	06/20/23
Sample No.:	-				
Depth (ft.) :	0-4				
Soil Description :	Fat Clay				

SAMPLE DESCRIPTION BEFORE SOAKING

Mold Number	E
Blows Per Layer	25
Wt of Wet Soil & Mold (gm)	11907.5
Weight of Mold (gm)	7821.5
Weight of Wet Soil (gm)	4086
Mold Volume (cu.ft)	0.0750
Container No.	
Wet Wt. Soil + Container (gm)	664.75
Dry Wt. Soil + Container (gm)	639.95
Wt. Container (gm)	474.57
Moisture Content (%)	15.00
Wet Density (pcf)	120.1
Dry Density (pcf)	104.4

SAMPLE PREPARATION

Wt of Hammer (Lbs)	10
No. of Layers	5
No. of Blows/Layer	25
Drop Height (inches)	18
Surcharge Weight (Lbs)	10
Max. Dry Density (pcf)	110.3
Molded Relative Comp (%)	94.7
Req'd % Moisture	15.4
No. of Trials	1
% Retained 3/4" Sieve	0.00%

DEFORMATION DURING SOAKING PERIOD

Sample Length (inch) 5

DATE	TIME	Mold No.:	E
		Dial Rdgs	Swell (in)
06/15/23	16:55	0.0640	
06/16/23	08:10	0.3550	
06/19/23	08:50	0.5100	0.4460
Percent Swell/Collapse (+/-)			8.92

AFTER SOAKING

Mold Number	E
Wt. of Wet Soil + Mold (gm)	12321
Weight of Mold (gm)	7822
Weight of Wet Soil (gm)	4499
Final Sample Volume (cu.ft)	0.0817
Container No.	
Wet Wt. Soil + Container (gm)	496.72
Dry Wt. Soil + Container (gm)	407.96
Wt. Container (gm)	142.57
Mosture Content (%)	33.4
Wet Density (pcf)	121.4
After Test Dry Density (pcf)	91.0

TEST LOAD DATA

Piston Diameter (inches): 1.954

Penetration (inch)	Mold No.: E LOAD (lb)	Stress (psi)
0.000	0	0.00
0.025	11	3.67
0.050	21	7.00
0.075	30	10.00
0.100	39	13.01
0.125	46	15.34
0.150	51	17.01
0.175	57	19.01
0.200	62	20.68
0.225	67	22.34
0.250	71	23.68
0.275	75	25.01
0.300	79	26.34
0.325	82	27.34
0.350	85	28.35
0.375	89	29.68
0.400	93	31.01
0.425	95	31.68
0.450	99	33.01
0.475	102	34.01
0.500	105	35.01

TEST RESULTS

CBR @ .1": **1**

CBR @ .2": **1**

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CALIFORNIA BEARING RATIO (CBR)
OF LABORATORY-COMPACTED SOIL
ASTM D 1883

Project Name: Darden Solar
Project No. : 60225172
Boring No.: B-133
Sample No.: -
Depth (ft.) : 0-4
Soil Description : Fat Clay

Tested By : ALB Date 06/15/23
Input By: NN Date 06/19/23
Checked By: AP Date 06/20/23

SAMPLE DESCRIPTION BEFORE SOAKING

Mold Number	F
Blows Per Layer	56
Wt of Wet Soil & Mold (gm)	12138
Weight of Mold (gm)	7806.5
Weight of Wet Soil (gm)	4332
Mold Volume (cu.ft)	0.0750
Container No.	
Wet Wt. Soil + Container (gm)	664.75
Dry Wt. Soil + Container (gm)	639.95
Wt. Container (gm)	474.57
Moisture Content (%)	15.00
Wet Density (pcf)	127.3
Dry Density (pcf)	110.7

DEFORMATION DURING SOAKING PERIOD

Sample Length (inch) 5

DATE	TIME	Mold No.:	F
		Dial Rdgs	Swell (in)
06/15/23	16:55	0.0700	
06/16/23	08:10	0.2570	
06/19/23	08:50	0.4100	0.3400
Percent Swell/Collapse (+/-)			6.80

AFTER SOAKING

Mold Number	F
Wt. of Wet Soil + Mold (gm)	12407
Weight of Mold (gm)	7807
Weight of Wet Soil (gm)	4600
Final Sample Volume (cu.ft)	0.0801
Container No.	
Wet Wt. Soil + Container (gm)	519.26
Dry Wt. Soil + Container (gm)	430.41
Wt. Container (gm)	149.84
Mosture Content (%)	31.7
Wet Density (pcf)	126.6
After Test Dry Density (pcf)	96.2

SAMPLE PREPARATION

Wt of Hammer (Lbs)	10
No. of Layers	5
No. of Blows/Layer	56
Drop Height (inches)	18
Surcharge Weight (Lbs)	10
Max. Dry Density (pcf)	110.3
Molded Relative Comp (%)	100.4
Req'd % Moisture	15.4
No. of Trials	1
% Retained 3/4" Sieve	0.00%

TEST LOAD DATA

Piston Diameter (inches): 1.954

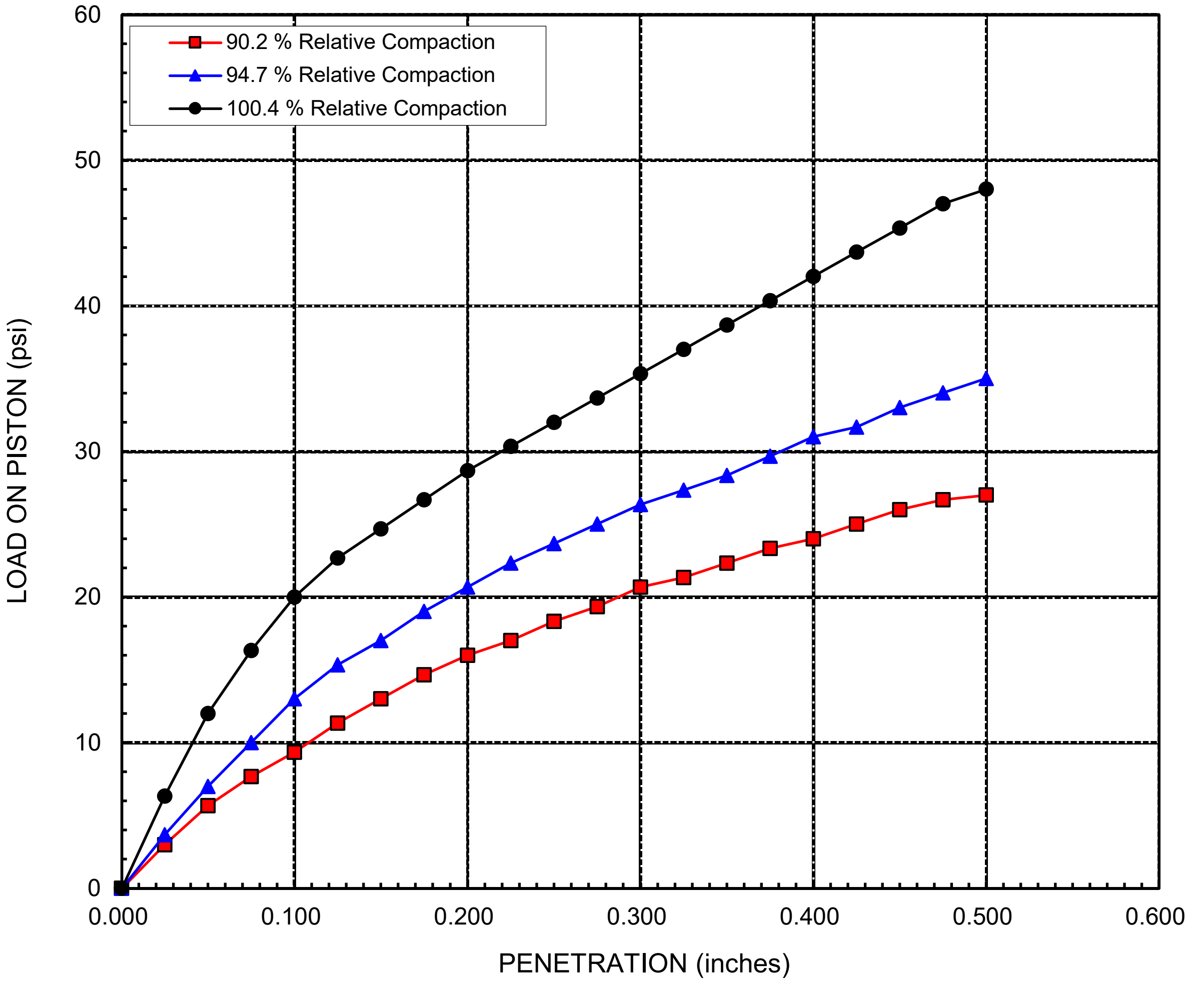
Penetration	Mold No.:	F
(inch)	LOAD (lb)	Stress (psi)
0.000	0	0.00
0.025	19	6.34
0.050	36	12.01
0.075	49	16.34
0.100	60	20.01
0.125	68	22.68
0.150	74	24.68
0.175	80	26.68
0.200	86	28.68
0.225	91	30.35
0.250	96	32.01
0.275	101	33.68
0.300	106	35.35
0.325	111	37.02
0.350	116	38.68
0.375	121	40.35
0.400	126	42.02
0.425	131	43.68
0.450	136	45.35
0.475	141	47.02
0.500	144	48.02

TEST RESULTS

CBR @ .1": 2
CBR @ .2": 2

CALIFORNIA BEARING RATIO (CBR)
OF LABORATORY-COMPACTED SOIL
ASTM D 1883

Project Name:	Darden Solar	Tested By :	ALB	Date:	06/15/23
Project No. :	60225172	Data Input By:	NN	Date:	06/19/23
Boring No.:	B-133	Checked By:	AP	Date:	06/20/23
Sample No.:	-				
Depth (ft.) :	0-4				
Soil Description :	Fat Clay				

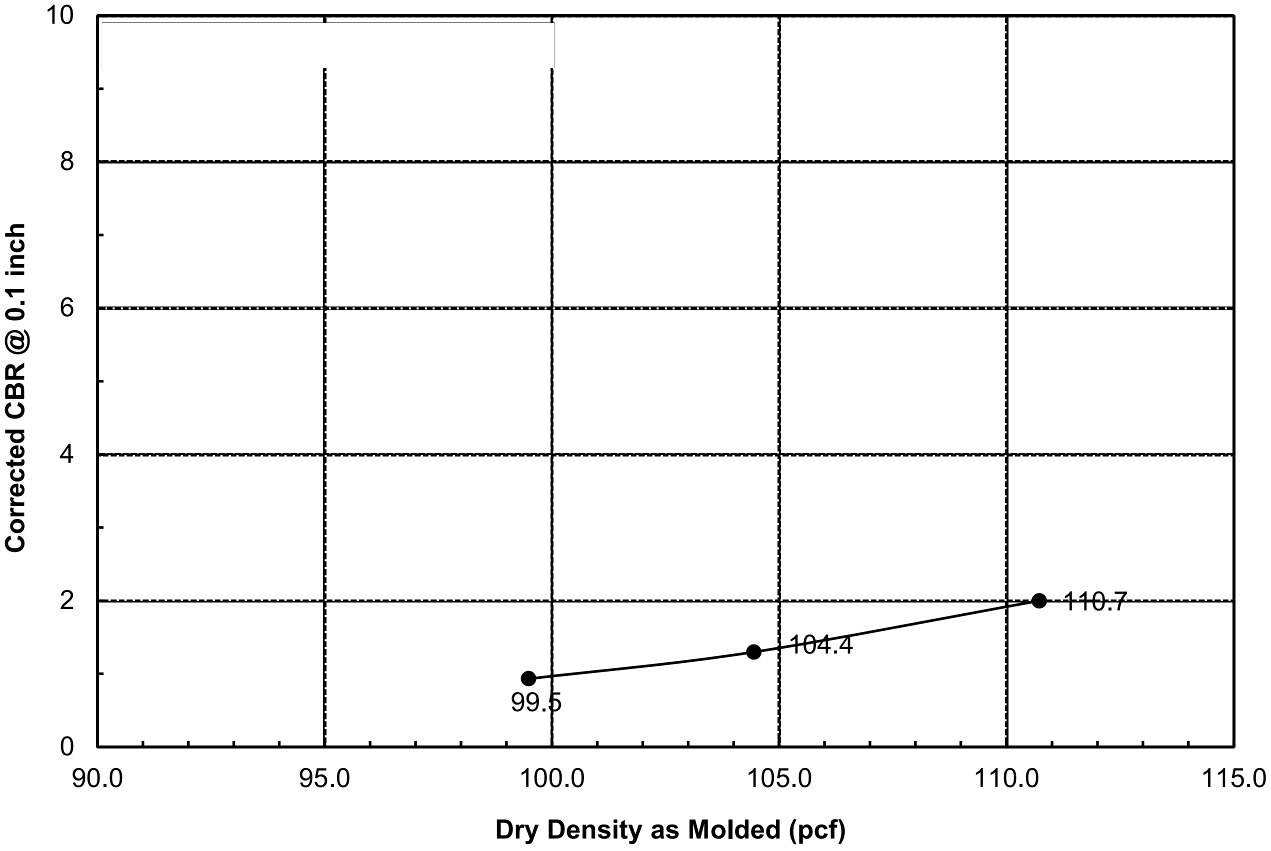


CALIFORNIA BEARING RATIO (CBR)
OF LABORATORY-COMPACTED SOIL
ASTM D 1883

Project Name:	Darden Solar	Tested By :	ALB	Date:	06/15/23
Project No. :	60225172	Data Input By:	NN	Date:	06/19/23
Boring No.:	B-133	Checked By:	AP	Date:	06/20/23
Sample No.:	-				
Depth (ft.) :	0-4				
Soil Description :	Fat Clay				

TEST RESULTS

Dry Density (pcf)	Maximum Dry Density by ASTM D 1557 (pcf)	Relative Compaction (%)	Blow Per Layer	CBR @0.1"	CBR @0.2"
99.5	110.3	90.2	10	1	1
104.4	110.3	94.7	25	1	1
110.7	110.3	100.4	56	2	2



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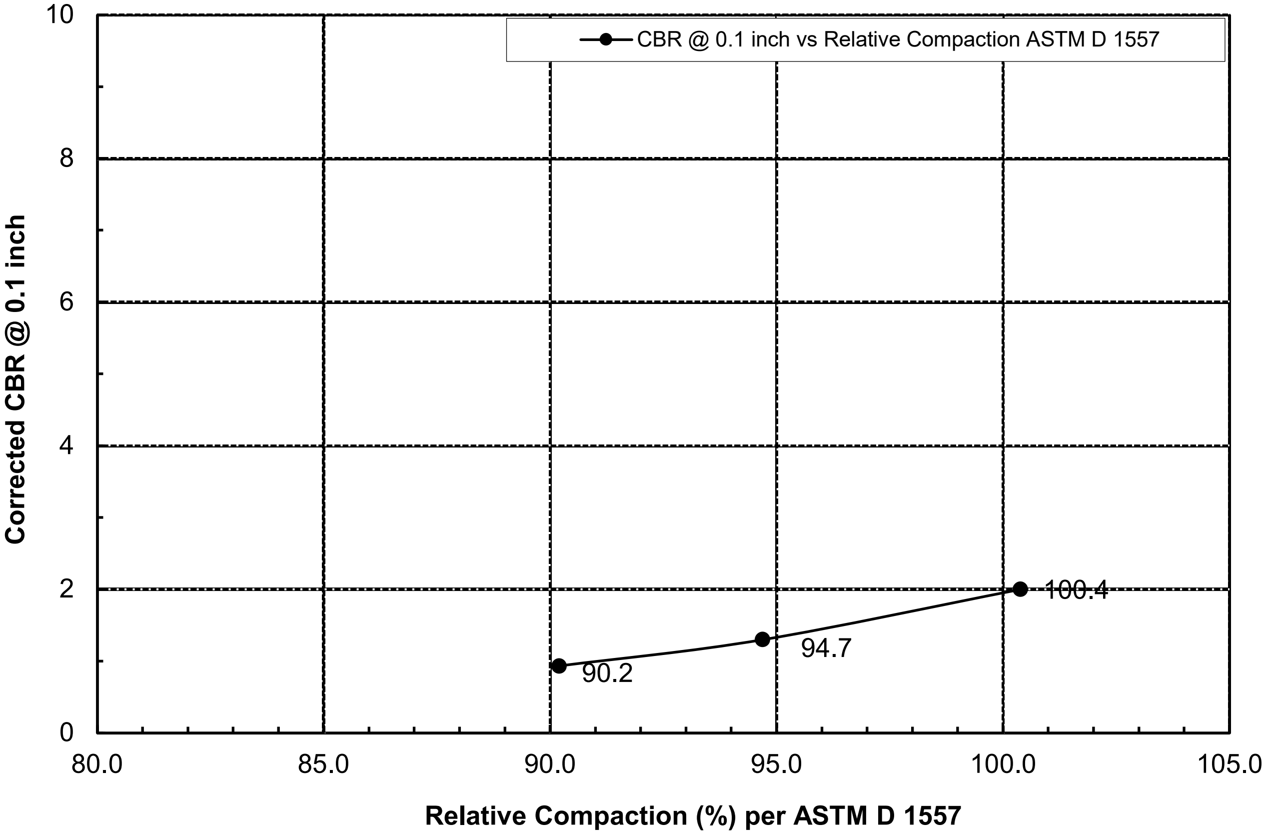
CALIFORNIA BEARING RATIO (CBR)
OF LABORATORY-COMPACTED SOIL
ASTM D 1883

Project Name:	Darden Solar	Tested By :	ALB	Date:	06/15/23
Project No. :	60225172	Data Input By:	NN	Date:	06/19/23
Boring No.:	B-133	Checked By:	AP	Date:	06/20/23
Sample No.:	-				
Depth (ft.) :	0-4				
Soil Description :	Fat Clay				

TEST RESULTS

Dry Density (pcf)	Maximum Dry Density by ASTM D 1557 (pcf)	Relative Compaction (%)	Blow Per Layer	CBR @0.1"	CBR @0.2"
99.5	110.3	90.2	10	1	1
104.4	110.3	94.7	25	1	1
110.7	110.3	100.4	56	2	2



CALIFORNIA BEARING RATIO (CBR)
OF LABORATORY-COMPACTED SOIL
ASTM D 1883

Project Name:	Darden Solar	Tested By :	ALB	Date	06/15/23
Project No. :	60225172	Input By:	NN	Date	06/19/23
Boring No.:	B-133	Checked By:	AP	Date	06/20/23
Sample No.:	-				
Depth (ft.) :	0-4				
Soil Description :	Fat Clay				

SAMPLE DESCRIPTION BEFORE SOAKING

Mold Number	D
Blows Per Layer	10
Wt of Wet Soil & Mold (gm)	11730
Weight of Mold (gm)	7838
Weight of Wet Soil (gm)	3892
Mold Volume (cu.ft)	0.0750
Container No.	
Wet Wt. Soil + Container (gm)	664.75
Dry Wt. Soil + Container (gm)	639.95
Wt. Container (gm)	474.57
Moisture Content (%)	15.00
Wet Density (pcf)	114.4
Dry Density (pcf)	99.5

SAMPLE PREPARATION

Wt of Hammer (Lbs)	10
No. of Layers	5
No. of Blows/Layer	10
Drop Height (inches)	18
Surcharge Weight (Lbs)	10
Max. Dry Density (pcf)	110.3
Molded Relative Comp (%)	90.2
Req'd % Moisture	15.4
No. of Trials	1
% Retained 3/4" Sieve	0.00%

DEFORMATION DURING SOAKING PERIOD

Sample Length (inch) 5

DATE	TIME	Mold No.:	D
		Dial Rdgs	Swell (in)
06/15/23	16:55	0.0710	
06/16/23	08:10	0.4520	
06/19/23	08:50	0.4890	0.4180
Percent Swell/Collapse (+/-)			8.36

AFTER SOAKING

Mold Number	D
Wt. of Wet Soil + Mold (gm)	12216
Weight of Mold (gm)	7838
Weight of Wet Soil (gm)	4378
Final Sample Volume (cu.ft)	0.0813
Container No.	
Wet Wt. Soil + Container (gm)	623.23
Dry Wt. Soil + Container (gm)	499.09
Wt. Container (gm)	151.29
Mosture Content (%)	35.7
Wet Density (pcf)	118.8
After Test Dry Density (pcf)	87.5

TEST LOAD DATA

Piston Diameter (inches): 1.954

Penetration	Mold No.: D	
(inch)	LOAD (lb)	Stress (psi)
0.000	0	0.00
0.025	9	3.00
0.050	17	5.67
0.075	23	7.67
0.100	28	9.34
0.125	34	11.34
0.150	39	13.01
0.175	44	14.67
0.200	48	16.01
0.225	51	17.01
0.250	55	18.34
0.275	58	19.34
0.300	62	20.68
0.325	64	21.34
0.350	67	22.34
0.375	70	23.34
0.400	72	24.01
0.425	75	25.01
0.450	78	26.01
0.475	80	26.68
0.500	81	27.01

TEST RESULTS

CBR @ .1": **1**

CBR @ .2": **1**

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CALIFORNIA BEARING RATIO (CBR)
OF LABORATORY-COMPACTED SOIL
ASTM D 1883

Project Name:	Darden Solar	Tested By :	ALB	Date	06/15/23
Project No. :	60225172	Input By:	NN	Date	06/19/23
Boring No.:	B-133	Checked By:	AP	Date	06/20/23
Sample No.:	-				
Depth (ft.) :	0-4				
Soil Description :	Fat Clay				

SAMPLE DESCRIPTION BEFORE SOAKING

Mold Number	E
Blows Per Layer	25
Wt of Wet Soil & Mold (gm)	11907.5
Weight of Mold (gm)	7821.5
Weight of Wet Soil (gm)	4086
Mold Volume (cu.ft)	0.0750
Container No.	
Wet Wt. Soil + Container (gm)	664.75
Dry Wt. Soil + Container (gm)	639.95
Wt. Container (gm)	474.57
Moisture Content (%)	15.00
Wet Density (pcf)	120.1
Dry Density (pcf)	104.4

SAMPLE PREPARATION

Wt of Hammer (Lbs)	10
No. of Layers	5
No. of Blows/Layer	25
Drop Height (inches)	18
Surcharge Weight (Lbs)	10
Max. Dry Density (pcf)	110.3
Molded Relative Comp (%)	94.7
Req'd % Moisture	15.4
No. of Trials	1
% Retained 3/4" Sieve	0.00%

DEFORMATION DURING SOAKING PERIOD

Sample Length (inch) 5

DATE	TIME	Mold No.:	E
		Dial Rdgs	Swell (in)
06/15/23	16:55	0.0640	
06/16/23	08:10	0.3550	
06/19/23	08:50	0.5100	0.4460
Percent Swell/Collapse (+/-)			8.92

AFTER SOAKING

Mold Number	E
Wt. of Wet Soil + Mold (gm)	12321
Weight of Mold (gm)	7822
Weight of Wet Soil (gm)	4499
Final Sample Volume (cu.ft)	0.0817
Container No.	
Wet Wt. Soil + Container (gm)	496.72
Dry Wt. Soil + Container (gm)	407.96
Wt. Container (gm)	142.57
Mosture Content (%)	33.4
Wet Density (pcf)	121.4
After Test Dry Density (pcf)	91.0

TEST LOAD DATA

Piston Diameter (inches): 1.954

Penetration (inch)	Mold No.: E LOAD (lb)	Stress (psi)
0.000	0	0.00
0.025	11	3.67
0.050	21	7.00
0.075	30	10.00
0.100	39	13.01
0.125	46	15.34
0.150	51	17.01
0.175	57	19.01
0.200	62	20.68
0.225	67	22.34
0.250	71	23.68
0.275	75	25.01
0.300	79	26.34
0.325	82	27.34
0.350	85	28.35
0.375	89	29.68
0.400	93	31.01
0.425	95	31.68
0.450	99	33.01
0.475	102	34.01
0.500	105	35.01

TEST RESULTS

CBR @ .1": 1
CBR @ .2": 1

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CALIFORNIA BEARING RATIO (CBR)
OF LABORATORY-COMPACTED SOIL

ASTM D 1883

Project Name: Darden Solar
Project No. : 60225172
Boring No.: B-133
Sample No.: -
Depth (ft.) : 0-4
Soil Description : Fat Clay

Tested By : ALB Date 06/15/23
Input By: NN Date 06/19/23
Checked By: AP Date 06/20/23

SAMPLE DESCRIPTION BEFORE SOAKING

Mold Number	F
Blows Per Layer	56
Wt of Wet Soil & Mold (gm)	12138
Weight of Mold (gm)	7806.5
Weight of Wet Soil (gm)	4332
Mold Volume (cu.ft)	0.0750
Container No.	
Wet Wt. Soil + Container (gm)	664.75
Dry Wt. Soil + Container (gm)	639.95
Wt. Container (gm)	474.57
Moisture Content (%)	15.00
Wet Density (pcf)	127.3
Dry Density (pcf)	110.7

SAMPLE PREPARATION

Wt of Hammer (Lbs)	10
No. of Layers	5
No. of Blows/Layer	56
Drop Height (inches)	18
Surcharge Weight (Lbs)	10
Max. Dry Density (pcf)	110.3
Molded Relative Comp (%)	100.4
Req'd % Moisture	15.4
No. of Trials	1
% Retained 3/4" Sieve	0.00%

DEFORMATION DURING SOAKING PERIOD

Sample Length (inch) 5

DATE	TIME	Mold No.:	F
		Dial Rdgs	Swell (in)
06/15/23	16:55	0.0700	
06/16/23	08:10	0.2570	
06/19/23	08:50	0.4100	0.3400
Percent Swell/Collapse (+/-)			6.80

AFTER SOAKING

Mold Number	F
Wt. of Wet Soil + Mold (gm)	12407
Weight of Mold (gm)	7807
Weight of Wet Soil (gm)	4600
Final Sample Volume (cu.ft)	0.0801
Container No.	
Wet Wt. Soil + Container (gm)	519.26
Dry Wt. Soil + Container (gm)	430.41
Wt. Container (gm)	149.84
Mosture Content (%)	31.7
Wet Density (pcf)	126.6
After Test Dry Density (pcf)	96.2

TEST LOAD DATA

Piston Diameter (inches): 1.954

Penetration (inch)	Mold No.: F LOAD (lb)	Stress (psi)
0.000	0	0.00
0.025	19	6.34
0.050	36	12.01
0.075	49	16.34
0.100	60	20.01
0.125	68	22.68
0.150	74	24.68
0.175	80	26.68
0.200	86	28.68
0.225	91	30.35
0.250	96	32.01
0.275	101	33.68
0.300	106	35.35
0.325	111	37.02
0.350	116	38.68
0.375	121	40.35
0.400	126	42.02
0.425	131	43.68
0.450	136	45.35
0.475	141	47.02
0.500	144	48.02

TEST RESULTS

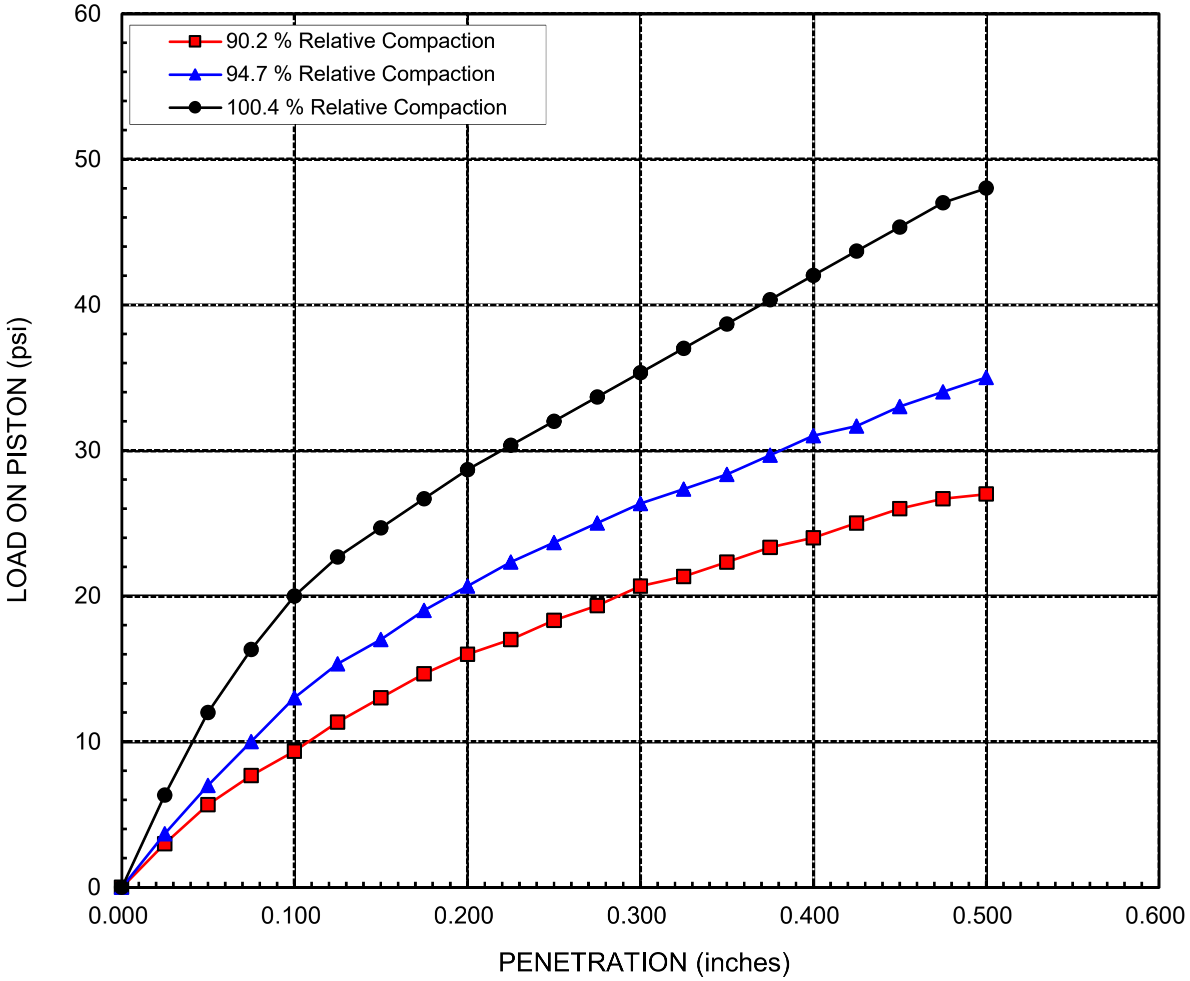
CBR @ .1": 2

CBR @ .2": 2

CALIFORNIA BEARING RATIO (CBR)
OF LABORATORY-COMPACTED SOIL
ASTM D 1883

Project Name: Darden Solar
Project No. : 60225172
Boring No.: B-133
Sample No.: -
Depth (ft.) : 0-4
Soil Description : Fat Clay

Tested By : ALB Date: 06/15/23
Data Input By: NN Date: 06/19/23
Checked By: AP Date: 06/20/23

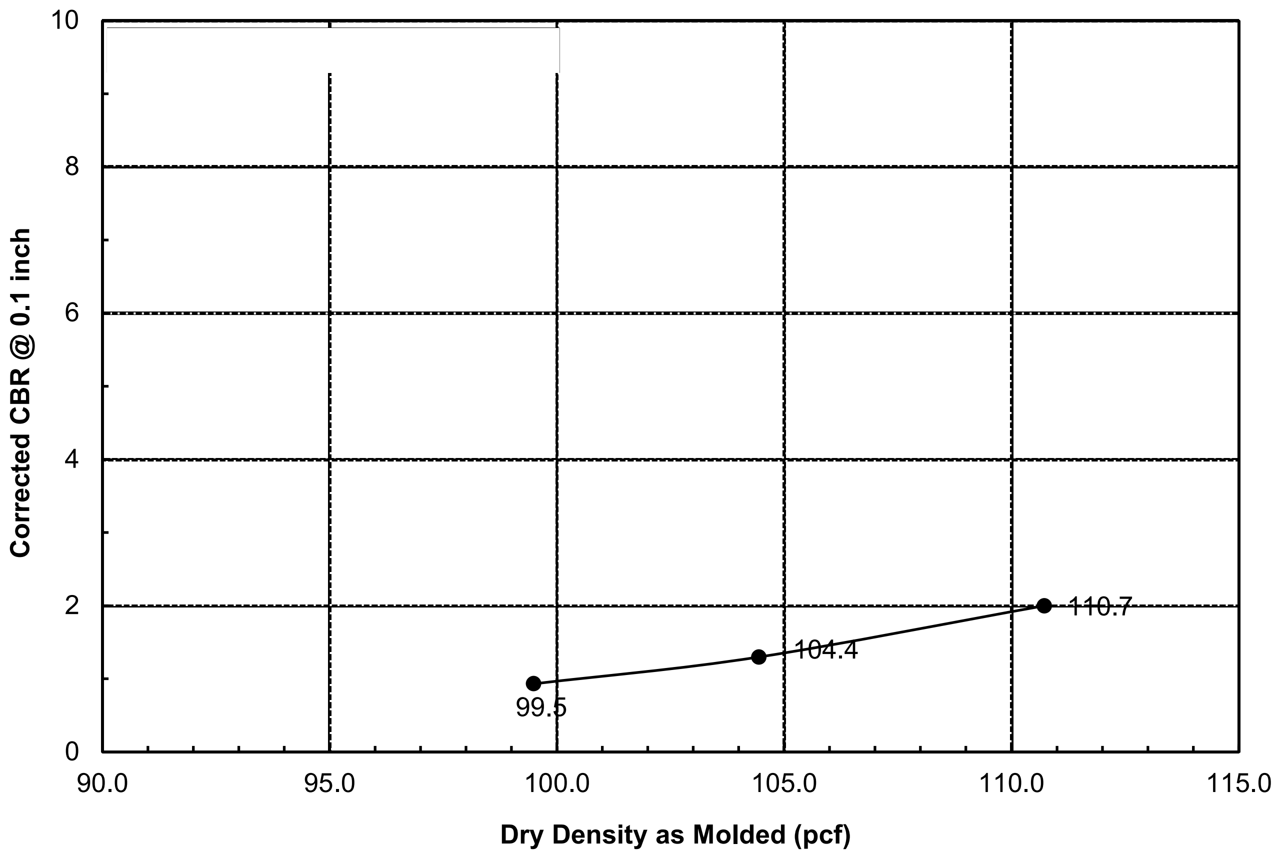


CALIFORNIA BEARING RATIO (CBR)
OF LABORATORY-COMPACTED SOIL
ASTM D 1883

Project Name:	Darden Solar	Tested By :	ALB	Date:	06/15/23
Project No. :	60225172	Data Input By:	NN	Date:	06/19/23
Boring No.:	B-133	Checked By:	AP	Date:	06/20/23
Sample No.:	-				
Depth (ft.) :	0-4				
Soil Description :	Fat Clay				

TEST RESULTS

Dry Density (pcf)	Maximum Dry Density by ASTM D 1557 (pcf)	Relative Compaction (%)	Blow Per Layer	CBR @0.1"	CBR @0.2"
99.5	110.3	90.2	10	1	1
104.4	110.3	94.7	25	1	1
110.7	110.3	100.4	56	2	2



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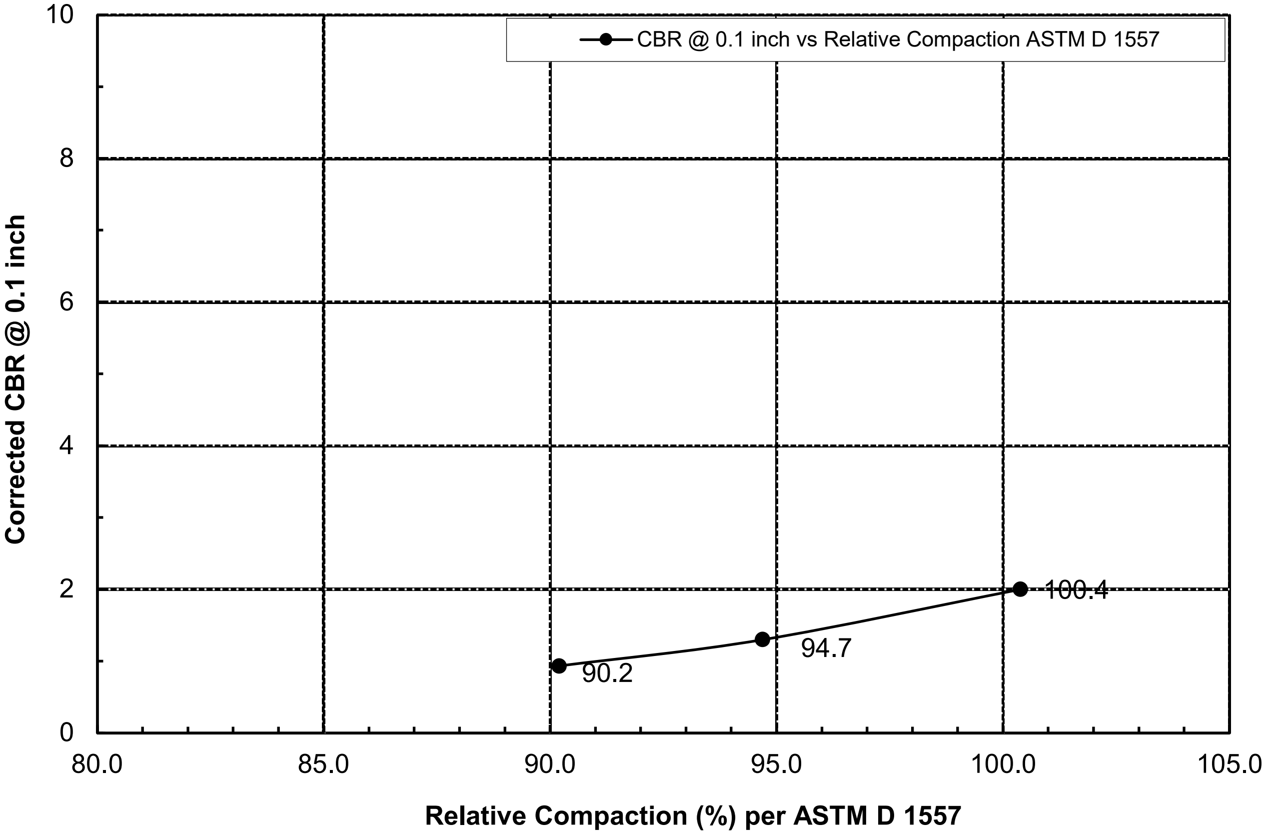
CALIFORNIA BEARING RATIO (CBR)
OF LABORATORY-COMPACTED SOIL
ASTM D 1883

Project Name:	Darden Solar	Tested By :	ALB	Date:	06/15/23
Project No. :	60225172	Data Input By:	NN	Date:	06/19/23
Boring No.:	B-133	Checked By:	AP	Date:	06/20/23
Sample No.:	-				
Depth (ft.) :	0-4				
Soil Description :	Fat Clay				

TEST RESULTS

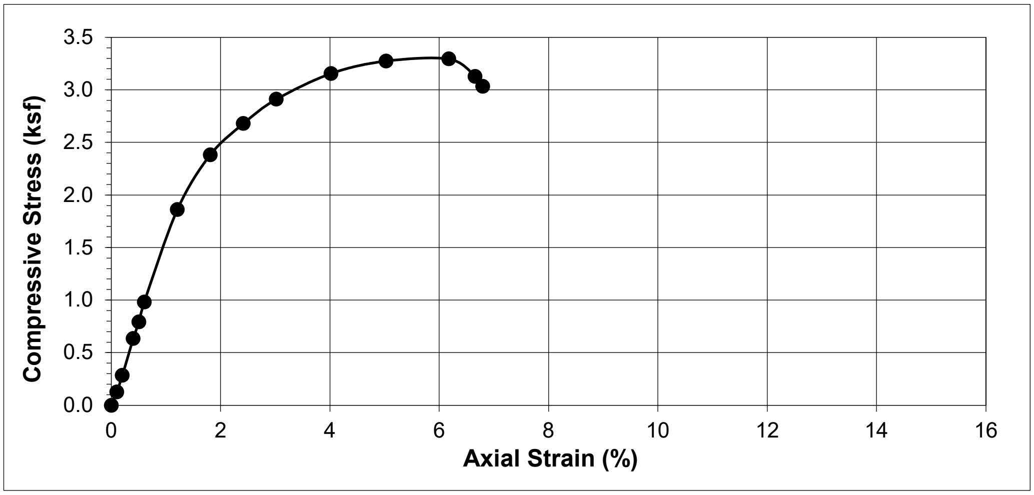
Dry Density (pcf)	Maximum Dry Density by ASTM D 1557 (pcf)	Relative Compaction (%)	Blow Per Layer	CBR @0.1"	CBR @0.2"
99.5	110.3	90.2	10	1	1
104.4	110.3	94.7	25	1	1
110.7	110.3	100.4	56	2	2



UNCONFINED COMPRESSION TEST RESULTS
ASTM D 2166

Project Name:	Darden Solar	Sample Type:	Mod Cal
Project No.:	60225172	Soil Description	Clay w/sand
Boring No.:	B-1	Dry Density (pcf):	103.6
Sample No.:	-	Moisture Content (%)	19.2
Depth (feet):	2.5	Test Date:	03/20/23

Sample Diameter (inch):	2.396	Wt. Wet Soil+Container(gms)	865.64
Sample Height (inch):	4.973	Wt. Dry Soil+Container(gms)	748.41
Sample Weight (gms):	727.55	Wt. Container (gms)	139.20



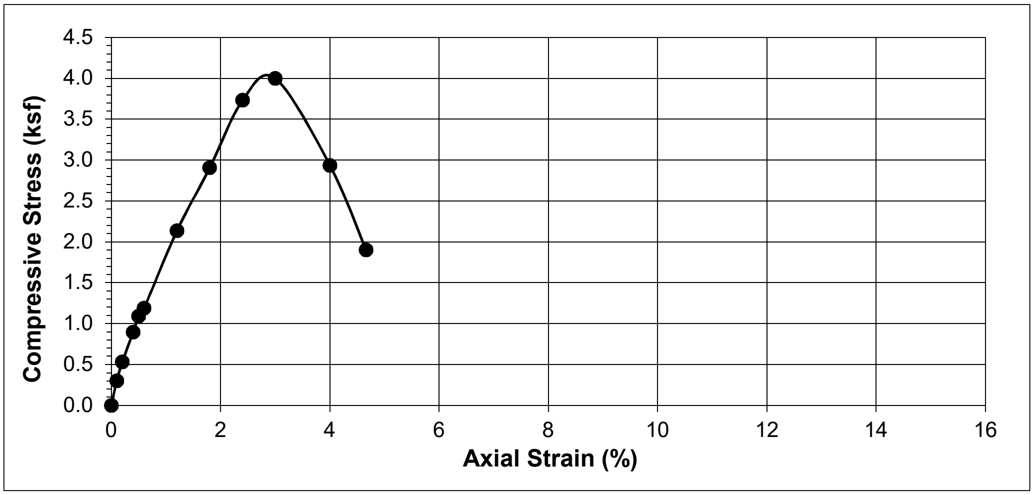
After Test

Load (lbs)	Deformation (inch)	Area (sq.in)	Compressive Stress (ksf)	Axial Strain (%)
0	0.000	4.51	0.00	0.00
4	0.005	4.51	0.13	0.10
9	0.010	4.52	0.29	0.20
20	0.020	4.53	0.64	0.40
25	0.025	4.53	0.79	0.50
31	0.030	4.54	0.98	0.60
59	0.060	4.57	1.86	1.21
76	0.090	4.59	2.38	1.81
86	0.120	4.62	2.68	2.41
94	0.150	4.65	2.91	3.02
103	0.200	4.70	3.16	4.02
108	0.250	4.75	3.27	5.03
110	0.307	4.81	3.30	6.17
105	0.331	4.83	3.13	6.66
102	0.338	4.84	3.04	6.80

Unconfined Compressive Strength (ksf) = **3.30**

UNCONFINED COMPRESSION TEST RESULTS
ASTM D 2166

Project Name:	Darden Solar	Sample Type:	Mod Cal
Project No.:	60225172	Soil Description	Clay
Boring No.:	B-4	Dry Density (pcf):	92.1
Sample No.:	-	Moisture Content (%)	22.5
Depth (feet):	5-6.5	Test Date:	06/12/23
Sample Diameter (inch):	2.349	Wt. Wet Soil+Container(gms)	787
Sample Height (inch):	4.999	Wt. Dry Soil+Container(gms)	669.36
Sample Weight (gms):	641.71	Wt. Container (gms)	146.46



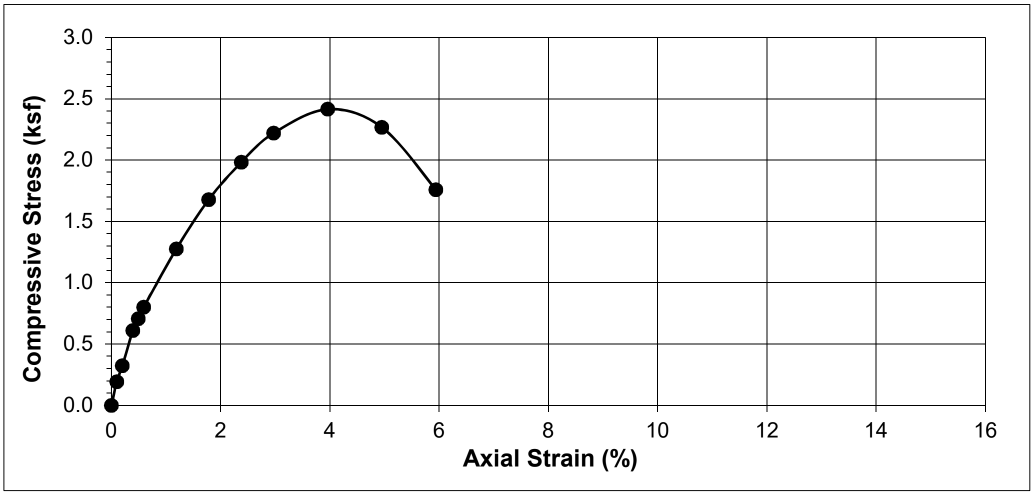
After Test

Load (lbs)	Deformation (inch)	Area (sq.in)	Compressive Stress (ksf)	Axial Strain (%)
0	0.000	4.33	0.00	0.00
9	0.005	4.34	0.30	0.10
16	0.010	4.34	0.53	0.20
27	0.020	4.35	0.89	0.40
33	0.025	4.35	1.09	0.50
36	0.030	4.36	1.19	0.60
65	0.060	4.39	2.13	1.20
89	0.090	4.41	2.90	1.80
115	0.120	4.44	3.73	2.40
124	0.150	4.47	4.00	3.00
92	0.200	4.51	2.94	4.00
60	0.233	4.54	1.90	4.66

Unconfined Compressive Strength (ksf) = **4.00**

UNCONFINED COMPRESSION TEST RESULTS
ASTM D 2166

Project Name:	Darden Solar	Sample Type:	Mod Cal
Project No.:	60225172	Soil Description	Clay
Boring No.:	B-25	Dry Density (pcf):	94.8
Sample No.:	-	Moisture Content (%)	23.8
Depth (feet):	2.5-4	Test Date:	06/12/23
Sample Diameter (inch):	2.385	Wt. Wet Soil+Container(gms)	841.39
Sample Height (inch):	5.048	Wt. Dry Soil+Container(gms)	708.12
Sample Weight (gms):	694.56	Wt. Container (gms)	147.89



After Test

Load (lbs)	Deformation (inch)	Area (sq.in)	Compressive Stress (ksf)	Axial Strain (%)
0	0.000	4.47	0.00	0.00
6	0.005	4.47	0.19	0.10
10	0.010	4.48	0.32	0.20
19	0.020	4.49	0.61	0.40
22	0.025	4.49	0.71	0.50
25	0.030	4.49	0.80	0.59
40	0.060	4.52	1.27	1.19
53	0.090	4.55	1.68	1.78
63	0.120	4.58	1.98	2.38
71	0.150	4.60	2.22	2.97
78	0.200	4.65	2.41	3.96
74	0.250	4.70	2.27	4.95
58	0.300	4.75	1.76	5.94

Unconfined Compressive Strength (ksf) = **2.41**

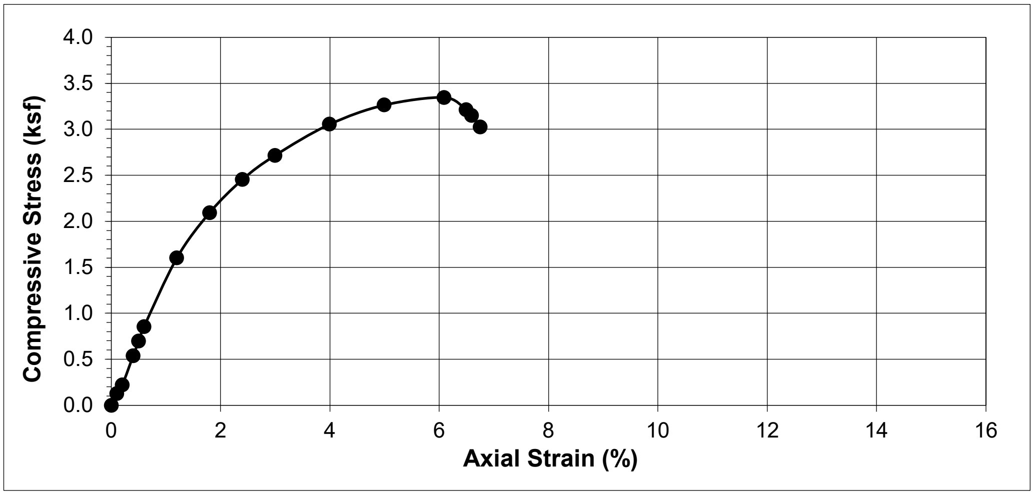
UNCONFINED COMPRESSION TEST RESULTS
ASTM D 2166

Project Name: Darden Solar
Project No.: 60225172
Boring No.: B-29
Sample No.: -
Depth (feet): 7.5

Sample Type: Mod Cal
Soil Description Clay
Dry Density (pcf): 89.6
Moisture Content (%) 30.0
Test Date: 03/20/23

Sample Diameter (inch): 2.400
Sample Height (inch): 5.009
Sample Weight (gms): 693.24

Wt. Wet Soil+Container(gms) 842.06
Wt. Dry Soil+Container(gms) 682.12
Wt. Container (gms) 149.86



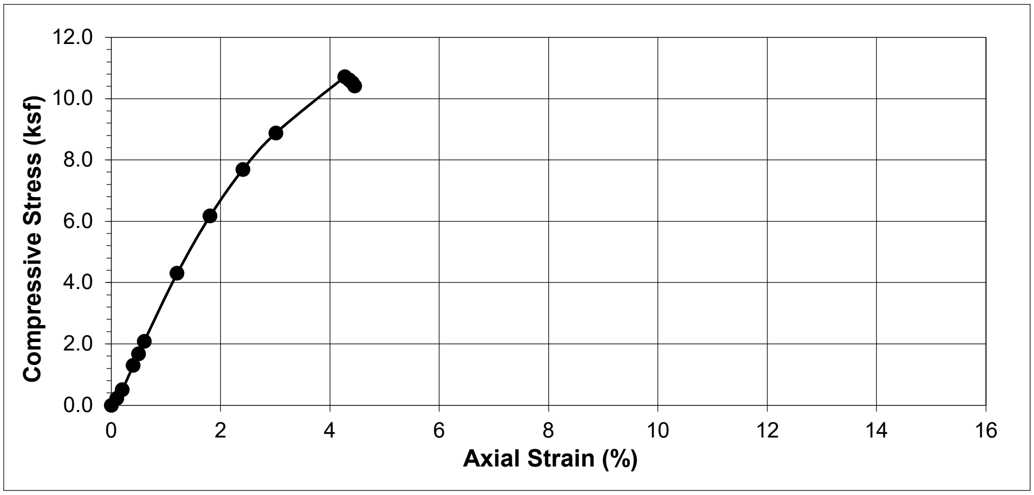
After Test

Load (lbs)	Deformation (inch)	Area (sq.in)	Compressive Stress (ksf)	Axial Strain (%)
0	0.000	4.53	0.00	0.00
4	0.005	4.53	0.13	0.10
7	0.010	4.53	0.22	0.20
17	0.020	4.54	0.54	0.40
22	0.025	4.55	0.70	0.50
27	0.030	4.55	0.85	0.60
51	0.060	4.58	1.60	1.20
67	0.090	4.61	2.09	1.80
79	0.120	4.64	2.45	2.40
88	0.150	4.66	2.72	2.99
100	0.200	4.71	3.06	3.99
108	0.250	4.76	3.27	4.99
112	0.305	4.82	3.35	6.09
108	0.325	4.84	3.21	6.49
106	0.330	4.84	3.15	6.59
102	0.338	4.85	3.03	6.75

Unconfined Compressive Strength (ksf) = **3.35**

UNCONFINED COMPRESSION TEST RESULTS
ASTM D 2166

Project Name:	Darden Solar	Sample Type:	Mod Cal
Project No.:	60225172	Soil Description	Clay
Boring No.:	B-57	Dry Density (pcf):	101.0
Sample No.:	-	Moisture Content (%)	16.8
Depth (feet):	2.5	Test Date:	03/20/23
Sample Diameter (inch):	2.402	Wt. Wet Soil+Container(gms)	837.68
Sample Height (inch):	4.984	Wt. Dry Soil+Container(gms)	737.77
Sample Weight (gms):	699.14	Wt. Container (gms)	142.53



After Test

Load (lbs)	Deformation (inch)	Area (sq.in)	Compressive Stress (ksf)	Axial Strain (%)
0	0.000	4.53	0.00	0.00
7	0.005	4.53	0.22	0.10
16	0.010	4.54	0.51	0.20
41	0.020	4.55	1.30	0.40
53	0.025	4.55	1.68	0.50
66	0.030	4.56	2.09	0.60
137	0.060	4.59	4.30	1.20
198	0.090	4.61	6.18	1.81
248	0.120	4.64	7.69	2.41
288	0.150	4.67	8.88	3.01
352	0.213	4.73	10.71	4.27
349	0.217	4.74	10.61	4.35
346	0.220	4.74	10.51	4.41
343	0.222	4.74	10.42	4.45

Unconfined Compressive Strength (ksf) = **10.71**

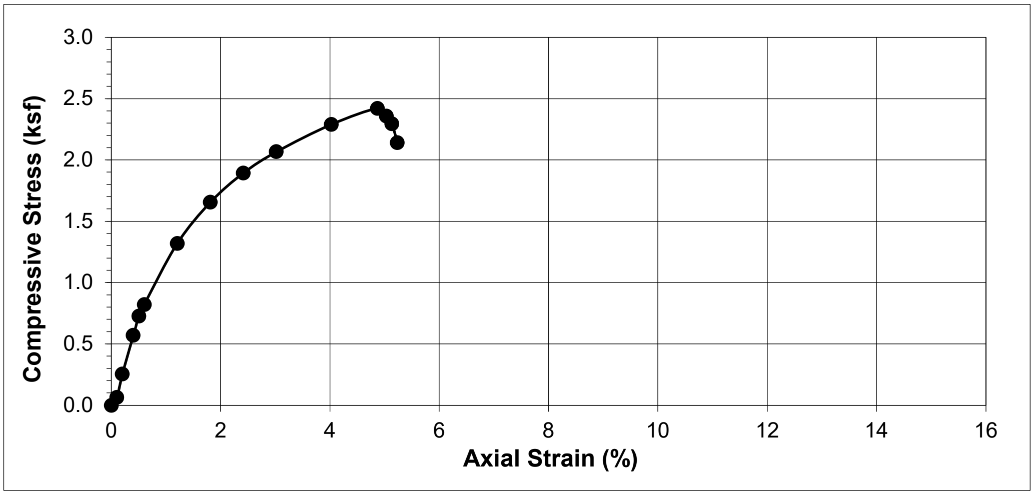
UNCONFINED COMPRESSION TEST RESULTS
ASTM D 2166

Project Name: Darden Solar
Project No.: 60225172
Boring No.: B-86
Sample No.: -
Depth (feet): 5

Sample Type: Mod Cal
Soil Description Clay
Dry Density (pcf): 90.6
Moisture Content (%) 28.1
Test Date: 03/20/23

Sample Diameter (inch): 2.400
Sample Height (inch): 4.968
Sample Weight (gms): 685.17

Wt. Wet Soil+Container(gms) 831.16
Wt. Dry Soil+Container(gms) 681.04
Wt. Container (gms) 147.22



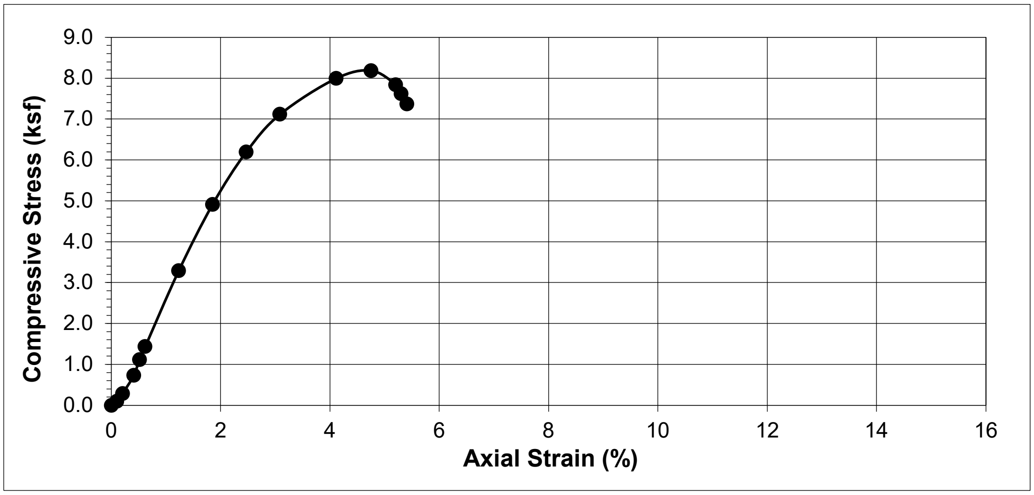
After Test

Load (lbs)	Deformation (inch)	Area (sq.in)	Compressive Stress (ksf)	Axial Strain (%)
0	0.000	4.53	0.00	0.00
2	0.005	4.53	0.06	0.10
8	0.010	4.53	0.25	0.20
18	0.020	4.54	0.57	0.40
23	0.025	4.55	0.73	0.50
26	0.030	4.55	0.82	0.60
42	0.060	4.58	1.32	1.21
53	0.090	4.61	1.66	1.81
61	0.120	4.64	1.89	2.42
67	0.150	4.67	2.07	3.02
75	0.200	4.71	2.29	4.03
80	0.242	4.76	2.42	4.87
78	0.250	4.76	2.36	5.03
76	0.255	4.77	2.29	5.13
71	0.260	4.78	2.14	5.23

Unconfined Compressive Strength (ksf) = **2.42**

UNCONFINED COMPRESSION TEST RESULTS
ASTM D 2166

Project Name:	Darden Solar	Sample Type:	Mod Cal
Project No.:	60225172	Soil Description	Clay
Boring No.:	B-114	Dry Density (pcf):	99.9
Sample No.:	-	Moisture Content (%)	22.9
Depth (feet):	5	Test Date:	03/20/23
Sample Diameter (inch):	2.391	Wt. Wet Soil+Container(gms)	846.73
Sample Height (inch):	4.864	Wt. Dry Soil+Container(gms)	715.53
Sample Weight (gms):	704.08	Wt. Container (gms)	143.38



After Test

Load (lbs)	Deformation (inch)	Area (sq.in)	Compressive Stress (ksf)	Axial Strain (%)
0	0.000	4.49	0.00	0.00
3	0.005	4.49	0.10	0.10
9	0.010	4.50	0.29	0.21
23	0.020	4.51	0.73	0.41
35	0.025	4.51	1.12	0.51
45	0.030	4.52	1.43	0.62
104	0.060	4.55	3.29	1.23
156	0.090	4.57	4.91	1.85
198	0.120	4.60	6.19	2.47
229	0.150	4.63	7.12	3.08
260	0.200	4.68	8.00	4.11
268	0.231	4.71	8.19	4.75
258	0.253	4.74	7.84	5.20
251	0.258	4.74	7.62	5.30
243	0.263	4.75	7.37	5.41

Unconfined Compressive Strength (ksf) = **8.19**

Geotherm USA

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September 6, 2023 (Revised September 7, 2023)

Terracon
23041 Avenida de la Carlota, Suite 350
Laguna Hills, CA 92653
Attn: Victor V. Nguyen

Re: Thermal Analysis of Native Soil Samples
Darden Solar – Cantua, CA (Project No. 60225172)

The following is the report of thermal dryout characterization tests conducted on the three (3) native soil samples from the referenced project sent to our laboratory.

Thermal Resistivity Tests: The samples were tested at either the 'optimum' or 'in-situ' moisture content, whichever was greater, and at 85% of the modified Proctor dry density ***provided by Terracon***. The tests were conducted in accordance with the IEEE standard 442-2017. The results are tabulated below and the thermal dryout curves are presented in **Figures 1 to 3.**

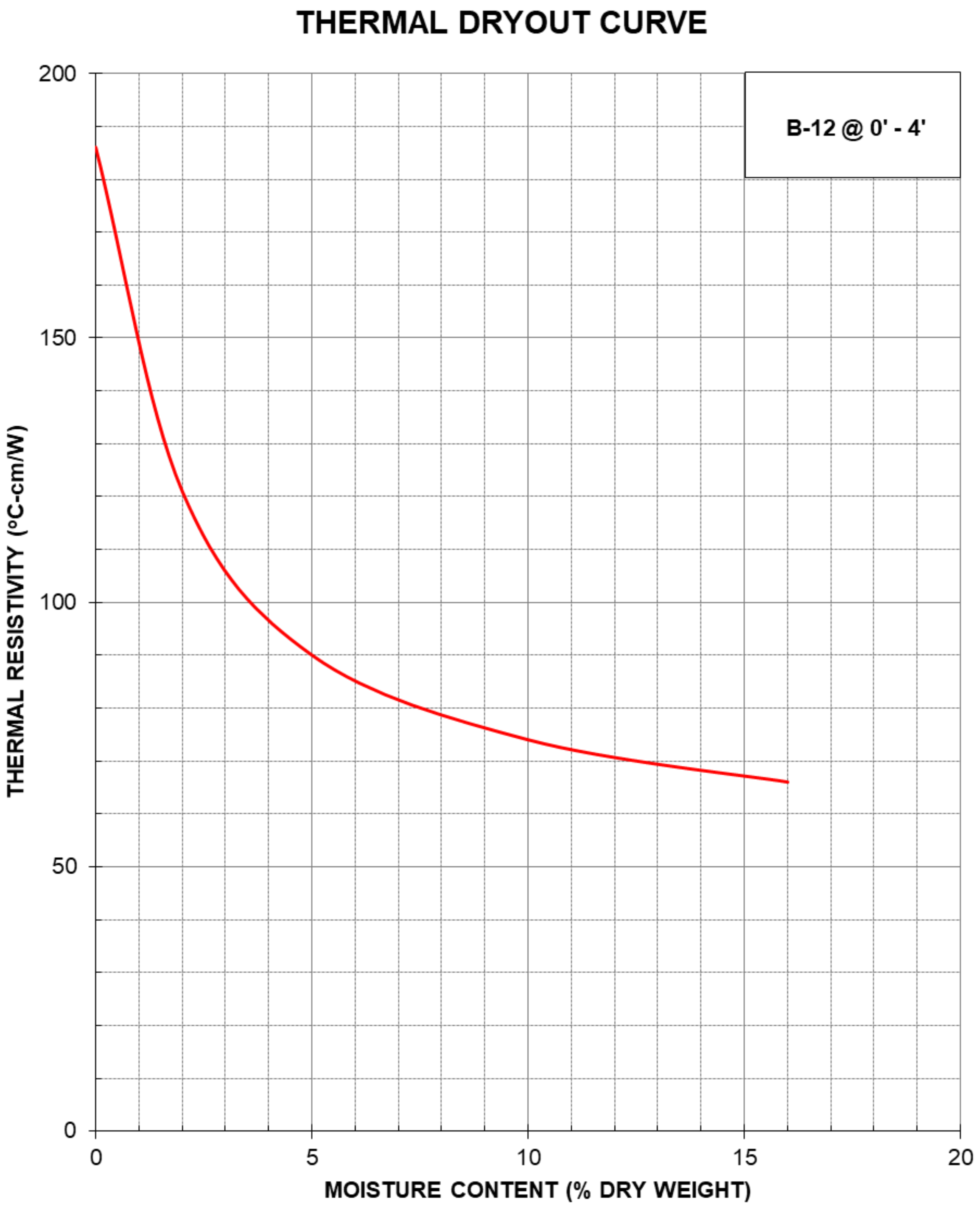
Sample ID, Description, Thermal Resistivity, Moisture Content and Density

Sample ID	Depth (ft)	Effort (%)	Description (Terracon)	Thermal Resistivity (°C-cm/W)		Moisture Content (%)	Dry Density (lb/ft^3)
				Wet	Dry		
B-12	0 – 4	85	Sandy Lean Clay (CL)	66	186	16	97
B-34	0 – 4	85	Sandy Lean Clay (CL)	62	178	17	97
B-53	0 – 4	85	Sandy Lean Clay (CL)	68	195	15	96

Please contact us if you have any questions or if we can be of further assistance.

Geotherm USA

Nimesh Patel



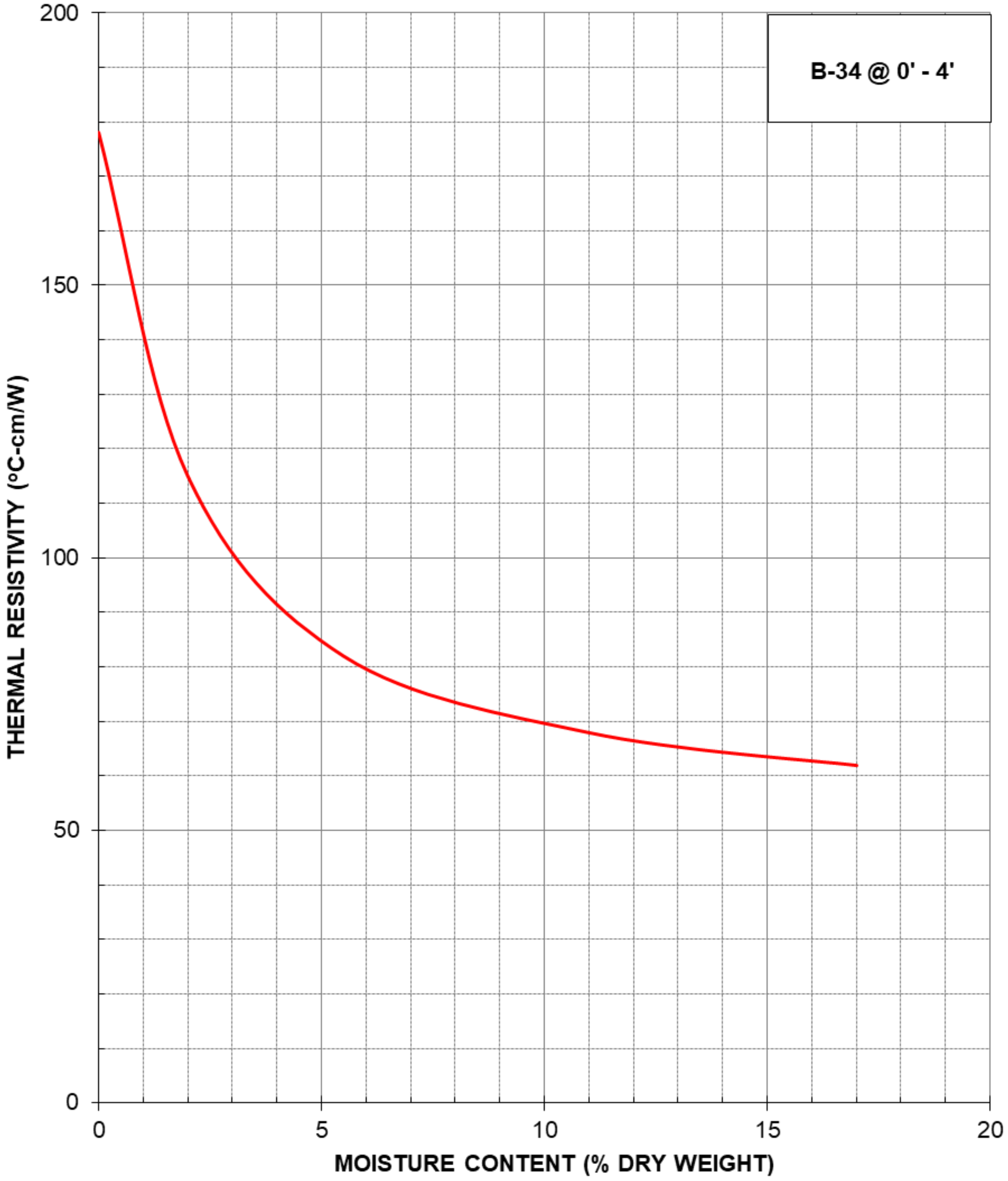
Terracon (Project No. 60225172)

Darden Solar – Coalinga, CA

Thermal Analysis of Native Soil Samples

September 2023 **Figure 1**

THERMAL DRYOUT CURVE

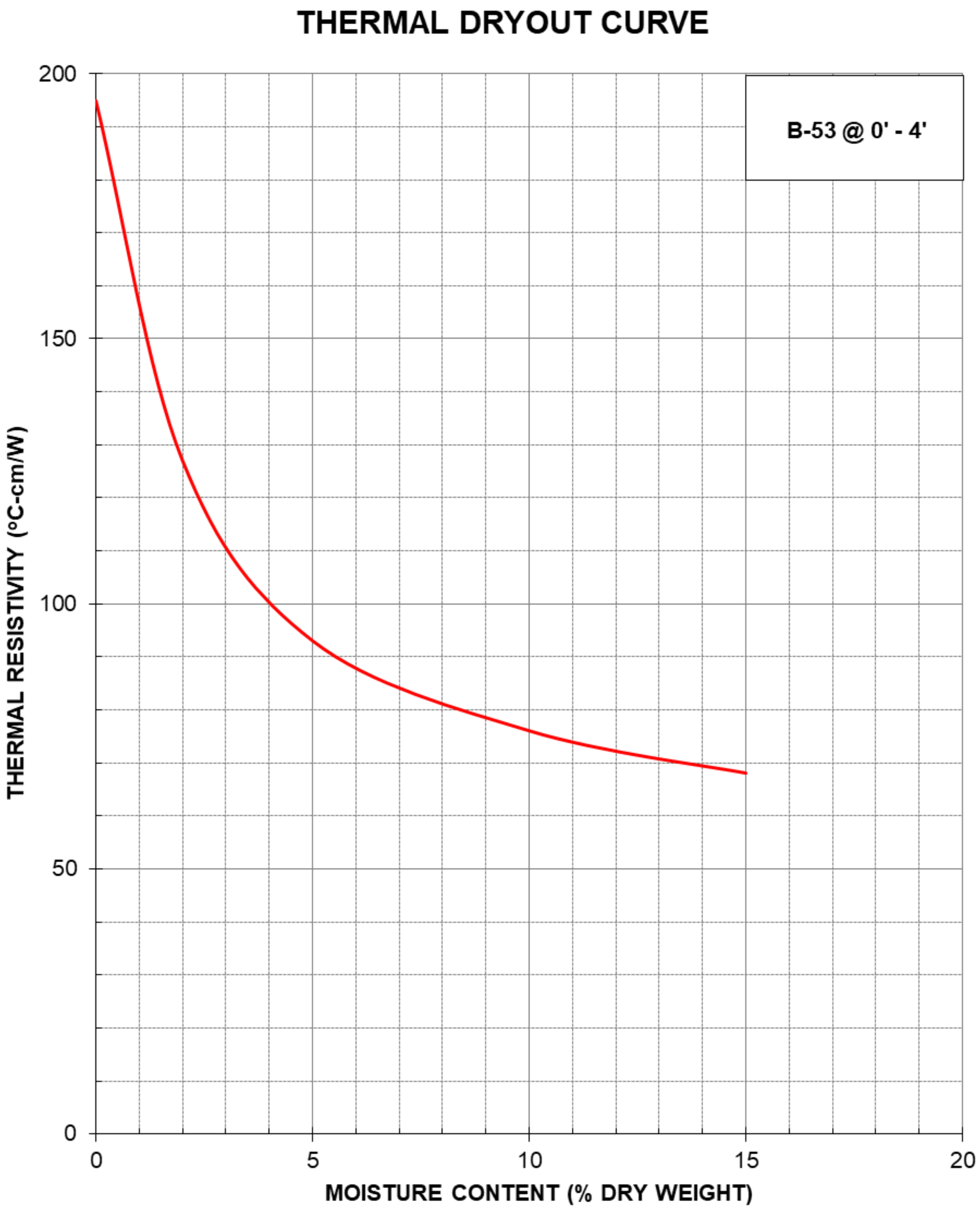


Terracon (Project No. 60225172)

Darden Solar – Coalinga, CA

Thermal Analysis of Native Soil Samples

September 2023 **Figure 2**



Terracon (Project No. 60225172)

Darden Solar – Coalinga, CA

Thermal Analysis of Native Soil Samples

September 2023 **Figure 3**

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April 24, 2023

Terracon
23041 Avenida de la Carlota, Suite 350
Laguna Hills, CA 92653
Attn: Victor V. Nguyen

Re: Thermal Analysis of Native Soil Samples
Darden Solar - Cantua Creek, CA (Project No. 60225172)

The following is the report of thermal dryout characterization tests conducted on seven (7) samples of native soil from the referenced project sent to our laboratory.

Thermal Resistivity Tests: The samples were tested at the 'specified' moisture content and 85% of the modified Proctor dry density ***provided by Terracon***. The tests were conducted in accordance with the IEEE standard 442-2017. The results are tabulated below and the thermal dryout curves are presented in **Figures 1 to 7.**

Sample ID, Description, Thermal Resistivity, Moisture Content and Density

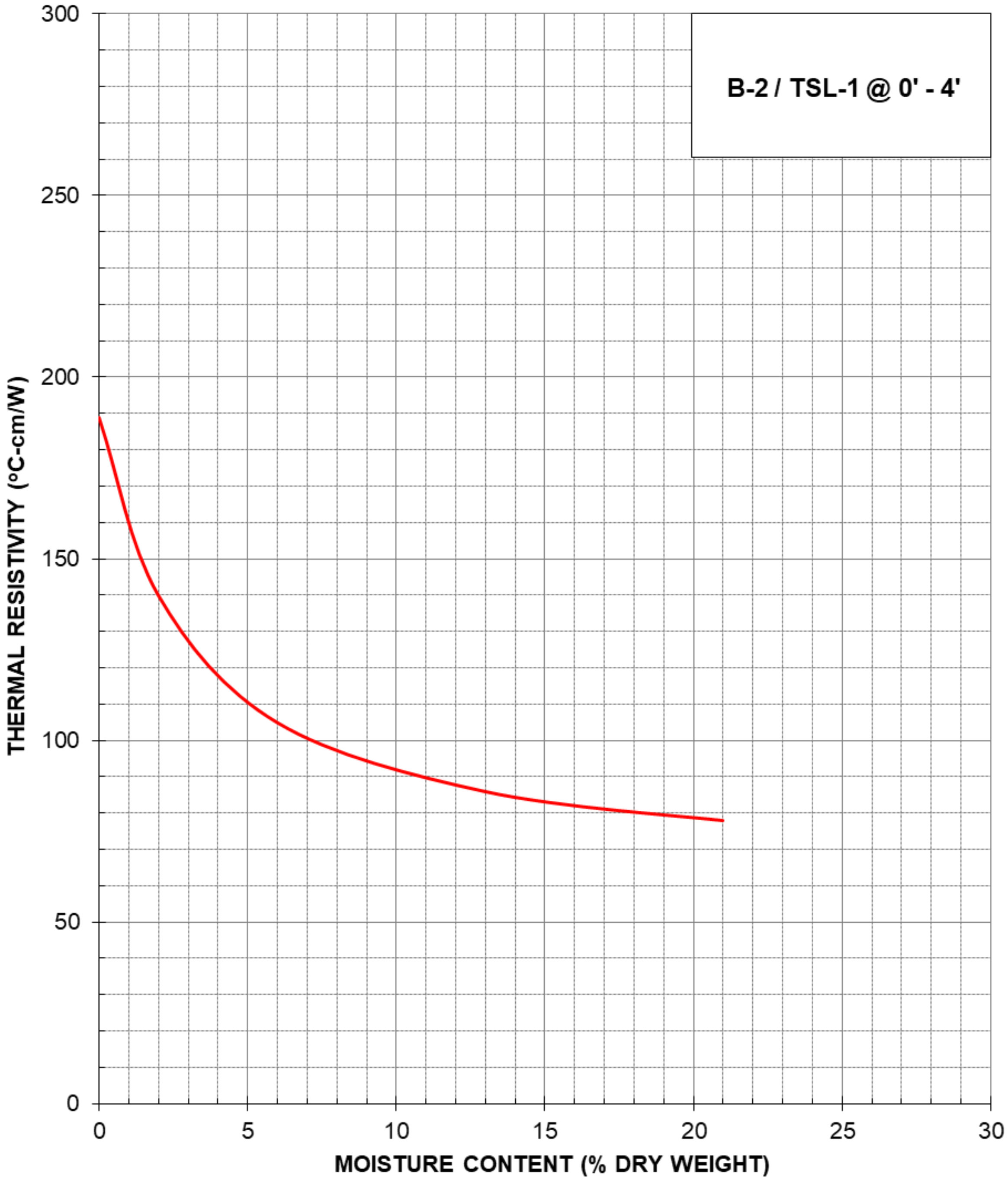
Sample ID	Depth (ft)	Description (*Terracon*)	Thermal Resistivity (°C-cm/W)		Moisture Content (%)	Dry Density (lb/ft^3)
			Wet	Dry		
B-2/TSL-1	0-4	(CL) Silty clay, Olive	78	189	21	99
B-35/TSL-21	0-4	(CL) Silty clay, Olive	92	248	20	90
B-37/TSL-5	0-4	(CL) Silty clay, Olive	82	212	21	97
B-83/TSL-9	0-4	(CL) Silty clay, Olive brown	84	206	20	95
B-104/TSL-12	0-4	(CL) Silty clay, Olive brown	94	217	16	96
B-116/TSL-13	0-4	(CL) Silty clay, Olive	90	224	19	94
B-121/TSL-10	0-4	(CL) Silty clay, Olive brown	93	229	25	93

Please contact us if you have any questions or if we can be of further assistance.

Geotherm USA

Nimesh Patel

THERMAL DRYOUT CURVE



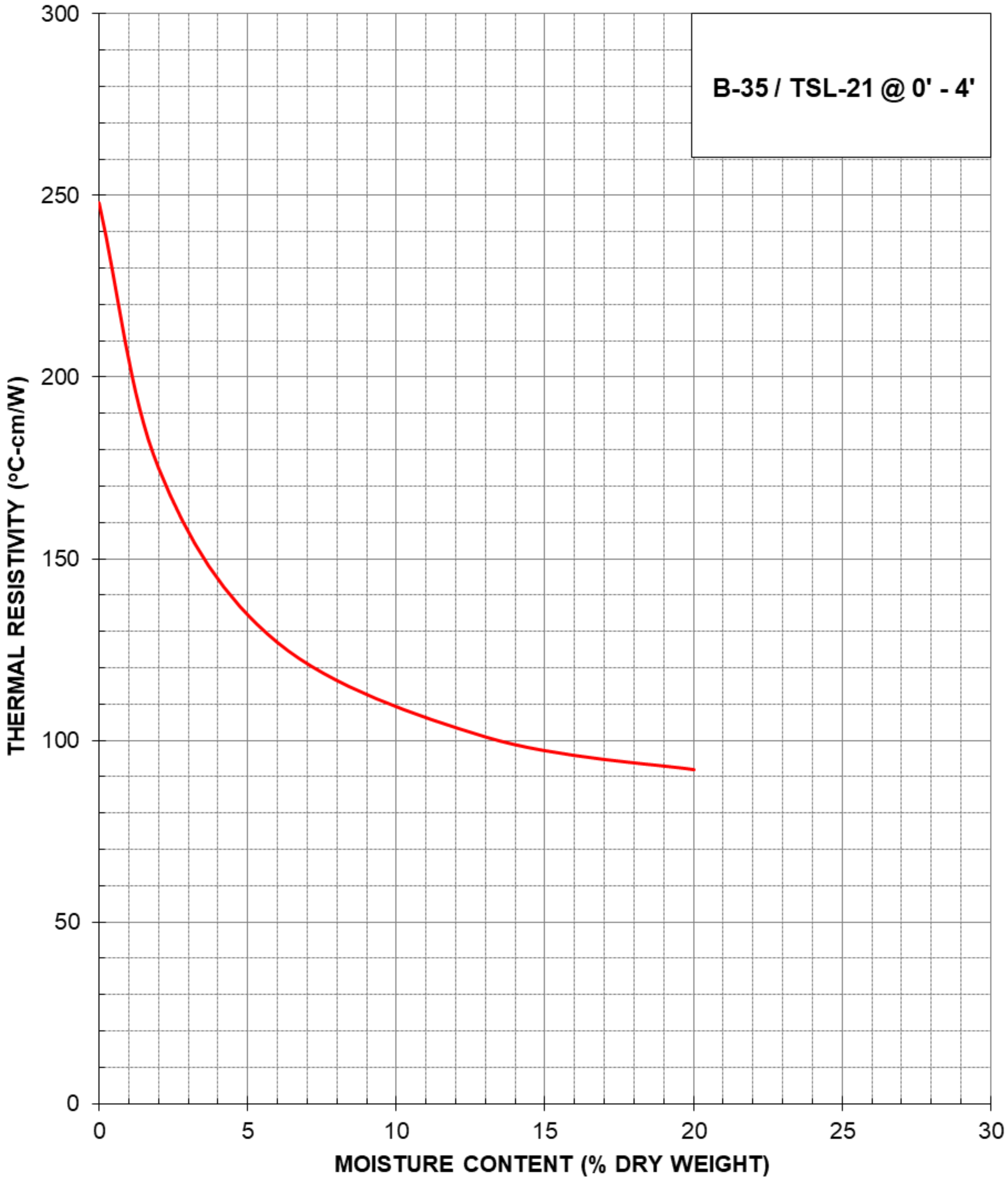
Terracon (Project No. 60225172)

Darden Solar - Cantua Creek, CA

Thermal Analysis of Native Soil Samples

April 2023 **Figure 1**

THERMAL DRYOUT CURVE



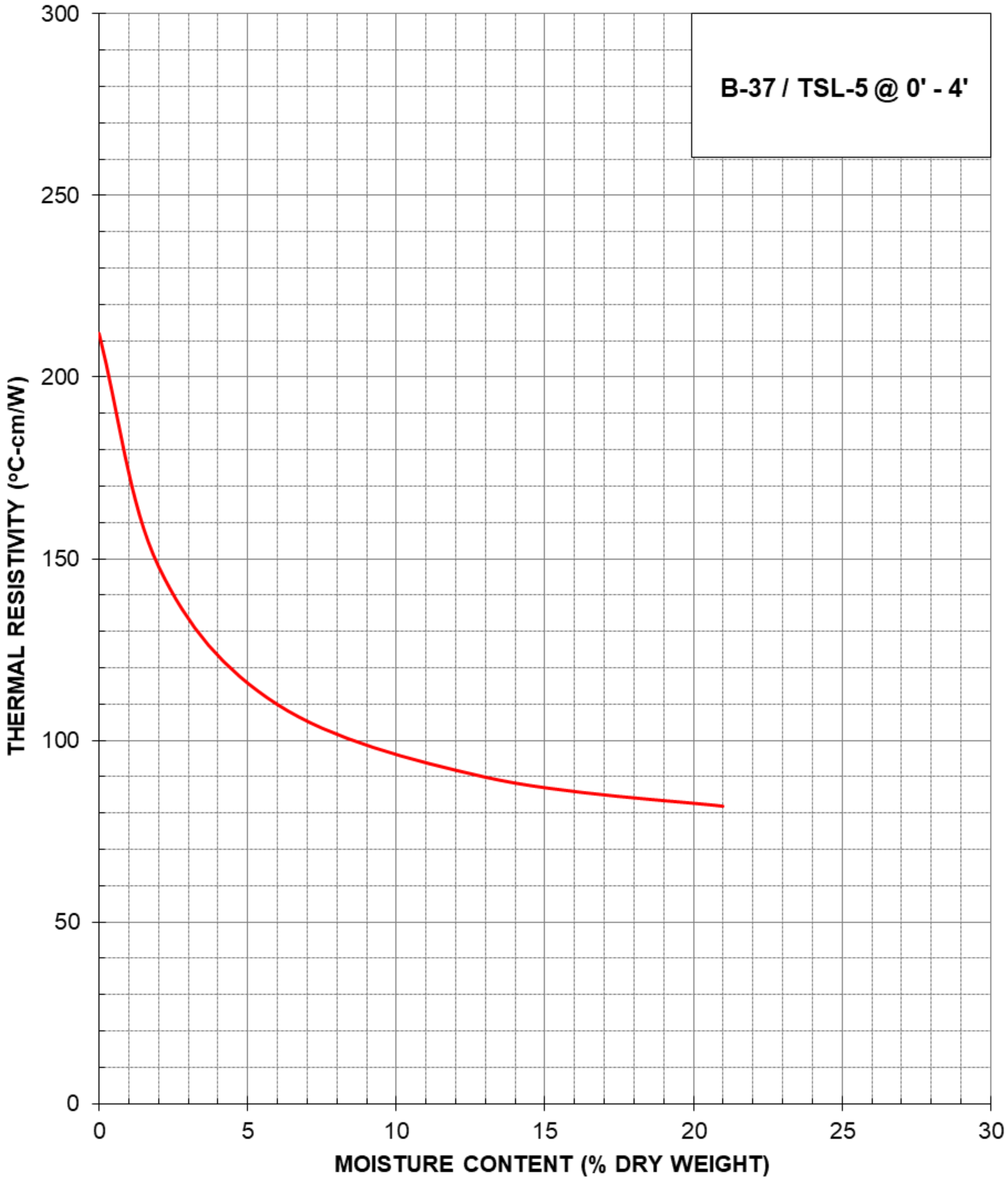
Terracon (Project No. 60225172)

Darden Solar - Cantua Creek, CA

Thermal Analysis of Native Soil Samples

April 2023 **Figure 2**

THERMAL DRYOUT CURVE



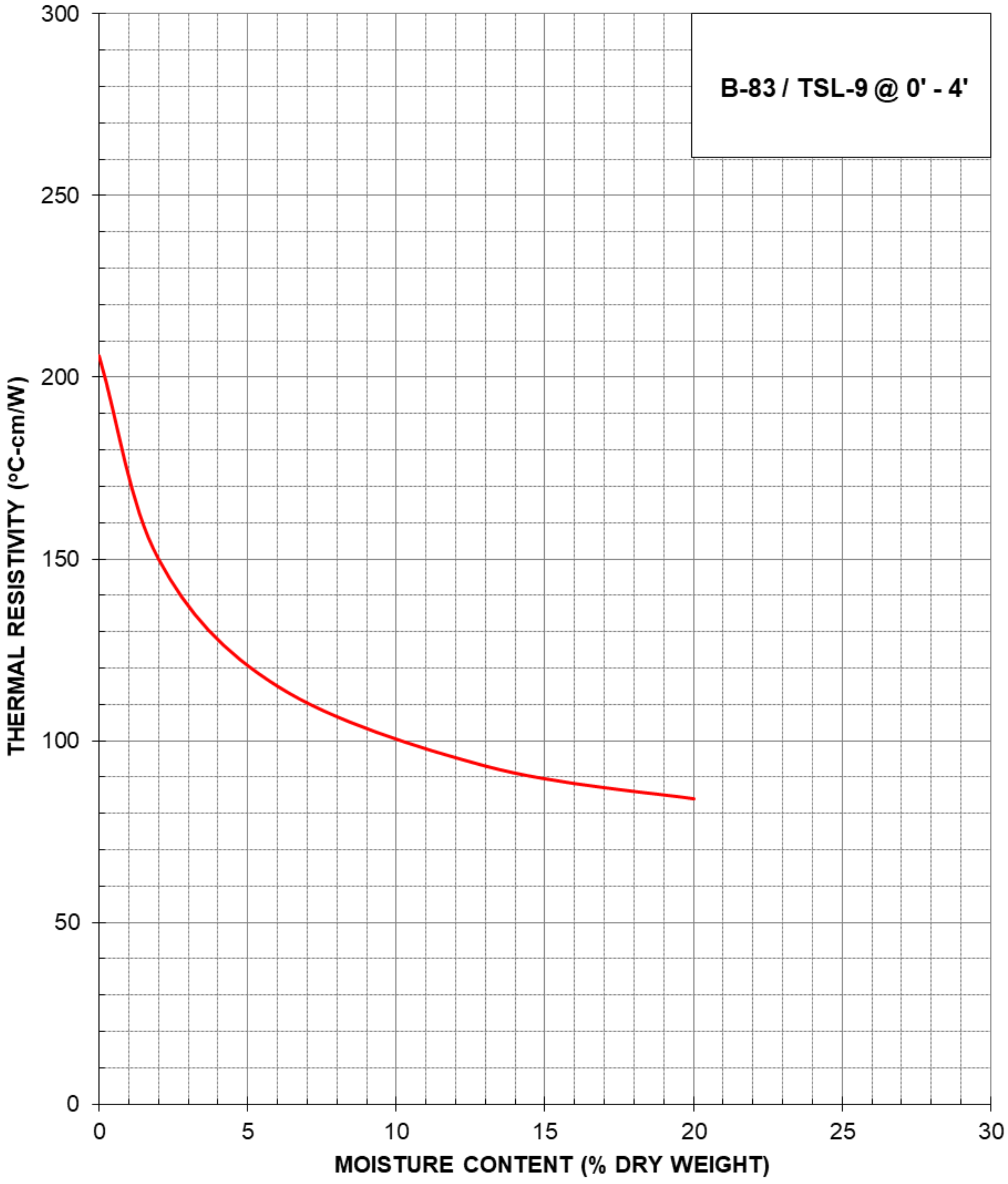
Terracon (Project No. 60225172)

Darden Solar - Cantua Creek, CA

Thermal Analysis of Native Soil Samples

April 2023 **Figure 3**

THERMAL DRYOUT CURVE

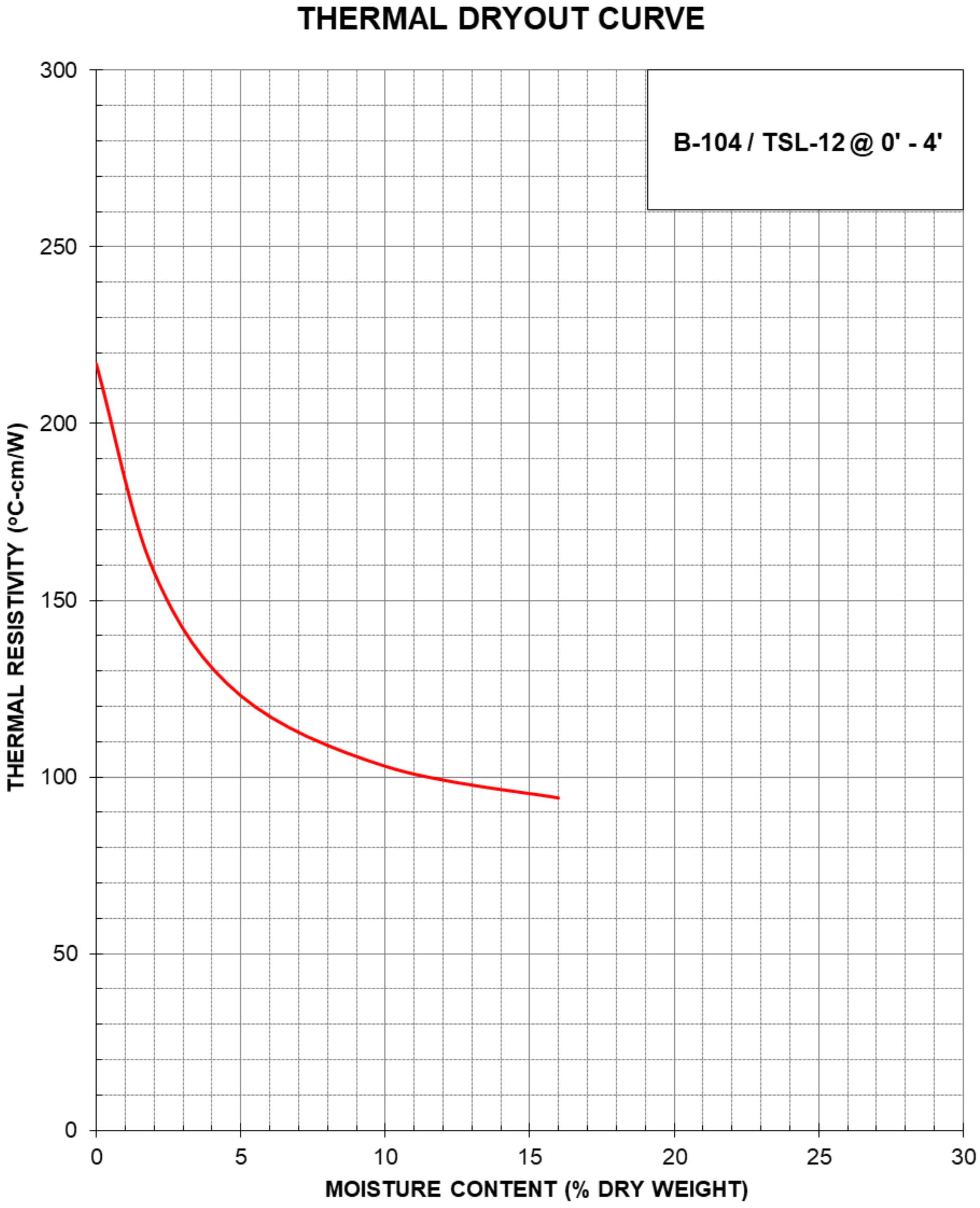


Terracon (Project No. 60225172)

Darden Solar - Cantua Creek, CA

Thermal Analysis of Native Soil Samples

April 2023 **Figure 4**



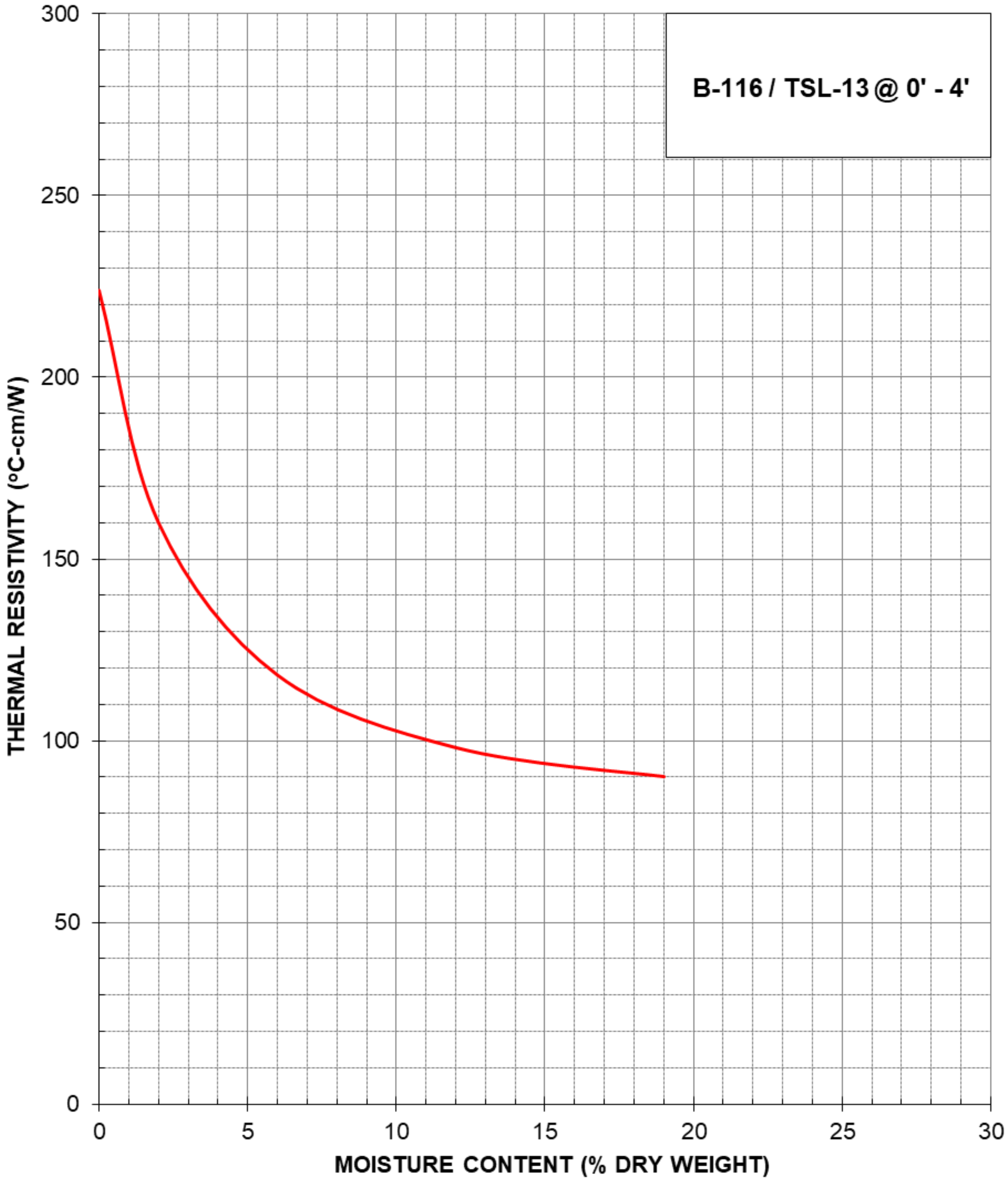
Terracon (Project No. 60225172)

Darden Solar - Cantua Creek, CA

Thermal Analysis of Native Soil Samples

April 2023 **Figure 5**

THERMAL DRYOUT CURVE



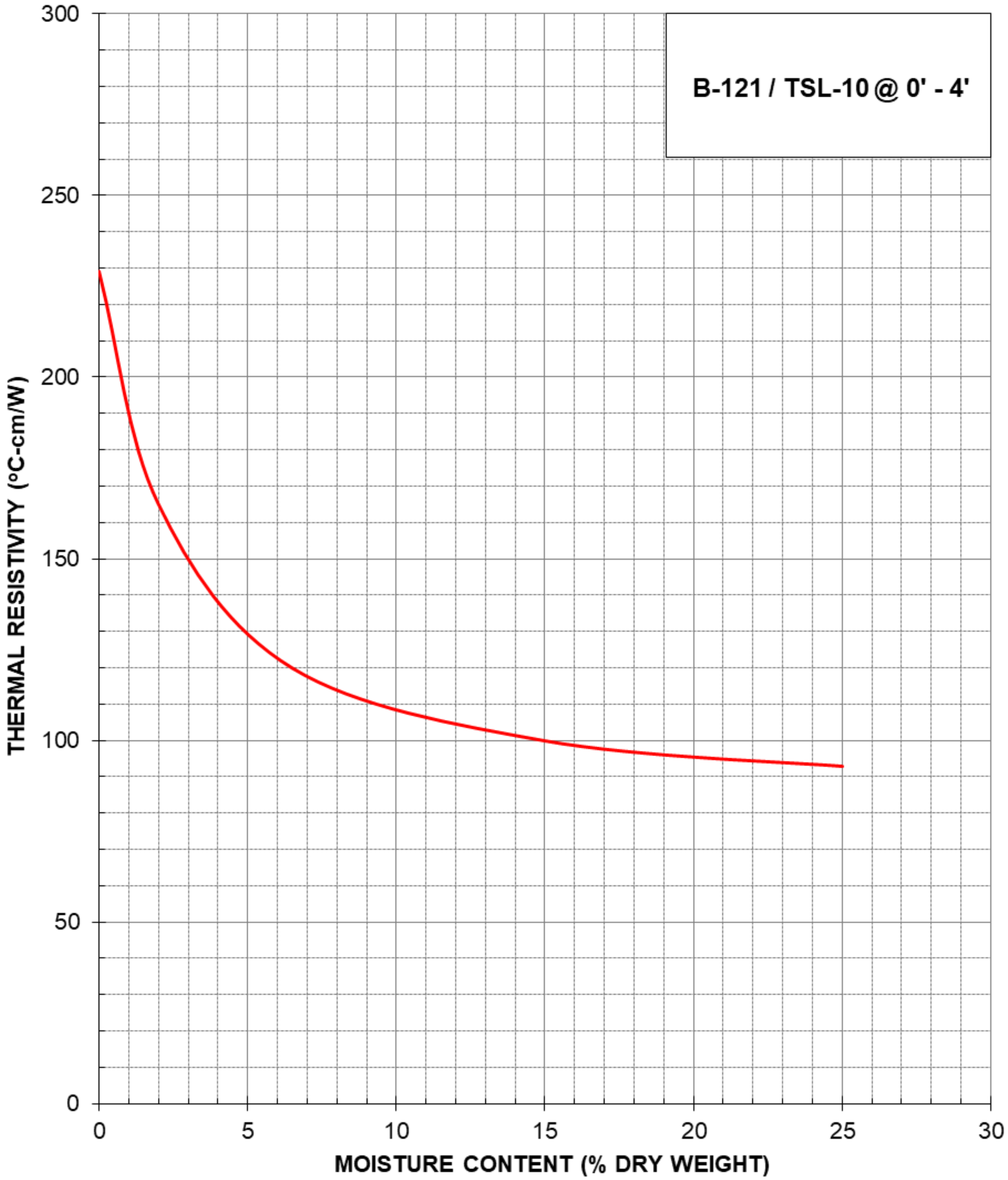
Terracon (Project No. 60225172)

Darden Solar - Cantua Creek, CA

Thermal Analysis of Native Soil Samples

April 2023 **Figure 6**

THERMAL DRYOUT CURVE



Terracon (Project No. 60225172)

Darden Solar - Cantua Creek, CA

Thermal Analysis of Native Soil Samples

April 2023 **Figure 7**

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June 26, 2023 (Revised August 21, 2023)

Terracon
23041 Avenida de la Carlota, Suite 350
Laguna Hills, CA 92653
Attn: Victor V. Nguyen

Re: Thermal Analysis of Native Soil Samples
Darden Solar – Fresno County, CA (Project No. 60225172)

The following is the report of thermal dryout characterization tests conducted on twelve (12) native soil samples from the referenced project sent to our laboratory.

Thermal Resistivity Tests: The samples were tested at either the optimum or in-situ moisture content, whichever was greater and 85% of the modified Proctor dry density ***provided by Terracon***. In addition, samples Sub-1 and BESS-1 were tested at 90% of the Modifies Proctor dry density. The tests were conducted in accordance with the IEEE standard 442-2017. The results are tabulated below and the thermal dryout curves are presented in **Figures 1 to 12.**

Sample ID, Description, Thermal Resistivity, Moisture Content and Density

Sample ID	Depth (ft)	Effort (%)	Description (Terracon)	Thermal Resistivity (°C-cm/W)		Moisture Content (%)	Dry Density (lb/ft^3)
				Wet	Dry		
B-10	0-4	85	Olive, silty clay	80	185	13	101
B-25	1-5	85	Olive, silty clay	87	198	14	96
B-46	0-4	85	Olive, silty clay	89	222	16	94
B-49	0-4	85	Olive, silty clay	90	216	16	94
B-71	0-4	85	Olive, silty clay	87	209	15	96
B-76	0-4	85	Olive, silty clay	94	223	16	93
B-102	0-4	85	Olive, silty clay	91	225	15	94

Sample ID, Description, Thermal Resistivity, Moisture Content and Density

Sample ID	Depth (ft)	Effort (%)	Description (Terracon)	Thermal Resistivity (°C-cm/W)		Moisture Content (%)	Dry Density (lb/ft^3)
				Wet	Dry		
B-106	0-4	85	Olive, silty clay	94	235	17	92
B-127	0-4	85	Olive, silty clay	86	207	16	96
B-132	0-4	85	Olive, silty clay	92	218	17	93
Sub-1	0-4	90	Olive, silty clay	83	205	18	100
BESS-1	0-4	90	Olive, silty clay	87	182	15	102

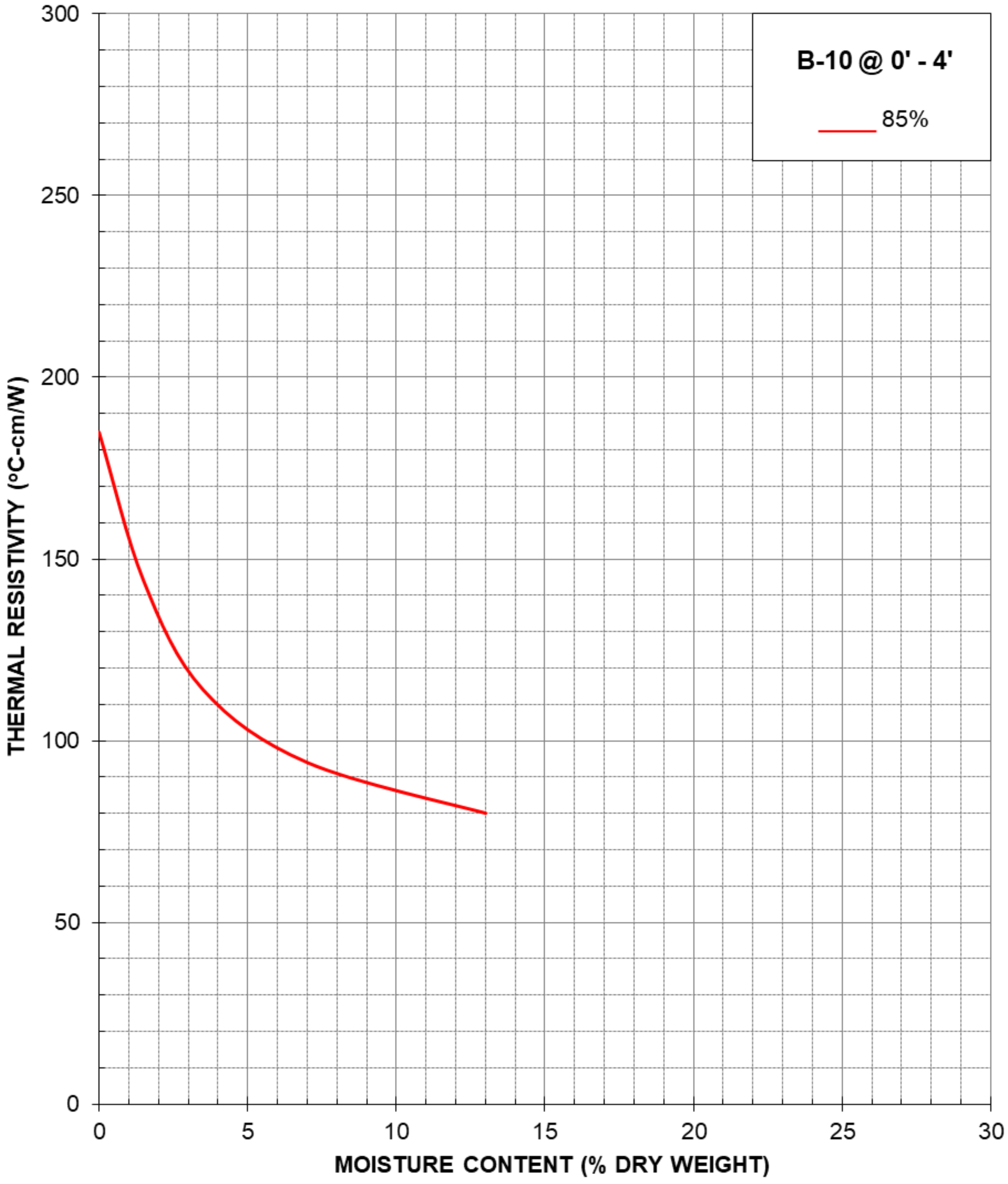
Comments: The thermal characteristic depicted in the dryout curves apply for the soils at their respective test dry density.

Please contact us if you have any questions or if we can be of further assistance.

Geotherm USA

Nimesh Patel

THERMAL DRYOUT CURVE



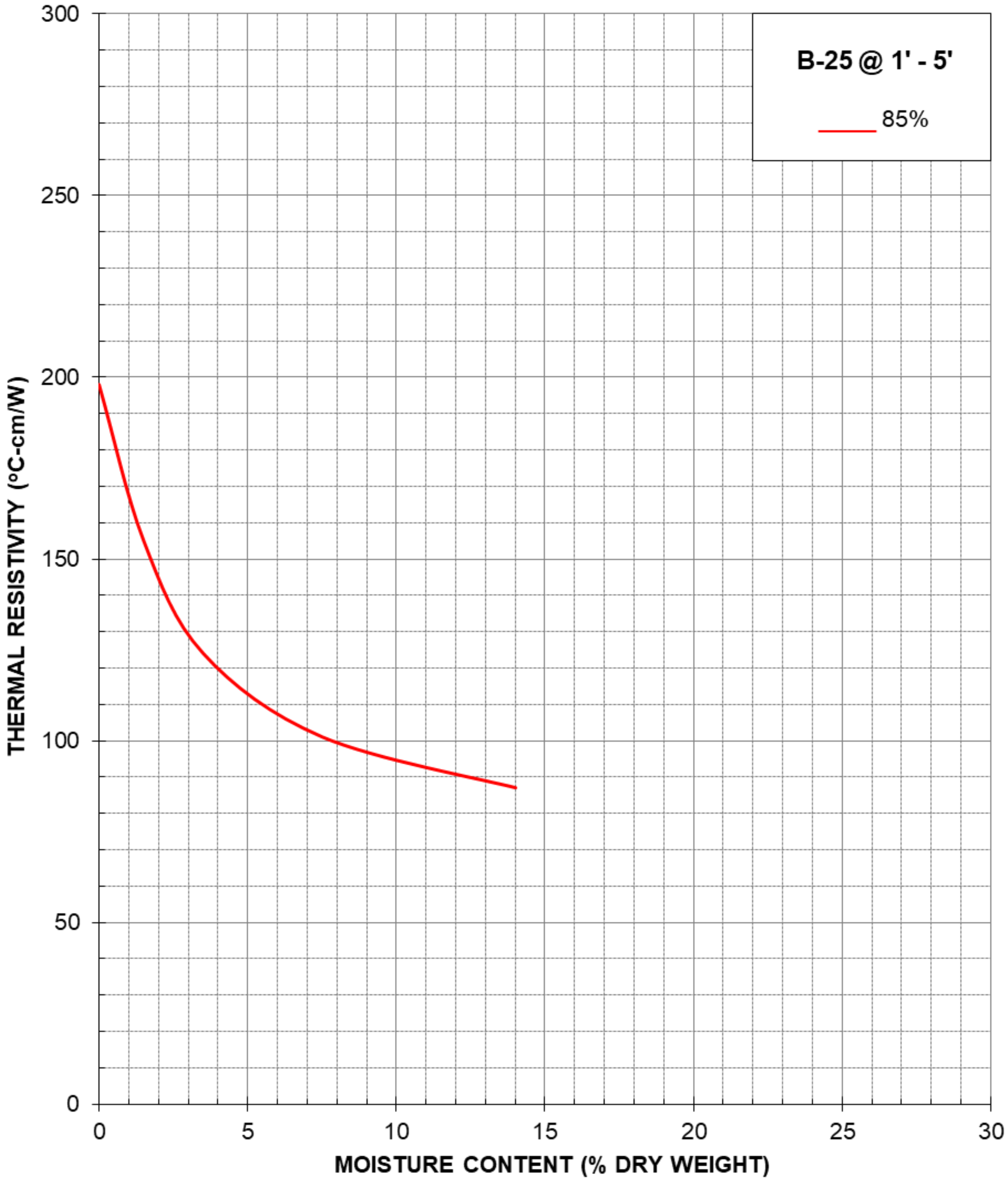
Terracon (Project No. 60225172)

Darden Solar – Fresno County, CA

Thermal Analysis of Native Soil Samples

June 2023 **Figure 1**

THERMAL DRYOUT CURVE



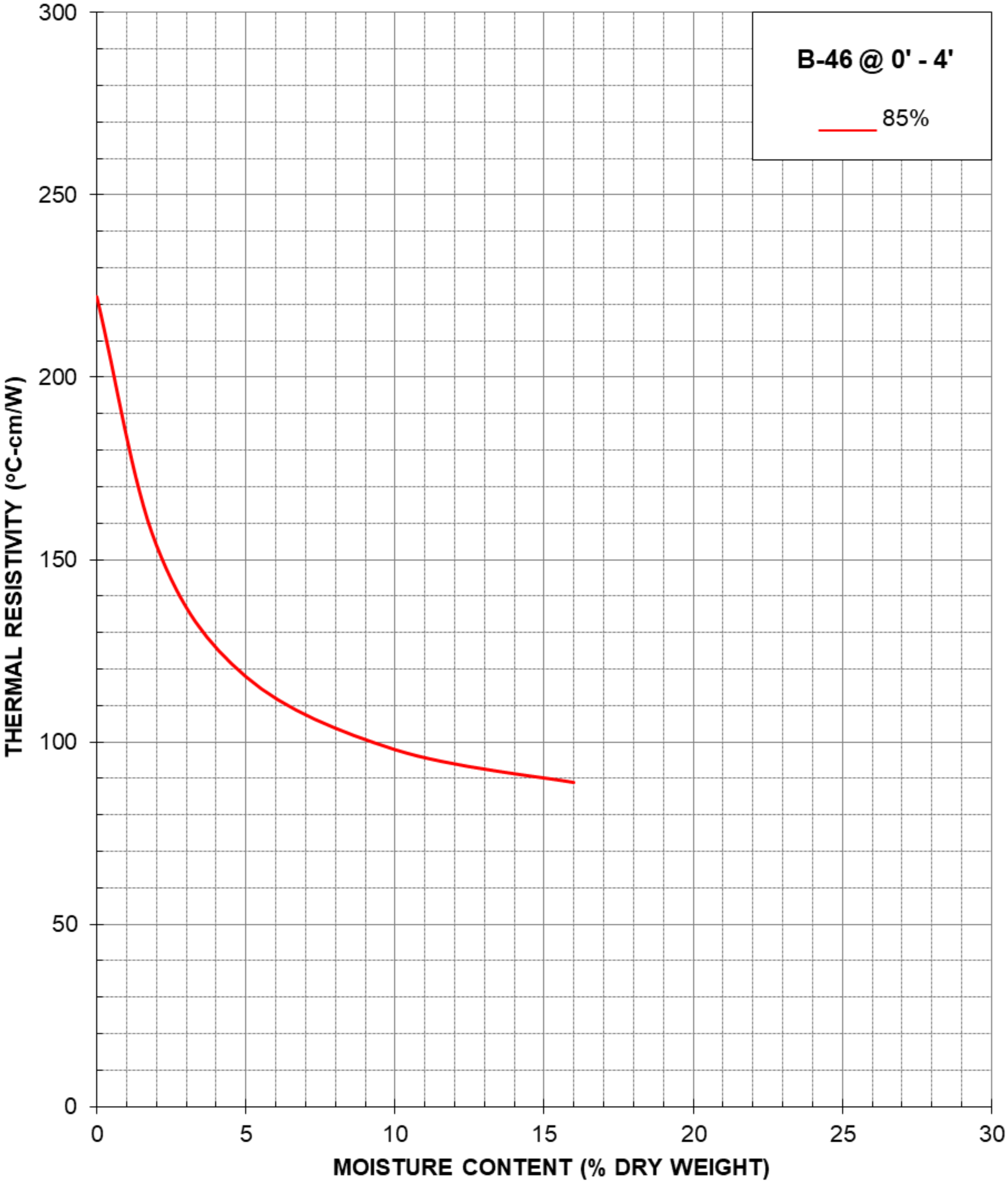
Terracon (Project No. 60225172)

Darden Solar – Fresno County, CA

Thermal Analysis of Native Soil Samples

June 2023 **Figure 2**

THERMAL DRYOUT CURVE



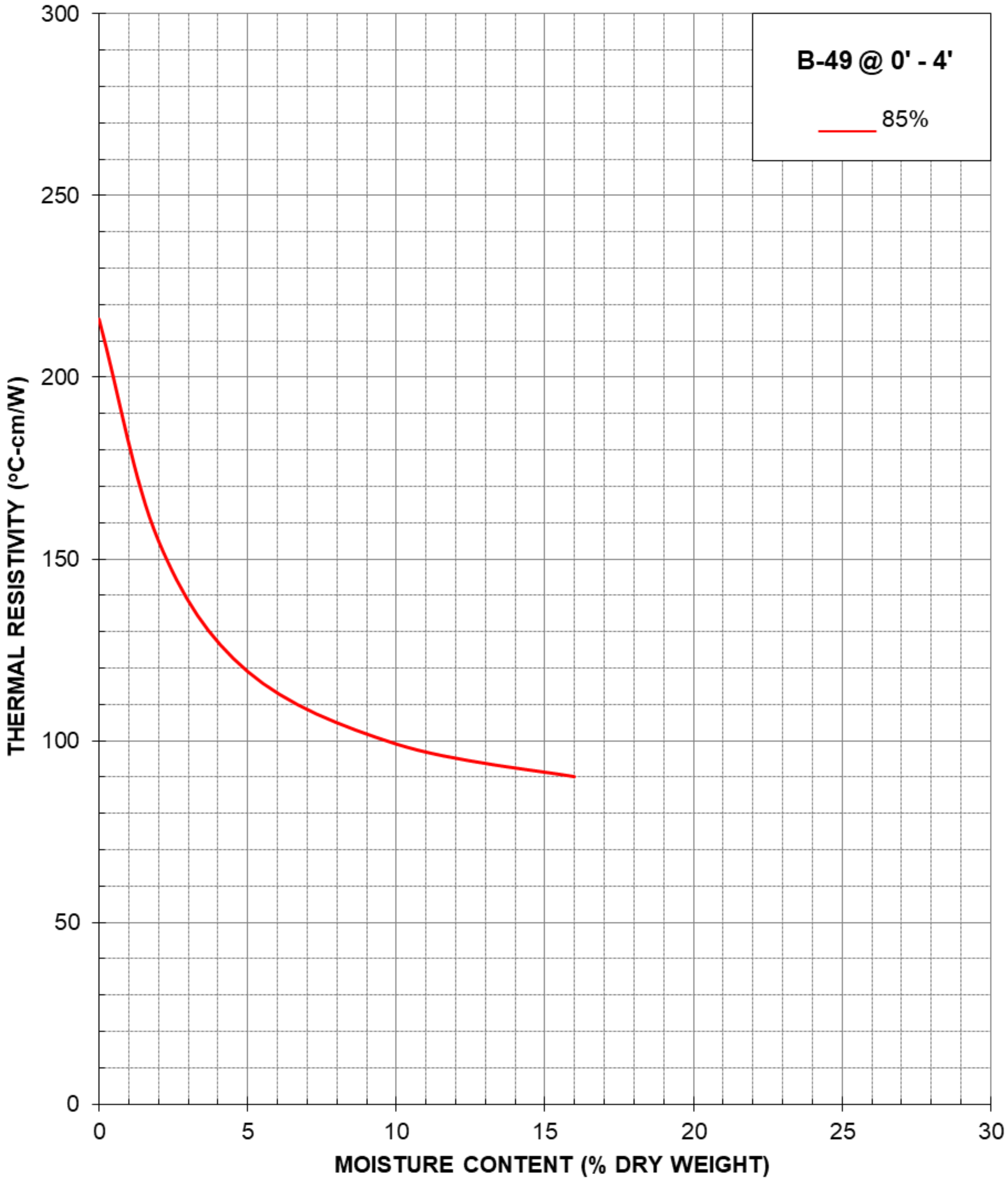
Terracon (Project No. 60225172)

Darden Solar – Fresno County, CA

Thermal Analysis of Native Soil Samples

June 2023 **Figure 3**

THERMAL DRYOUT CURVE



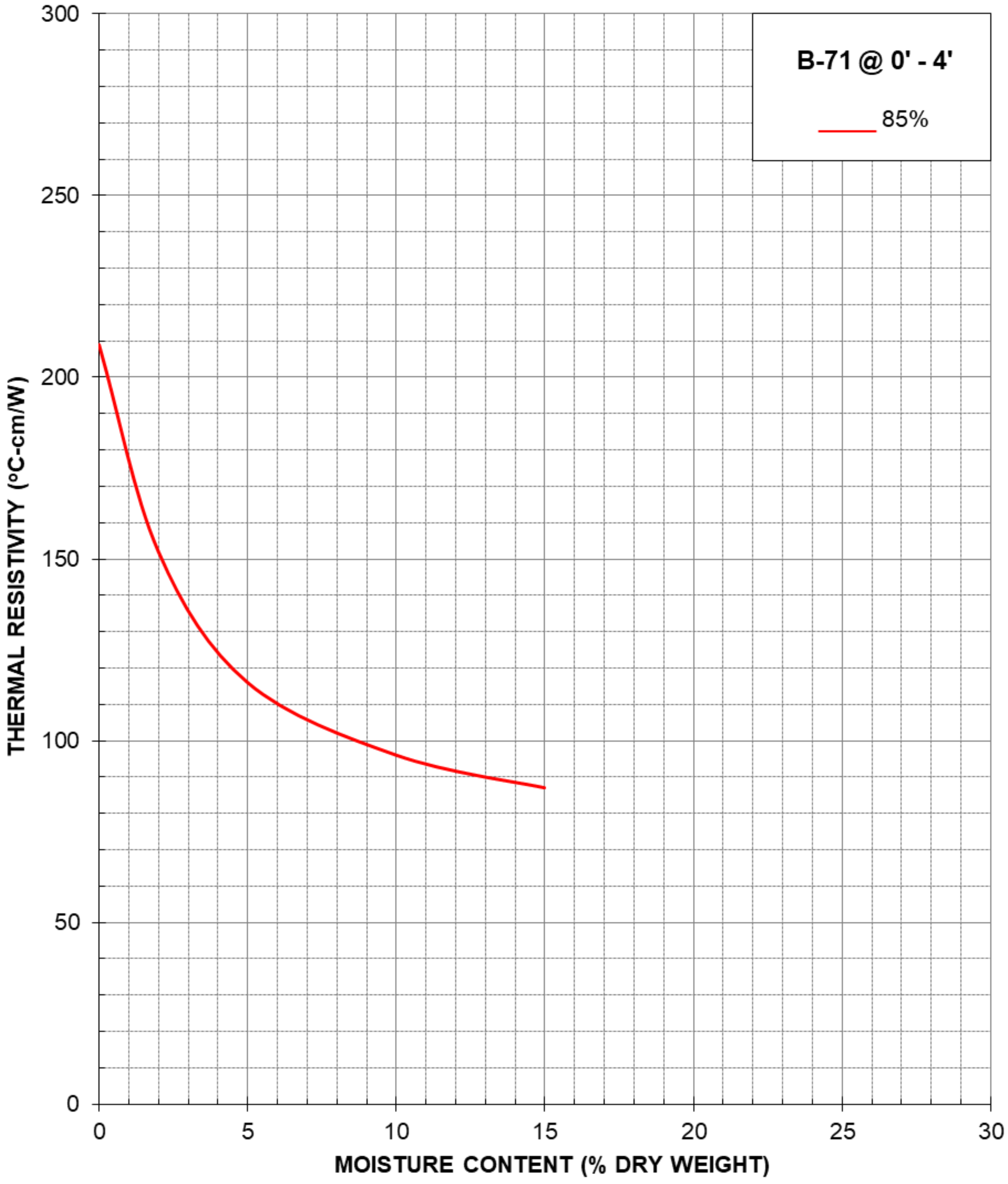
Terracon (Project No. 60225172)

Darden Solar – Fresno County, CA

Thermal Analysis of Native Soil Samples

June 2023 **Figure 4**

THERMAL DRYOUT CURVE



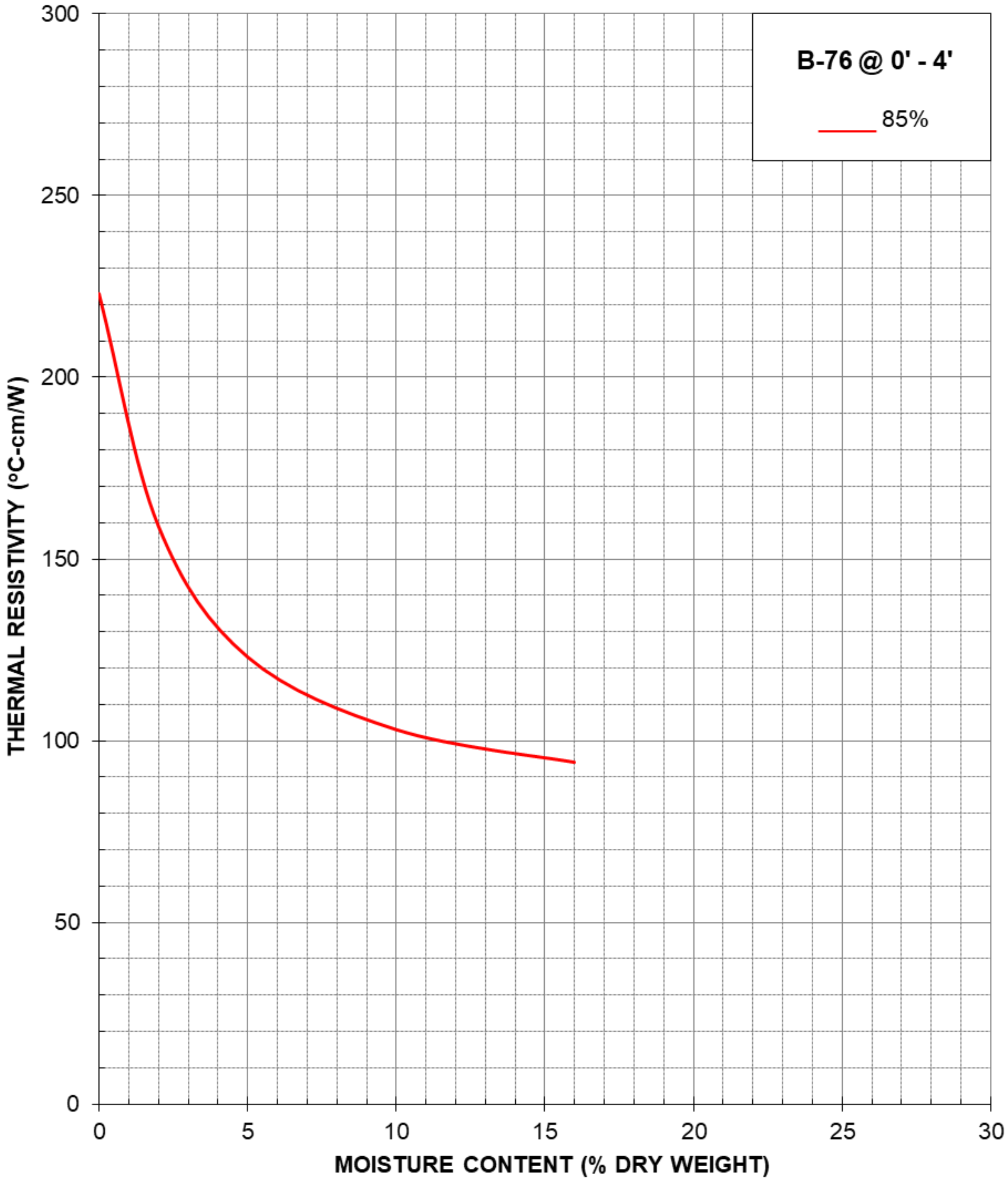
Terracon (Project No. 60225172)

Darden Solar – Fresno County, CA

Thermal Analysis of Native Soil Samples

June 2023 **Figure 5**

THERMAL DRYOUT CURVE



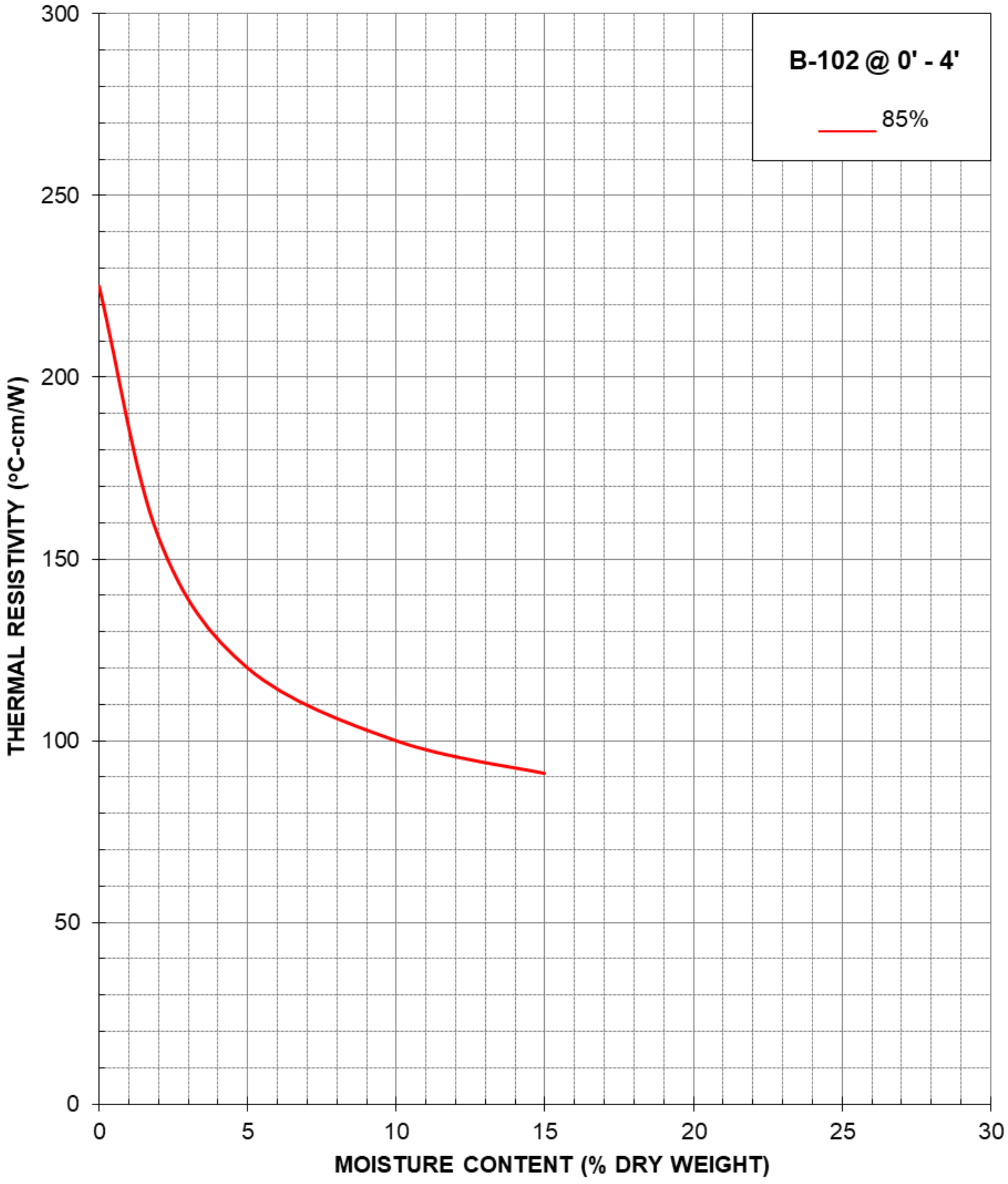
Terracon (Project No. 60225172)

Darden Solar – Fresno County, CA

Thermal Analysis of Native Soil Samples

June 2023 **Figure 6**

THERMAL DRYOUT CURVE

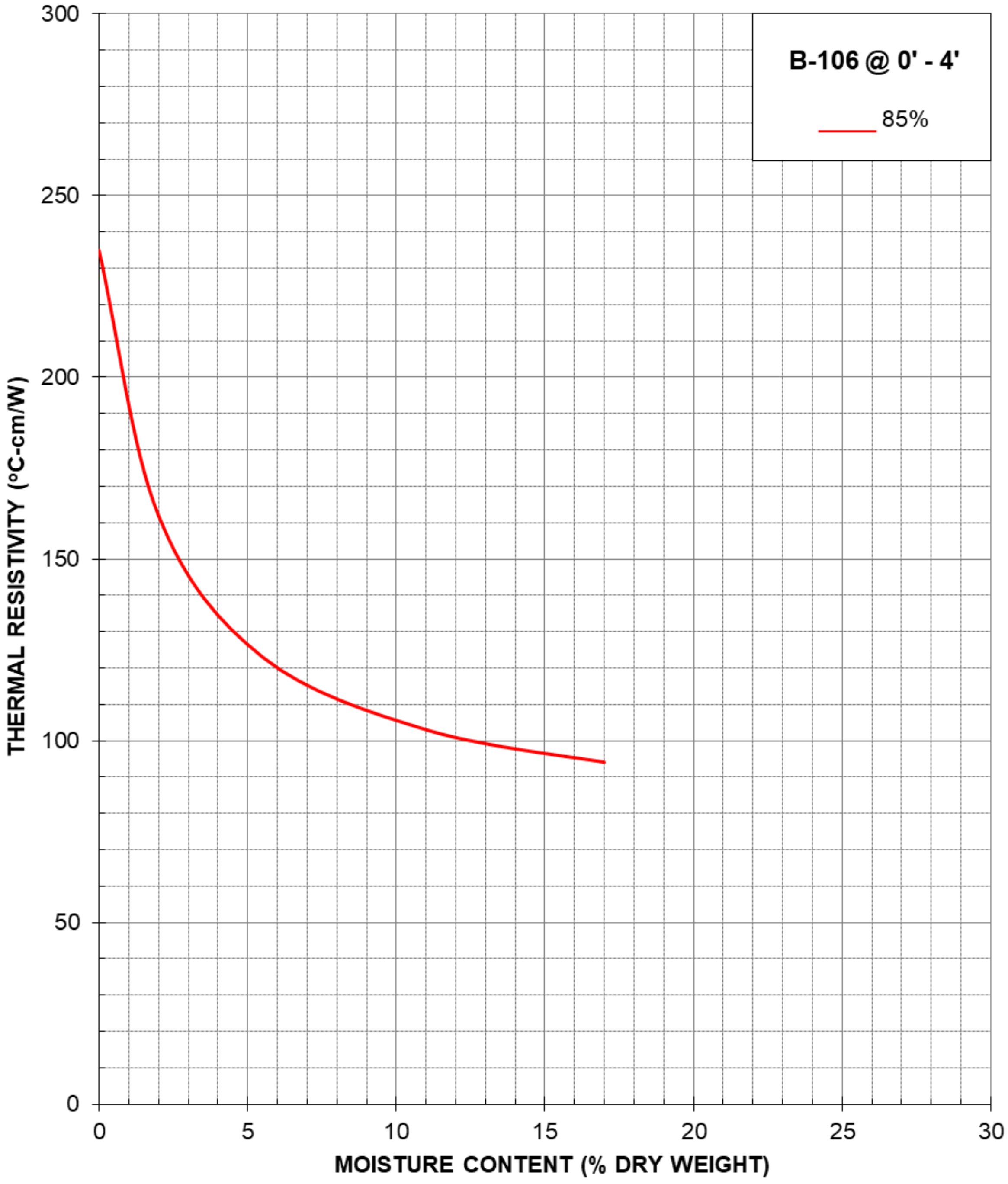


Terracon (Project No. 60225172)

Darden Solar – Fresno County, CA

Thermal Analysis of Native Soil Samples

THERMAL DRYOUT CURVE



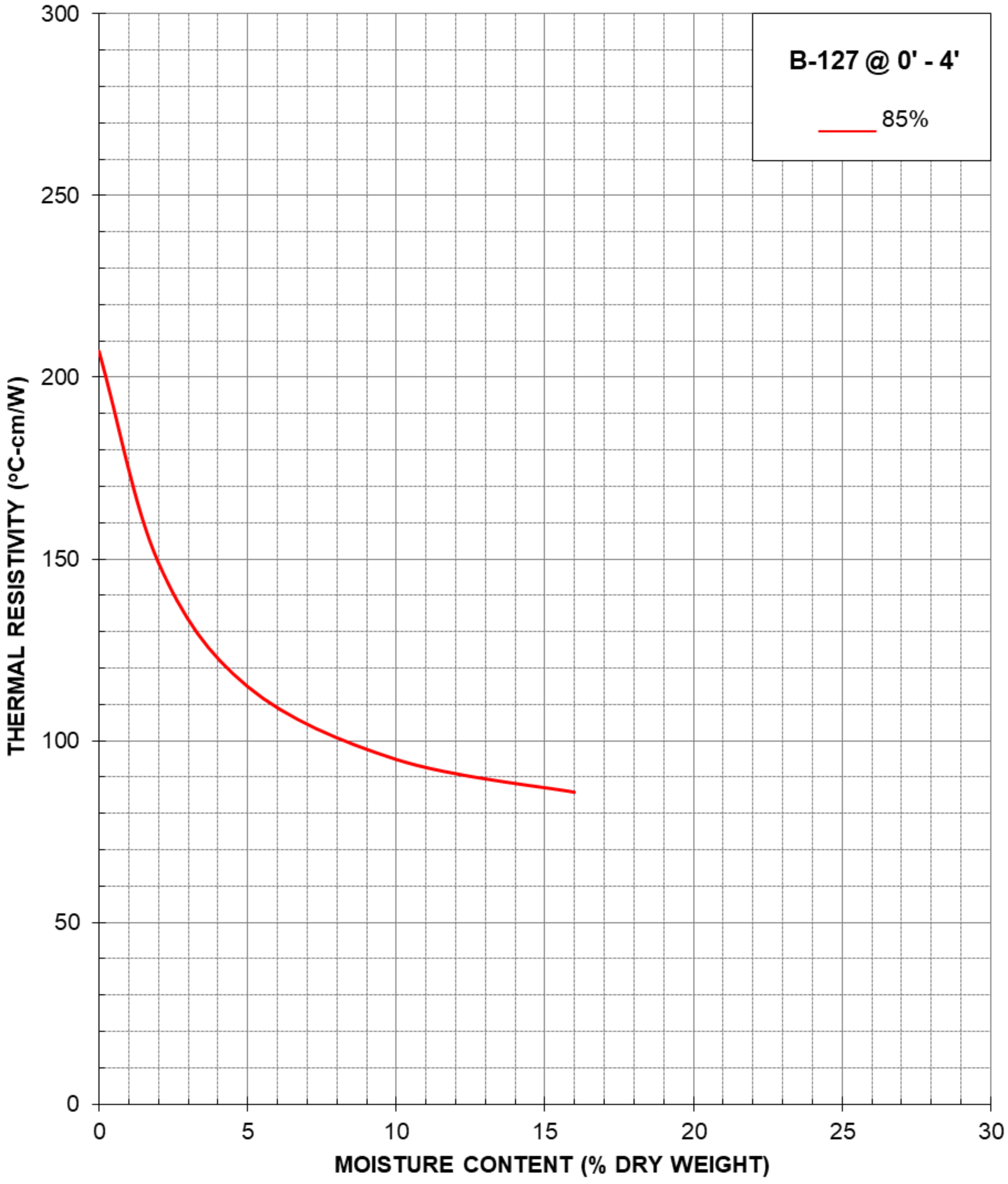
Terracon (Project No. 60225172)

Darden Solar – Fresno County, CA

Thermal Analysis of Native Soil Samples

June 2023 **Figure 8**

THERMAL DRYOUT CURVE

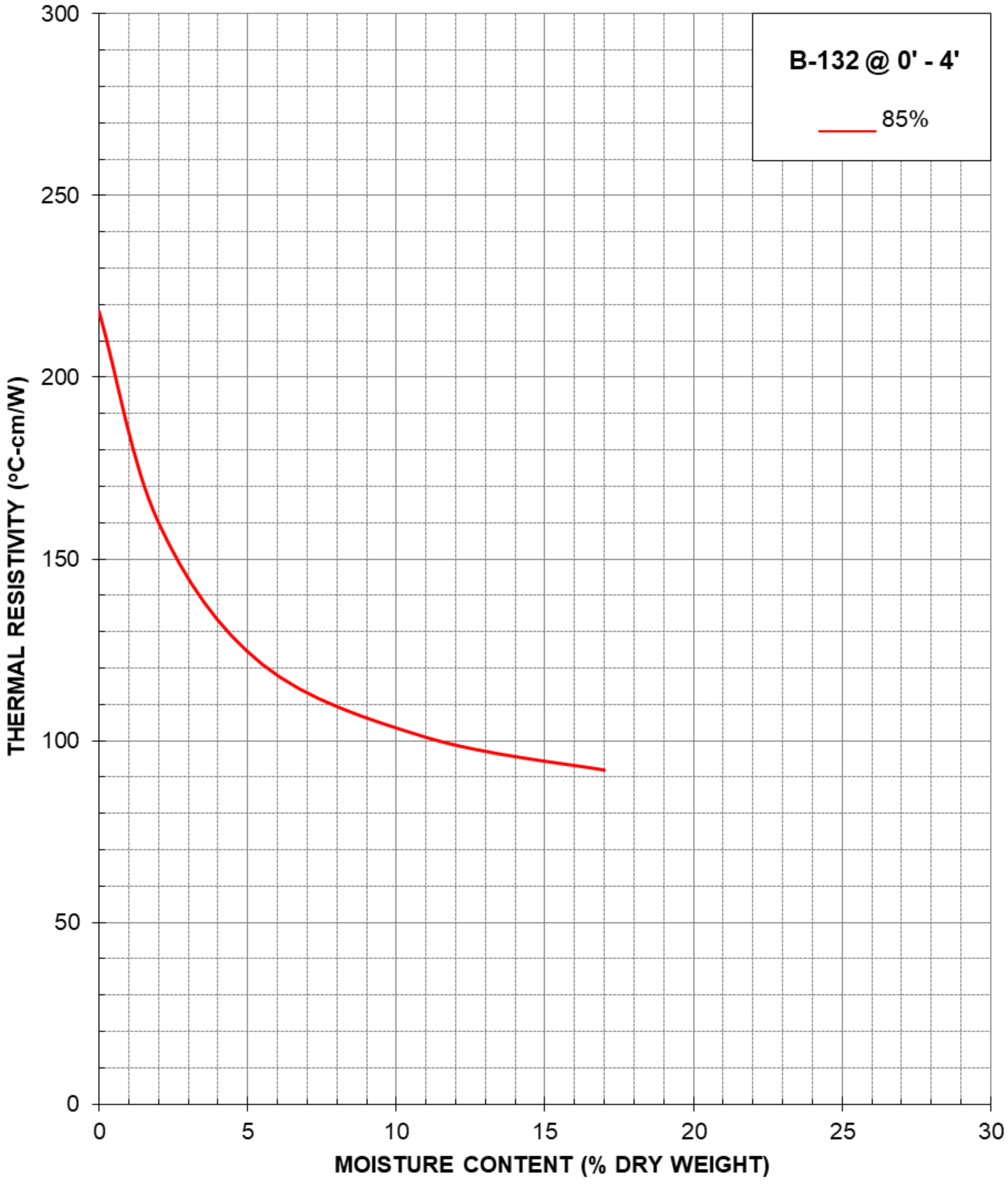


Terracon (Project No. 60225172)

Darden Solar – Fresno County, CA

Thermal Analysis of Native Soil Samples

THERMAL DRYOUT CURVE



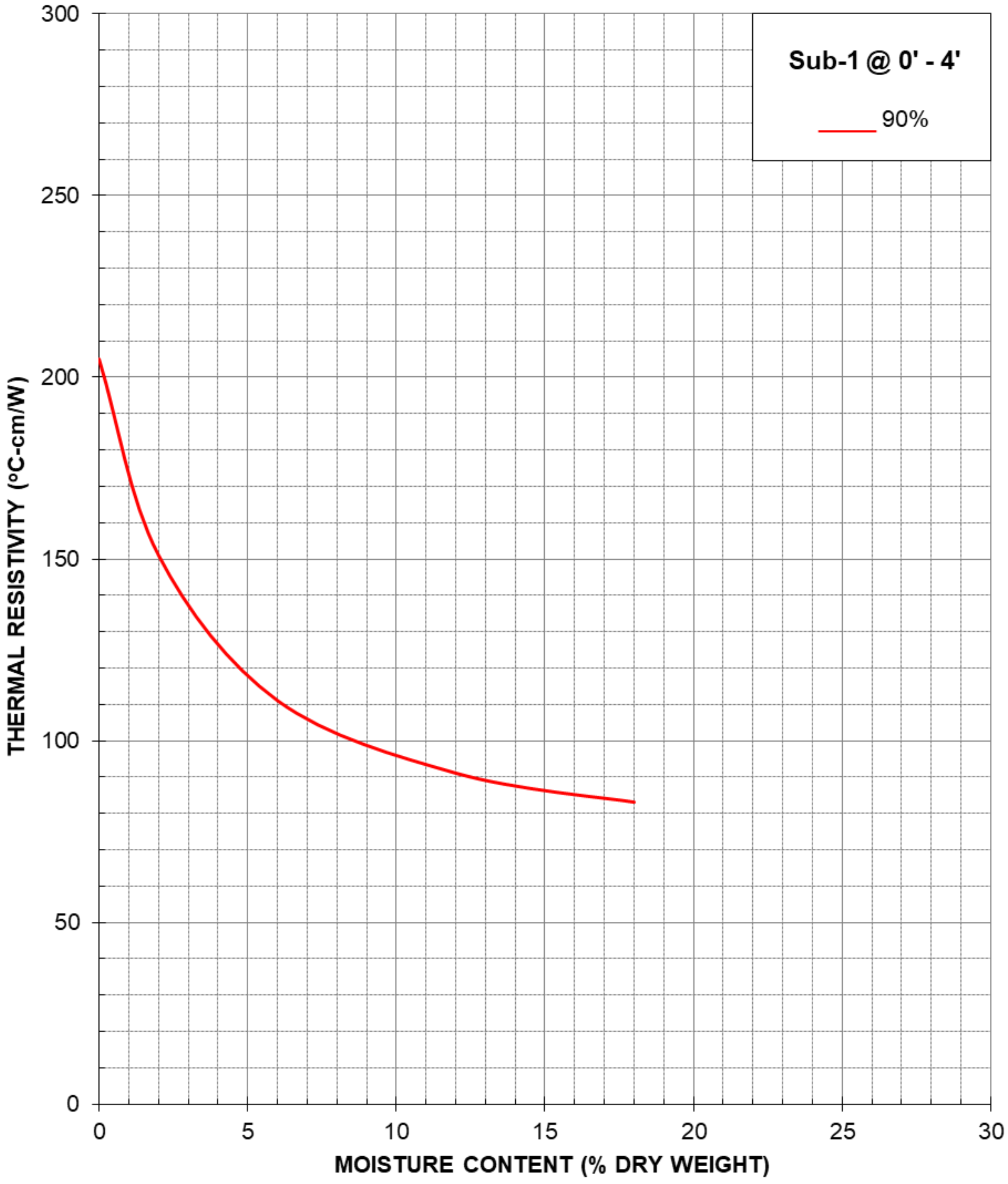
Terracon (Project No. 60225172)

Darden Solar – Fresno County, CA

Thermal Analysis of Native Soil Samples

June 2023 **Figure 10**

THERMAL DRYOUT CURVE



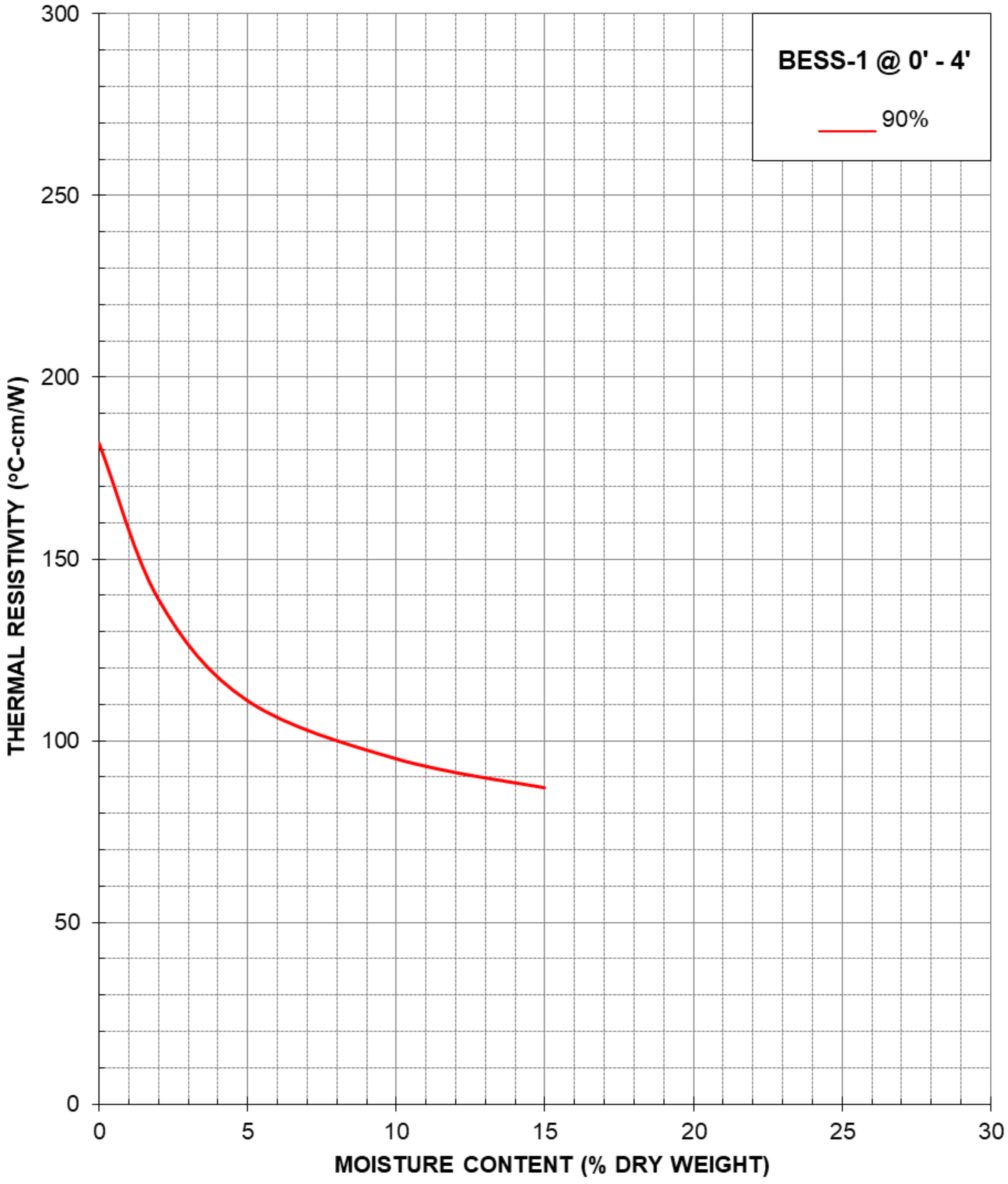
Terracon (Project No. 60225172)

Darden Solar – Fresno County, CA

Thermal Analysis of Native Soil Samples

June 2023 **Figure 11**

THERMAL DRYOUT CURVE



Terracon (Project No. 60225172)

Darden Solar – Fresno County, CA

Thermal Analysis of Native Soil Samples

June 2023 **Figure 12**

Geotherm USA

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http://www.geothermusa.com

September 21, 2023

Terracon
23041 Avenida de la Carlota, Suite 350
Laguna Hills, CA 92653
Attn: Victor V. Nguyen

Re: Thermal Analysis of Native Soil Samples
Darden Solar – Coalinga, CA (Project No. 60225172)

The following is the report of thermal dryout characterization tests conducted on three (3) native soil samples from the referenced project sent to our laboratory.

Thermal Resistivity Tests: The samples were tested at the 'optimum' moisture content and 85% of the modified Proctor dry density ***provided by Terracon.*** The tests were conducted in accordance with the IEEE standard 442-2017. The results are tabulated below and the thermal dryout curves are presented in **Figures 1 to 3.**

Sample ID, Description, Thermal Resistivity, Moisture Content and Density

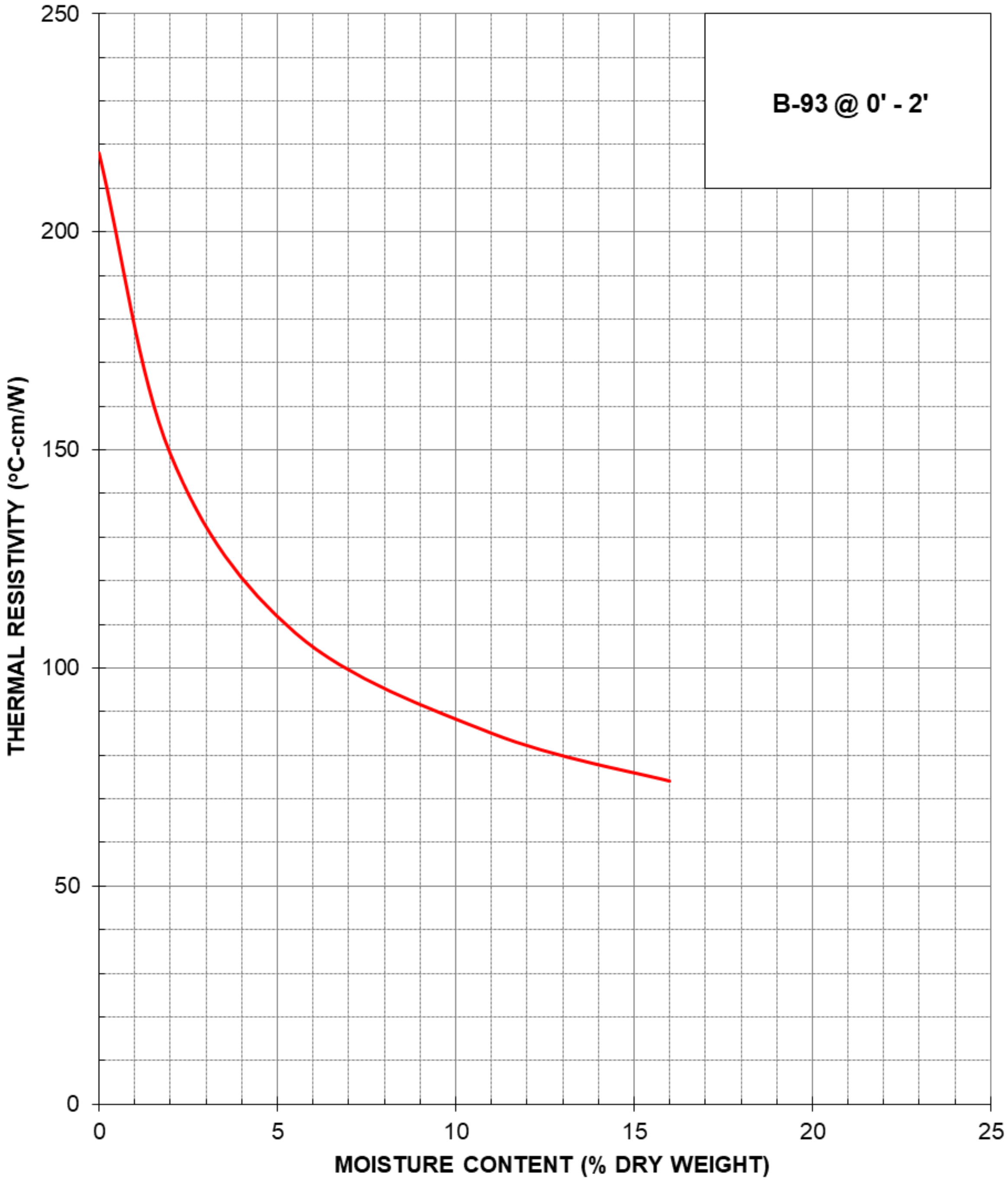
Sample ID	Depth (ft)	Effort (%)	Description (Terracon)	Thermal Resistivity (°C-cm/W)		Moisture Content (%)	Dry Density (lb/ft³)
				Wet	Dry		
B-93	0 - 2	85	Fat Clay	74	218	16	90
B-130	0 - 2	85	Lean Clay w/ sand	68	222	15	94
B-132	0 - 2	85	Lean Clay w/ sand	69	213	16	94

Please contact us if you have any questions or if we can be of further assistance.

Geotherm USA

Nimesh Patel

THERMAL DRYOUT CURVE



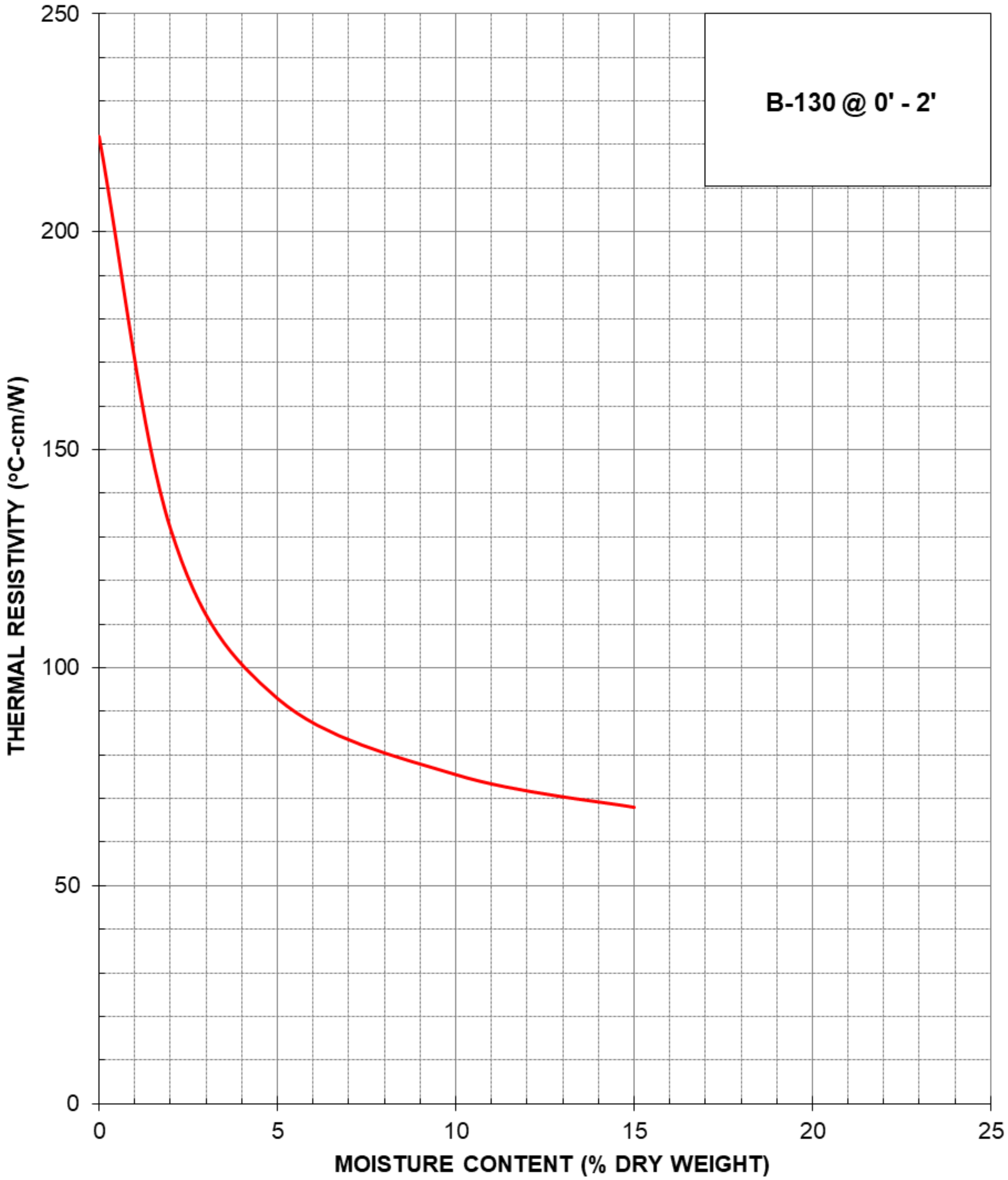
Terracon (Project No. 60225172)

Darden Solar – Coalinga, CA

Thermal Analysis of Native Soil Samples

September 2023 **Figure 1**

THERMAL DRYOUT CURVE



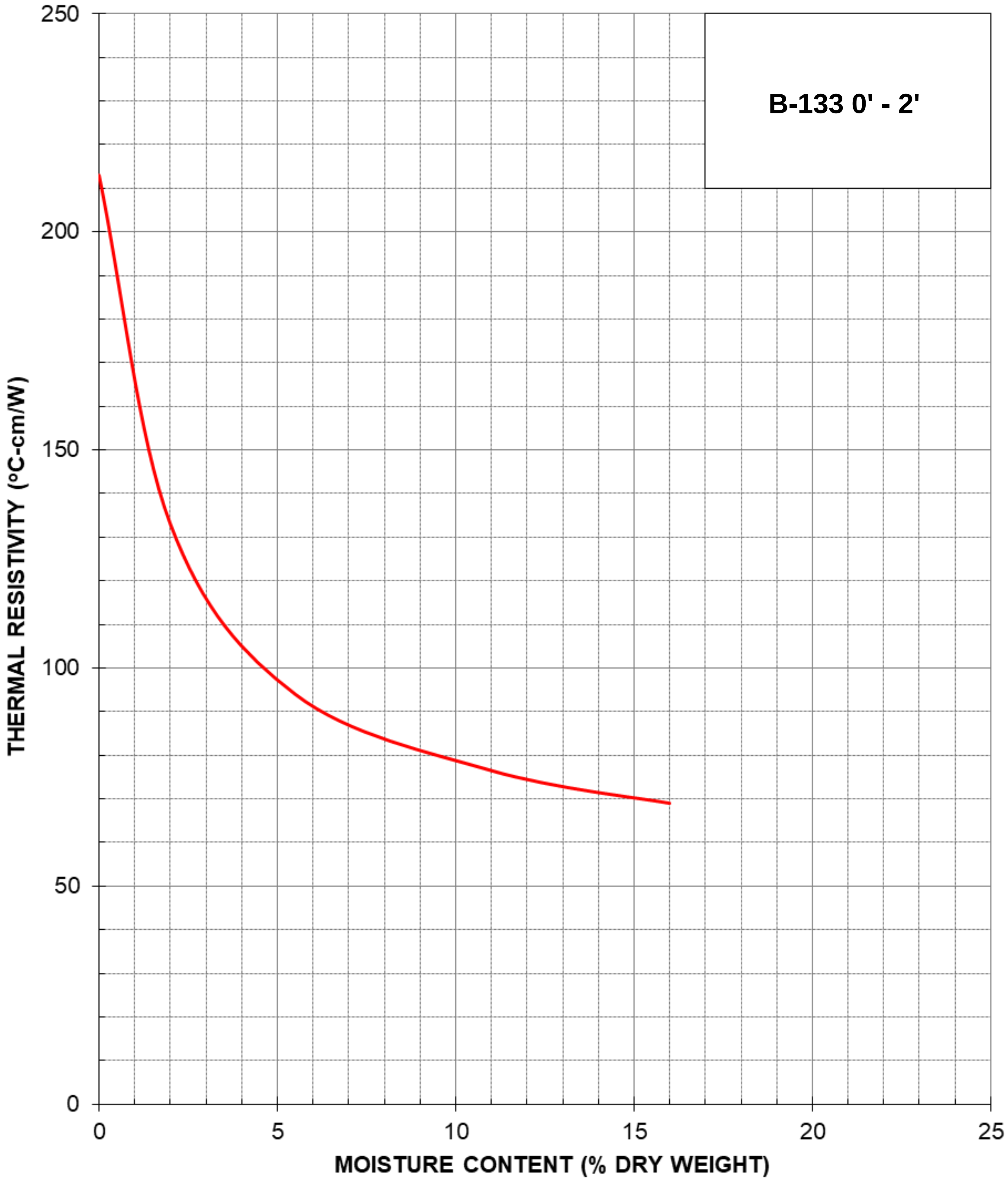
Terracon (Project No. 60225172)

Darden Solar – Coalinga, CA

Thermal Analysis of Native Soil Samples

September 2023 **Figure 2**

THERMAL DRYOUT CURVE



Terracon (Project No. 60225172)

Darden Solar – Coalinga, CA

Thermal Analysis of Native Soil Samples

Field Soil Electrical Resistivity Test Results

Contents:

Field Electrical Resistivity Test Procedures

Field measurements of soil electrical resistivity were performed by Terracon. Field measurements of soil electrical resistivity were performed in general accordance with ASTM Test Method G 57, and IEEE Standard 81, using the Wenner Four-Electrode. The Wenner arrangement (equal electrode spacing) was used with the following “a” spacings:

- 0.5, 1, 2, 5, 10, and 15 feet at ninety-two (92) locations within the solar array areas
- 0.5, 1, 2, 5, 10, 15, 25, 75, 100, 150, and 200 feet at one (1) location within the BESS (ER-85), substation (ER-86), alternate substation (ER-94), and switchyard area (ER-95).

The “a” spacing is generally considered to be the depth of influence of the test. The testing was performed in both a north-south and an east-west orientation at each location.

Electrical Resistivity Test Locations

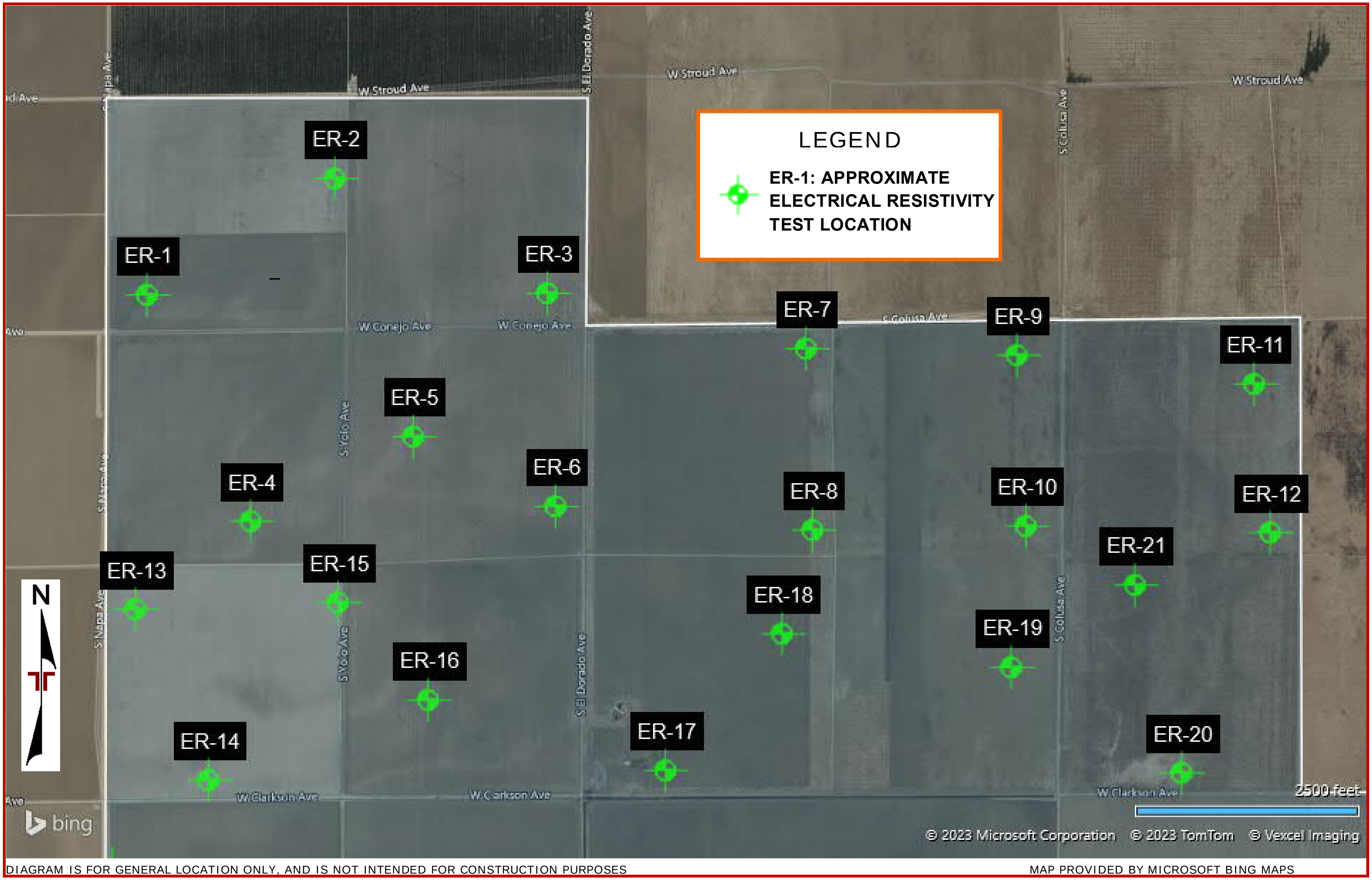


DIAGRAM IS FOR GENERAL LOCATION ONLY, AND IS NOT INTENDED FOR CONSTRUCTION PURPOSES

MAP PROVIDED BY MICROSOFT BING MAPS

Electrical Resistivity Test Locations

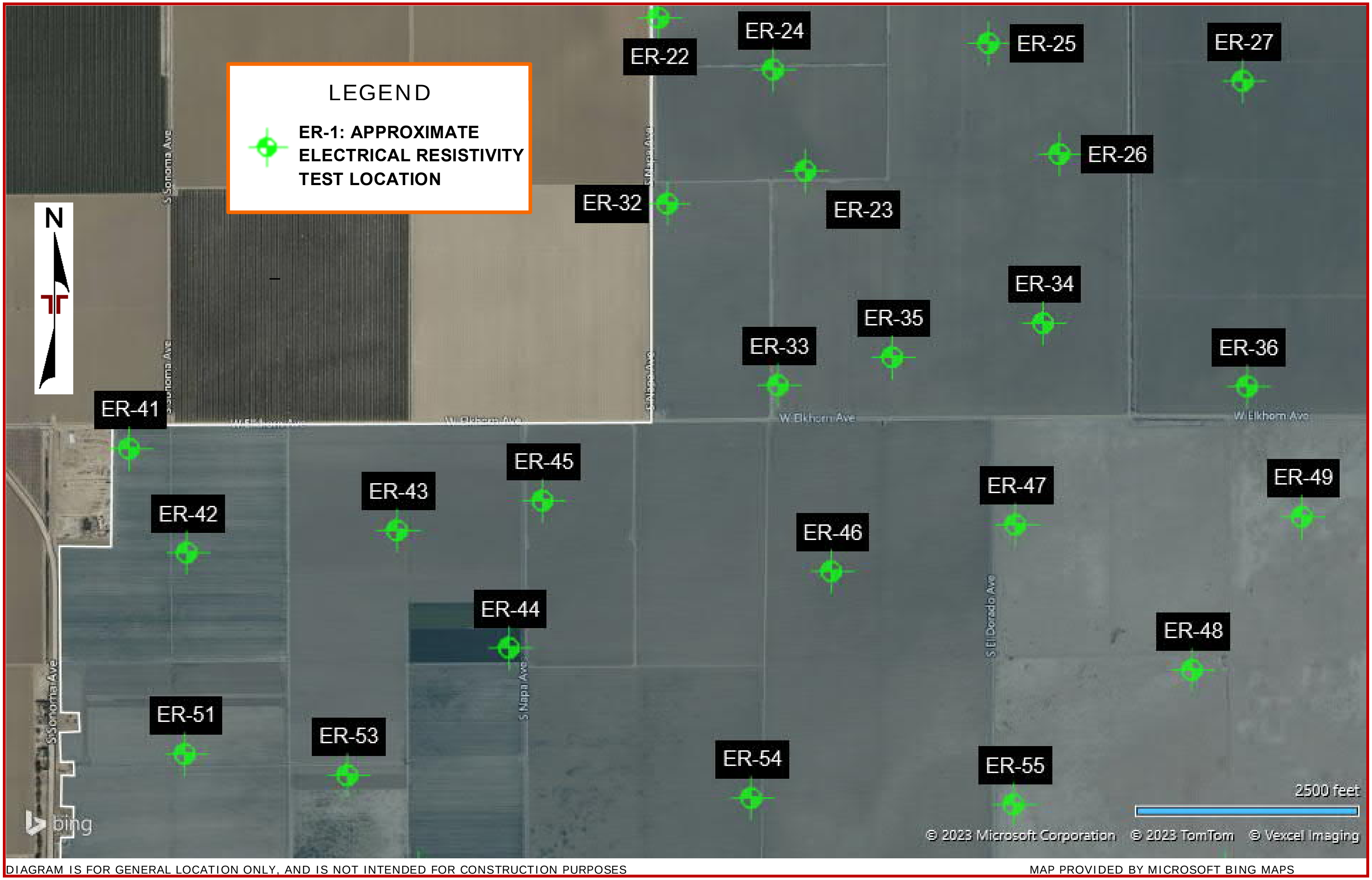


DIAGRAM IS FOR GENERAL LOCATION ONLY, AND IS NOT INTENDED FOR CONSTRUCTION PURPOSES

MAP PROVIDED BY MICROSOFT BING MAPS

Electrical Resistivity Test Locations

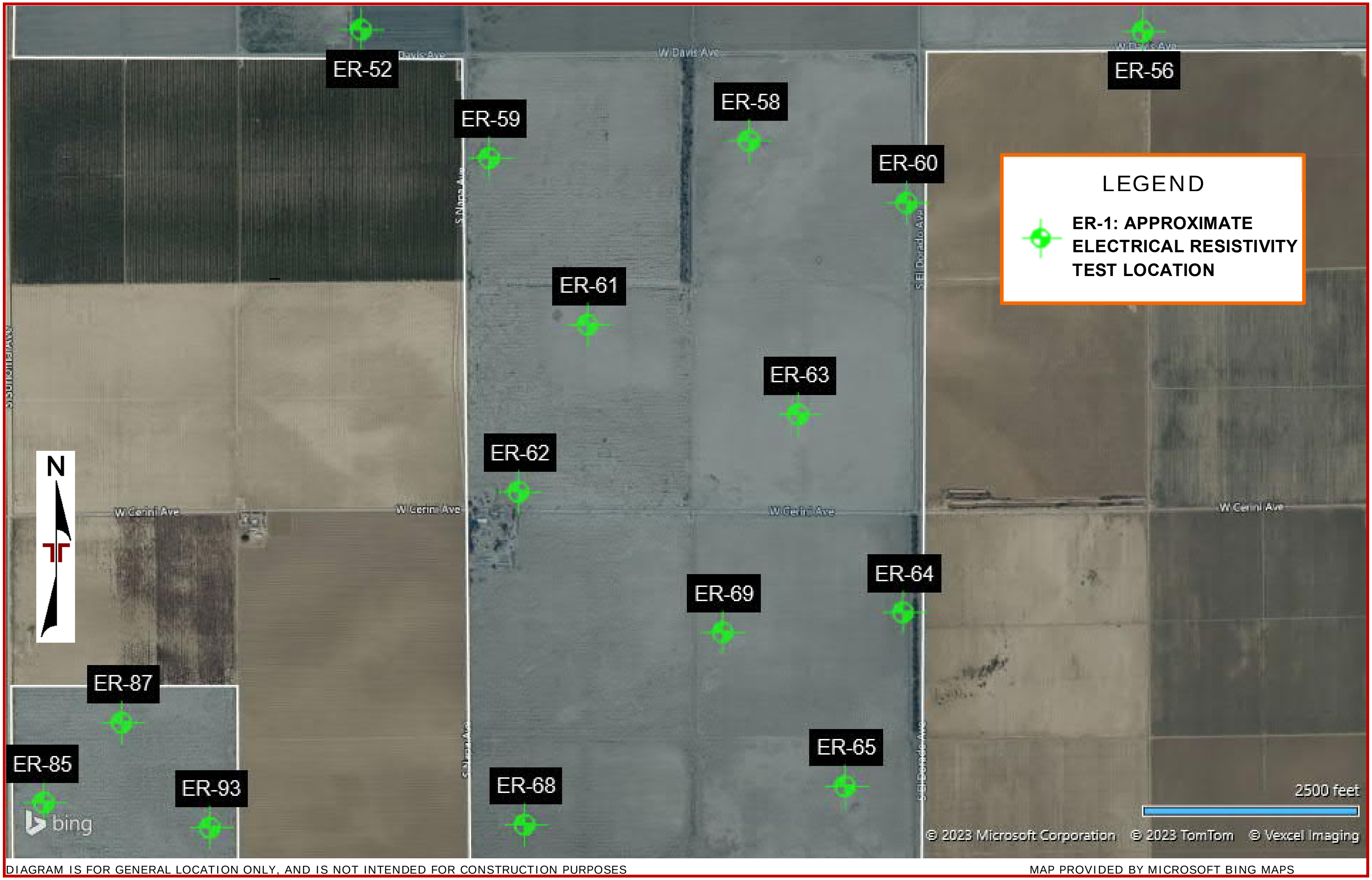


DIAGRAM IS FOR GENERAL LOCATION ONLY, AND IS NOT INTENDED FOR CONSTRUCTION PURPOSES

MAP PROVIDED BY MICROSOFT BING MAPS

Electrical Resistivity Test Locations

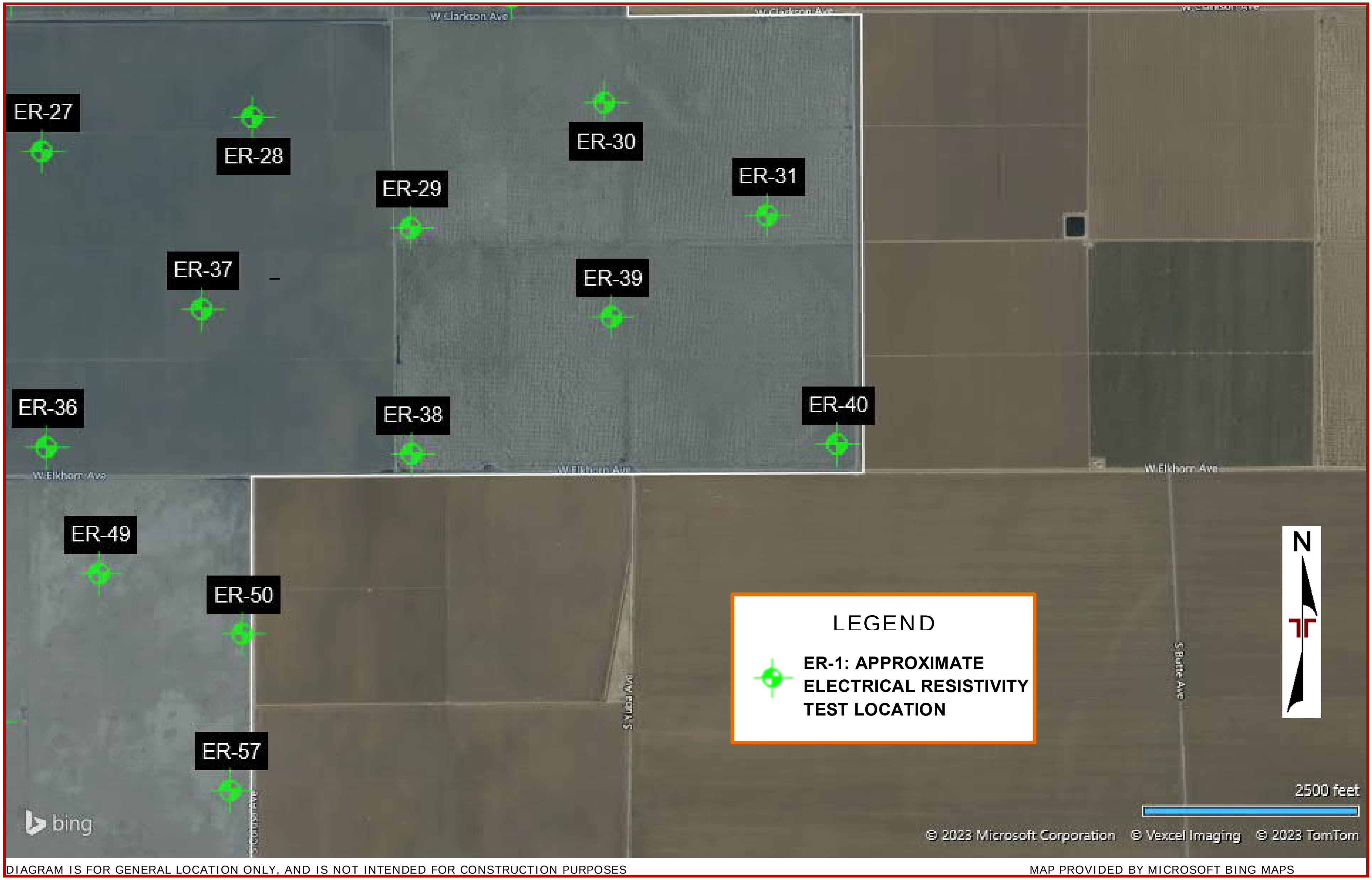


DIAGRAM IS FOR GENERAL LOCATION ONLY, AND IS NOT INTENDED FOR CONSTRUCTION PURPOSES

MAP PROVIDED BY MICROSOFT BING MAPS

Electrical Resistivity Test Locations

DIAGRAM IS FOR GENERAL LOCATION ONLY, AND IS NOT INTENDED FOR CONSTRUCTION PURPOSES

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Electrical Resistivity Test Locations

DIAGRAM IS FOR GENERAL LOCATION ONLY, AND IS NOT INTENDED FOR CONSTRUCTION PURPOSES

MAP PROVIDED BY MICROSOFT BING MAPS

FIELD ELECTRICAL RESISTIVITY DATA SHEET

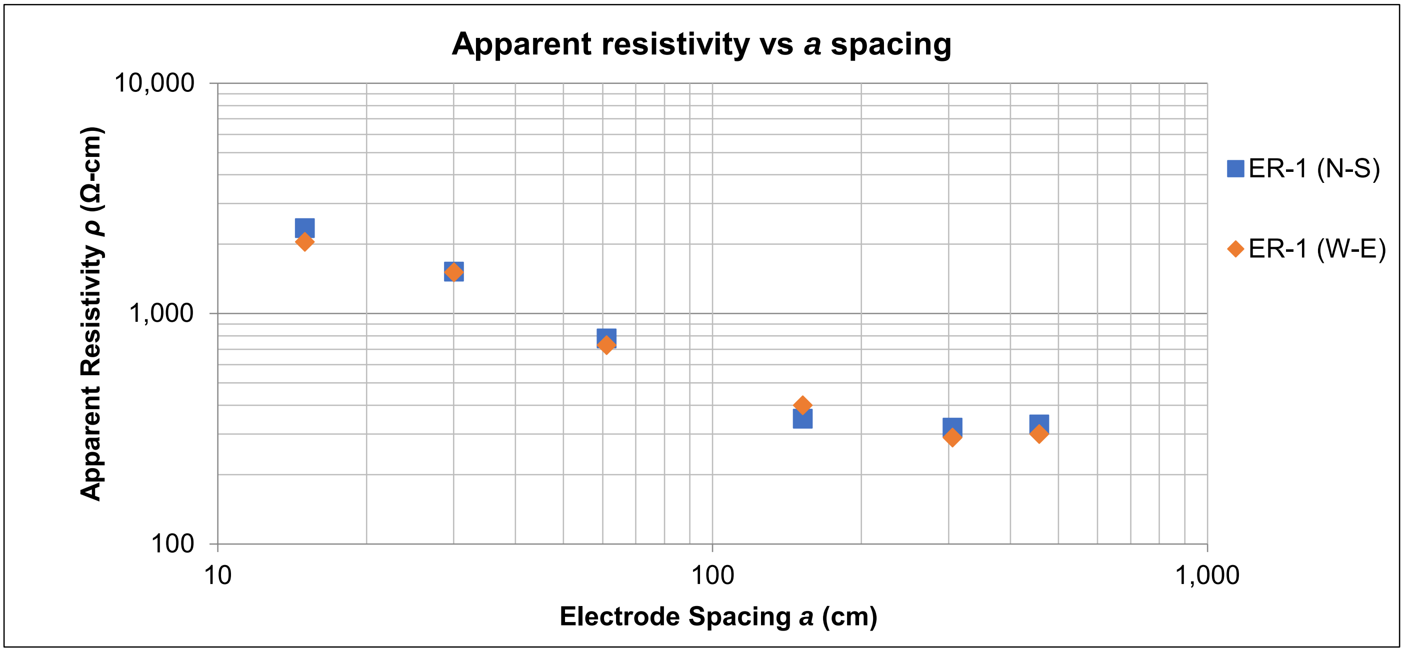
Darden Solar Facility ■ Cantua Creek, Fresno County, California
October 13, 2023 ■ Terracon Project No. 60225172

Array Loc.	**ER-1** (36.517375°N, 120.223487°W)		
Instrument	L&R Instruments - Ultra Mini Res	**Weather**	Clear, high of 56°F.
Serial #	SN-214U	**Ground Cond.**	Fallow field.
Cal. Check	2/14/2023	**Tested By**	H. Philson
Test Date	February 14, 2023	**Method**	Wenner 4-pin ASTM G57-06 (2012); IEEE 81-2012
Notes & Conflicts	Arrays oriented N-S and W-E with a common midpoint.		

Apparent resistivity ρ is calculated as :

$$\rho = \frac{4\pi a R}{1 + \frac{2a}{\sqrt{a^2 + 4b^2}} - \frac{a}{\sqrt{a^2 + b^2}}}$$

Electrode Spacing *a*		**Electrode Depth *b***		**ER-1 (N-S)**		**ER-1 (W-E)**	
(feet)	(centimeters)	(inches)	(centimeters)	Measured Resistance *R*	Apparent Resistivity *ρ*	Measured Resistance *R*	Apparent Resistivity *ρ*
				Ω	(Ω-cm)	Ω	(Ω-cm)
0.5	15	1	3	23.40	2350	20.40	2050
1	30	1	3	7.925	1520	7.888	1510
2	61	2	5	2.005	780	1.875	730
5	152	6	15	0.3630	350	0.4070	400
10	305	12	30	0.1635	320	0.1475	290
15	457	12	30	0.1135	330	0.1054	300



FIELD ELECTRICAL RESISTIVITY DATA SHEET

Darden Solar Facility ■ Cantua Creek, Fresno County, California
October 13, 2023 ■ Terracon Project No. 60225172

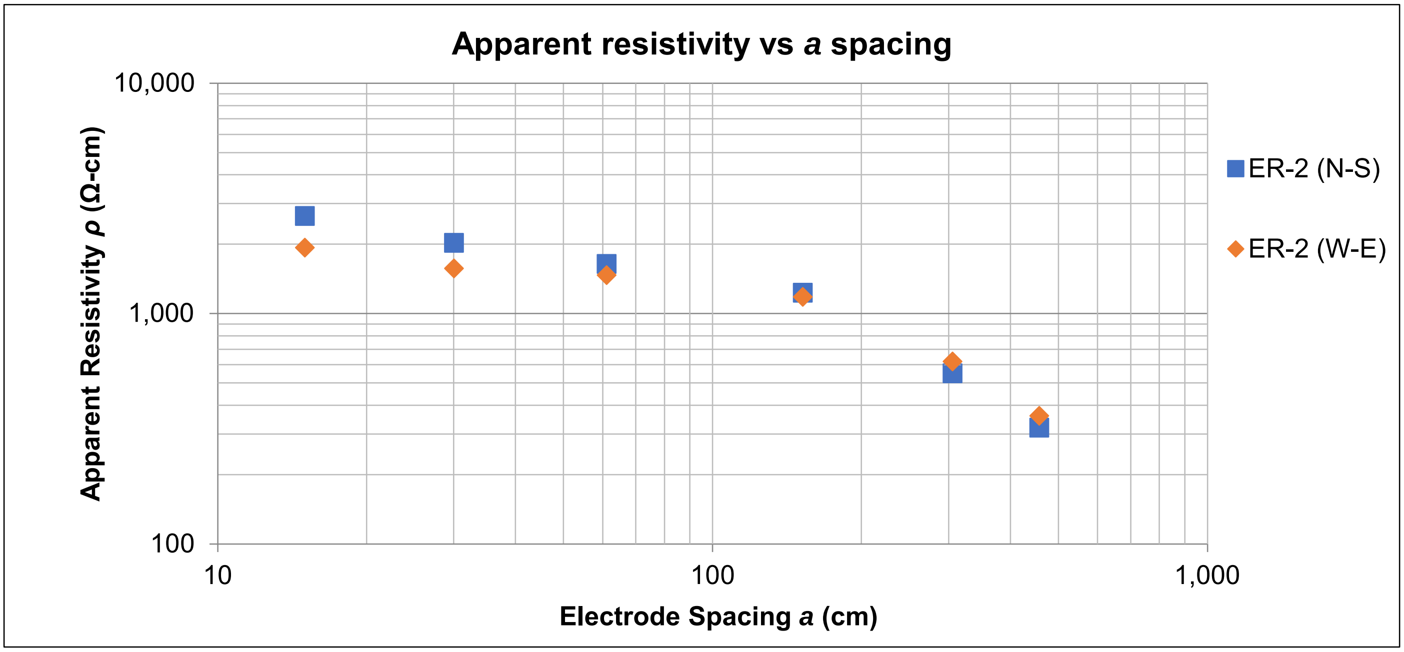
NORCAL
GEOPHYSICAL CONSULTANTS INC.
A Terracon COMPANY

Array Loc.	**ER-2** (36.520955°N, 120.216299°W)		
Instrument	L&R Instruments - Ultra Mini Res	**Weather**	Clear, high of 56°F.
Serial #	SN-214U	**Ground Cond.**	Fallow field.
Cal. Check	2/14/2023	**Tested By**	H. Philson
Test Date	February 14, 2023	**Method**	Wenner 4-pin ASTM G57-06 (2012); IEEE 81-2012
Notes & Conflicts	Arrays oriented N-S and W-E with a common midpoint.		

Apparent resistivity ρ is calculated as :

$$\rho = \frac{4\pi a R}{1 + \frac{2a}{\sqrt{a^2 + 4b^2}} - \frac{a}{\sqrt{a^2 + b^2}}}$$

Electrode Spacing *a*		**Electrode Depth *b***		**ER-2 (N-S)**		**ER-2 (W-E)**	
(feet)	(centimeters)	(inches)	(centimeters)	Measured Resistance *R*	Apparent Resistivity *ρ*	Measured Resistance *R*	Apparent Resistivity *ρ*
				Ω	(Ω-cm)	Ω	(Ω-cm)
0.5	15	1	3	26.40	2650	19.20	1930
1	30	1	3	10.570	2030	8.163	1570
2	61	2	5	4.235	1640	3.792	1470
5	152	6	15	1.2710	1230	1.2140	1180
10	305	12	30	0.2815	550	0.3184	620
15	457	12	30	0.1092	320	0.1245	360



FIELD ELECTRICAL RESISTIVITY DATA SHEET

Darden Solar Facility ■ Cantua Creek, Fresno County, California
October 13, 2023 ■ Terracon Project No. 60225172

NORCAL GEOPHYSICAL CONSULTANTS INC.
A Terracon COMPANY

Array Loc. **ER-3** (36.517426°N, 120.208167°W)

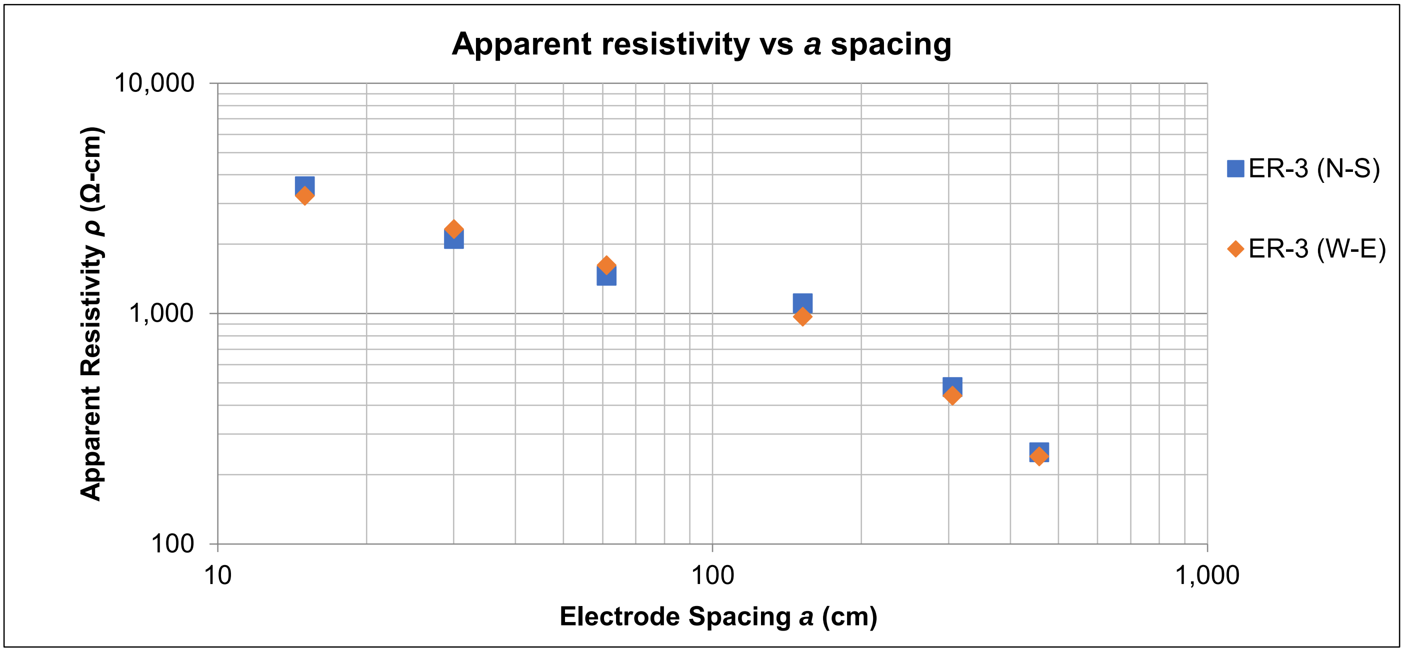
Instrument	L&R Instruments - Ultra Mini Res	**Weather**	Clear, high of 56°F.
Serial #	SN-214U	**Ground Cond.**	Fallow field.
Cal. Check	2/14/2023	**Tested By**	H. Philson
Test Date	February 14, 2023	**Method**	Wenner 4-pin ASTM G57-06 (2012); IEEE 81-2012

Notes & Conflicts Arrays oriented N-S and W-E with a common midpoint.

Apparent resistivity ρ is calculated as :

$$\rho = \frac{4\pi a R}{1 + \frac{2a}{\sqrt{a^2 + 4b^2}} - \frac{a}{\sqrt{a^2 + b^2}}}$$

Electrode Spacing *a*		**Electrode Depth *b***		**ER-3 (N-S)**		**ER-3 (W-E)**	
(feet)	(centimeters)	(inches)	(centimeters)	Measured Resistance *R* Ω	Apparent Resistivity *ρ* (Ω-cm)	Measured Resistance *R* Ω	Apparent Resistivity *ρ* (Ω-cm)
0.5	15	1	3	35.50	3570	32.30	3240
1	30	1	3	10.980	2110	12.160	2330
2	61	2	5	3.755	1460	4.180	1620
5	152	6	15	1.1440	1110	1.0000	970
10	305	12	30	0.2454	480	0.2277	440
15	457	12	30	0.0852	250	0.0835	240



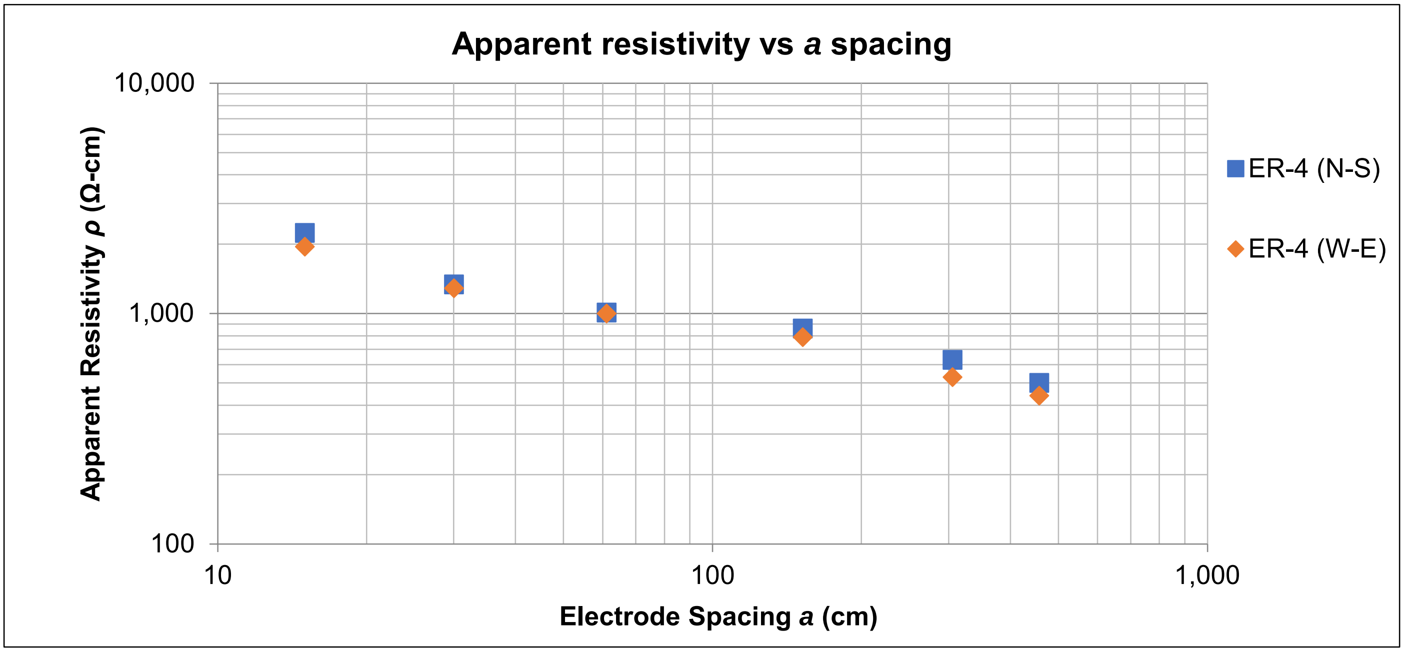
FIELD ELECTRICAL RESISTIVITY DATA SHEET

Darden Solar Facility ■ Cantua Creek, Fresno County, California
October 13, 2023 ■ Terracon Project No. 60225172

Array Loc.	**ER-4** (36.510409°N, 120.219520°W)		
Instrument	L&R Instruments - Ultra Mini Res	**Weather**	Clear, high of 56°F.
Serial #	SN-214U	**Ground Cond.**	Fallow field.
Cal. Check	2/14/2023	**Tested By**	H. Philson
Test Date	February 14, 2023	**Method**	Wenner 4-pin ASTM G57-06 (2012); IEEE 81-2012
Notes & Conflicts	Arrays oriented N-S and W-E with a common midpoint.		

Apparent resistivity ρ is calculated as :
$$\rho = \frac{4\pi aR}{1 + \frac{2a}{\sqrt{a^2 + 4b^2}} - \frac{a}{\sqrt{a^2 + b^2}}}$$

Electrode Spacing *a*		**Electrode Depth *b***		**ER-4 (N-S)**		**ER-4 (W-E)**	
(feet)	(centimeters)	(inches)	(centimeters)	Measured Resistance *R*	Apparent Resistivity *ρ*	Measured Resistance *R*	Apparent Resistivity *ρ*
				Ω	(Ω-cm)	Ω	(Ω-cm)
0.5	15	1	3	22.30	2240	19.40	1950
1	30	1	3	6.965	1340	6.737	1290
2	61	2	5	2.600	1010	2.591	1000
5	152	6	15	0.8850	860	0.8142	790
10	305	12	30	0.3247	630	0.2697	530
15	457	12	30	0.1725	500	0.1535	440



FIELD ELECTRICAL RESISTIVITY DATA SHEET

Darden Solar Facility ■ Cantua Creek, Fresno County, California
October 13, 2023 ■ Terracon Project No. 60225172

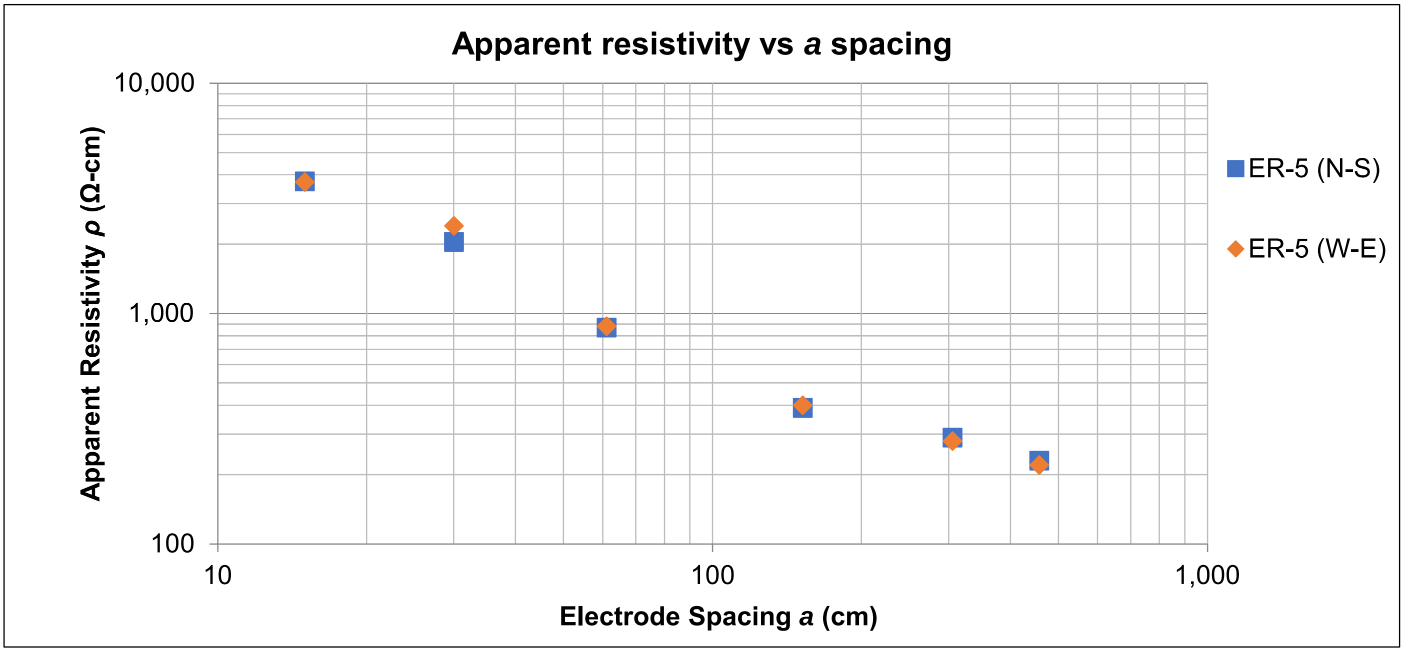
Array Loc. **ER-5** (36.513011°N, 120.213300°W)

Instrument	L&R Instruments - Ultra Mini Res	**Weather**	Clear, high of 56°F.
Serial #	SN-214U	**Ground Cond.**	Fallow field.
Cal. Check	2/14/2023	**Tested By**	H. Philson
Test Date	February 14, 2023	**Method**	Wenner 4-pin ASTM G57-06 (2012); IEEE 81-2012

Notes & Conflicts Arrays oriented N-S and W-E with a common midpoint.

Apparent resistivity ρ is calculated as : $\rho = \dfrac{4\pi aR}{1 + \dfrac{2a}{\sqrt{a^2 + 4b^2}} - \dfrac{a}{\sqrt{a^2 + b^2}}}$

Electrode Spacing *a*		**Electrode Depth *b***		**ER-5 (N-S)**		**ER-5 (W-E)**	
(feet)	(centimeters)	(inches)	(centimeters)	Measured Resistance *R*	Apparent Resistivity ρ	Measured Resistance *R*	Apparent Resistivity ρ
				Ω	(Ω-cm)	Ω	(Ω-cm)
0.5	15	1	3	37.30	3750	37.00	3720
1	30	1	3	10.700	2050	12.500	2400
2	61	2	5	2.240	870	2.267	880
5	152	6	15	0.3977	390	0.4135	400
10	305	12	30	0.1502	290	0.1430	280
15	457	12	30	0.0810	230	0.0748	220



FIELD ELECTRICAL RESISTIVITY DATA SHEET

Darden Solar Facility ■ Cantua Creek, Fresno County, California
October 13, 2023 ■ Terracon Project No. 60225172

NORCAL GEOPHYSICAL CONSULTANTS INC.
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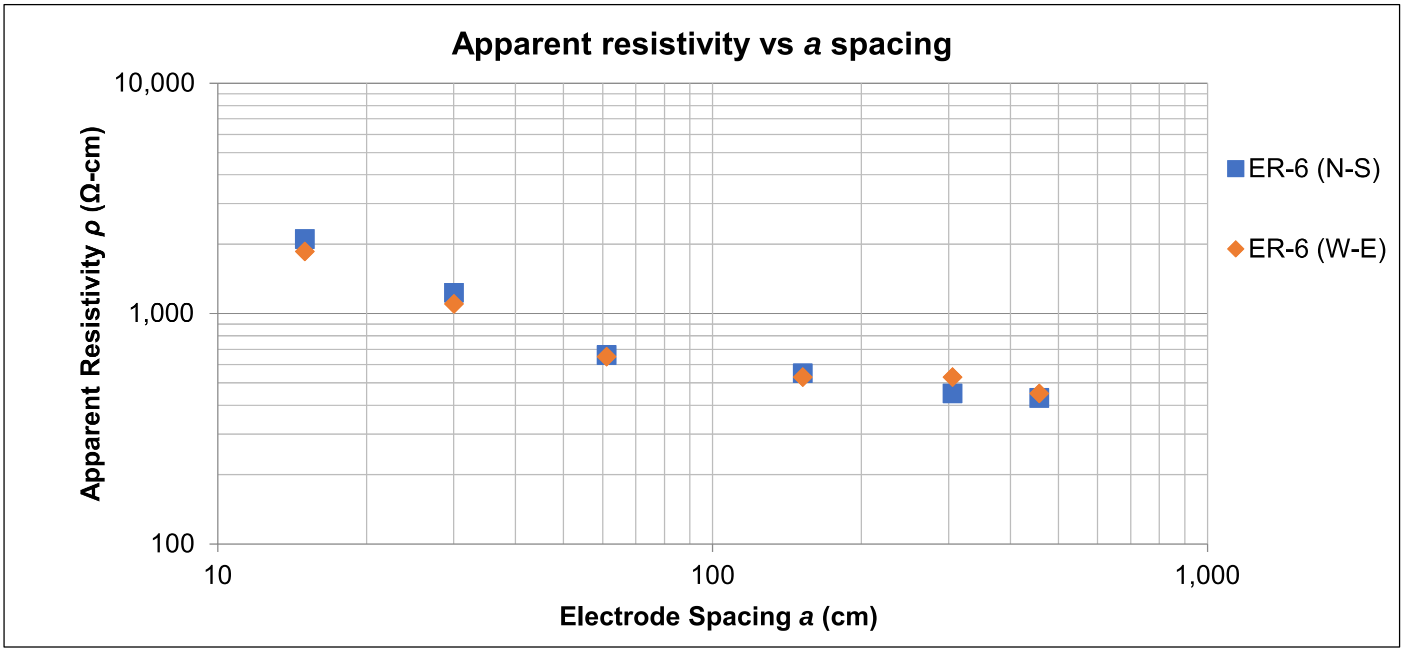
Array Loc. **ER-6** (36.510866°N, 120.207855°W)

Instrument	L&R Instruments - Ultra Mini Res	**Weather**	Clear, high of 56°F.
Serial #	SN-214U	**Ground Cond.**	Fallow field.
Cal. Check	2/14/2023	**Tested By**	H. Philson
Test Date	February 14, 2023	**Method**	Wenner 4-pin ASTM G57-06 (2012); IEEE 81-2012

Notes & Conflicts Arrays oriented N-S and W-E with a common midpoint.

Apparent resistivity ρ is calculated as : $$\rho = \frac{4\pi a R}{1 + \frac{2a}{\sqrt{a^2 + 4b^2}} - \frac{a}{\sqrt{a^2 + b^2}}}$$

Electrode Spacing *a*		**Electrode Depth *b***		**ER-6 (N-S)**		**ER-6 (W-E)**	
(feet)	(centimeters)	(inches)	(centimeters)	Measured Resistance *R*	Apparent Resistivity *ρ*	Measured Resistance *R*	Apparent Resistivity *ρ*
				Ω	(Ω-cm)	Ω	(Ω-cm)
0.5	15	1	3	21.00	2110	18.50	1860
1	30	1	3	6.420	1230	5.762	1100
2	61	2	5	1.708	660	1.684	650
5	152	6	15	0.5678	550	0.5455	530
10	305	12	30	0.2330	450	0.2705	530
15	457	12	30	0.1470	430	0.1551	450



FIELD ELECTRICAL RESISTIVITY DATA SHEET

Darden Solar Facility ■ Cantua Creek, Fresno County, California
October 13, 2023 ■ Terracon Project No. 60225172

Array Loc. **ER-7** (36.515722°N, 120.198260°W)

Instrument L&R Instruments - Ultra Mini Res

Weather Clear, high of 56°F.

Serial # SN-214U

Ground Cond. Fallow field.

Cal. Check 2/14/2023

Tested By H. Philson

Test Date February 14, 2023

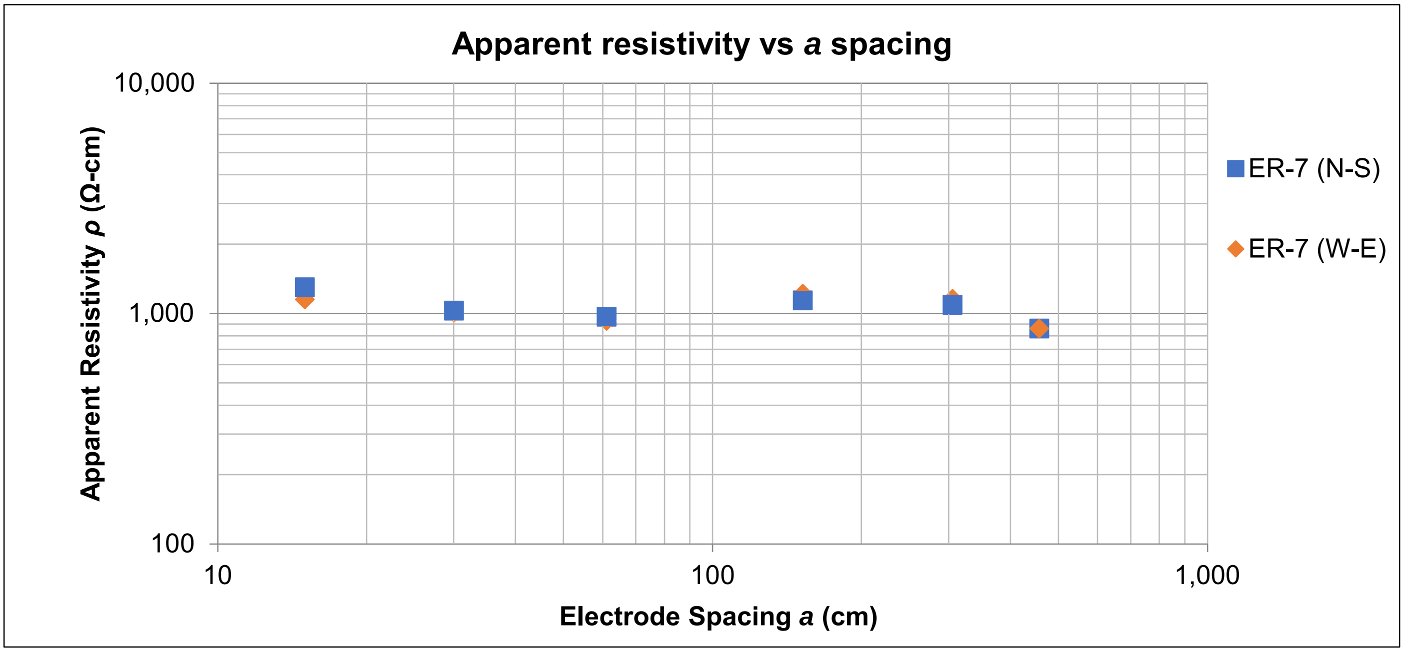
Method Wenner 4-pin ASTM G57-06 (2012); IEEE 81-2012

Notes & Conflicts Arrays oriented N-S and W-E with a common midpoint.

Apparent resistivity ρ is calculated as :

$$\rho = \frac{4\pi aR}{1 + \frac{2a}{\sqrt{a^2 + 4b^2}} - \frac{a}{\sqrt{a^2 + b^2}}}$$

Electrode Spacing *a*		**Electrode Depth *b***		**ER-7 (N-S)**		**ER-7 (W-E)**	
(feet)	(centimeters)	(inches)	(centimeters)	Measured Resistance *R*	Apparent Resistivity *ρ*	Measured Resistance *R*	Apparent Resistivity *ρ*
				Ω	(Ω-cm)	Ω	(Ω-cm)
0.5	15	1	3	12.91	1300	11.45	1150
1	30	1	3	5.346	1030	5.253	1010
2	61	2	5	2.508	970	2.409	930
5	152	6	15	1.1750	1140	1.2590	1220
10	305	12	30	0.5602	1090	0.5965	1160
15	457	12	30	0.2990	860	0.2958	860



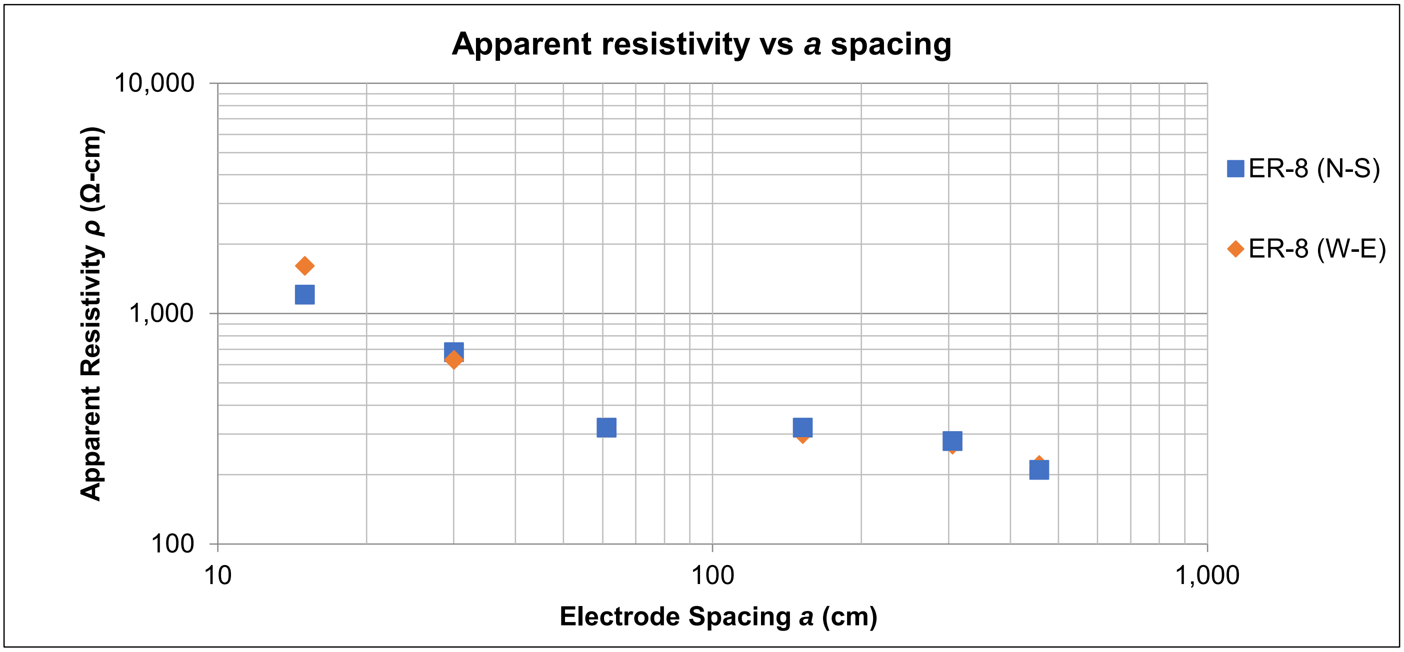
FIELD ELECTRICAL RESISTIVITY DATA SHEET

Darden Solar Facility ■ Cantua Creek, Fresno County, California
October 13, 2023 ■ Terracon Project No. 60225172

Array Loc.	**ER-8** (36.510138°N, 120.198009°W)		
Instrument	L&R Instruments - Ultra Mini Res	**Weather**	Clear, high of 54°F.
Serial #	SN-214U	**Ground Cond.**	Fallow field.
Cal. Check	2/14/2023	**Tested By**	H. Philson
Test Date	February 15, 2023	**Method**	Wenner 4-pin ASTM G57-06 (2012); IEEE 81-2012
Notes & Conflicts	Arrays oriented N-S and W-E with a common midpoint.		

Apparent resistivity ρ is calculated as : $\rho = \dfrac{4\pi aR}{1 + \dfrac{2a}{\sqrt{a^2 + 4b^2}} - \dfrac{a}{\sqrt{a^2 + b^2}}}$

Electrode Spacing *a*		**Electrode Depth *b***		**ER-8 (N-S)**		**ER-8 (W-E)**	
(feet)	(centimeters)	(inches)	(centimeters)	Measured Resistance *R* Ω	Apparent Resistivity *ρ* (Ω-cm)	Measured Resistance *R* Ω	Apparent Resistivity *ρ* (Ω-cm)
0.5	15	1	3	12.07	1210	16.02	1610
1	30	1	3	3.542	680	3.273	630
2	61	2	5	0.8292	320	0.8355	320
5	152	6	15	0.3331	320	0.3135	300
10	305	12	30	0.1450	280	0.1371	270
15	457	12	30	0.0722	210	0.0771	220



FIELD ELECTRICAL RESISTIVITY DATA SHEET

Darden Solar Facility ■ Cantua Creek, Fresno County, California
October 13, 2023 ■ Terracon Project No. 60225172

NORCAL GEOPHYSICAL CONSULTANTS INC. A Terracon COMPANY

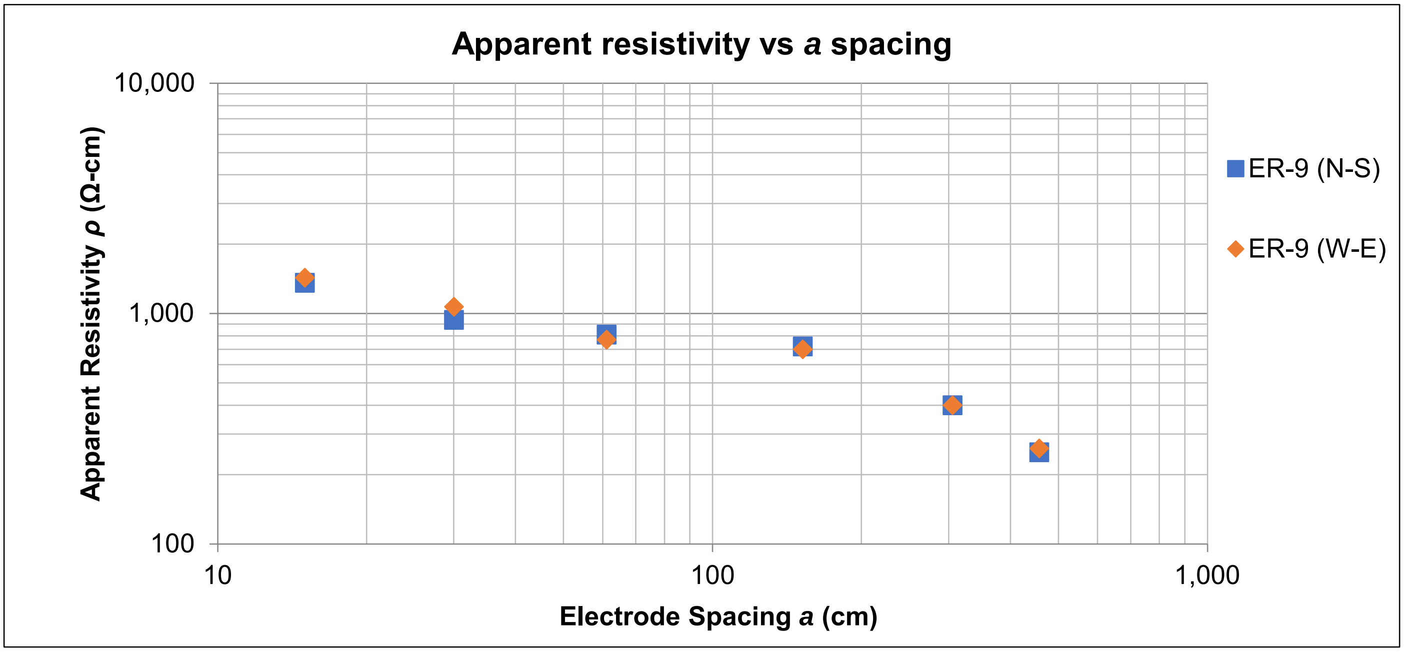
Array Loc. **ER-9** (36.515521°N, 120.190187°W)

Instrument	L&R Instruments - Ultra Mini Res	**Weather**	Clear, high of 54°F.
Serial #	SN-214U	**Ground Cond.**	Fallow field.
Cal. Check	2/14/2023	**Tested By**	H. Philson
Test Date	February 15, 2023	**Method**	Wenner 4-pin ASTM G57-06 (2012); IEEE 81-2012

Notes & Conflicts Arrays oriented N-S and W-E with a common midpoint.

Apparent resistivity ρ is calculated as : $\rho = \dfrac{4\pi a R}{1 + \dfrac{2a}{\sqrt{a^2 + 4b^2}} - \dfrac{a}{\sqrt{a^2 + b^2}}}$

Electrode Spacing *a*		**Electrode Depth *b***		**ER-9 (N-S)**		**ER-9 (W-E)**	
(feet)	(centimeters)	(inches)	(centimeters)	Measured Resistance *R* Ω	Apparent Resistivity *ρ* (Ω-cm)	Measured Resistance *R* Ω	Apparent Resistivity *ρ* (Ω-cm)
0.5	15	1	3	13.57	1360	14.20	1430
1	30	1	3	4.914	940	5.591	1070
2	61	2	5	2.084	810	1.977	770
5	152	6	15	0.7392	720	0.7177	700
10	305	12	30	0.2031	400	0.2066	400
15	457	12	30	0.0861	250	0.0905	260



FIELD ELECTRICAL RESISTIVITY DATA SHEET

Darden Solar Facility ■ Cantua Creek, Fresno County, California
October 13, 2023 ■ Terracon Project No. 60225172

Array Loc. **ER-10** (36.510262°N, 120.189845°W)

Instrument L&R Instruments - Ultra Mini Res

Weather Clear, high of 54°F.

Serial # SN-214U

Ground Cond. Fallow field.

Cal. Check 2/14/2023

Tested By H. Philson

Test Date February 15, 2023

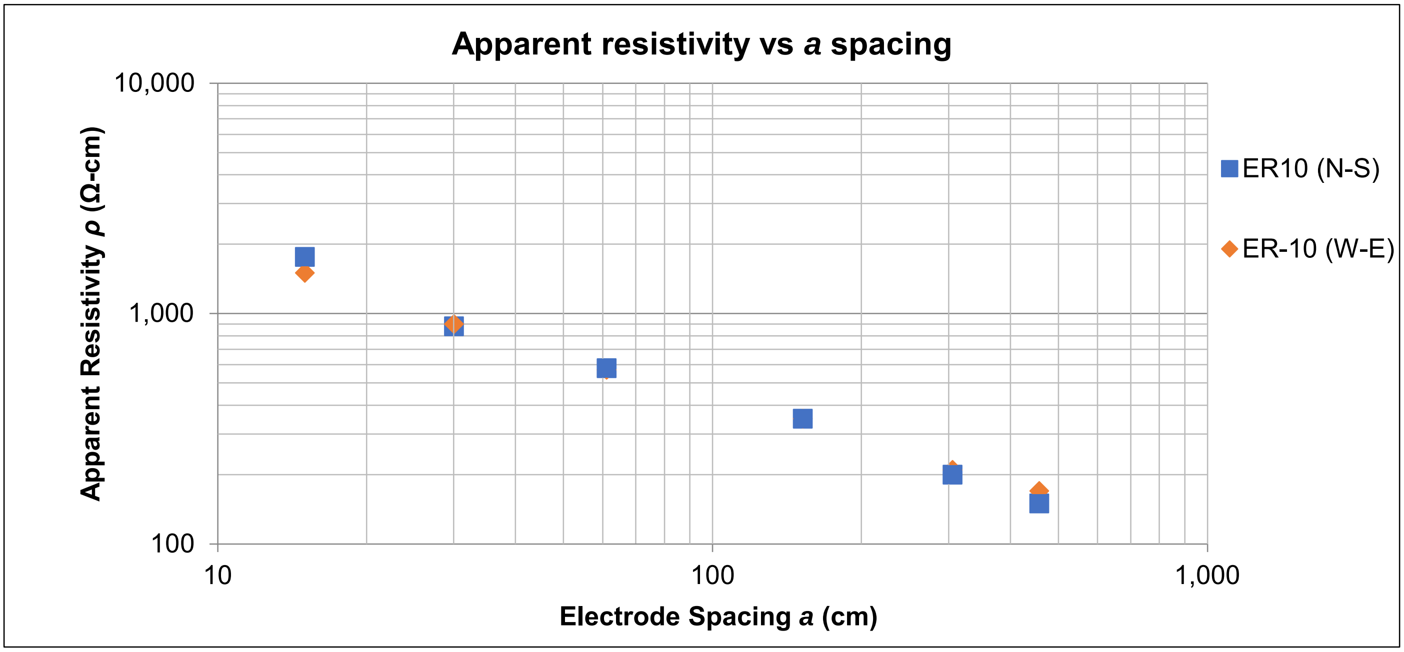
Method Wenner 4-pin ASTM G57-06 (2012); IEEE 81-2012

Notes & Conflicts Arrays oriented N-S and W-E with a common midpoint.

Apparent resistivity ρ is calculated as :

$$\rho = \frac{4\pi a R}{1 + \frac{2a}{\sqrt{a^2 + 4b^2}} - \frac{a}{\sqrt{a^2 + b^2}}}$$

Electrode Spacing *a*		**Electrode Depth *b***		**ER10 (N-S)**		**ER-10 (W-E)**	
(feet)	(centimeters)	(inches)	(centimeters)	Measured Resistance *R*	Apparent Resistivity *ρ*	Measured Resistance *R*	Apparent Resistivity *ρ*
				Ω	(Ω-cm)	Ω	(Ω-cm)
0.5	15	1	3	17.51	1760	14.91	1500
1	30	1	3	4.574	880	4.683	900
2	61	2	5	1.495	580	1.465	570
5	152	6	15	0.3632	350	0.3621	350
10	305	12	30	0.1042	200	0.1065	210
15	457	12	30	0.0533	150	0.0572	170



FIELD ELECTRICAL RESISTIVITY DATA SHEET

Darden Solar Facility ■ Cantua Creek, Fresno County, California

October 13, 2023 ■ Terracon Project No. 60225172

NORCAL GEOPHYSICAL CONSULTANTS INC.
A Terracon COMPANY

Array Loc. **ER-11** (36.514637°N, 120.181111°W)

Instrument L&R Instruments - Ultra Mini Res

Weather Clear, high of 54°F.

Serial # SN-214U

Ground Cond. Fallow field.

Cal. Check 2/14/2023

Tested By H. Philson

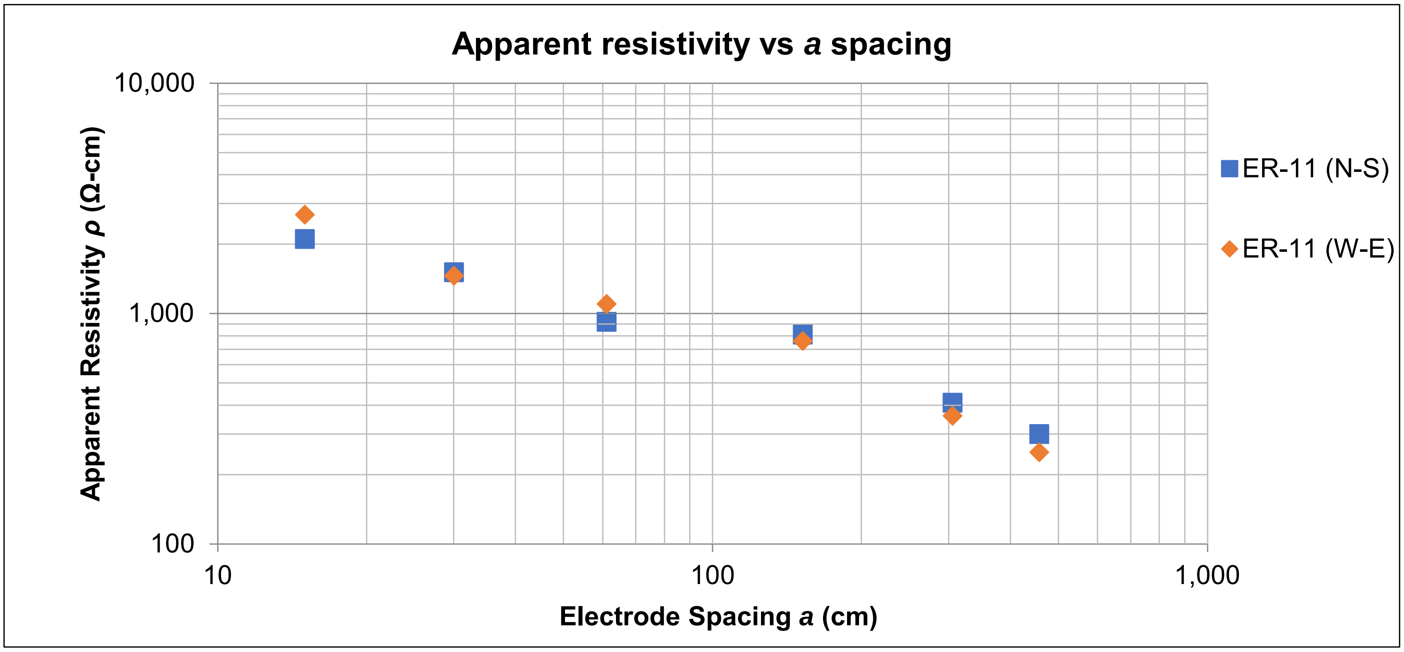
Test Date February 15, 2023

Method Wenner 4-pin ASTM G57-06 (2012); IEEE 81-2012

Notes & Conflicts Arrays oriented N-S and W-E with a common midpoint.

Apparent resistivity ρ is calculated as : $\rho = \dfrac{4\pi a R}{1 + \dfrac{2a}{\sqrt{a^2 + 4b^2}} - \dfrac{a}{\sqrt{a^2 + b^2}}}$

Electrode Spacing *a*		**Electrode Depth *b***		**ER-11 (N-S)**		**ER-11 (W-E)**	
(feet)	(centimeters)	(inches)	(centimeters)	Measured Resistance *R*	Apparent Resistivity *ρ*	Measured Resistance *R*	Apparent Resistivity *ρ*
				Ω	(Ω-cm)	Ω	(Ω-cm)
0.5	15	1	3	21.00	2110	26.80	2690
1	30	1	3	7.885	1510	7.605	1460
2	61	2	5	2.371	920	2.835	1100
5	152	6	15	0.8341	810	0.7825	760
10	305	12	30	0.2091	410	0.1851	360
15	457	12	30	0.1025	300	0.0852	250



FIELD ELECTRICAL RESISTIVITY DATA SHEET

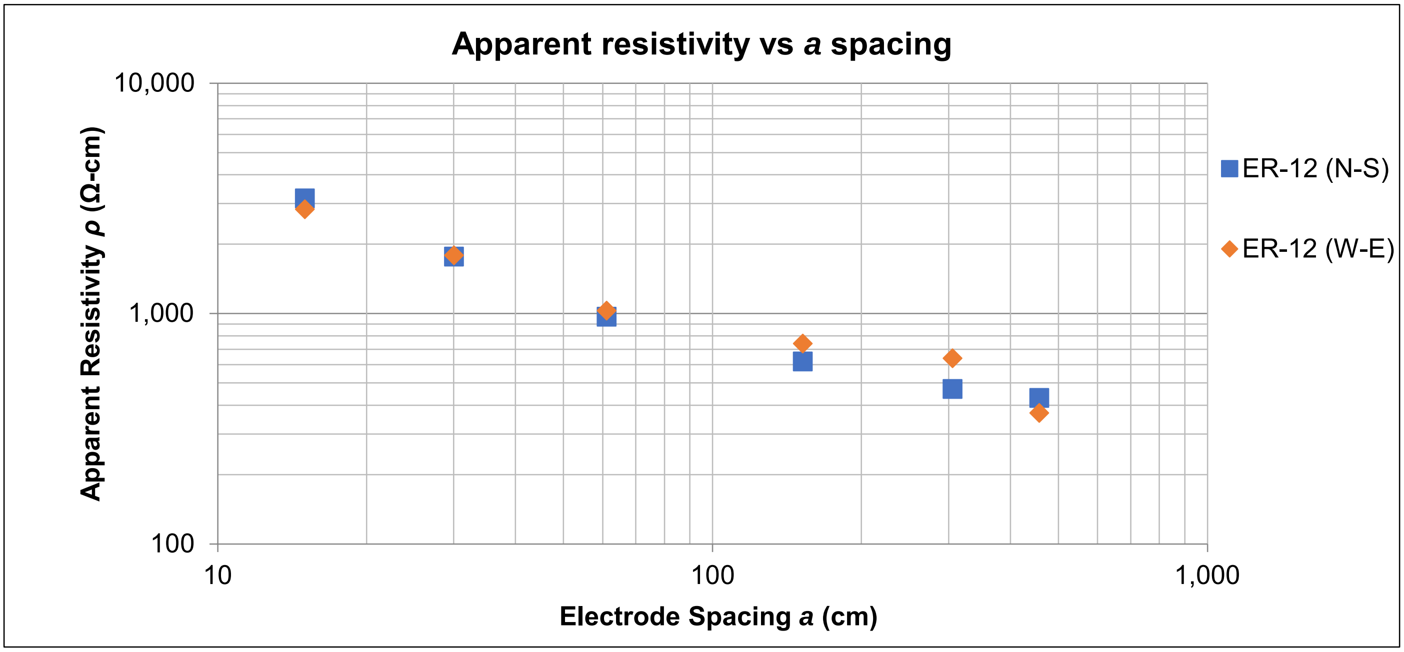
Darden Solar Facility ■ Cantua Creek, Fresno County, California
October 13, 2023 ■ Terracon Project No. 60225172

Array Loc.	**ER-12** (36.510059°N, 120.180495°W)		
Instrument	L&R Instruments - Ultra Mini Res	**Weather**	Clear, high of 54°F.
Serial #	SN-214U	**Ground Cond.**	Fallow field.
Cal. Check	2/14/2023	**Tested By**	H. Philson
Test Date	February 15, 2023	**Method**	Wenner 4-pin ASTM G57-06 (2012); IEEE 81-2012
Notes & Conflicts	Arrays oriented N-S and W-E with a common midpoint.		

Apparent resistivity ρ is calculated as :

$$\rho = \frac{4\pi a R}{1 + \frac{2a}{\sqrt{a^2 + 4b^2}} - \frac{a}{\sqrt{a^2 + b^2}}}$$

Electrode Spacing *a*		**Electrode Depth *b***		**ER-12 (N-S)**		**ER-12 (W-E)**	
(feet)	(centimeters)	(inches)	(centimeters)	Measured Resistance *R*	Apparent Resistivity ρ	Measured Resistance *R*	Apparent Resistivity ρ
				Ω	(Ω-cm)	Ω	(Ω-cm)
0.5	15	1	3	31.50	3160	28.30	2840
1	30	1	3	9.237	1770	9.311	1790
2	61	2	5	2.508	970	2.649	1030
5	152	6	15	0.6355	620	0.7615	740
10	305	12	30	0.2391	470	0.3301	640
15	457	12	30	0.1481	430	0.1271	370



FIELD ELECTRICAL RESISTIVITY DATA SHEET

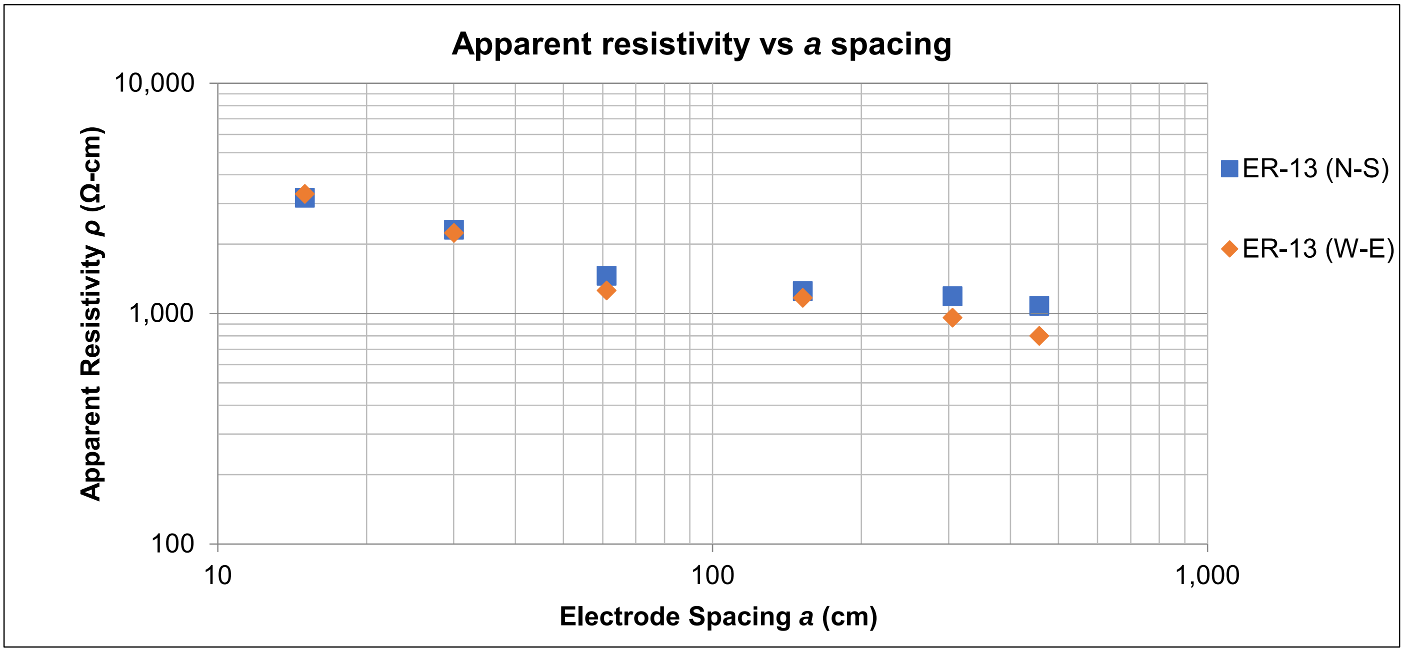
Darden Solar Facility ■ Cantua Creek, Fresno County, California
October 13, 2023 ■ Terracon Project No. 60225172

Array Loc.	**ER-13** (36.507696°N, 120.223937°W)		
Instrument	L&R Instruments - Ultra Mini Res	**Weather**	Clear, high of 54°F.
Serial #	SN-214U	**Ground Cond.**	Fallow field.
Cal. Check	2/14/2023	**Tested By**	H. Philson
Test Date	February 15, 2023	**Method**	Wenner 4-pin ASTM G57-06 (2012); IEEE 81-2012
Notes & Conflicts	Arrays oriented N-S and W-E with a common midpoint.		

Apparent resistivity ρ is calculated as :

$$\rho = \frac{4\pi a R}{1 + \frac{2a}{\sqrt{a^2 + 4b^2}} - \frac{a}{\sqrt{a^2 + b^2}}}$$

Electrode Spacing *a*		**Electrode Depth *b***		**ER-13 (N-S)**		**ER-13 (W-E)**	
(feet)	(centimeters)	(inches)	(centimeters)	Measured Resistance *R*	Apparent Resistivity *ρ*	Measured Resistance *R*	Apparent Resistivity *ρ*
				Ω	(Ω-cm)	Ω	(Ω-cm)
0.5	15	1	3	31.70	3180	32.90	3310
1	30	1	3	12.03	2310	11.66	2240
2	61	2	5	3.768	1460	3.239	1260
5	152	6	15	1.287	1250	1.202	1170
10	305	12	30	0.6116	1190	0.4921	960
15	457	12	30	0.3745	1080	0.2765	800



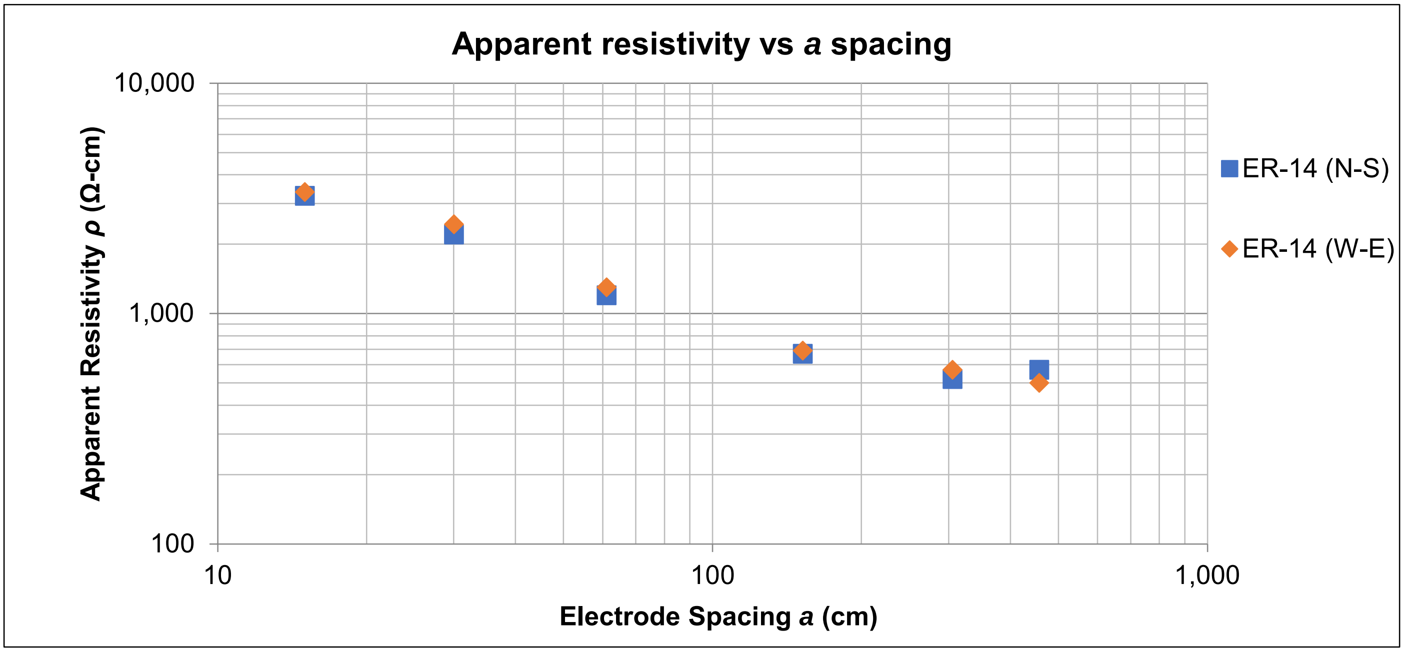
FIELD ELECTRICAL RESISTIVITY DATA SHEET

Darden Solar Facility ■ Cantua Creek, Fresno County, California
October 13, 2023 ■ Terracon Project No. 60225172

Array Loc.	**ER-14** (36.502442°N, 120.221133°W)		
Instrument	L&R Instruments - Ultra Mini Res	**Weather**	Clear, high of 54°F.
Serial #	SN-214U	**Ground Cond.**	Fallow field.
Cal. Check	2/14/2023	**Tested By**	H. Philson
Test Date	February 15, 2023	**Method**	Wenner 4-pin ASTM G57-06 (2012); IEEE 81-2012
Notes & Conflicts	Arrays oriented N-S and W-E with a common midpoint.		

Apparent resistivity ρ is calculated as : $\rho = \dfrac{4\pi a R}{1 + \dfrac{2a}{\sqrt{a^2 + 4b^2}} - \dfrac{a}{\sqrt{a^2 + b^2}}}$

Electrode Spacing *a*		**Electrode Depth *b***		**ER-14 (N-S)**		**ER-14 (W-E)**	
(feet)	(centimeters)	(inches)	(centimeters)	Measured Resistance *R*	Apparent Resistivity ρ	Measured Resistance *R*	Apparent Resistivity ρ
				Ω	(Ω-cm)	Ω	(Ω-cm)
0.5	15	1	3	32.30	3240	33.50	3370
1	30	1	3	11.480	2200	12.720	2440
2	61	2	5	3.102	1200	3.341	1300
5	152	6	15	0.6891	670	0.7067	690
10	305	12	30	0.2683	520	0.2944	570
15	457	12	30	0.1972	570	0.1718	500



FIELD ELECTRICAL RESISTIVITY DATA SHEET

Darden Solar Facility ■ Cantua Creek, Fresno County, California
October 13, 2023 ■ Terracon Project No. 60225172

NORCAL GEOPHYSICAL CONSULTANTS INC.
A Terracon COMPANY

Array Loc. **ER-15** (36.507908°N, 120.216176°W)

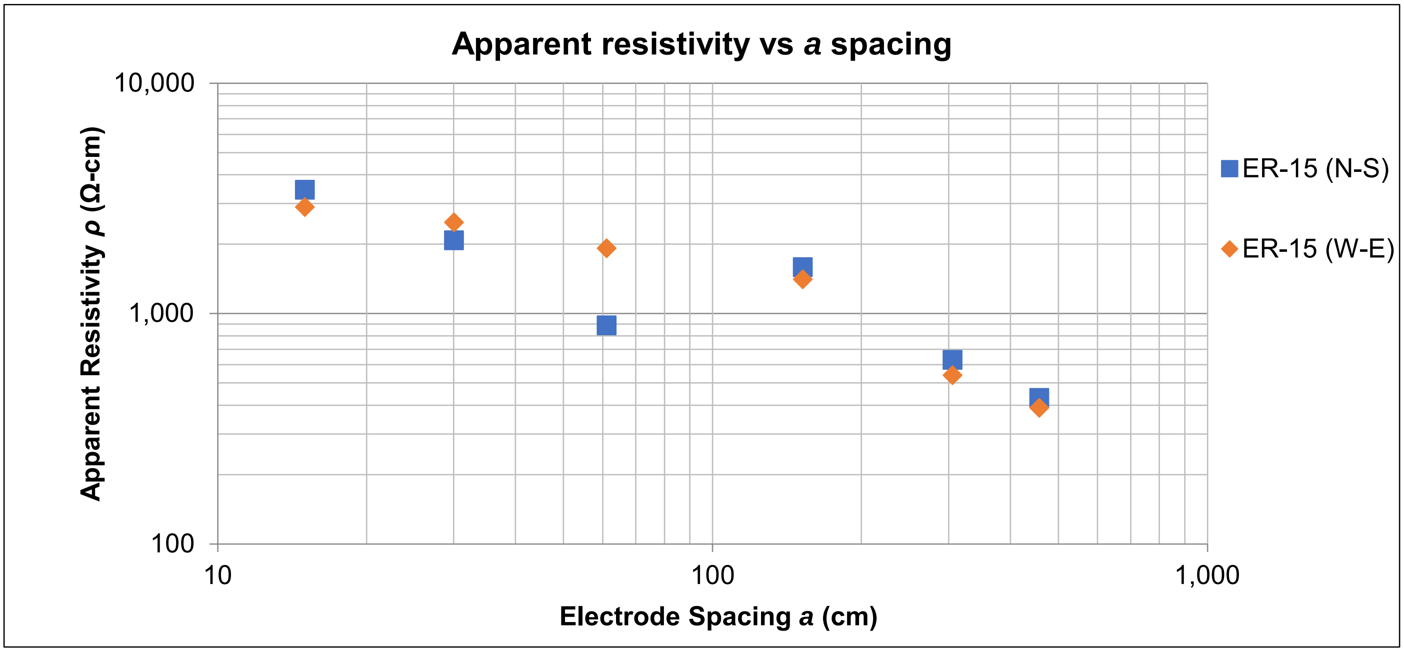
Instrument	L&R Instruments - Ultra Mini Res	**Weather**	Clear, high of 54°F.
Serial #	SN-214U	**Ground Cond.**	Fallow field.
Cal. Check	2/14/2023	**Tested By**	H. Philson
Test Date	February 15, 2023	**Method**	Wenner 4-pin ASTM G57-06 (2012); IEEE 81-2012

Notes & Conflicts Arrays oriented N-S and W-E with a common midpoint. Possible noisy reading at a=2-ft on N-S array.

Apparent resistivity ρ is calculated as :

$$\rho = \frac{4\pi a R}{1 + \frac{2a}{\sqrt{a^2 + 4b^2}} - \frac{a}{\sqrt{a^2 + b^2}}}$$

Electrode Spacing *a*		**Electrode Depth *b***		**ER-15 (N-S)**		**ER-15 (W-E)**	
(feet)	(centimeters)	(inches)	(centimeters)	Measured Resistance *R*	Apparent Resistivity *ρ*	Measured Resistance *R*	Apparent Resistivity *ρ*
				Ω	(Ω-cm)	Ω	(Ω-cm)
0.5	15	1	3	34.30	3450	28.90	2900
1	30	1	3	10.860	2080	13.000	2490
2	61	2	5	2.303	890	4.956	1920
5	152	6	15	1.6410	1590	1.4510	1410
10	305	12	30	0.3228	630	0.2760	540
15	457	12	30	0.1503	430	0.1334	390



FIELD ELECTRICAL RESISTIVITY DATA SHEET

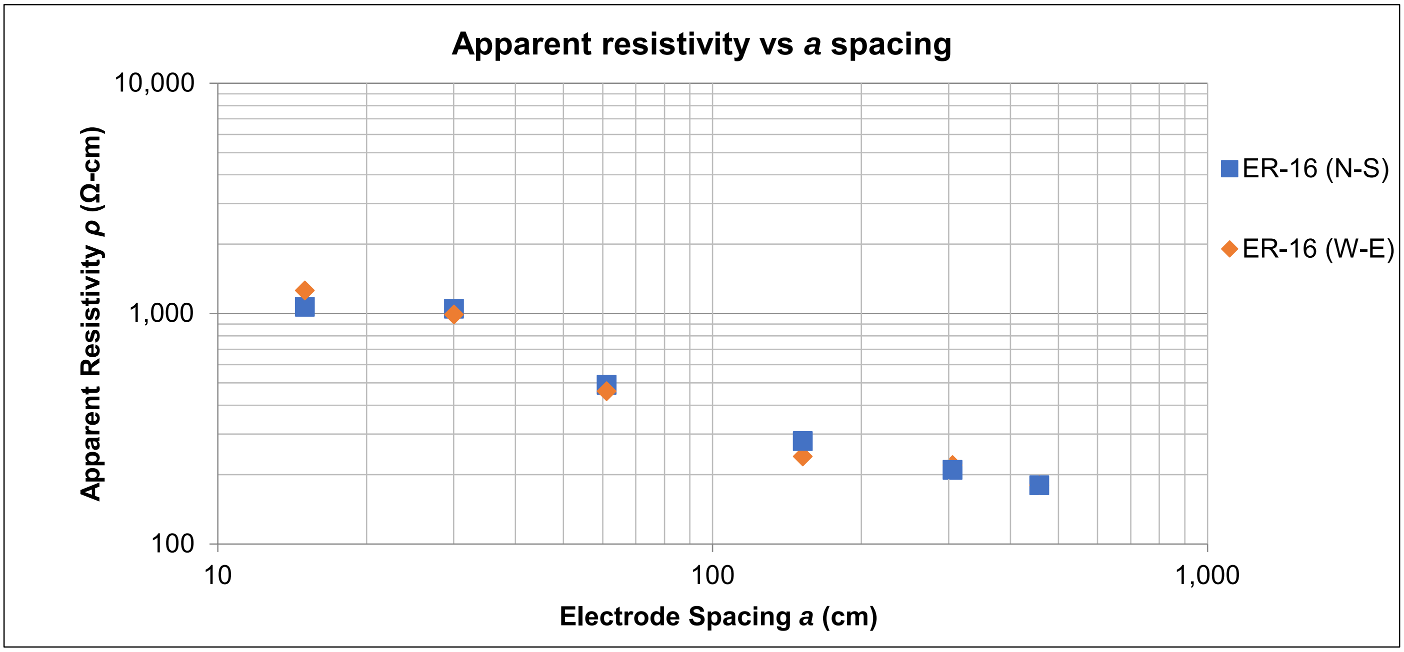
Darden Solar Facility ■ Cantua Creek, Fresno County, California
October 13, 2023 ■ Terracon Project No. 60225172

Array Loc.	**ER-16** (36.504903°N, 120.212730°W)		
Instrument	L&R Instruments - Ultra Mini Res	**Weather**	Clear, high of 60°F.
Serial #	SN-214U	**Ground Cond.**	Fallow field.
Cal. Check	2/14/2023	**Tested By**	H. Philson
Test Date	February 16, 2023	**Method**	Wenner 4-pin ASTM G57-06 (2012); IEEE 81-2012
Notes & Conflicts	Arrays oriented N-S and W-E with a common midpoint.		

Apparent resistivity ρ is calculated as :

$$\rho = \frac{4\pi aR}{1 + \frac{2a}{\sqrt{a^2 + 4b^2}} - \frac{a}{\sqrt{a^2 + b^2}}}$$

Electrode Spacing *a*		**Electrode Depth *b***		**ER-16 (N-S)**		**ER-16 (W-E)**	
(feet)	(centimeters)	(inches)	(centimeters)	Measured Resistance *R*	Apparent Resistivity *ρ*	Measured Resistance *R*	Apparent Resistivity *ρ*
				Ω	(Ω-cm)	Ω	(Ω-cm)
0.5	15	1	3	10.67	1070	12.51	1260
1	30	1	3	5.457	1050	5.163	990
2	61	2	5	1.271	490	1.187	460
5	152	6	15	0.2861	280	0.2476	240
10	305	12	30	0.1072	210	0.1112	220
15	457	12	30	0.0631	180	0.0624	180



FIELD ELECTRICAL RESISTIVITY DATA SHEET

Darden Solar Facility ■ Cantua Creek, Fresno County, California
October 13, 2023 ■ Terracon Project No. 60225172

Array Loc. **ER-17** (36.502741°N, 120.203645°W)

Instrument L&R Instruments - Ultra Mini Res

Weather Clear, high of 60°F.

Serial # SN-214U

Ground Cond. Fallow field.

Cal. Check 2/14/2023

Tested By H. Philson

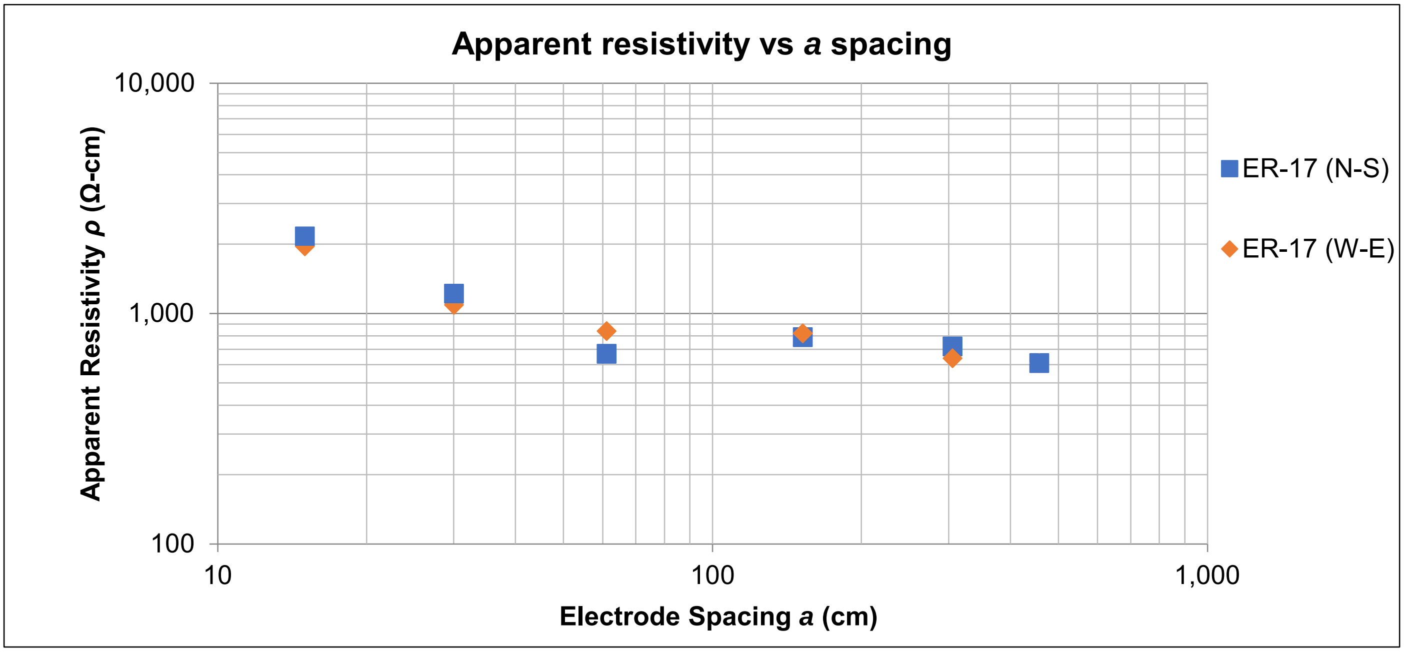
Test Date February 16, 2023

Method Wenner 4-pin ASTM G57-06 (2012); IEEE 81-2012

Notes & Conflicts Arrays oriented N-S and W-E with a common midpoint.

Apparent resistivity ρ is calculated as : $\rho = \dfrac{4\pi a R}{1 + \dfrac{2a}{\sqrt{a^2 + 4b^2}} - \dfrac{a}{\sqrt{a^2 + b^2}}}$

Electrode Spacing *a*		**Electrode Depth *b***		**ER-17 (N-S)**		**ER-17 (W-E)**	
(feet)	(centimeters)	(inches)	(centimeters)	Measured Resistance *R*	Apparent Resistivity *ρ*	Measured Resistance *R*	Apparent Resistivity *ρ*
				Ω	(Ω-cm)	Ω	(Ω-cm)
0.5	15	1	3	21.50	2160	19.50	1960
1	30	1	3	6.388	1220	5.675	1090
2	61	2	5	1.737	670	2.159	840
5	152	6	15	0.8095	790	0.8404	820
10	305	12	30	0.3685	720	0.3293	640
15	457	12	30	0.2116	610	0.2112	610



FIELD ELECTRICAL RESISTIVITY DATA SHEET

Darden Solar Facility ■ Cantua Creek, Fresno County, California
October 13, 2023 ■ Terracon Project No. 60225172

Array Loc. **ER-18** (36.506943°N, 120.199173°W)

Instrument L&R Instruments - Ultra Mini Res

Weather Clear, high of 60°F.

Serial # SN-214U

Ground Cond. Fallow field.

Cal. Check 2/14/2023

Tested By H. Philson

Test Date February 17, 2023

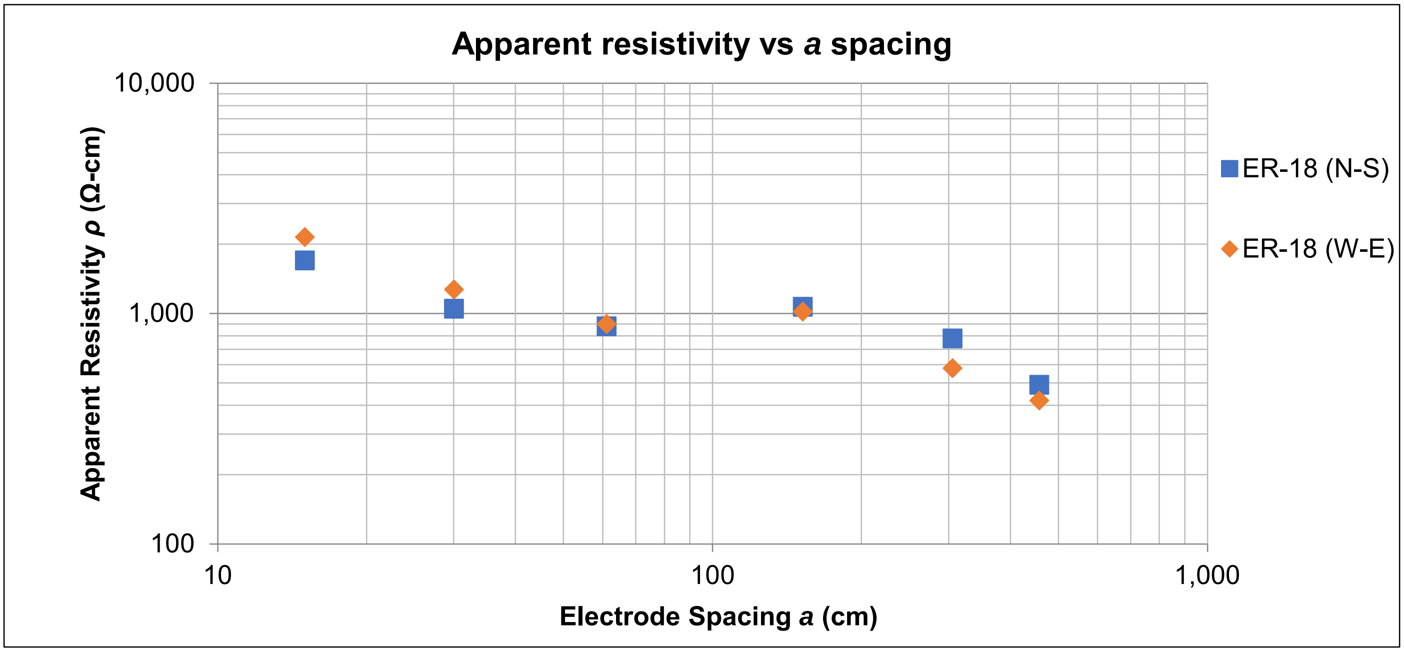
Method Wenner 4-pin ASTM G57-06 (2012); IEEE 81-2012

Notes & Conflicts Arrays oriented N-S and W-E with a common midpoint.

Apparent resistivity ρ is calculated as :

$$\rho = \frac{4\pi aR}{1 + \frac{2a}{\sqrt{a^2 + 4b^2}} - \frac{a}{\sqrt{a^2 + b^2}}}$$

Electrode Spacing *a*		**Electrode Depth *b***		**ER-18 (N-S)**		**ER-18 (W-E)**	
(feet)	(centimeters)	(inches)	(centimeters)	Measured Resistance *R*	Apparent Resistivity *ρ*	Measured Resistance *R*	Apparent Resistivity *ρ*
				Ω	(Ω-cm)	Ω	(Ω-cm)
0.5	15	1	3	16.90	1700	21.40	2150
1	30	1	3	5.494	1050	6.611	1270
2	61	2	5	2.272	880	2.322	900
5	152	6	15	1.1070	1070	1.0510	1020
10	305	12	30	0.4003	780	0.2955	580
15	457	12	30	0.1687	490	0.1446	420



FIELD ELECTRICAL RESISTIVITY DATA SHEET

Darden Solar Facility ■ Cantua Creek, Fresno County, California
October 13, 2023 ■ Terracon Project No. 60225172

NORCAL GEOPHYSICAL CONSULTANTS INC. A Terracon COMPANY

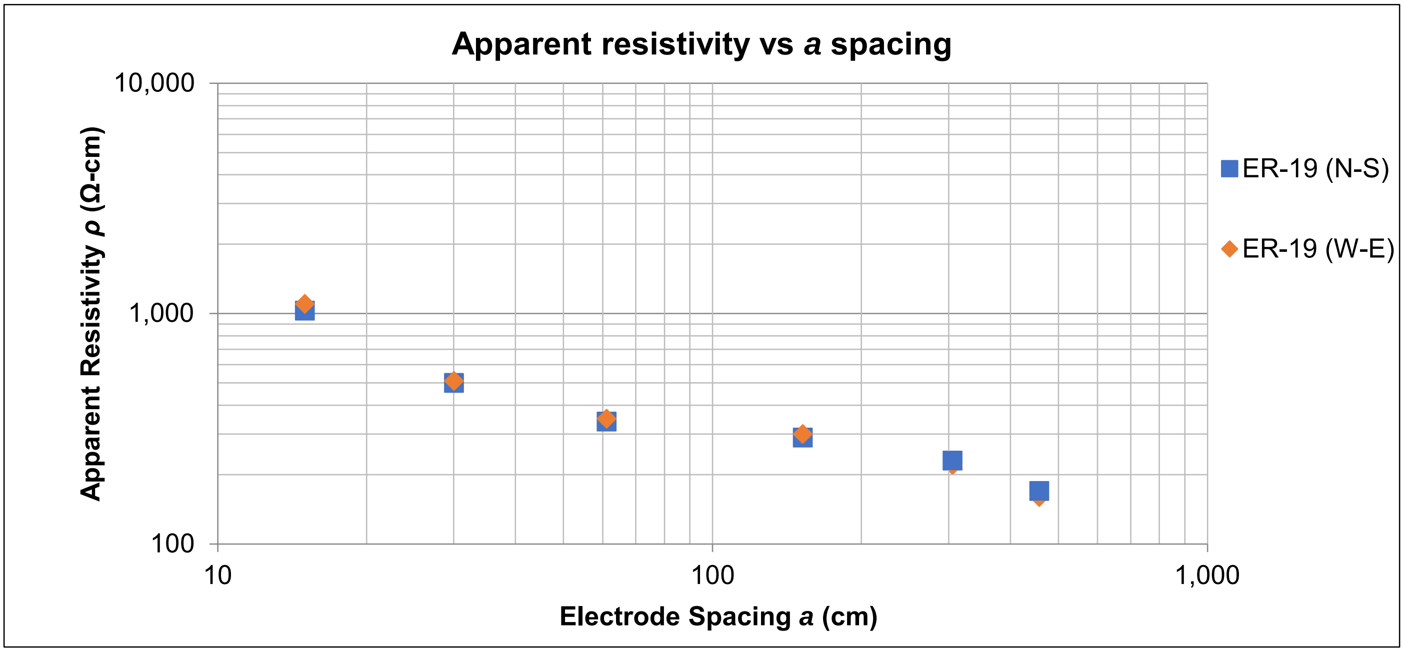
Array Loc. **ER-19** (36.505909°N, 120.190405°W)

Instrument	L&R Instruments - Ultra Mini Res	**Weather**	Clear, high of 60°F.
Serial #	SN-214U	**Ground Cond.**	Fallow field.
Cal. Check	2/14/2023	**Tested By**	H. Philson
Test Date	February 17, 2023	**Method**	Wenner 4-pin ASTM G57-06 (2012); IEEE 81-2012

Notes & Conflicts Arrays oriented N-S and W-E with a common midpoint.

Apparent resistivity ρ is calculated as : $\rho = \dfrac{4\pi a R}{1 + \dfrac{2a}{\sqrt{a^2 + 4b^2}} - \dfrac{a}{\sqrt{a^2 + b^2}}}$

Electrode Spacing *a*		**Electrode Depth *b***		**ER-19 (N-S)**		**ER-19 (W-E)**	
(feet)	(centimeters)	(inches)	(centimeters)	Measured Resistance *R*	Apparent Resistivity *ρ*	Measured Resistance *R*	Apparent Resistivity *ρ*
				Ω	(Ω-cm)	Ω	(Ω-cm)
0.5	15	1	3	10.23	1030	10.91	1100
1	30	1	3	2.615	500	2.682	510
2	61	2	5	0.8652	340	0.8919	350
5	152	6	15	0.2991	290	0.3053	300
10	305	12	30	0.1171	230	0.1122	220
15	457	12	30	0.0597	170	0.0569	160



FIELD ELECTRICAL RESISTIVITY DATA SHEET

Darden Solar Facility ■ Cantua Creek, Fresno County, California
October 13, 2023 ■ Terracon Project No. 60225172

NORCAL GEOPHYSICAL CONSULTANTS INC.
A Terracon COMPANY

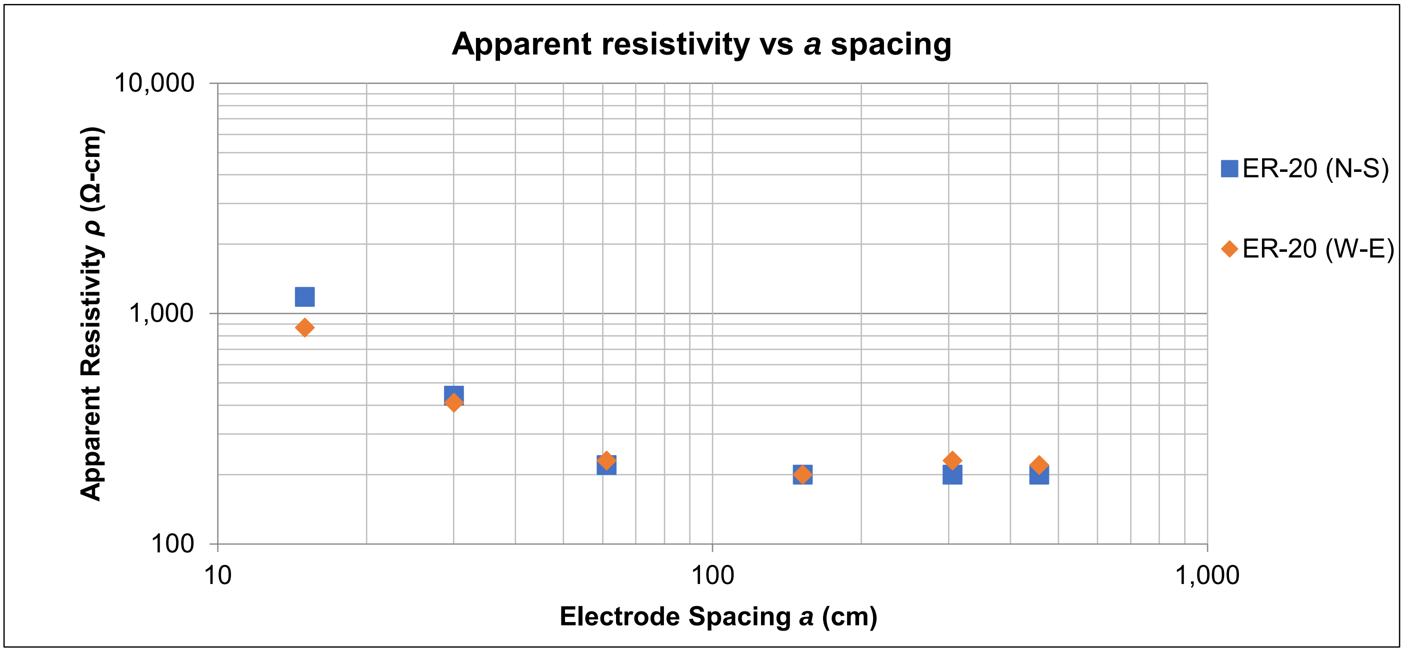
Array Loc. **ER-20** (36.502665°N, 120.183887°W)

Instrument	L&R Instruments - Ultra Mini Res	**Weather**	Clear, high of 60°F.
Serial #	SN-214U	**Ground Cond.**	Fallow field.
Cal. Check	2/14/2023	**Tested By**	H. Philson
Test Date	February 17, 2023	**Method**	Wenner 4-pin ASTM G57-06 (2012); IEEE 81-2012

Notes & Conflicts Arrays oriented N-S and W-E with a common midpoint.

Apparent resistivity ρ is calculated as :
$$\rho = \frac{4\pi a R}{1 + \frac{2a}{\sqrt{a^2 + 4b^2}} - \frac{a}{\sqrt{a^2 + b^2}}}$$

Electrode Spacing *a*		**Electrode Depth *b***		**ER-20 (N-S)**		**ER-20 (W-E)**	
(feet)	(centimeters)	(inches)	(centimeters)	Measured Resistance *R*	Apparent Resistivity ρ	Measured Resistance *R*	Apparent Resistivity ρ
				Ω	(Ω-cm)	Ω	(Ω-cm)
0.5	15	1	3	11.79	1180	8.613	870
1	30	1	3	2.301	440	2.151	410
2	61	2	5	0.5633	220	0.5832	230
5	152	6	15	0.2071	200	0.2009	200
10	305	12	30	0.1035	200	0.1202	230
15	457	12	30	0.0691	200	0.0763	220



FIELD ELECTRICAL RESISTIVITY DATA SHEET

Darden Solar Facility ■ Cantua Creek, Fresno County, California
October 13, 2023 ■ Terracon Project No. 60225172

Array Loc. **ER-21** (36.508446°N, 120.185669°W)

Instrument L&R Instruments - Ultra Mini Res

Weather Clear, high of 60°F.

Serial # SN-214U

Ground Cond. Fallow field.

Cal. Check 2/14/2023

Tested By H. Philson

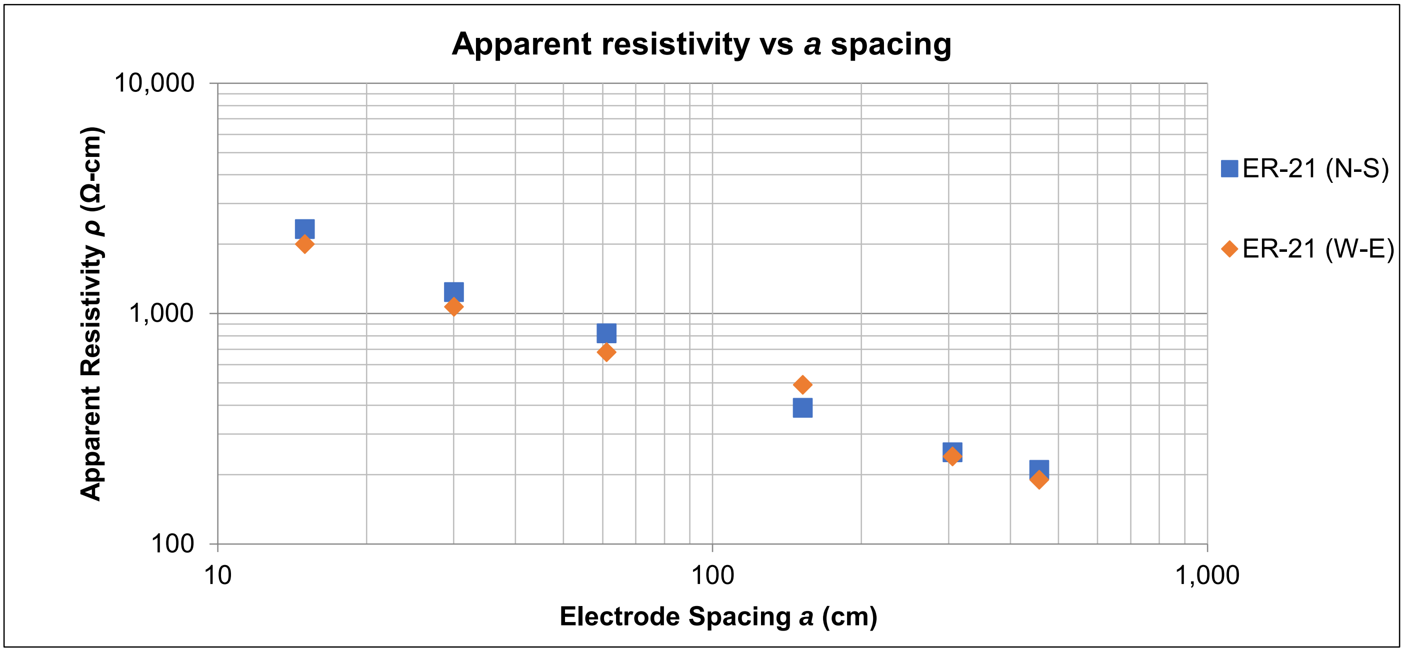
Test Date February 17, 2023

Method Wenner 4-pin ASTM G57-06 (2012); IEEE 81-2012

Notes & Conflicts Arrays oriented N-S and W-E with a common midpoint.

Apparent resistivity ρ is calculated as : $$\rho = \frac{4\pi a R}{1 + \frac{2a}{\sqrt{a^2 + 4b^2}} - \frac{a}{\sqrt{a^2 + b^2}}}$$

Electrode Spacing *a*		**Electrode Depth *b***		**ER-21 (N-S)**		**ER-21 (W-E)**	
(feet)	(centimeters)	(inches)	(centimeters)	Measured Resistance *R*	Apparent Resistivity ρ	Measured Resistance *R*	Apparent Resistivity ρ
				Ω	(Ω-cm)	Ω	(Ω-cm)
0.5	15	1	3	23.20	2330	19.90	2000
1	30	1	3	6.462	1240	5.582	1070
2	61	2	5	2.102	820	1.751	680
5	152	6	15	0.4065	390	0.5041	490
10	305	12	30	0.1285	250	0.1213	240
15	457	12	30	0.0712	210	0.0671	190



FIELD ELECTRICAL RESISTIVITY DATA SHEET

Darden Solar Facility ■ Cantua Creek, Fresno County, California
October 13, 2023 ■ Terracon Project No. 60225172

NORCAL GEOPHYSICAL CONSULTANTS INC.
A Terracon COMPANY

Array Loc. **ER-22** (36.499705°N, 120.224811°W)

Instrument L&R Instruments - Ultra Mini Res

Serial # SN-214U

Cal. Check 2/14/2023

Test Date February 17, 2023

Weather Clear, high of 60°F.

Ground Cond. Fallow field.

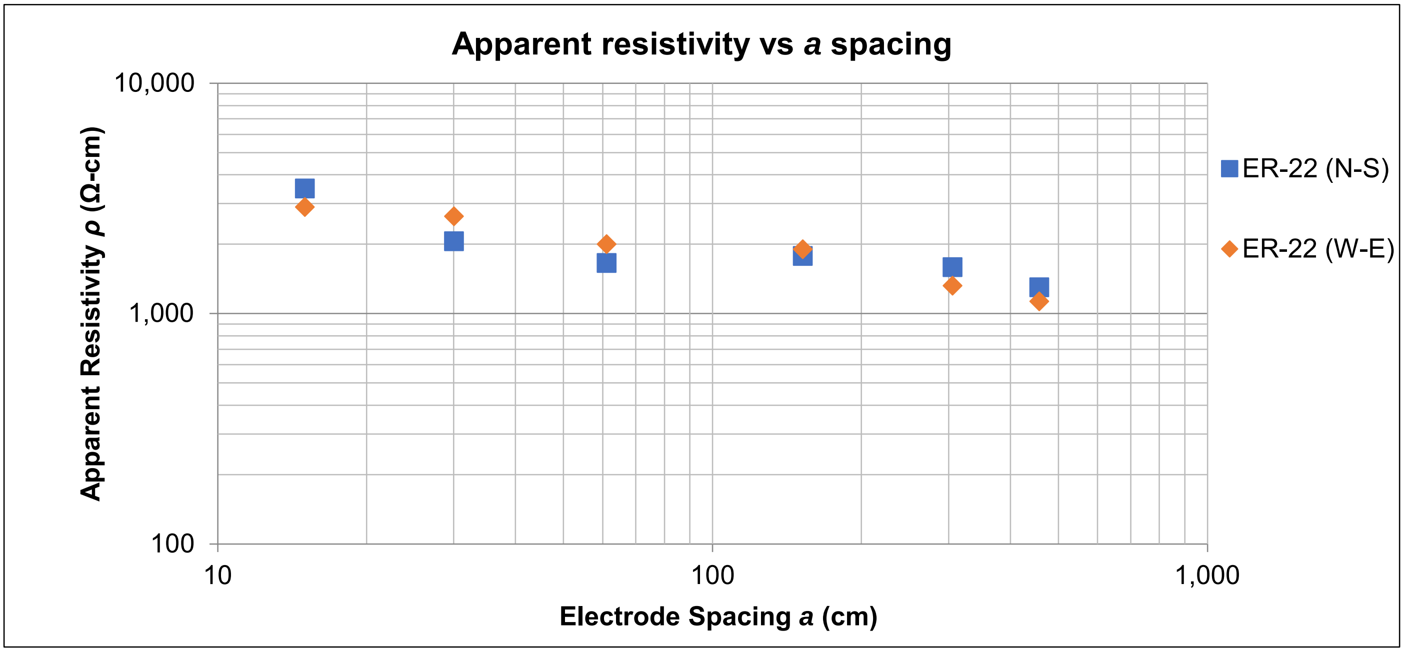
Tested By H. Philson

Method Wenner 4-pin ASTM G57-06 (2012); IEEE 81-2012

Notes & Conflicts Arrays oriented N-S and W-E with a common midpoint.

Apparent resistivity ρ is calculated as : $\rho = \dfrac{4\pi a R}{1 + \dfrac{2a}{\sqrt{a^2 + 4b^2}} - \dfrac{a}{\sqrt{a^2 + b^2}}}$

Electrode Spacing *a*		**Electrode Depth *b***		**ER-22 (N-S)**		**ER-22 (W-E)**	
(feet)	(centimeters)	(inches)	(centimeters)	Measured Resistance *R*	Apparent Resistivity *ρ*	Measured Resistance *R*	Apparent Resistivity *ρ*
				Ω	(Ω-cm)	Ω	(Ω-cm)
0.5	15	1	3	34.70	3490	28.90	2900
1	30	1	3	10.72	2060	13.79	2640
2	61	2	5	4.292	1660	5.155	2000
5	152	6	15	1.838	1780	1.956	1900
10	305	12	30	0.8169	1590	0.6752	1320
15	457	12	30	0.4486	1300	0.3922	1130



FIELD ELECTRICAL RESISTIVITY DATA SHEET

Darden Solar Facility ■ Cantua Creek, Fresno County, California
October 13, 2023 ■ Terracon Project No. 60225172

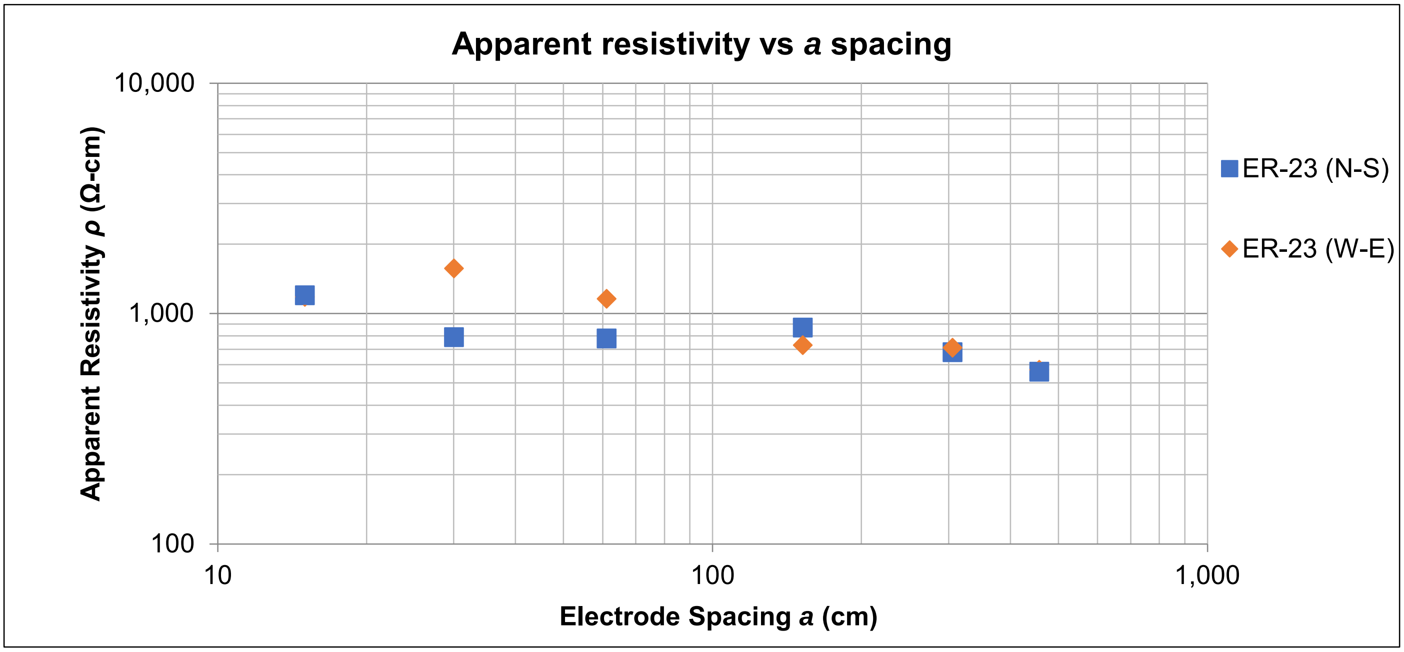
Array Loc. **ER-23** (36.494995°N, 120.219177°W)

Instrument	L&R Instruments - Ultra Mini Res	**Weather**	Clear, high of 60°F.
Serial #	SN-214U	**Ground Cond.**	Fallow field.
Cal. Check	2/14/2023	**Tested By**	H. Philson
Test Date	February 17, 2023	**Method**	Wenner 4-pin ASTM G57-06 (2012); IEEE 81-2012

Notes & Conflicts Arrays oriented N-S and W-E with a common midpoint.

Apparent resistivity ρ is calculated as : $$\rho = \frac{4\pi a R}{1 + \frac{2a}{\sqrt{a^2 + 4b^2}} - \frac{a}{\sqrt{a^2 + b^2}}}$$

Electrode Spacing *a*		**Electrode Depth *b***		**ER-23 (N-S)**		**ER-23 (W-E)**	
(feet)	(centimeters)	(inches)	(centimeters)	Measured Resistance *R*	Apparent Resistivity ρ	Measured Resistance *R*	Apparent Resistivity ρ
				Ω	(Ω-cm)	Ω	(Ω-cm)
0.5	15	1	3	11.94	1200	11.73	1180
1	30	1	3	4.128	790	8.175	1570
2	61	2	5	2.015	780	2.981	1160
5	152	6	15	0.8962	870	0.7535	730
10	305	12	30	0.3475	680	0.3647	710
15	457	12	30	0.1932	560	0.1963	570



FIELD ELECTRICAL RESISTIVITY DATA SHEET

Darden Solar Facility ■ Cantua Creek, Fresno County, California
October 13, 2023 ■ Terracon Project No. 60225172

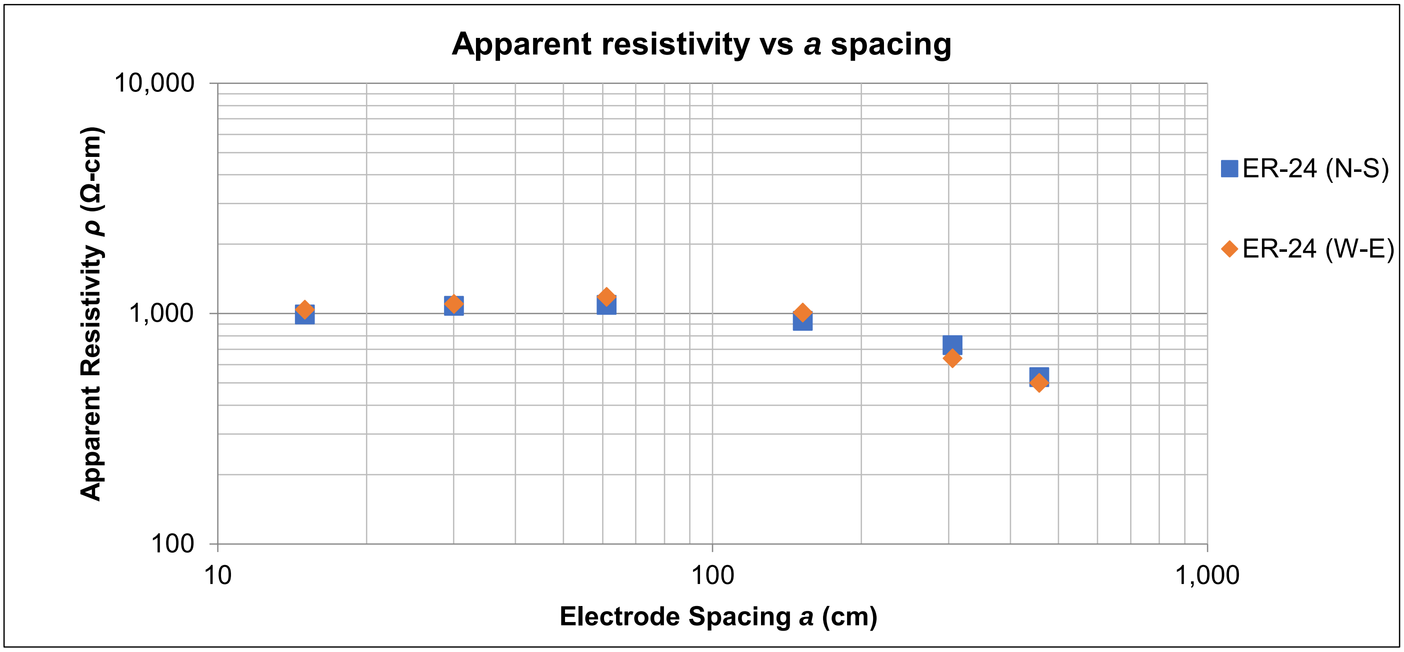
Array Loc. **ER-24** (36.498109°N, 120.220407°W)

Instrument	L&R Instruments - Ultra Mini Res	**Weather**	Clear, high of 60°F.
Serial #	SN-214U	**Ground Cond.**	Fallow field.
Cal. Check	2/14/2023	**Tested By**	H. Philson
Test Date	February 17, 2023	**Method**	Wenner 4-pin ASTM G57-06 (2012); IEEE 81-2012

Notes & Conflicts Arrays oriented N-S and W-E with a common midpoint.

Apparent resistivity ρ is calculated as : $\rho = \dfrac{4\pi aR}{1 + \dfrac{2a}{\sqrt{a^2 + 4b^2}} - \dfrac{a}{\sqrt{a^2 + b^2}}}$

Electrode Spacing *a*		**Electrode Depth *b***		**ER-24 (N-S)**		**ER-24 (W-E)**	
(feet)	(centimeters)	(inches)	(centimeters)	Measured Resistance *R* Ω	Apparent Resistivity *ρ* (Ω-cm)	Measured Resistance *R* Ω	Apparent Resistivity *ρ* (Ω-cm)
0.5	15	1	3	9.90	990	10.36	1040
1	30	1	3	5.631	1080	5.725	1100
2	61	2	5	2.817	1090	3.031	1180
5	152	6	15	0.9588	930	1.0390	1010
10	305	12	30	0.3731	730	0.3275	640
15	457	12	30	0.1845	530	0.1717	500



FIELD ELECTRICAL RESISTIVITY DATA SHEET

Darden Solar Facility ■ Cantua Creek, Fresno County, California
October 13, 2023 ■ Terracon Project No. 60225172

Array Loc. **ER-25** (36.498925°N, 120.212169°W)

Instrument L&R Instruments - Ultra Mini Res

Weather Clear, high of 68°F.

Serial # SN-214U

Ground Cond. Fallow field.

Cal. Check 2/14/2023

Tested By H. Philson

Test Date February 20, 2023

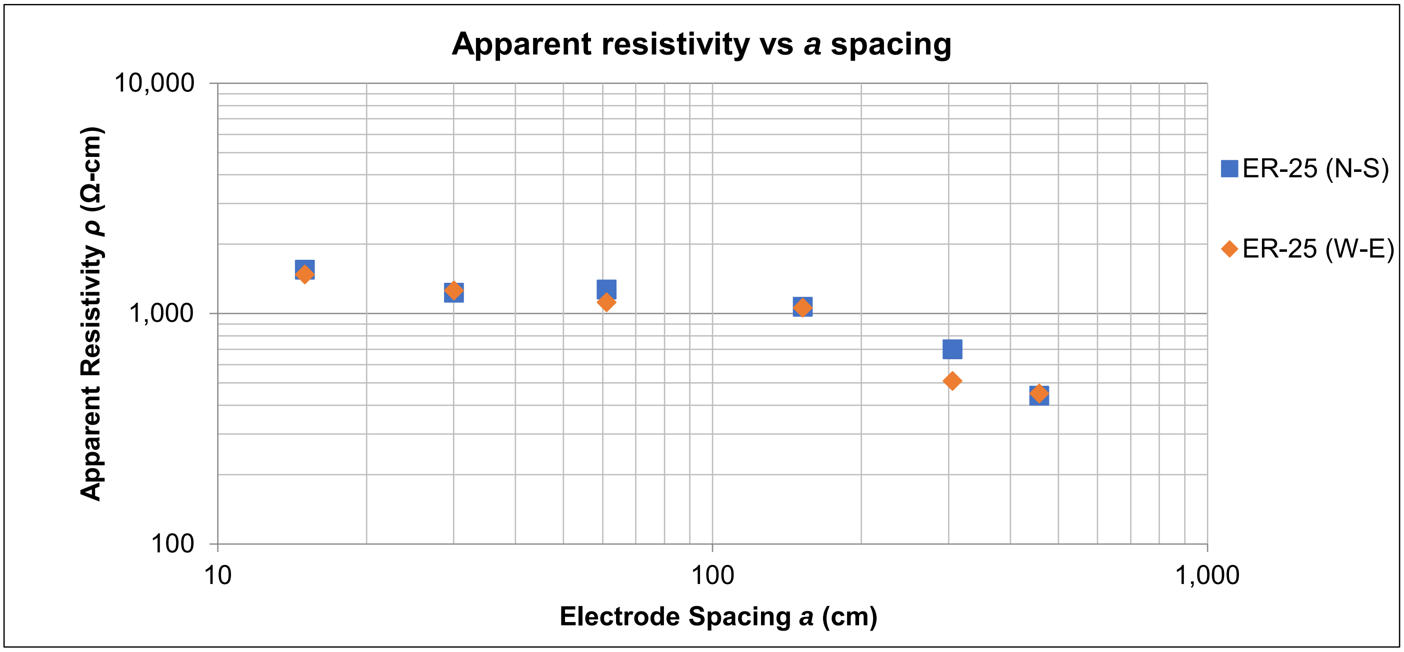
Method Wenner 4-pin ASTM G57-06 (2012); IEEE 81-2012

Notes & Conflicts Arrays oriented N-S and W-E with a common midpoint.

Apparent resistivity ρ is calculated as :

$$\rho = \frac{4\pi a R}{1 + \frac{2a}{\sqrt{a^2 + 4b^2}} - \frac{a}{\sqrt{a^2 + b^2}}}$$

Electrode Spacing *a*		**Electrode Depth *b***		**ER-25 (N-S)**		**ER-25 (W-E)**	
(feet)	(centimeters)	(inches)	(centimeters)	Measured Resistance *R*	Apparent Resistivity *ρ*	Measured Resistance *R*	Apparent Resistivity *ρ*
				Ω	(Ω-cm)	Ω	(Ω-cm)
0.5	15	1	3	15.40	1550	14.74	1480
1	30	1	3	6.405	1230	6.573	1260
2	61	2	5	3.277	1270	2.899	1120
5	152	6	15	1.1050	1070	1.0950	1060
10	305	12	30	0.3592	700	0.2615	510
15	457	12	30	0.1514	440	0.1572	450



FIELD ELECTRICAL RESISTIVITY DATA SHEET

Darden Solar Facility ■ Cantua Creek, Fresno County, California
October 13, 2023 ■ Terracon Project No. 60225172

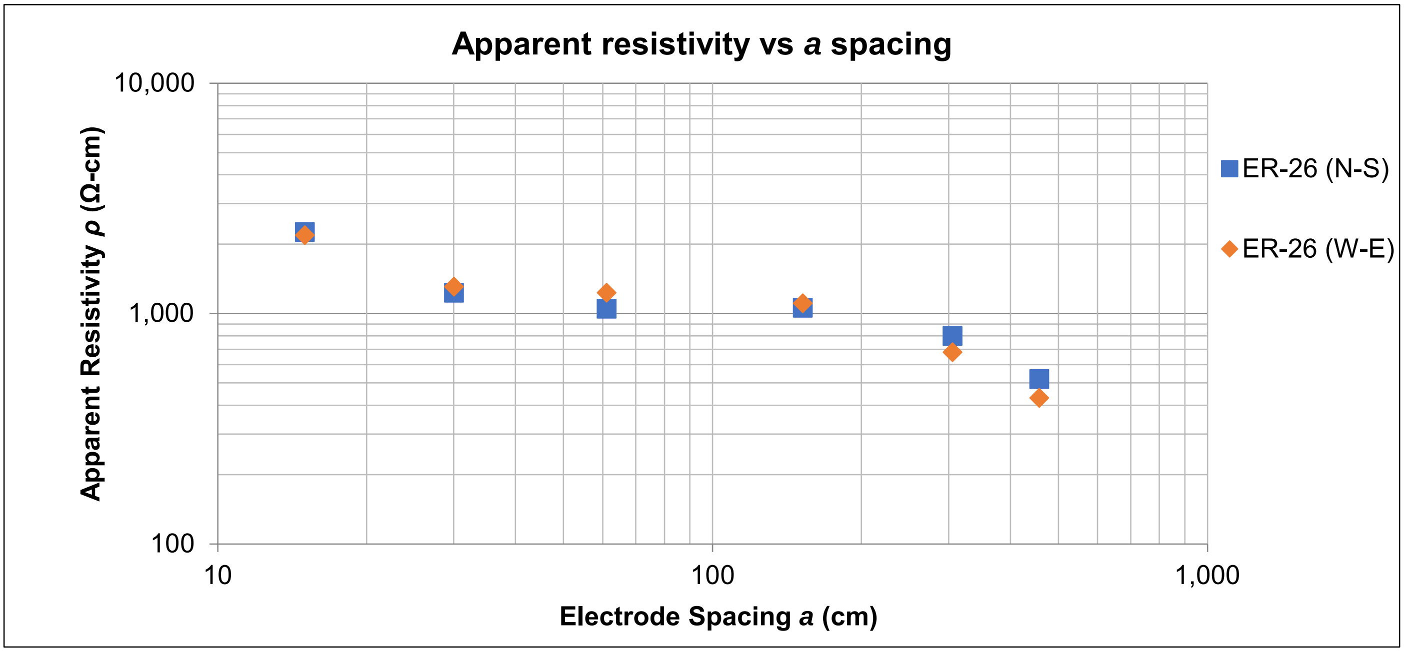
Array Loc. **ER-26** (36.495512°N, 120.209458°W)

Instrument	L&R Instruments - Ultra Mini Res	**Weather**	Clear, high of 68°F.
Serial #	SN-214U	**Ground Cond.**	Fallow field.
Cal. Check	2/14/2023	**Tested By**	H. Philson
Test Date	February 20, 2023	**Method**	Wenner 4-pin ASTM G57-06 (2012); IEEE 81-2012

Notes & Conflicts Arrays oriented N-S and W-E with a common midpoint.

Apparent resistivity ρ is calculated as :
$$\rho = \frac{4\pi a R}{1 + \frac{2a}{\sqrt{a^2 + 4b^2}} - \frac{a}{\sqrt{a^2 + b^2}}}$$

Electrode Spacing *a*		**Electrode Depth *b***		**ER-26 (N-S)**		**ER-26 (W-E)**	
(feet)	(centimeters)	(inches)	(centimeters)	Measured Resistance *R*	Apparent Resistivity *ρ*	Measured Resistance *R*	Apparent Resistivity *ρ*
				Ω	(Ω-cm)	Ω	(Ω-cm)
0.5	15	1	3	22.50	2260	21.80	2190
1	30	1	3	6.437	1230	6.841	1310
2	61	2	5	2.707	1050	3.162	1230
5	152	6	15	1.091	1060	1.141	1110
10	305	12	30	0.4092	800	0.3478	680
15	457	12	30	0.1786	520	0.1492	430



FIELD ELECTRICAL RESISTIVITY DATA SHEET

Darden Solar Facility ■ Cantua Creek, Fresno County, California
October 13, 2023 ■ Terracon Project No. 60225172

NORCAL GEOPHYSICAL CONSULTANTS INC.
A Terracon COMPANY

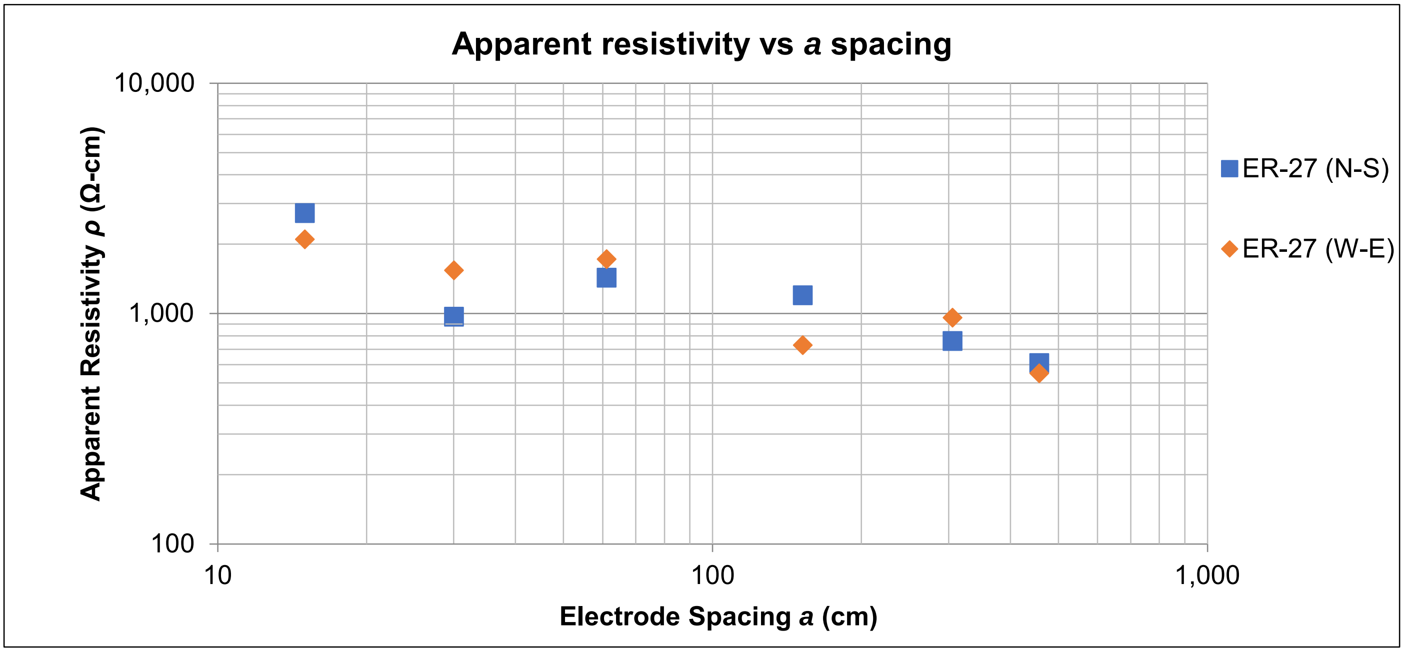
Array Loc. **ER-27** (36.497761°N, 120.202444°W)

Instrument	L&R Instruments - Ultra Mini Res	**Weather**	Clear, high of 68°F.
Serial #	SN-214U	**Ground Cond.**	Fallow field.
Cal. Check	2/14/2023	**Tested By**	H. Philson
Test Date	February 20, 2023	**Method**	Wenner 4-pin ASTM G57-06 (2012); IEEE 81-2012

Notes & Conflicts Arrays oriented N-S and W-E with a common midpoint.

Apparent resistivity ρ is calculated as : $$\rho = \frac{4\pi a R}{1 + \frac{2a}{\sqrt{a^2 + 4b^2}} - \frac{a}{\sqrt{a^2 + b^2}}}$$

Electrode Spacing *a*		**Electrode Depth *b***		**ER-27 (N-S)**		**ER-27 (W-E)**	
(feet)	(centimeters)	(inches)	(centimeters)	Measured Resistance *R* Ω	Apparent Resistivity *ρ* (Ω-cm)	Measured Resistance *R* Ω	Apparent Resistivity *ρ* (Ω-cm)
0.5	15	1	3	27.20	2730	20.90	2100
1	30	1	3	5.063	970	8.009	1540
2	61	2	5	3.679	1430	4.427	1720
5	152	6	15	1.231	1200	0.7556	730
10	305	12	30	0.3885	760	0.4926	960
15	457	12	30	0.2102	610	0.1887	550



FIELD ELECTRICAL RESISTIVITY DATA SHEET

Darden Solar Facility ■ Cantua Creek, Fresno County, California
October 13, 2023 ■ Terracon Project No. 60225172

Array Loc. **ER-28** (36.498849°N, 120.194133°W)

Instrument L&R Instruments - Ultra Mini Res

Weather Clear, high of 68°F.

Serial # SN-214U

Ground Cond. Fallow field.

Cal. Check 2/14/2023

Tested By H. Philson

Test Date February 20, 2023

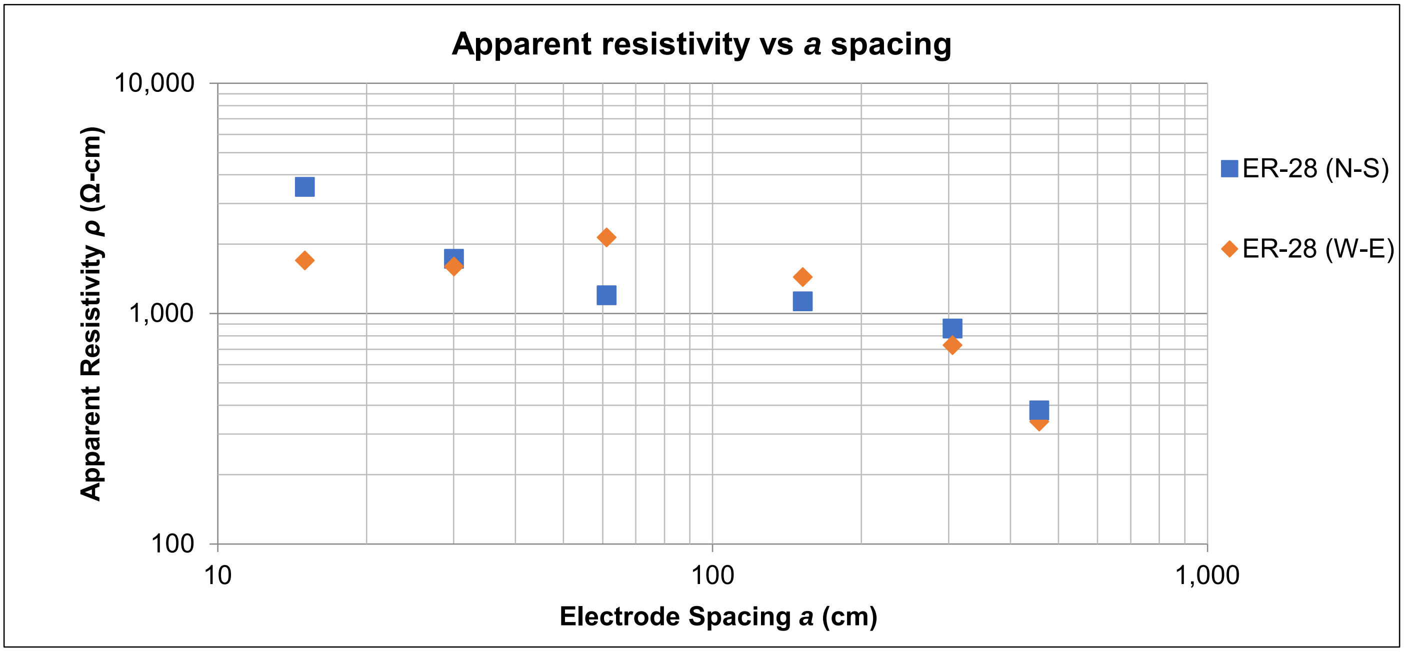
Method Wenner 4-pin ASTM G57-06 (2012); IEEE 81-2012

Notes & Conflicts Arrays oriented N-S and W-E with a common midpoint.

Apparent resistivity ρ is calculated as :

$$\rho = \frac{4\pi a R}{1 + \frac{2a}{\sqrt{a^2 + 4b^2}} - \frac{a}{\sqrt{a^2 + b^2}}}$$

Electrode Spacing *a*		**Electrode Depth *b***		**ER-28 (N-S)**		**ER-28 (W-E)**	
(feet)	(centimeters)	(inches)	(centimeters)	Measured Resistance *R*	Apparent Resistivity ρ	Measured Resistance *R*	Apparent Resistivity ρ
				Ω	(Ω-cm)	Ω	(Ω-cm)
0.5	15	1	3	35.30	3550	16.90	1700
1	30	1	3	9.039	1730	8.370	1600
2	61	2	5	3.094	1200	5.512	2140
5	152	6	15	1.1620	1130	1.4820	1440
10	305	12	30	0.4397	860	0.3751	730
15	457	12	30	0.1311	380	0.1174	340



FIELD ELECTRICAL RESISTIVITY DATA SHEET

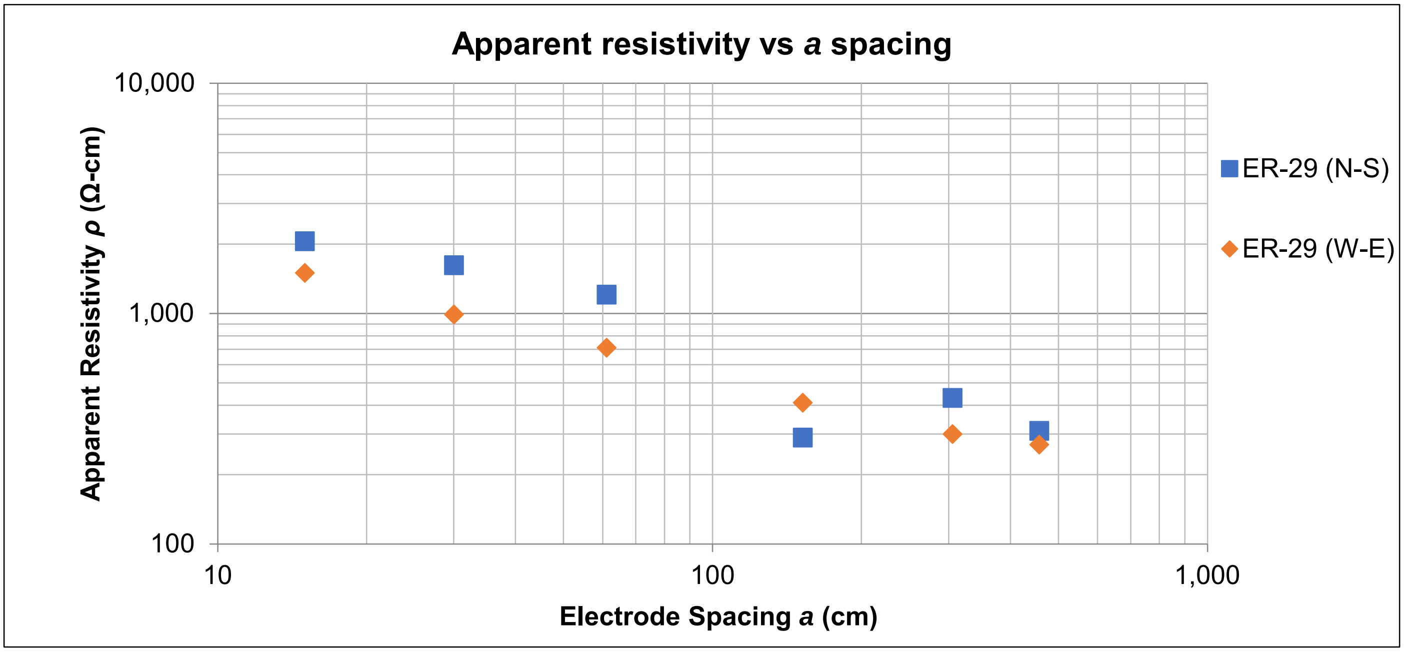
Darden Solar Facility ■ Cantua Creek, Fresno County, California
October 13, 2023 ■ Terracon Project No. 60225172

NORCAL GEOPHYSICAL CONSULTANTS INC.
A Terracon COMPANY

Array Loc.	**ER-29** (36.495334°N, 120.187883°W)		
Instrument	L&R Instruments - Ultra Mini Res	**Weather**	Clear, high of 68°F.
Serial #	SN-214U	**Ground Cond.**	Fallow field.
Cal. Check	2/14/2023	**Tested By**	H. Philson
Test Date	February 20, 2023	**Method**	Wenner 4-pin ASTM G57-06 (2012); IEEE 81-2012
Notes & Conflicts	Arrays oriented N-S and W-E with a common midpoint.		

Apparent resistivity ρ is calculated as :
$$\rho = \frac{4\pi a R}{1 + \frac{2a}{\sqrt{a^2 + 4b^2}} - \frac{a}{\sqrt{a^2 + b^2}}}$$

Electrode Spacing *a*		**Electrode Depth *b***		**ER-29 (N-S)**		**ER-29 (W-E)**	
(feet)	(centimeters)	(inches)	(centimeters)	Measured Resistance *R*	Apparent Resistivity *ρ*	Measured Resistance *R*	Apparent Resistivity *ρ*
				Ω	(Ω-cm)	Ω	(Ω-cm)
0.5	15	1	3	20.50	2060	14.90	1500
1	30	1	3	8.433	1620	5.154	990
2	61	2	5	3.125	1210	1.844	710
5	152	6	15	0.3030	290	0.4265	410
10	305	12	30	0.2211	430	0.1551	300
15	457	12	30	0.1061	310	0.0918	270



FIELD ELECTRICAL RESISTIVITY DATA SHEET

Darden Solar Facility ■ Cantua Creek, Fresno County, California
October 13, 2023 ■ Terracon Project No. 60225172

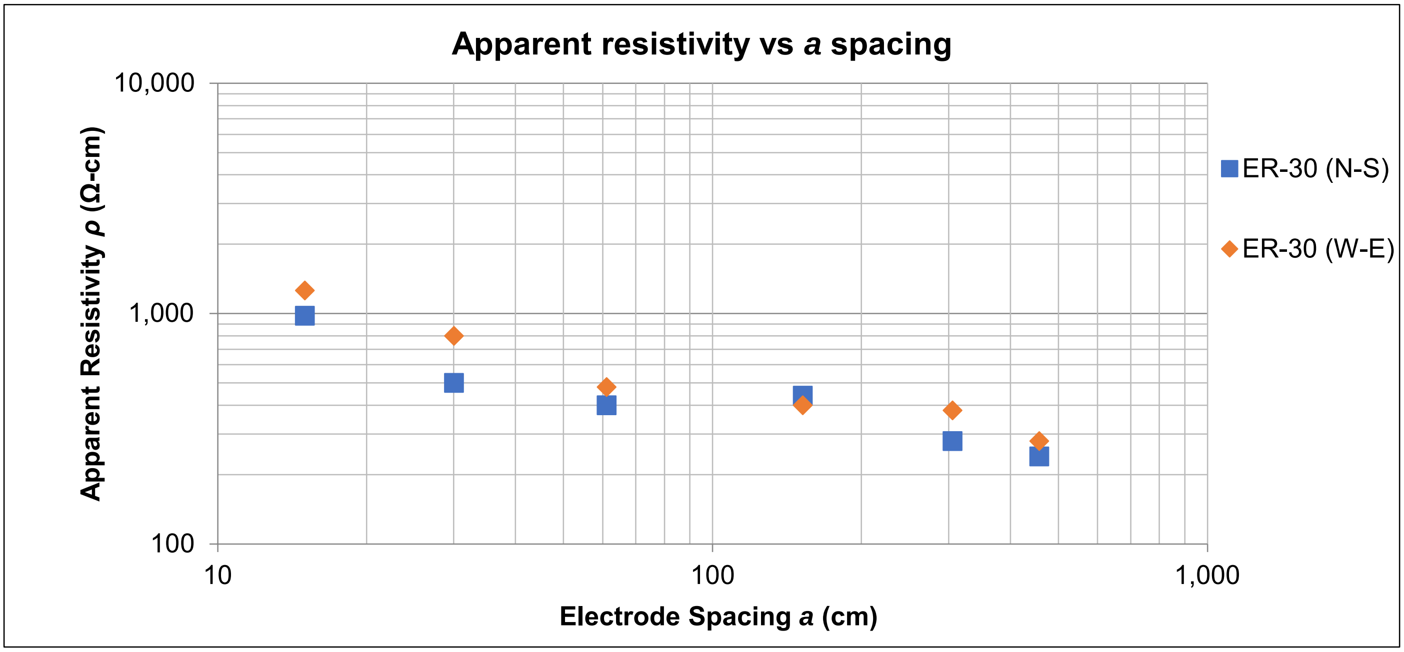
NORCAL GEOPHYSICAL CONSULTANTS INC.
A Terracon COMPANY

Array Loc.	**ER-30** (36.499317°N, 120.180214°W)		
Instrument	L&R Instruments - Ultra Mini Res	**Weather**	Clear, high of 68°F.
Serial #	SN-214U	**Ground Cond.**	Fallow field.
Cal. Check	2/14/2023	**Tested By**	H. Philson
Test Date	February 20, 2023	**Method**	Wenner 4-pin ASTM G57-06 (2012); IEEE 81-2012
Notes & Conflicts	Arrays oriented N-S and W-E with a common midpoint.		

Apparent resistivity ρ is calculated as :

$$\rho = \frac{4\pi a R}{1 + \frac{2a}{\sqrt{a^2 + 4b^2}} - \frac{a}{\sqrt{a^2 + b^2}}}$$

Electrode Spacing *a*		**Electrode Depth *b***		**ER-30 (N-S)**		**ER-30 (W-E)**	
(feet)	(centimeters)	(inches)	(centimeters)	Measured Resistance *R*	Apparent Resistivity *ρ*	Measured Resistance *R*	Apparent Resistivity *ρ*
				Ω	(Ω-cm)	Ω	(Ω-cm)
0.5	15	1	3	9.725	980	12.55	1260
1	30	1	3	2.605	500	4.196	800
2	61	2	5	1.032	400	1.235	480
5	152	6	15	0.4566	440	0.4139	400
10	305	12	30	0.1425	280	0.1933	380
15	457	12	30	0.0815	240	0.0966	280



FIELD ELECTRICAL RESISTIVITY DATA SHEET

Darden Solar Facility ■ Cantua Creek, Fresno County, California
October 13, 2023 ■ Terracon Project No. 60225172

NORCAL GEOPHYSICAL CONSULTANTS INC. A Terracon COMPANY

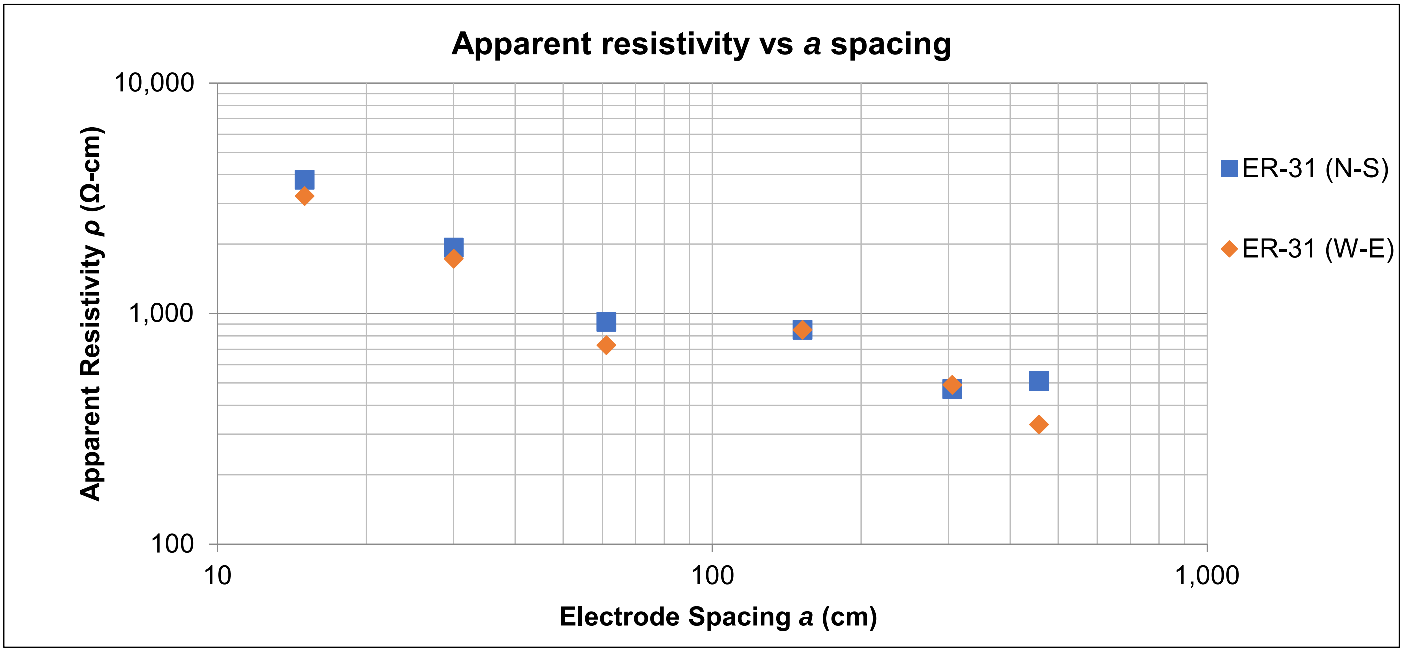
Array Loc. **ER-31** (36.495726°N, 120.173779°W)

Instrument	L&R Instruments - Ultra Mini Res	**Weather**	Clear, high of 51°F.
Serial #	SN-214U	**Ground Cond.**	Fallow field.
Cal. Check	2/14/2023	**Tested By**	H. Philson
Test Date	February 22, 2023	**Method**	Wenner 4-pin ASTM G57-06 (2012); IEEE 81-2012

Notes & Conflicts Arrays oriented N-S and W-E with a common midpoint.

Apparent resistivity ρ is calculated as : $$\rho = \frac{4\pi aR}{1 + \frac{2a}{\sqrt{a^2 + 4b^2}} - \frac{a}{\sqrt{a^2 + b^2}}}$$

Electrode Spacing *a*		**Electrode Depth *b***		**ER-31 (N-S)**		**ER-31 (W-E)**	
(feet)	(centimeters)	(inches)	(centimeters)	Measured Resistance *R* Ω	Apparent Resistivity *ρ* (Ω-cm)	Measured Resistance *R* Ω	Apparent Resistivity *ρ* (Ω-cm)
0.5	15	1	3	37.80	3800	32.20	3230
1	30	1	3	10.06	1930	9.002	1730
2	61	2	5	2.371	920	1.886	730
5	152	6	15	0.8729	850	0.8795	850
10	305	12	30	0.2433	470	0.2537	490
15	457	12	30	0.1765	510	0.1128	330



FIELD ELECTRICAL RESISTIVITY DATA SHEET

Darden Solar Facility ■ Cantua Creek, Fresno County, California
October 13, 2023 ■ Terracon Project No. 60225172

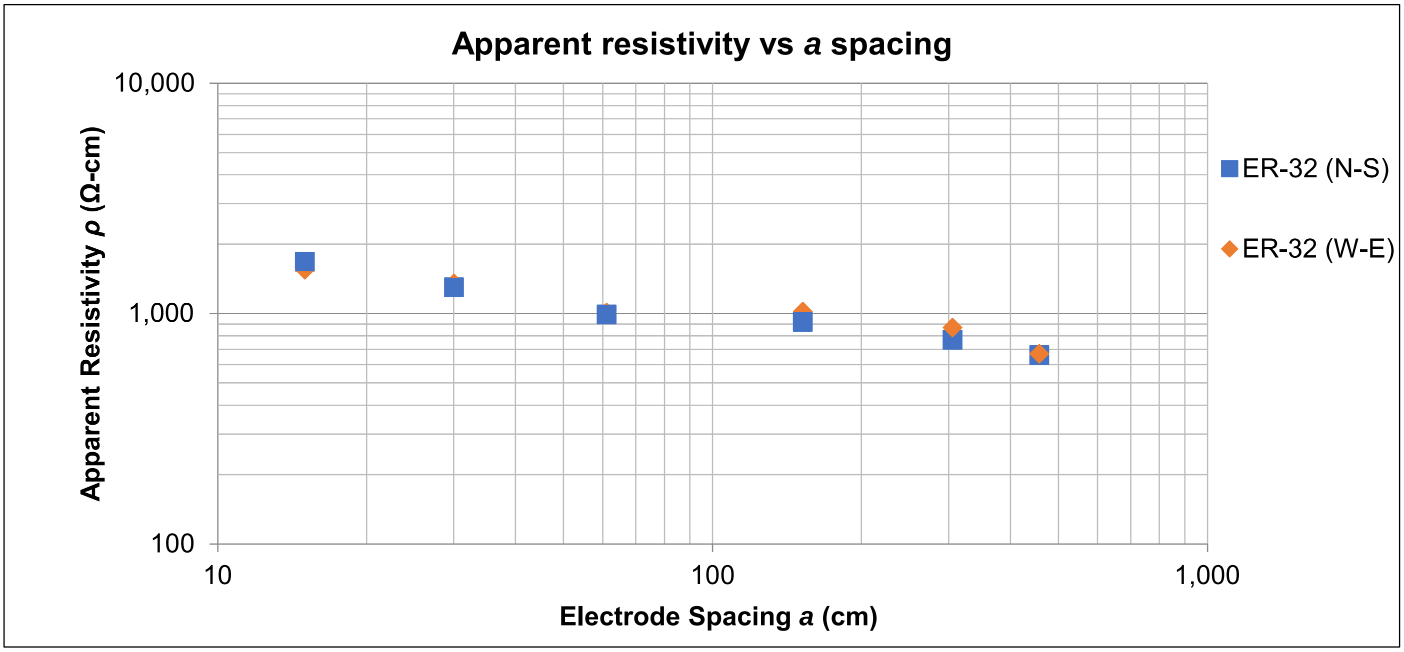
Array Loc. **ER-32** (36.493984°N, 120.224467°W)

Instrument	L&R Instruments - Ultra Mini Res	**Weather**	Clear, high of 51°F.
Serial #	SN-214U	**Ground Cond.**	Fallow field.
Cal. Check	2/14/2023	**Tested By**	H. Philson
Test Date	February 22, 2023	**Method**	Wenner 4-pin ASTM G57-06 (2012); IEEE 81-2012

Notes & Conflicts Arrays oriented N-S and W-E with a common midpoint.

Apparent resistivity ρ is calculated as : $$\rho = \frac{4\pi a R}{1 + \frac{2a}{\sqrt{a^2 + 4b^2}} - \frac{a}{\sqrt{a^2 + b^2}}}$$

Electrode Spacing *a*		**Electrode Depth *b***		**ER-32 (N-S)**		**ER-32 (W-E)**	
(feet)	(centimeters)	(inches)	(centimeters)	Measured Resistance *R*	Apparent Resistivity *ρ*	Measured Resistance *R*	Apparent Resistivity *ρ*
				Ω	(Ω-cm)	Ω	(Ω-cm)
0.5	15	1	3	16.70	1680	15.44	1550
1	30	1	3	6.761	1300	7.015	1350
2	61	2	5	2.562	990	2.602	1010
5	152	6	15	0.9462	920	1.054	1020
10	305	12	30	0.3936	770	0.4475	870
15	457	12	30	0.2288	660	0.2321	670



FIELD ELECTRICAL RESISTIVITY DATA SHEET

Darden Solar Facility ■ Cantua Creek, Fresno County, California

October 13, 2023 ■ Terracon Project No. 60225172

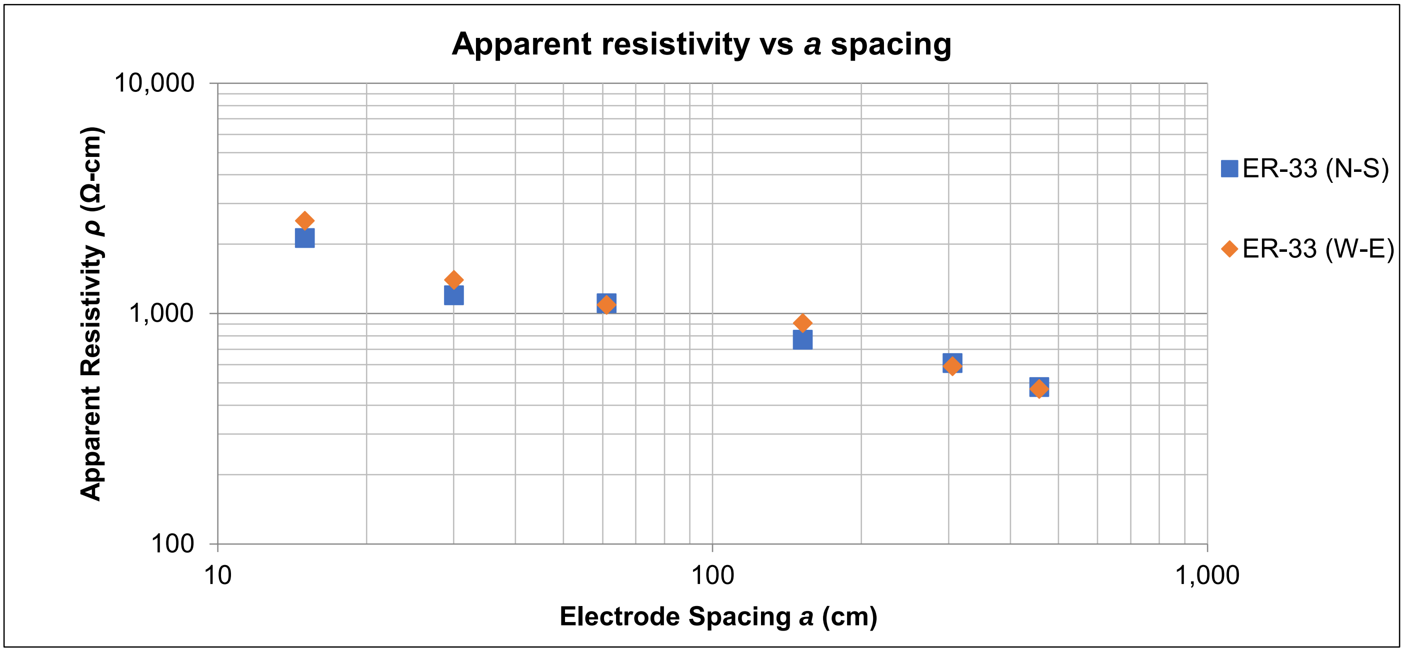
NORCAL GEOPHYSICAL CONSULTANTS INC.
A Terracon COMPANY

Array Loc.	**ER-33** (36.488395°N, 120.220226°W)		
Instrument	L&R Instruments - Ultra Mini Res	**Weather**	Clear, high of 51°F.
Serial #	SN-214U	**Ground Cond.**	Fallow field.
Cal. Check	2/14/2023	**Tested By**	H. Philson
Test Date	February 22, 2023	**Method**	Wenner 4-pin ASTM G57-06 (2012); IEEE 81-2012
Notes & Conflicts	Arrays oriented N-S and W-E with a common midpoint.		

Apparent resistivity ρ is calculated as :

$$\rho = \frac{4\pi a R}{1 + \frac{2a}{\sqrt{a^2 + 4b^2}} - \frac{a}{\sqrt{a^2 + b^2}}}$$

Electrode Spacing *a*		**Electrode Depth *b***		**ER-33 (N-S)**		**ER-33 (W-E)**	
(feet)	(centimeters)	(inches)	(centimeters)	Measured Resistance *R*	Apparent Resistivity ρ	Measured Resistance *R*	Apparent Resistivity ρ
				Ω	(Ω-cm)	Ω	(Ω-cm)
0.5	15	1	3	21.20	2130	25.20	2530
1	30	1	3	6.235	1200	7.319	1400
2	61	2	5	2.856	1110	2.819	1090
5	152	6	15	0.7977	770	0.9362	910
10	305	12	30	0.3114	610	0.3025	590
15	457	12	30	0.1653	480	0.1611	470



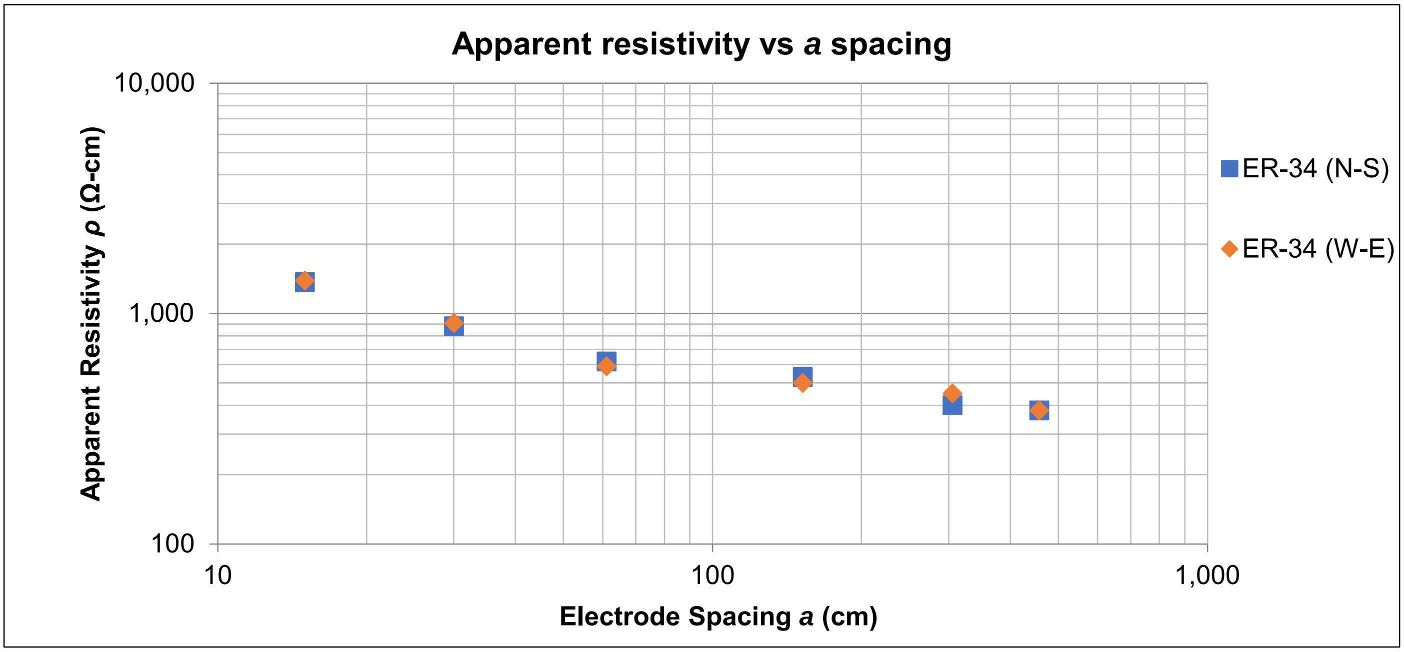
FIELD ELECTRICAL RESISTIVITY DATA SHEET

Darden Solar Facility ■ Cantua Creek, Fresno County, California
October 13, 2023 ■ Terracon Project No. 60225172

Array Loc.	**ER-34** (36.490306°N, 120.210079°W)		
Instrument	L&R Instruments - Ultra Mini Res	**Weather**	Clear, high of 51°F.
Serial #	SN-214U	**Ground Cond.**	Fallow field.
Cal. Check	2/14/2023	**Tested By**	H. Philson
Test Date	February 22, 2023	**Method**	Wenner 4-pin ASTM G57-06 (2012); IEEE 81-2012
Notes & Conflicts	Arrays oriented N-S and W-E with a common midpoint.		

Apparent resistivity ρ is calculated as :
$$\rho = \frac{4\pi a R}{1 + \frac{2a}{\sqrt{a^2 + 4b^2}} - \frac{a}{\sqrt{a^2 + b^2}}}$$

Electrode Spacing *a*		**Electrode Depth *b***		**ER-34 (N-S)**		**ER-34 (W-E)**	
(feet)	(centimeters)	(inches)	(centimeters)	Measured Resistance *R*	Apparent Resistivity *ρ*	Measured Resistance *R*	Apparent Resistivity *ρ*
				Ω	(Ω-cm)	Ω	(Ω-cm)
0.5	15	1	3	13.64	1370	13.86	1390
1	30	1	3	4.612	880	4.732	910
2	61	2	5	1.592	620	1.529	590
5	152	6	15	0.5435	530	0.5136	500
10	305	12	30	0.2072	400	0.2328	450
15	457	12	30	0.1321	380	0.1315	380



FIELD ELECTRICAL RESISTIVITY DATA SHEET

Darden Solar Facility ■ Cantua Creek, Fresno County, California
October 13, 2023 ■ Terracon Project No. 60225172

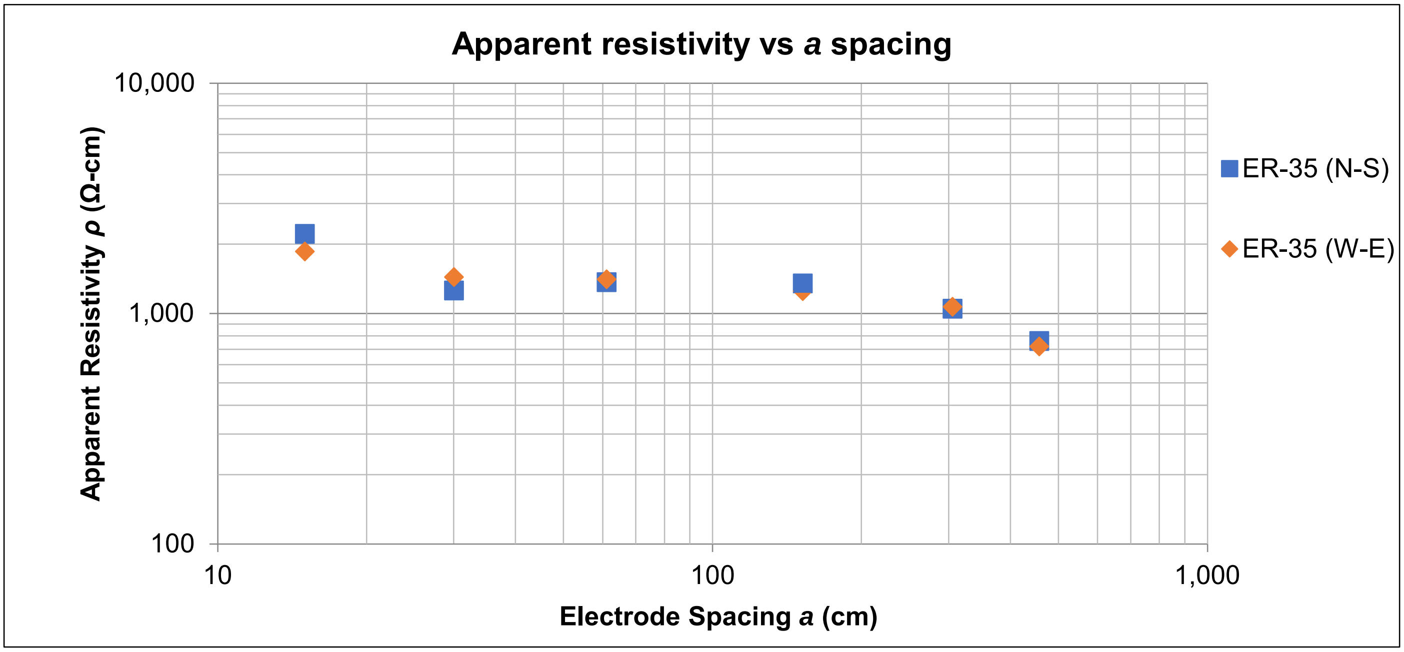
Array Loc. **ER-35** (36.489257°N, 120.215852°W)

Instrument	L&R Instruments - Ultra Mini Res	**Weather**	Clear, high of 51°F.
Serial #	SN-214U	**Ground Cond.**	Fallow field.
Cal. Check	2/14/2023	**Tested By**	H. Philson
Test Date	February 22, 2023	**Method**	Wenner 4-pin ASTM G57-06 (2012); IEEE 81-2012

Notes & Conflicts Arrays oriented N-S and W-E with a common midpoint.

Apparent resistivity ρ is calculated as : $\rho = \dfrac{4\pi a R}{1 + \dfrac{2a}{\sqrt{a^2 + 4b^2}} - \dfrac{a}{\sqrt{a^2 + b^2}}}$

Electrode Spacing *a*		**Electrode Depth *b***		**ER-35 (N-S)**		**ER-35 (W-E)**	
(feet)	(centimeters)	(inches)	(centimeters)	Measured Resistance *R*	Apparent Resistivity *ρ*	Measured Resistance *R*	Apparent Resistivity *ρ*
				Ω	(Ω-cm)	Ω	(Ω-cm)
0.5	15	1	3	22.10	2220	18.50	1860
1	30	1	3	6.582	1260	7.485	1440
2	61	2	5	3.535	1370	3.646	1410
5	152	6	15	1.388	1350	1.285	1250
10	305	12	30	0.5412	1050	0.5501	1070
15	457	12	30	0.2625	760	0.2474	720



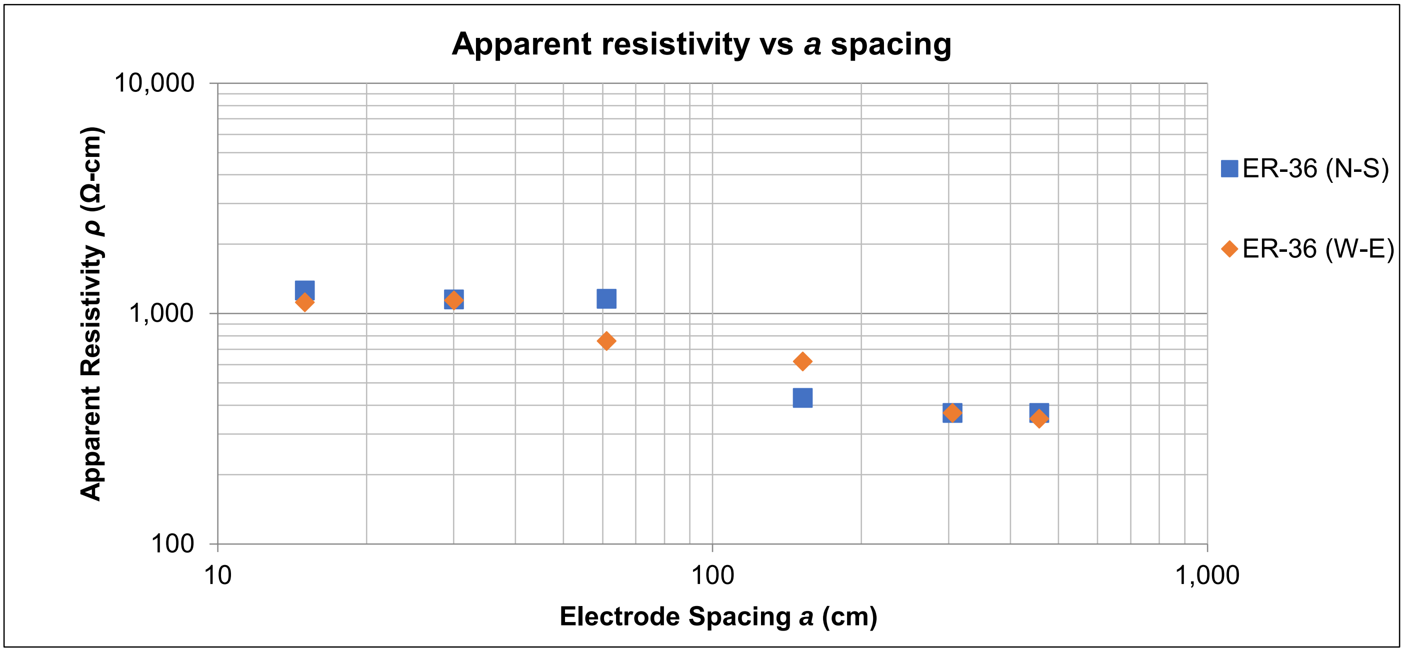
FIELD ELECTRICAL RESISTIVITY DATA SHEET

Darden Solar Facility ■ Cantua Creek, Fresno County, California
October 13, 2023 ■ Terracon Project No. 60225172

Array Loc.	**ER-36** (36.488359°N, 120.202268°W)		
Instrument	L&R Instruments - Ultra Mini Res	**Weather**	Clear, high of 51°F.
Serial #	SN-214U	**Ground Cond.**	Fallow field.
Cal. Check	2/14/2023	**Tested By**	H. Philson
Test Date	February 22, 2023	**Method**	Wenner 4-pin ASTM G57-06 (2012); IEEE 81-2012
Notes & Conflicts	Arrays oriented N-S and W-E with a common midpoint.		

Apparent resistivity ρ is calculated as : $\rho = \dfrac{4\pi a R}{1 + \dfrac{2a}{\sqrt{a^2 + 4b^2}} - \dfrac{a}{\sqrt{a^2 + b^2}}}$

Electrode Spacing *a*		**Electrode Depth *b***		**ER-36 (N-S)**		**ER-36 (W-E)**	
(feet)	(centimeters)	(inches)	(centimeters)	Measured Resistance *R*	Apparent Resistivity *ρ*	Measured Resistance *R*	Apparent Resistivity *ρ*
				Ω	(Ω-cm)	Ω	(Ω-cm)
0.5	15	1	3	12.54	1260	11.13	1120
1	30	1	3	6.018	1150	5.921	1140
2	61	2	5	2.982	1160	1.961	760
5	152	6	15	0.4385	430	0.6414	620
10	305	12	30	0.1882	370	0.1903	370
15	457	12	30	0.1269	370	0.1195	350



FIELD ELECTRICAL RESISTIVITY DATA SHEET

Darden Solar Facility ■ Cantua Creek, Fresno County, California
October 13, 2023 ■ Terracon Project No. 60225172

Array Loc. **ER-37** (36.492740°N, 120.196125°W)

Instrument L&R Instruments - Ultra Mini Res

Weather Clear, high of 50°F.

Serial # SN-214U

Ground Cond. Fallow field.

Cal. Check 2/14/2023

Tested By H. Philson

Test Date February 23, 2023

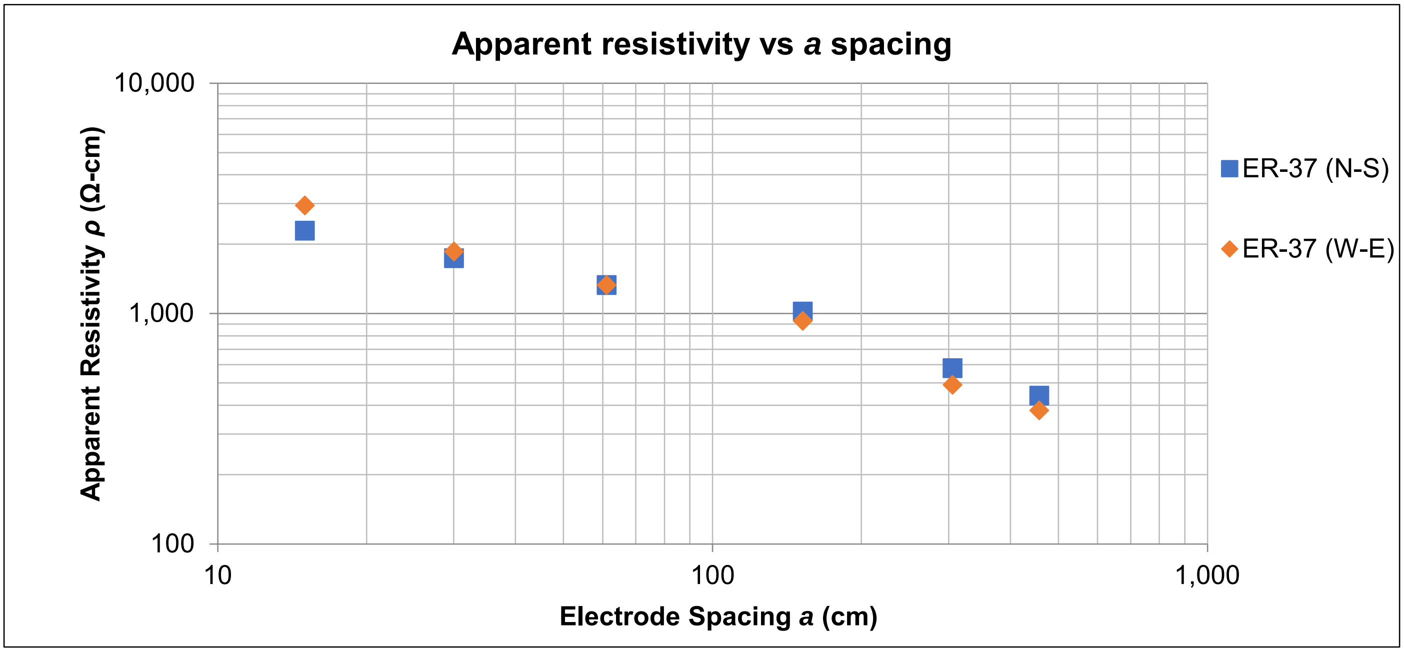
Method Wenner 4-pin ASTM G57-06 (2012); IEEE 81-2012

Notes & Conflicts Arrays oriented N-S and W-E with a common midpoint.

Apparent resistivity ρ is calculated as :

$$\rho = \frac{4\pi a R}{1 + \frac{2a}{\sqrt{a^2 + 4b^2}} - \frac{a}{\sqrt{a^2 + b^2}}}$$

Electrode Spacing *a*		**Electrode Depth *b***		**ER-37 (N-S)**		**ER-37 (W-E)**	
(feet)	(centimeters)	(inches)	(centimeters)	Measured Resistance *R*	Apparent Resistivity *ρ*	Measured Resistance *R*	Apparent Resistivity *ρ*
				Ω	(Ω-cm)	Ω	(Ω-cm)
0.5	15	1	3	22.80	2290	29.40	2950
1	30	1	3	9.082	1740	9.682	1860
2	61	2	5	3.424	1330	3.423	1330
5	152	6	15	1.048	1020	0.9592	930
10	305	12	30	0.2952	580	0.2493	490
15	457	12	30	0.1516	440	0.1302	380



FIELD ELECTRICAL RESISTIVITY DATA SHEET

Darden Solar Facility ■ Cantua Creek, Fresno County, California
October 13, 2023 ■ Terracon Project No. 60225172

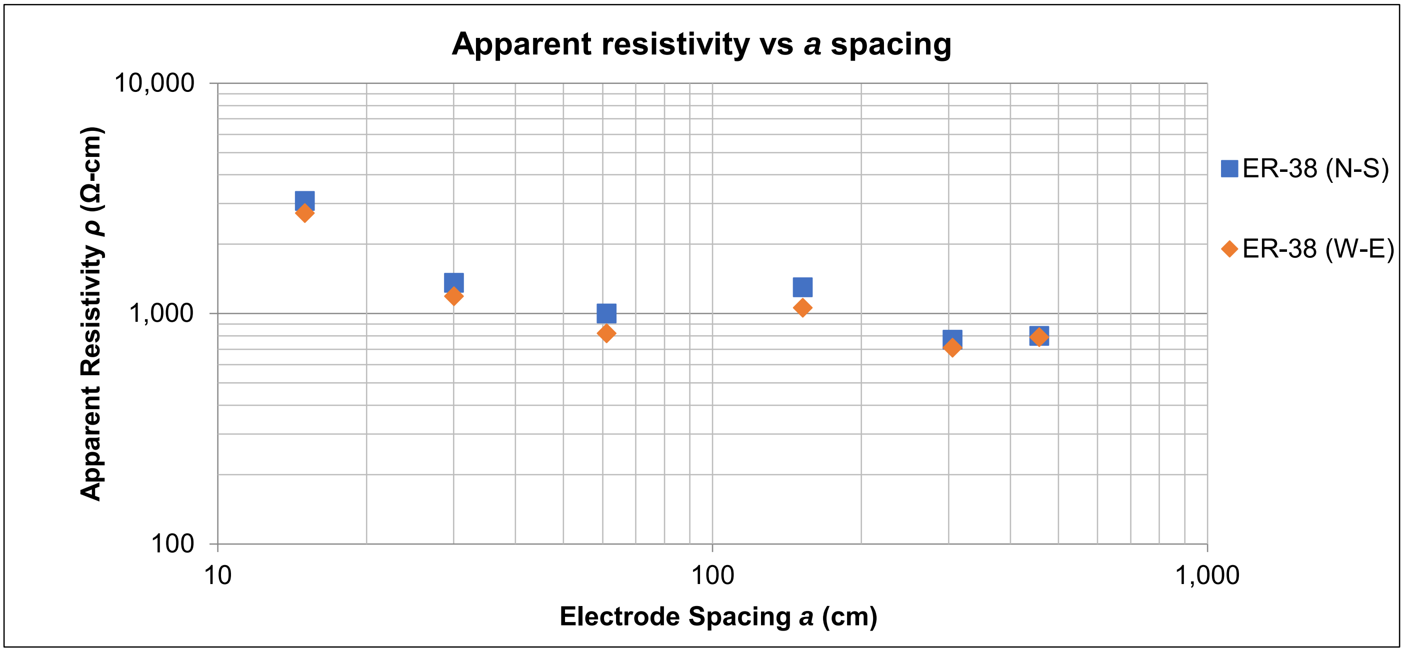
NORCAL GEOPHYSICAL CONSULTANTS INC.
A Terracon COMPANY

Array Loc.	**ER-38** (36.488145°N, 120.187834°W)		
Instrument	L&R Instruments - Ultra Mini Res	**Weather**	Clear, high of 50°F.
Serial #	SN-214U	**Ground Cond.**	Fallow field.
Cal. Check	2/14/2023	**Tested By**	H. Philson
Test Date	February 23, 2023	**Method**	Wenner 4-pin ASTM G57-06 (2012); IEEE 81-2012
Notes & Conflicts	Arrays oriented N-S and W-E with a common midpoint.		

Apparent resistivity ρ is calculated as :

$$\rho = \frac{4\pi a R}{1 + \frac{2a}{\sqrt{a^2 + 4b^2}} - \frac{a}{\sqrt{a^2 + b^2}}}$$

Electrode Spacing *a*		**Electrode Depth *b***		**ER-38 (N-S)**		**ER-38 (W-E)**	
(feet)	(centimeters)	(inches)	(centimeters)	Measured Resistance *R*	Apparent Resistivity *ρ*	Measured Resistance *R*	Apparent Resistivity *ρ*
				Ω	(Ω-cm)	Ω	(Ω-cm)
0.5	15	1	3	30.70	3080	27.20	2730
1	30	1	3	7.105	1360	6.189	1190
2	61	2	5	2.589	1000	2.111	820
5	152	6	15	1.342	1300	1.088	1060
10	305	12	30	0.3973	770	0.3631	710
15	457	12	30	0.2759	800	0.2739	790



FIELD ELECTRICAL RESISTIVITY DATA SHEET

Darden Solar Facility ■ Cantua Creek, Fresno County, California
October 13, 2023 ■ Terracon Project No. 60225172

Array Loc. **ER-39** (36.492499°N, 120.179939°W)

Instrument L&R Instruments - Ultra Mini Res

Weather Clear, high of 50°F.

Serial # SN-214U

Ground Cond. Fallow field.

Cal. Check 2/14/2023

Tested By H. Philson

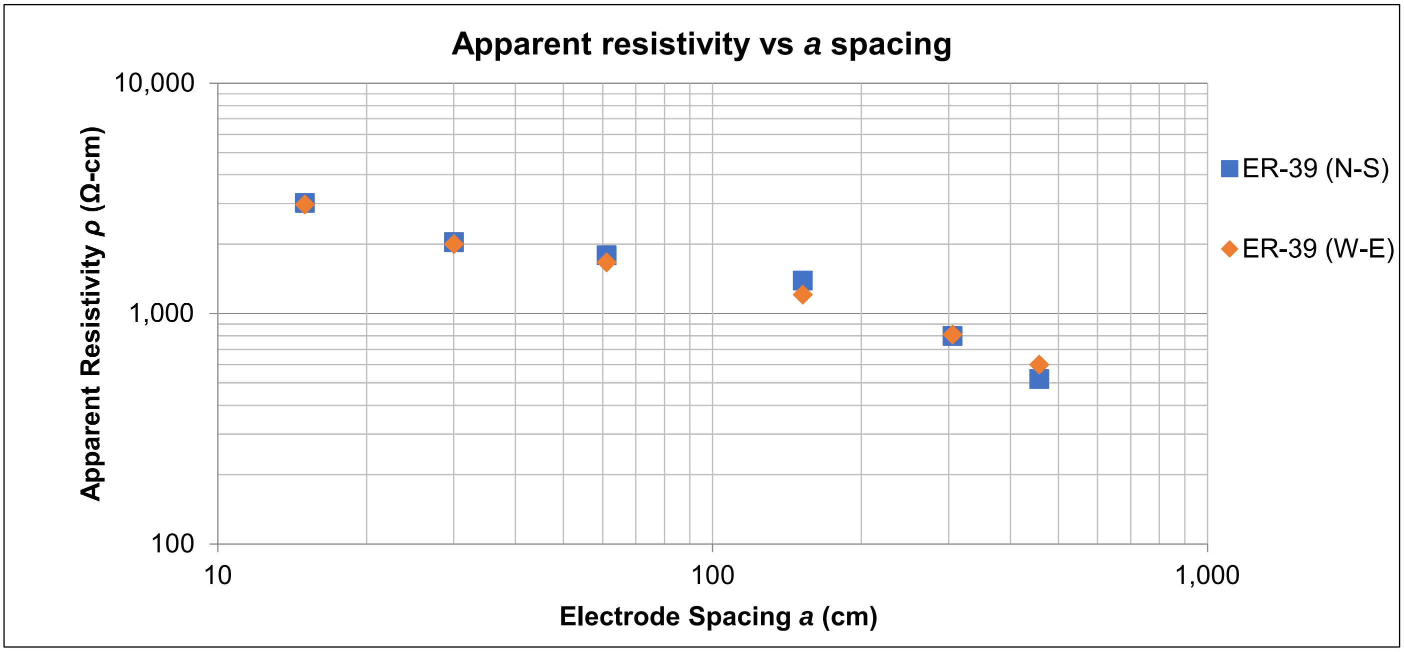
Test Date February 23, 2023

Method Wenner 4-pin ASTM G57-06 (2012); IEEE 81-2012

Notes & Conflicts Arrays oriented N-S and W-E with a common midpoint.

Apparent resistivity ρ is calculated as : $$\rho = \frac{4\pi a R}{1 + \frac{2a}{\sqrt{a^2 + 4b^2}} - \frac{a}{\sqrt{a^2 + b^2}}}$$

Electrode Spacing *a*		**Electrode Depth *b***		**ER-39 (N-S)**		**ER-39 (W-E)**	
(feet)	(centimeters)	(inches)	(centimeters)	Measured Resistance *R*	Apparent Resistivity *ρ*	Measured Resistance *R*	Apparent Resistivity *ρ*
				Ω	(Ω-cm)	Ω	(Ω-cm)
0.5	15	1	3	30.10	3020	29.70	2980
1	30	1	3	10.62	2040	10.45	2000
2	61	2	5	4.622	1790	4.303	1670
5	152	6	15	1.432	1390	1.245	1210
10	305	12	30	0.4102	800	0.4135	810
15	457	12	30	0.1795	520	0.2065	600



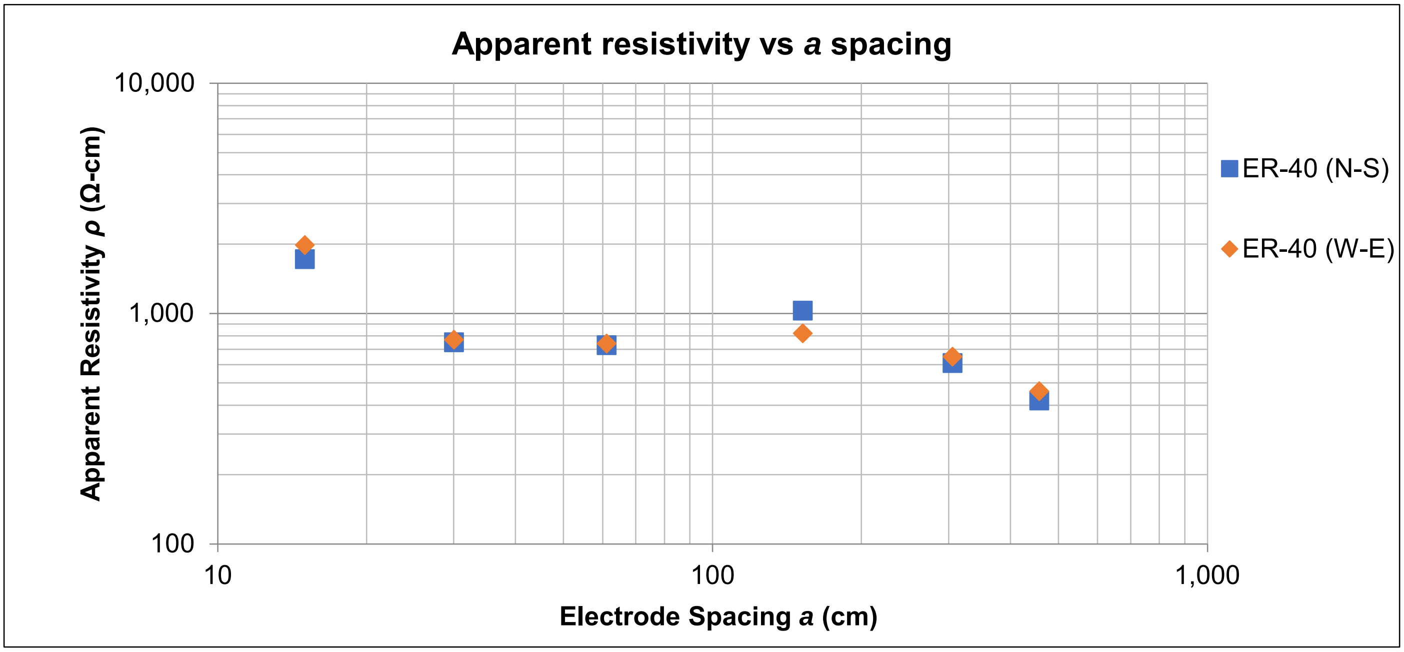
FIELD ELECTRICAL RESISTIVITY DATA SHEET

Darden Solar Facility ■ Cantua Creek, Fresno County, California
October 13, 2023 ■ Terracon Project No. 60225172

Array Loc.	**ER-40** (36.488459°N, 120.171018°W)		
Instrument	L&R Instruments - Ultra Mini Res	**Weather**	Clear, high of 50°F.
Serial #	SN-214U	**Ground Cond.**	Fallow field.
Cal. Check	2/14/2023	**Tested By**	H. Philson
Test Date	February 23, 2023	**Method**	Wenner 4-pin ASTM G57-06 (2012); IEEE 81-2012
Notes & Conflicts	Arrays oriented N-S and W-E with a common midpoint.		

Apparent resistivity ρ is calculated as : $$\rho = \frac{4\pi a R}{1 + \frac{2a}{\sqrt{a^2 + 4b^2}} - \frac{a}{\sqrt{a^2 + b^2}}}$$

Electrode Spacing *a*		**Electrode Depth *b***		**ER-40 (N-S)**		**ER-40 (W-E)**	
(feet)	(centimeters)	(inches)	(centimeters)	Measured Resistance *R*	Apparent Resistivity *ρ*	Measured Resistance *R*	Apparent Resistivity *ρ*
				Ω	(Ω-cm)	Ω	(Ω-cm)
0.5	15	1	3	17.15	1720	19.75	1980
1	30	1	3	3.915	750	4.035	770
2	61	2	5	1.892	730	1.911	740
5	152	6	15	1.063	1030	0.8415	820
10	305	12	30	0.3155	610	0.3315	650
15	457	12	30	0.1461	420	0.1586	460



FIELD ELECTRICAL RESISTIVITY DATA SHEET

Darden Solar Facility ■ Cantua Creek, Fresno County, California
October 13, 2023 ■ Terracon Project No. 60225172

NORCAL GEOPHYSICAL CONSULTANTS INC. A Terracon COMPANY

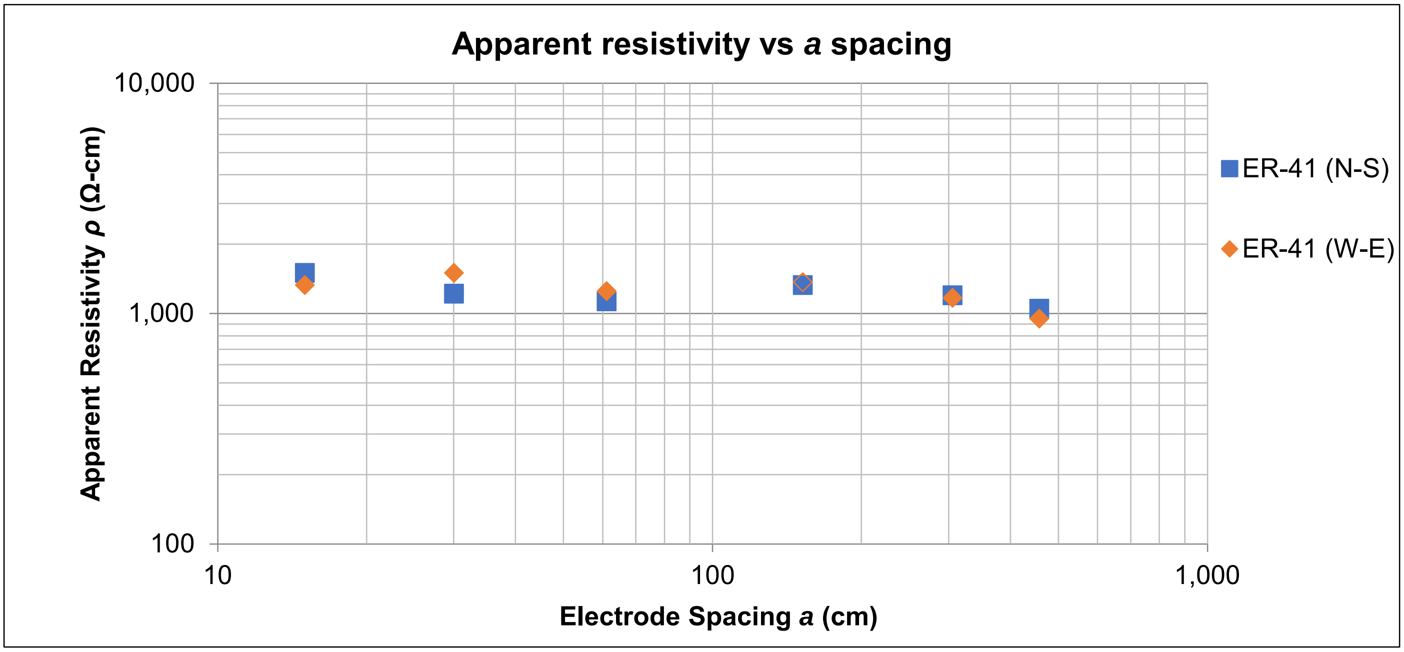
Array Loc. **ER-41** (36.486443°N, 120.245063°W)

Instrument	AGI SuperSting R1	**Weather**	Sunny, windy, High 52°F.
Serial #	SP0303161	**Ground Cond.**	Vegetated, silty, sandy soil
Cal. Check	4/8/2022	**Tested By**	T. Black
Test Date	February 15, 2023	**Method**	Wenner 4-pin ASTM G57-06 (2012); IEEE 81-2012

Notes & Conflicts Arrays oriented N-S and W-E with a common midpoint.

Apparent resistivity ρ is calculated as : $$\rho = \frac{4\pi a R}{1 + \frac{2a}{\sqrt{a^2 + 4b^2}} - \frac{a}{\sqrt{a^2 + b^2}}}$$

Electrode Spacing *a*		**Electrode Depth *b***		**ER-41 (N-S)**		**ER-41 (W-E)**	
(feet)	(centimeters)	(inches)	(centimeters)	Measured Resistance *R*	Apparent Resistivity *ρ*	Measured Resistance *R*	Apparent Resistivity *ρ*
				Ω	(Ω-cm)	Ω	(Ω-cm)
0.5	15	1	3	14.96	1500	13.20	1330
1	30	1	3	6.358	1220	7.804	1500
2	61	2	5	2.909	1130	3.215	1250
5	152	6	15	1.3680	1330	1.4150	1370
10	305	12	30	0.6140	1200	0.6009	1170
15	457	12	30	0.3645	1050	0.3274	950



FIELD ELECTRICAL RESISTIVITY DATA SHEET

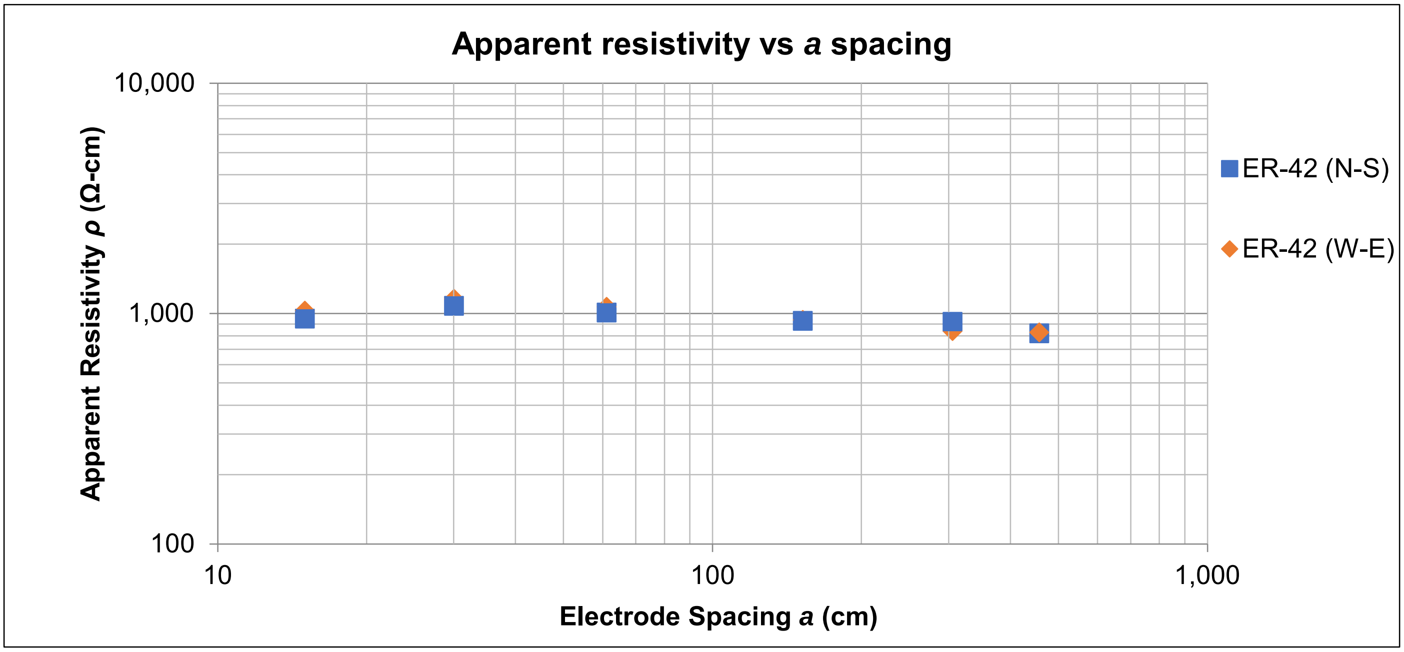
Darden Solar Facility ■ Cantua Creek, Fresno County, California
October 13, 2023 ■ Terracon Project No. 60225172

NORCAL GEOPHYSICAL CONSULTANTS INC.
A Terracon COMPANY

Array Loc.	**ER-42** (36.483253°N, 120.242775°W)		
Instrument	AGI SuperSting R1	**Weather**	Sunny, High 59°F.
Serial #	SP0303161	**Ground Cond.**	Vegetated, silty, sandy soil
Cal. Check	4/8/2022	**Tested By**	T. Black
Test Date	February 14, 2023	**Method**	Wenner 4-pin ASTM G57-06 (2012); IEEE 81-2012
Notes & Conflicts	Arrays oriented N-S and W-E with a common midpoint.		

Apparent resistivity ρ is calculated as : $$\rho = \frac{4\pi a R}{1 + \frac{2a}{\sqrt{a^2 + 4b^2}} - \frac{a}{\sqrt{a^2 + b^2}}}$$

Electrode Spacing *a*		**Electrode Depth *b***		**ER-42 (N-S)**		**ER-42 (W-E)**	
(feet)	(centimeters)	(inches)	(centimeters)	Measured Resistance *R*	Apparent Resistivity *ρ*	Measured Resistance *R*	Apparent Resistivity *ρ*
				Ω	(Ω-cm)	Ω	(Ω-cm)
0.5	15	1	3	9.501	950	10.23	1030
1	30	1	3	5.624	1080	6.054	1160
2	61	2	5	2.609	1010	2.753	1070
5	152	6	15	0.9527	930	0.9634	940
10	305	12	30	0.4713	920	0.4299	840
15	457	12	30	0.2823	820	0.2861	830



FIELD ELECTRICAL RESISTIVITY DATA SHEET

Darden Solar Facility ■ Cantua Creek, Fresno County, California
October 13, 2023 ■ Terracon Project No. 60225172

NORCAL GEOPHYSICAL CONSULTANTS INC.
A Terracon COMPANY

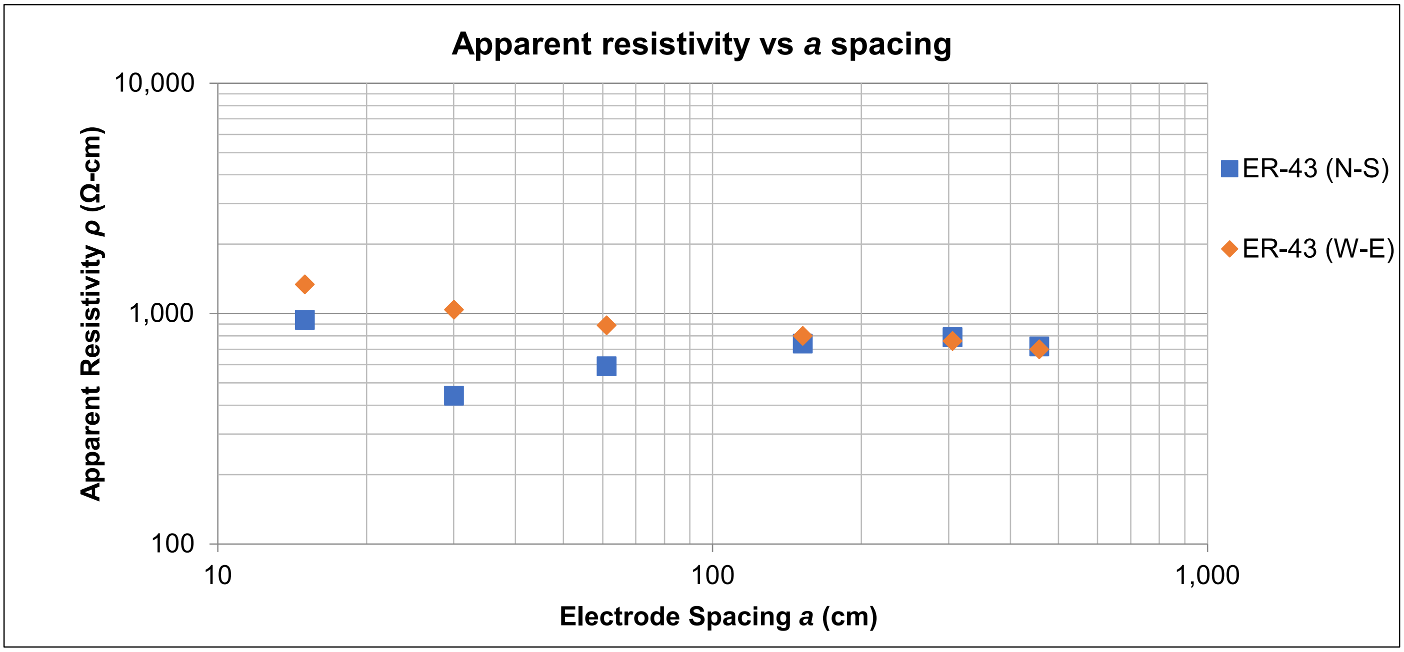
Array Loc. **ER-43** (36.483912°N, 120.234899°W)

Instrument	AGI SuperSting R1	**Weather**	Sunny, windy, High 52°F.
Serial #	SP0303161	**Ground Cond.**	Silty, sandy soil
Cal. Check	4/8/2022	**Tested By**	T. Black
Test Date	February 15, 2023	**Method**	Wenner 4-pin ASTM G57-06 (2012); IEEE 81-2012

Notes & Conflicts Arrays oriented N-S and W-E with a common midpoint.

Apparent resistivity ρ is calculated as : $\rho = \dfrac{4\pi aR}{1 + \dfrac{2a}{\sqrt{a^2 + 4b^2}} - \dfrac{a}{\sqrt{a^2 + b^2}}}$

Electrode Spacing *a*		**Electrode Depth *b***		**ER-43 (N-S)**		**ER-43 (W-E)**	
(feet)	(centimeters)	(inches)	(centimeters)	Measured Resistance *R*	Apparent Resistivity *ρ*	Measured Resistance *R*	Apparent Resistivity *ρ*
				Ω	(Ω-cm)	Ω	(Ω-cm)
0.5	15	1	3	9.393	940	13.33	1340
1	30	1	3	2.309	440	5.445	1040
2	61	2	5	1.517	590	2.303	890
5	152	6	15	0.7644	740	0.8238	800
10	305	12	30	0.4063	790	0.3914	760
15	457	12	30	0.2481	720	0.2432	700



FIELD ELECTRICAL RESISTIVITY DATA SHEET

Darden Solar Facility ■ Cantua Creek, Fresno County, California
October 13, 2023 ■ Terracon Project No. 60225172

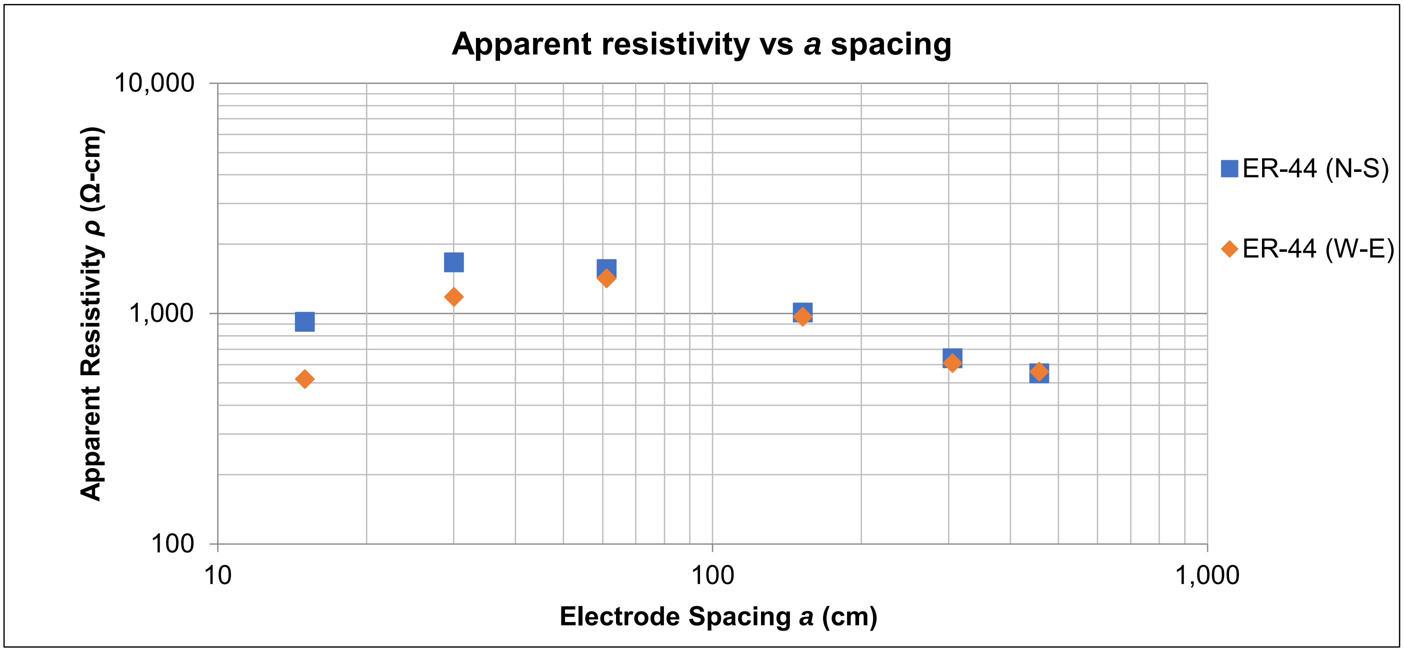
NORCAL GEOPHYSICAL CONSULTANTS INC.
A Terracon COMPANY

Array Loc.	**ER-44** (36.480385°N, 120.230524°W)		
Instrument	AGI SuperSting R1	**Weather**	Sunny, High 59°F.
Serial #	SP0303161	**Ground Cond.**	Silty, sandy soil
Cal. Check	4/8/2022	**Tested By**	T. Black
Test Date	February 15, 2023	**Method**	Wenner 4-pin ASTM G57-06 (2012); IEEE 81-2012
Notes & Conflicts	Arrays oriented N-S and W-E with a common midpoint.		

Apparent resistivity ρ is calculated as :

$$\rho = \frac{4\pi a R}{1 + \frac{2a}{\sqrt{a^2 + 4b^2}} - \frac{a}{\sqrt{a^2 + b^2}}}$$

Electrode Spacing *a*		**Electrode Depth *b***		**ER-44 (N-S)**		**ER-44 (W-E)**	
(feet)	(centimeters)	(inches)	(centimeters)	Measured Resistance *R*	Apparent Resistivity ρ	Measured Resistance *R*	Apparent Resistivity ρ
				Ω	(Ω-cm)	Ω	(Ω-cm)
0.5	15	1	3	9.188	920	5.129	520
1	30	1	3	8.686	1670	6.132	1180
2	61	2	5	4.026	1560	3.672	1420
5	152	6	15	1.0390	1010	0.9992	970
10	305	12	30	0.3265	640	0.3122	610
15	457	12	30	0.1901	550	0.1921	560



FIELD ELECTRICAL RESISTIVITY DATA SHEET

Darden Solar Facility ■ Cantua Creek, Fresno County, California
October 13, 2023 ■ Terracon Project No. 60225172

Array Loc. **ER-45** (36.484831°N, 120.229225°W)

Instrument AGI SuperSting R1

Weather Sunny, High 52°F.

Serial # SP0303161

Ground Cond. Silty, sandy soil

Cal. Check 4/8/2022

Tested By T. Black

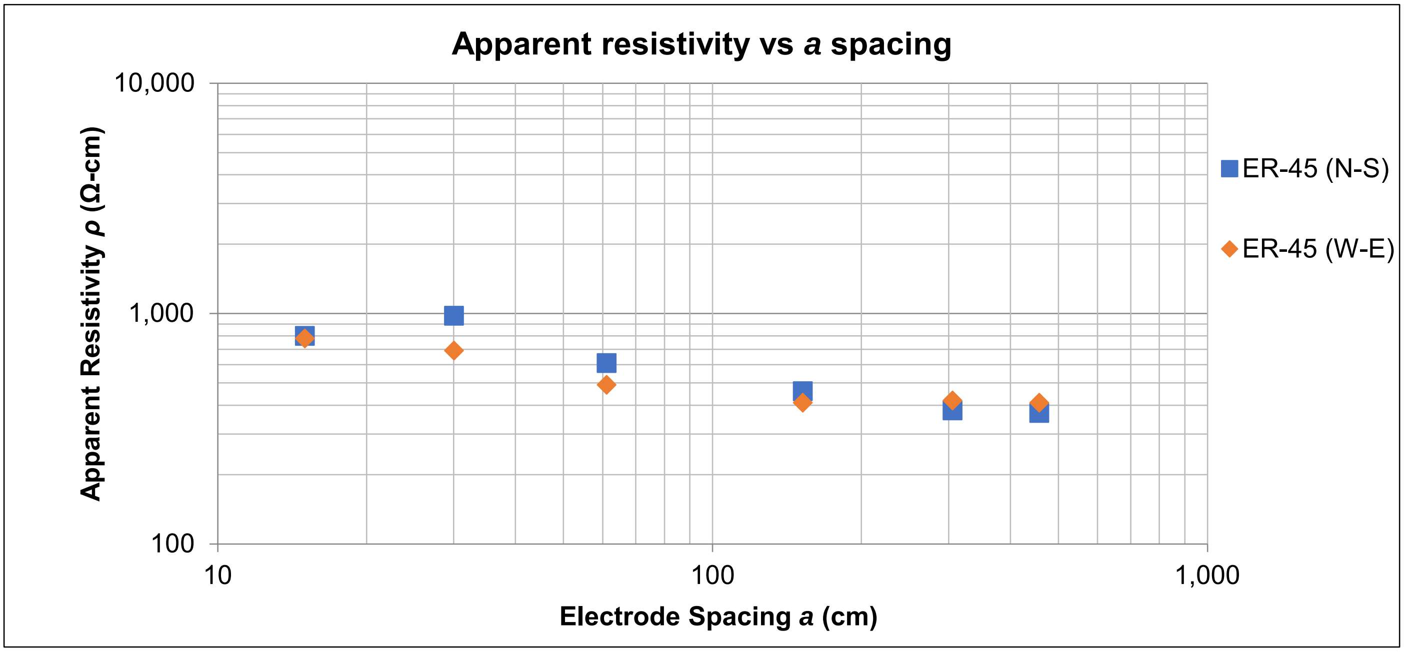
Test Date February 15, 2023

Method Wenner 4-pin ASTM G57-06 (2012); IEEE 81-2012

Notes & Conflicts Arrays oriented N-S and W-E with a common midpoint.

Apparent resistivity ρ is calculated as :
$$\rho = \frac{4\pi a R}{1 + \frac{2a}{\sqrt{a^2 + 4b^2}} - \frac{a}{\sqrt{a^2 + b^2}}}$$

Electrode Spacing *a*		**Electrode Depth *b***		**ER-45 (N-S)**		**ER-45 (W-E)**	
(feet)	(centimeters)	(inches)	(centimeters)	Measured Resistance *R*	Apparent Resistivity *ρ*	Measured Resistance *R*	Apparent Resistivity *ρ*
				Ω	(Ω-cm)	Ω	(Ω-cm)
0.5	15	1	3	7.999	800	7.778	780
1	30	1	3	5.094	980	3.597	690
2	61	2	5	1.584	610	1.255	490
5	152	6	15	0.4698	460	0.4192	410
10	305	12	30	0.1937	380	0.2147	420
15	457	12	30	0.1296	370	0.1410	410



FIELD ELECTRICAL RESISTIVITY DATA SHEET

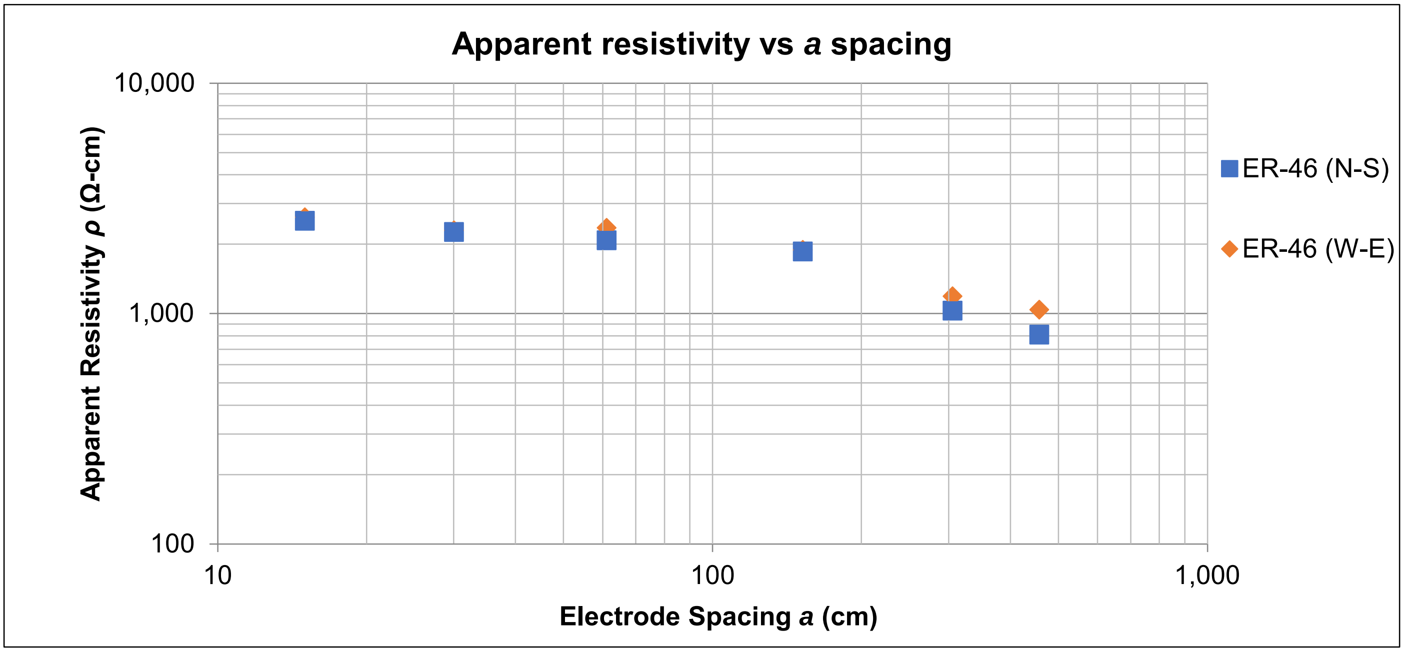
Darden Solar Facility ■ Cantua Creek, Fresno County, California
October 13, 2023 ■ Terracon Project No. 60225172

NORCAL GEOPHYSICAL CONSULTANTS INC.
A Terracon COMPANY

Array Loc.	**ER-46** (36.482665°N, 120.218183°W)		
Instrument	L&R Instruments - Ultra Mini Res	**Weather**	Partly cloudy, high of 48°F.
Serial #	SN-214U	**Ground Cond.**	Fallow field.
Cal. Check	2/14/2023	**Tested By**	H. Philson
Test Date	February 23, 2023	**Method**	Wenner 4-pin ASTM G57-06 (2012); IEEE 81-2012
Notes & Conflicts	Arrays oriented N-S and W-E with a common midpoint.		

Apparent resistivity ρ is calculated as : $\rho = \dfrac{4\pi aR}{1 + \dfrac{2a}{\sqrt{a^2 + 4b^2}} - \dfrac{a}{\sqrt{a^2 + b^2}}}$

Electrode Spacing *a*		**Electrode Depth *b***		**ER-46 (N-S)**		**ER-46 (W-E)**	
(feet)	(centimeters)	(inches)	(centimeters)	Measured Resistance *R*	Apparent Resistivity *ρ*	Measured Resistance *R*	Apparent Resistivity *ρ*
				Ω	(Ω-cm)	Ω	(Ω-cm)
0.5	15	1	3	25.20	2530	26.10	2620
1	30	1	3	11.77	2260	12.01	2300
2	61	2	5	5.367	2080	6.086	2360
5	152	6	15	1.9170	1860	1.9450	1890
10	305	12	30	0.5295	1030	0.6095	1190
15	457	12	30	0.2808	810	0.3587	1040



FIELD ELECTRICAL RESISTIVITY DATA SHEET

Darden Solar Facility ■ Cantua Creek, Fresno County, California
October 13, 2023 ■ Terracon Project No. 60225172

NORCAL GEOPHYSICAL CONSULTANTS INC.
A Terracon COMPANY

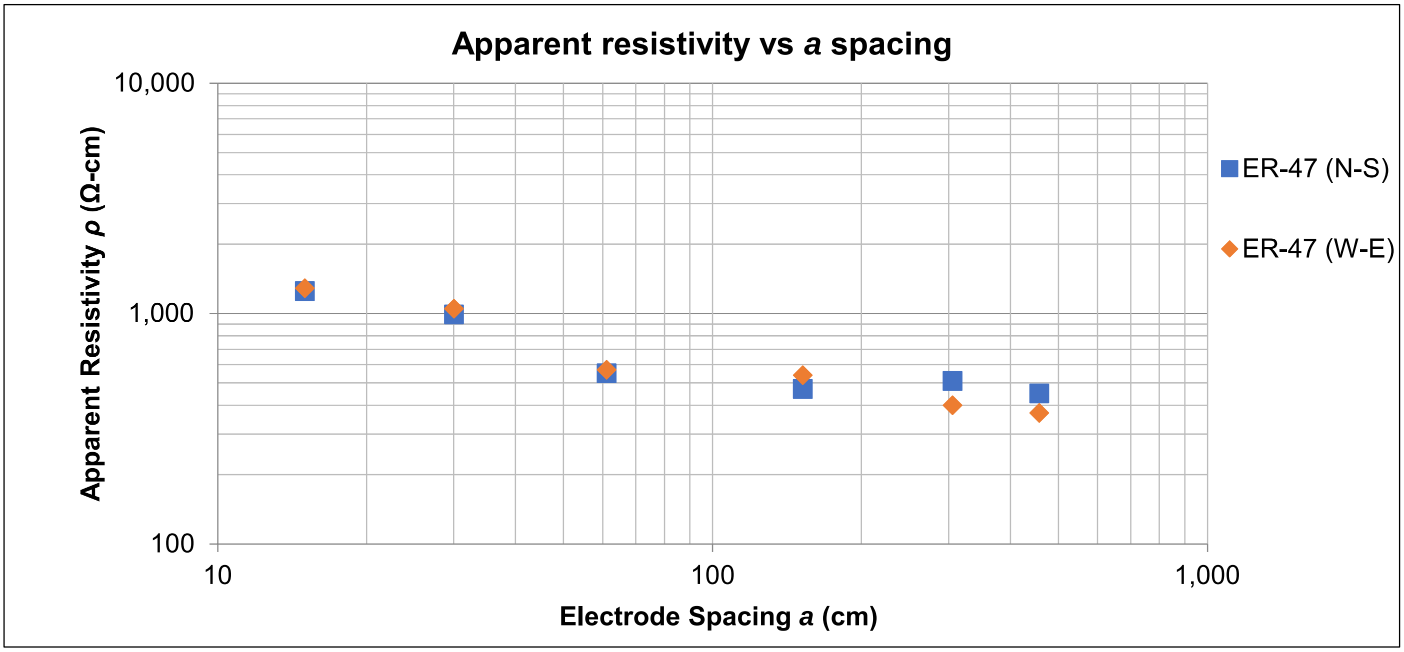
Array Loc. **ER-47** (36.484039°N, 120.211215°W)

Instrument	AGI SuperSting R1	**Weather**	Partly cloudy, High 48°F.
Serial #	SP0303161	**Ground Cond.**	Vegetated, silty, sandy soil
Cal. Check	4/8/2022	**Tested By**	T. Black
Test Date	February 23, 2023	**Method**	Wenner 4-pin ASTM G57-06 (2012); IEEE 81-2012

Notes & Conflicts Arrays oriented N-S and W-E with a common midpoint.

Apparent resistivity ρ is calculated as : $\rho = \dfrac{4\pi a R}{1 + \dfrac{2a}{\sqrt{a^2 + 4b^2}} - \dfrac{a}{\sqrt{a^2 + b^2}}}$

Electrode Spacing *a*		**Electrode Depth *b***		**ER-47 (N-S)**		**ER-47 (W-E)**	
(feet)	(centimeters)	(inches)	(centimeters)	Measured Resistance *R* Ω	Apparent Resistivity *ρ* (Ω-cm)	Measured Resistance *R* Ω	Apparent Resistivity *ρ* (Ω-cm)
0.5	15	1	3	12.43	1250	12.89	1290
1	30	1	3	5.144	990	5.474	1050
2	61	2	5	1.431	550	1.467	570
5	152	6	15	0.4803	470	0.5608	540
10	305	12	30	0.2592	510	0.2048	400
15	457	12	30	0.1541	450	0.1277	370



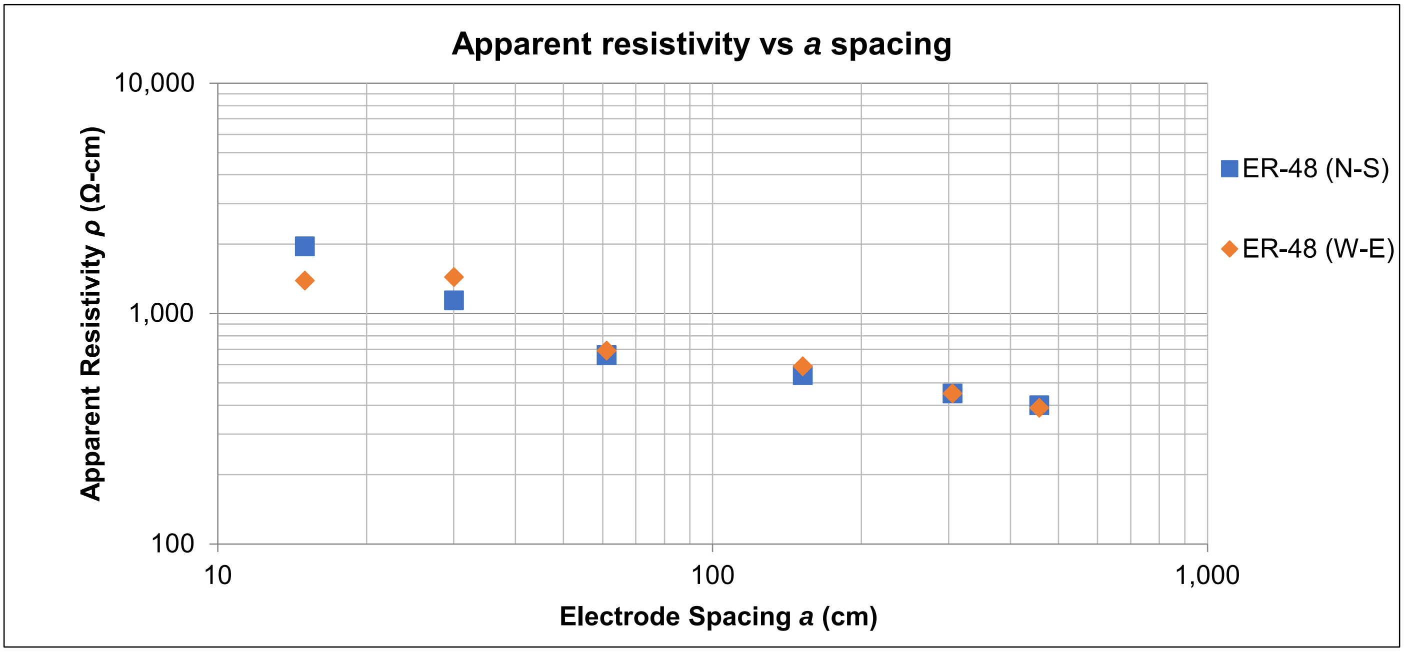
FIELD ELECTRICAL RESISTIVITY DATA SHEET

Darden Solar Facility ■ Cantua Creek, Fresno County, California
October 13, 2023 ■ Terracon Project No. 60225172

Array Loc.	**ER-48** (36.478554°N, 120.203998°W)		
Instrument	AGI SuperSting R1	**Weather**	Partly cloudy, High 48°F.
Serial #	SP0303161	**Ground Cond.**	Vegetated, silty, sandy soil
Cal. Check	4/8/2022	**Tested By**	T. Black
Test Date	February 23, 2023	**Method**	Wenner 4-pin ASTM G57-06 (2012); IEEE 81-2012
Notes & Conflicts	Arrays oriented N-S and W-E with a common midpoint.		

Apparent resistivity ρ is calculated as : $$\rho = \frac{4\pi a R}{1 + \frac{2a}{\sqrt{a^2 + 4b^2}} - \frac{a}{\sqrt{a^2 + b^2}}}$$

Electrode Spacing *a*		**Electrode Depth *b***		**ER-48 (N-S)**		**ER-48 (W-E)**	
(feet)	(centimeters)	(inches)	(centimeters)	Measured Resistance *R*	Apparent Resistivity ρ	Measured Resistance *R*	Apparent Resistivity ρ
				Ω	(Ω-cm)	Ω	(Ω-cm)
0.5	15	1	3	19.51	1960	13.82	1390
1	30	1	3	5.942	1140	7.521	1440
2	61	2	5	1.698	660	1.779	690
5	152	6	15	0.5519	540	0.6091	590
10	305	12	30	0.2313	450	0.2321	450
15	457	12	30	0.1392	400	0.1340	390



FIELD ELECTRICAL RESISTIVITY DATA SHEET

Darden Solar Facility ■ Cantua Creek, Fresno County, California
October 13, 2023 ■ Terracon Project No. 60225172

NORCAL GEOPHYSICAL CONSULTANTS INC. A Terracon COMPANY

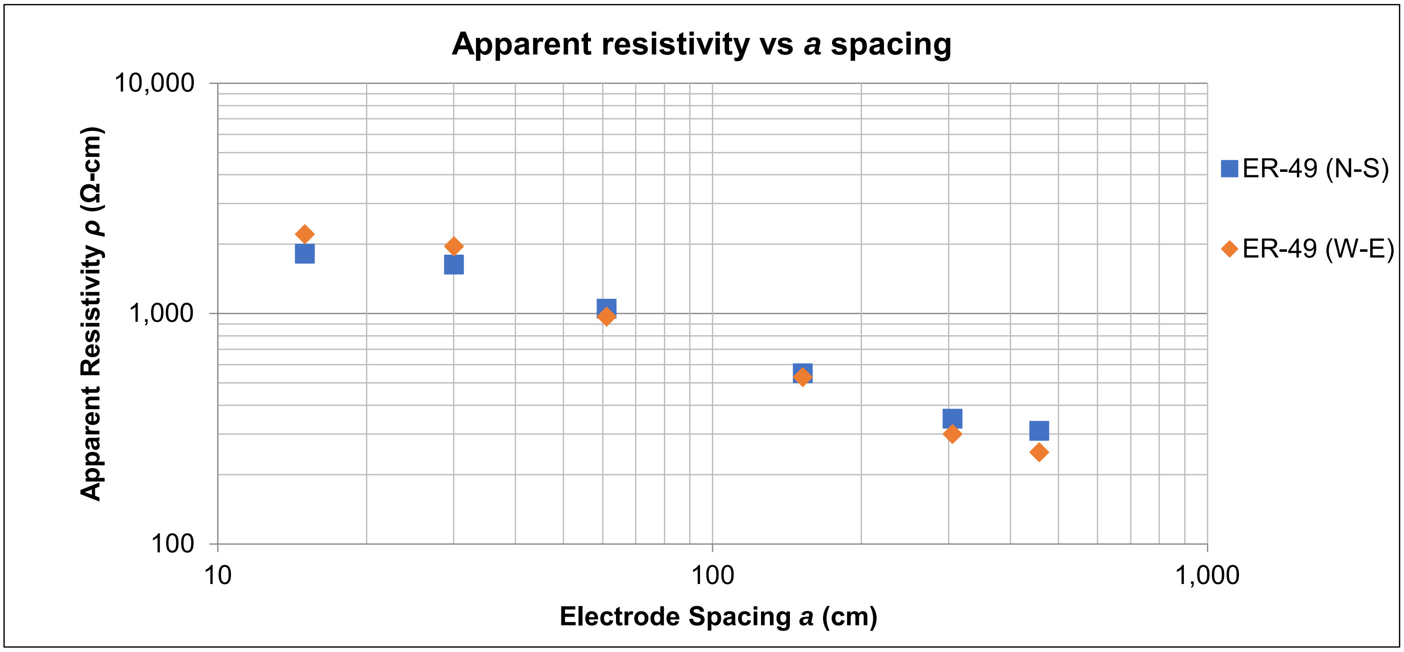
Array Loc. **ER-49** (36.483758°N, 120.200426°W)

Instrument	AGI SuperSting R1	**Weather**	Partly cloudy, High 48°F.
Serial #	SP0303161	**Ground Cond.**	Vegetated, silty, sandy soil
Cal. Check	4/8/2022	**Tested By**	T. Black
Test Date	February 23, 2023	**Method**	Wenner 4-pin ASTM G57-06 (2012); IEEE 81-2012

Notes & Conflicts Arrays oriented N-S and W-E with a common midpoint.

Apparent resistivity ρ is calculated as : $\rho = \dfrac{4\pi aR}{1 + \dfrac{2a}{\sqrt{a^2 + 4b^2}} - \dfrac{a}{\sqrt{a^2 + b^2}}}$

Electrode Spacing *a*		**Electrode Depth *b***		**ER-49 (N-S)**		**ER-49 (W-E)**	
(feet)	(centimeters)	(inches)	(centimeters)	Measured Resistance *R* Ω	Apparent Resistivity ρ (Ω-cm)	Measured Resistance *R* Ω	Apparent Resistivity ρ (Ω-cm)
0.5	15	1	3	18.16	1820	22.04	2210
1	30	1	3	8.485	1630	10.230	1960
2	61	2	5	2.700	1050	2.511	970
5	152	6	15	0.5672	550	0.5482	530
10	305	12	30	0.1810	350	0.1522	300
15	457	12	30	0.1088	310	0.0862	250



FIELD ELECTRICAL RESISTIVITY DATA SHEET

Darden Solar Facility ■ Cantua Creek, Fresno County, California
October 13, 2023 ■ Terracon Project No. 60225172

Array Loc. **ER-50** (36.482194°N, 120.194482°W)

Instrument AGI SuperSting R1

Weather Partly cloudy, High 48°F.

Serial # SP0303161

Ground Cond. Vegetated, silty, sandy soil

Cal. Check 4/8/2022

Tested By T. Black

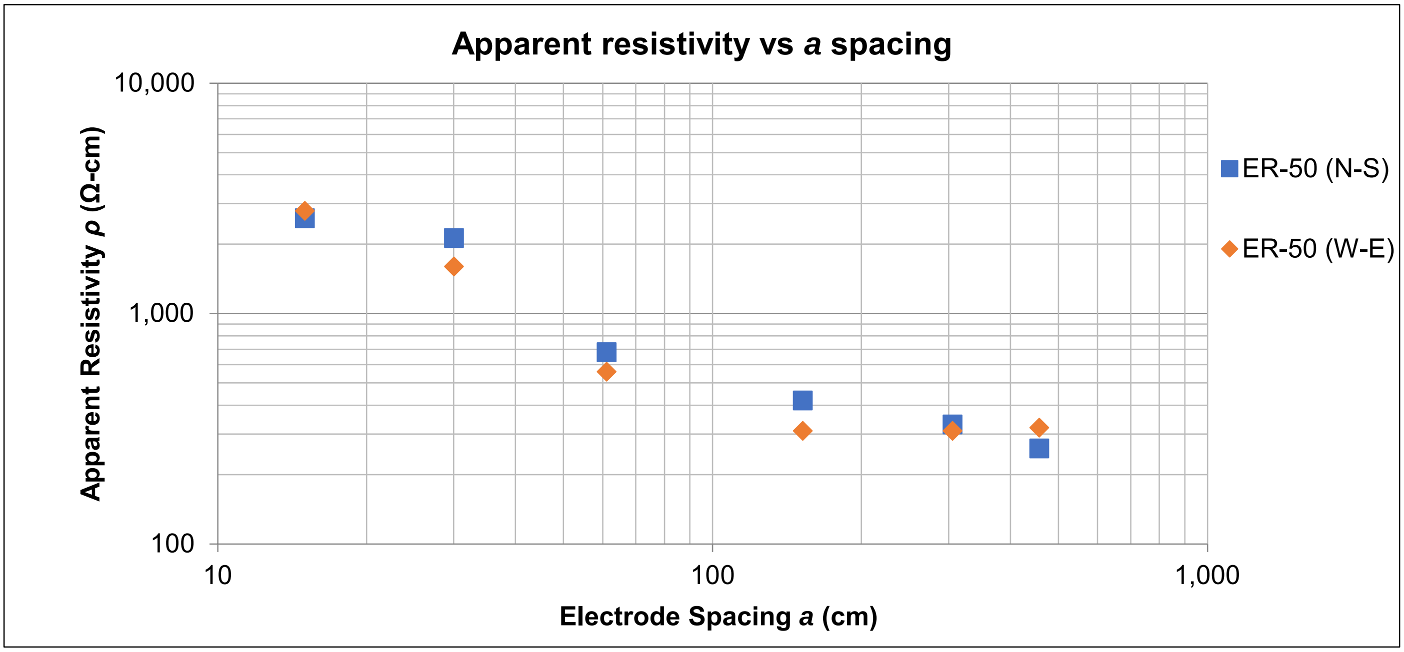
Test Date February 23, 2023

Method Wenner 4-pin ASTM G57-06 (2012); IEEE 81-2012

Notes & Conflicts Arrays oriented N-S and W-E with a common midpoint.

Apparent resistivity ρ is calculated as :
$$\rho = \frac{4\pi a R}{1 + \frac{2a}{\sqrt{a^2 + 4b^2}} - \frac{a}{\sqrt{a^2 + b^2}}}$$

Electrode Spacing *a*		**Electrode Depth *b***		**ER-50 (N-S)**		**ER-50 (W-E)**	
(feet)	(centimeters)	(inches)	(centimeters)	Measured Resistance *R*	Apparent Resistivity ρ	Measured Resistance *R*	Apparent Resistivity ρ
				Ω	(Ω-cm)	Ω	(Ω-cm)
0.5	15	1	3	25.76	2590	27.73	2790
1	30	1	3	11.120	2130	8.366	1600
2	61	2	5	1.758	680	1.448	560
5	152	6	15	0.4288	420	0.3224	310
10	305	12	30	0.1717	330	0.1615	310
15	457	12	30	0.0900	260	0.1094	320



FIELD ELECTRICAL RESISTIVITY DATA SHEET

Darden Solar Facility ■ Cantua Creek, Fresno County, California
October 13, 2023 ■ Terracon Project No. 60225172

NORCAL GEOPHYSICAL CONSULTANTS INC.
A Terracon COMPANY

Array Loc. **ER-51** (36.476875°N, 120.242912°W)

Instrument AGI SuperSting R1

Weather Sunny windy, High 59°F.

Serial # SP0303161

Ground Cond. Silty, sandy soil

Cal. Check 4/8/2022

Tested By T. Black

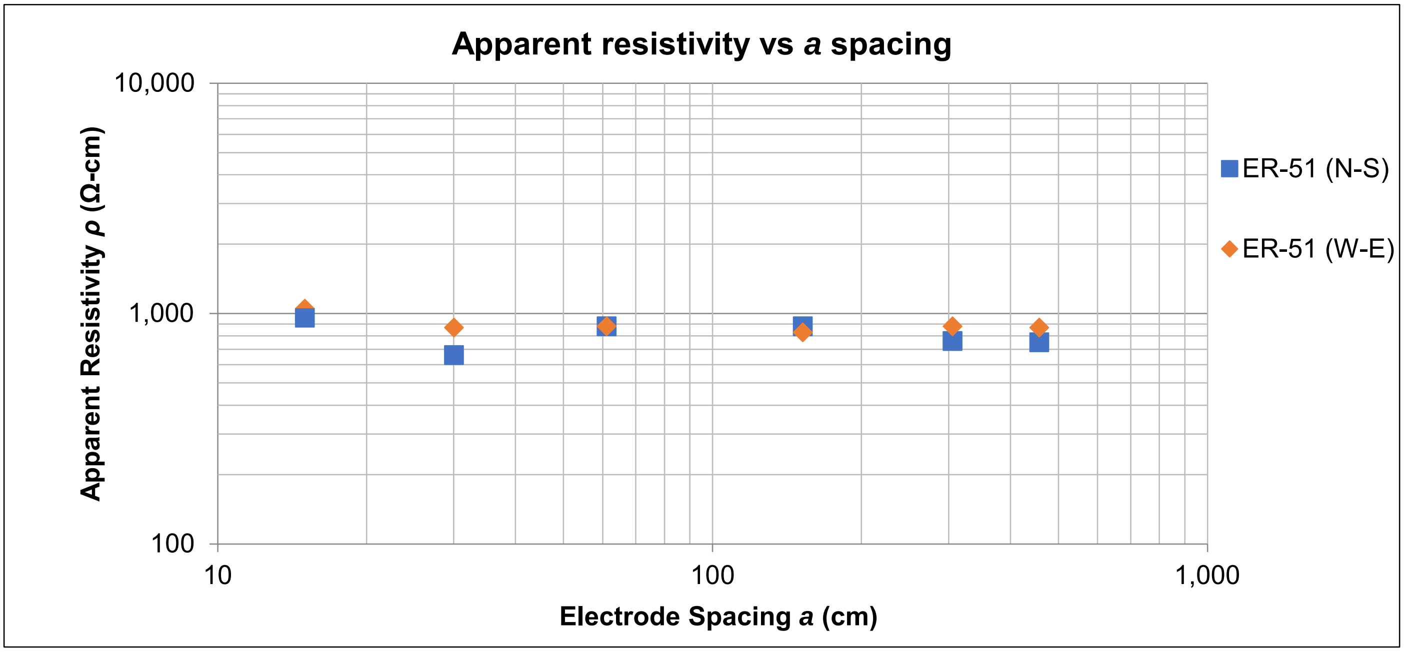
Test Date February 14, 2023

Method Wenner 4-pin ASTM G57-06 (2012); IEEE 81-2012

Notes & Conflicts Arrays oriented N-S and W-E with a common midpoint.

Apparent resistivity ρ is calculated as : $\rho = \dfrac{4\pi a R}{1 + \dfrac{2a}{\sqrt{a^2 + 4b^2}} - \dfrac{a}{\sqrt{a^2 + b^2}}}$

Electrode Spacing *a*		**Electrode Depth *b***		**ER-51 (N-S)**		**ER-51 (W-E)**	
(feet)	(centimeters)	(inches)	(centimeters)	Measured Resistance *R*	Apparent Resistivity *ρ*	Measured Resistance *R*	Apparent Resistivity *ρ*
				Ω	(Ω-cm)	Ω	(Ω-cm)
0.5	15	1	3	9.566	960	10.48	1050
1	30	1	3	3.461	660	4.550	870
2	61	2	5	2.274	880	2.277	880
5	152	6	15	0.9080	880	0.8586	830
10	305	12	30	0.3915	760	0.4520	880
15	457	12	30	0.2578	750	0.3000	870



FIELD ELECTRICAL RESISTIVITY DATA SHEET

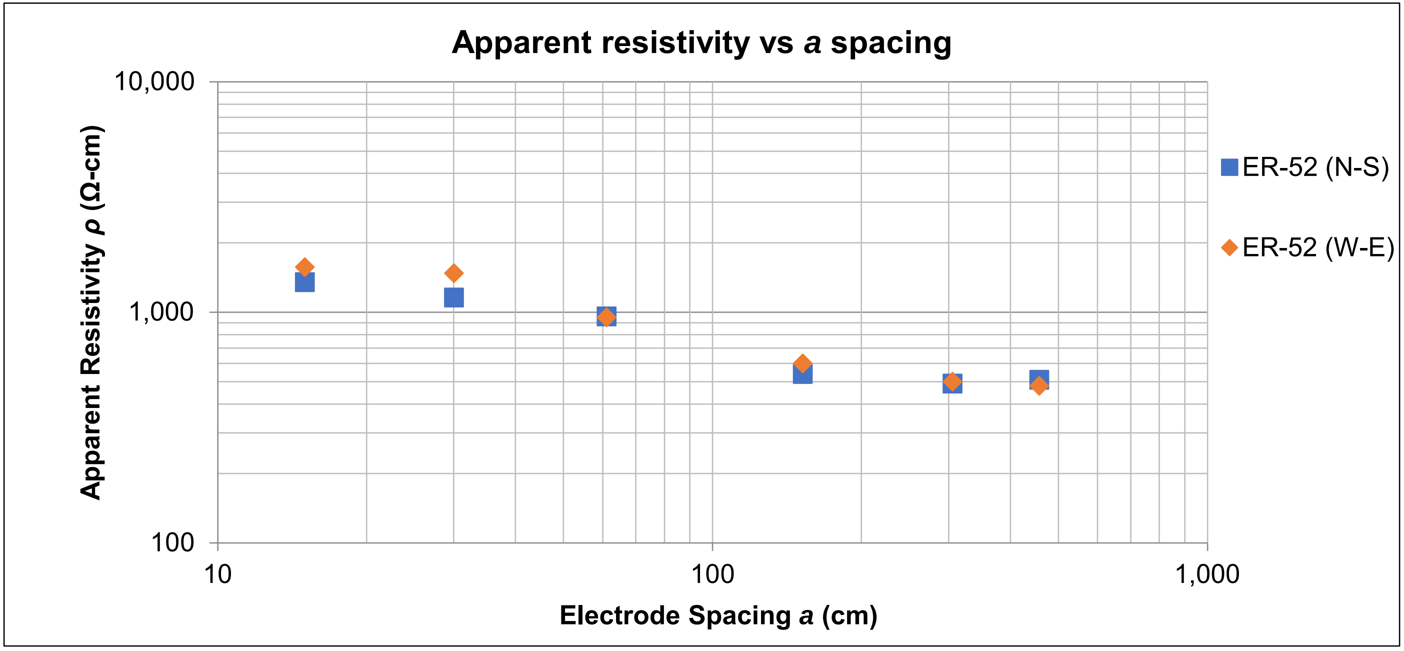
Darden Solar Facility ■ Cantua Creek, Fresno County, California
October 13, 2023 ■ Terracon Project No. 60225172

Array Loc.	**ER-52** (36.473281°N, 120.233980°W)		
Instrument	AGI SuperSting R1	**Weather**	Sunny, High 59°F.
Serial #	SP0303161	**Ground Cond.**	Silty, sandy soil
Cal. Check	4/8/2022	**Tested By**	T. Black
Test Date	February 14, 2023	**Method**	Wenner 4-pin ASTM G57-06 (2012); IEEE 81-2012
Notes & Conflicts	Arrays oriented N-S and W-E with a common midpoint.		

Apparent resistivity ρ is calculated as :

$$\rho = \frac{4\pi a R}{1 + \frac{2a}{\sqrt{a^2 + 4b^2}} - \frac{a}{\sqrt{a^2 + b^2}}}$$

Electrode Spacing *a*		**Electrode Depth *b***		**ER-52 (N-S)**		**ER-52 (W-E)**	
(feet)	(centimeters)	(inches)	(centimeters)	Measured Resistance *R*	Apparent Resistivity *ρ*	Measured Resistance *R*	Apparent Resistivity *ρ*
				Ω	(Ω-cm)	Ω	(Ω-cm)
0.5	15	1	3	13.48	1350	15.62	1570
1	30	1	3	6.068	1160	7.709	1480
2	61	2	5	2.488	960	2.447	950
5	152	6	15	0.5532	540	0.6201	600
10	305	12	30	0.2520	490	0.2579	500
15	457	12	30	0.1755	510	0.1651	480



FIELD ELECTRICAL RESISTIVITY DATA SHEET

Darden Solar Facility ■ Cantua Creek, Fresno County, California
October 13, 2023 ■ Terracon Project No. 60225172

NORCAL GEOPHYSICAL CONSULTANTS INC.
A Terracon COMPANY

Array Loc. **ER-53** (36.476329°N, 120.236612°W)

Instrument AGI SuperSting R1

Weather Sunny, High 59°F.

Serial # SP0303161

Ground Cond. Silty, sandy soil

Cal. Check 4/8/2022

Tested By T. Black

Test Date February 14, 2023

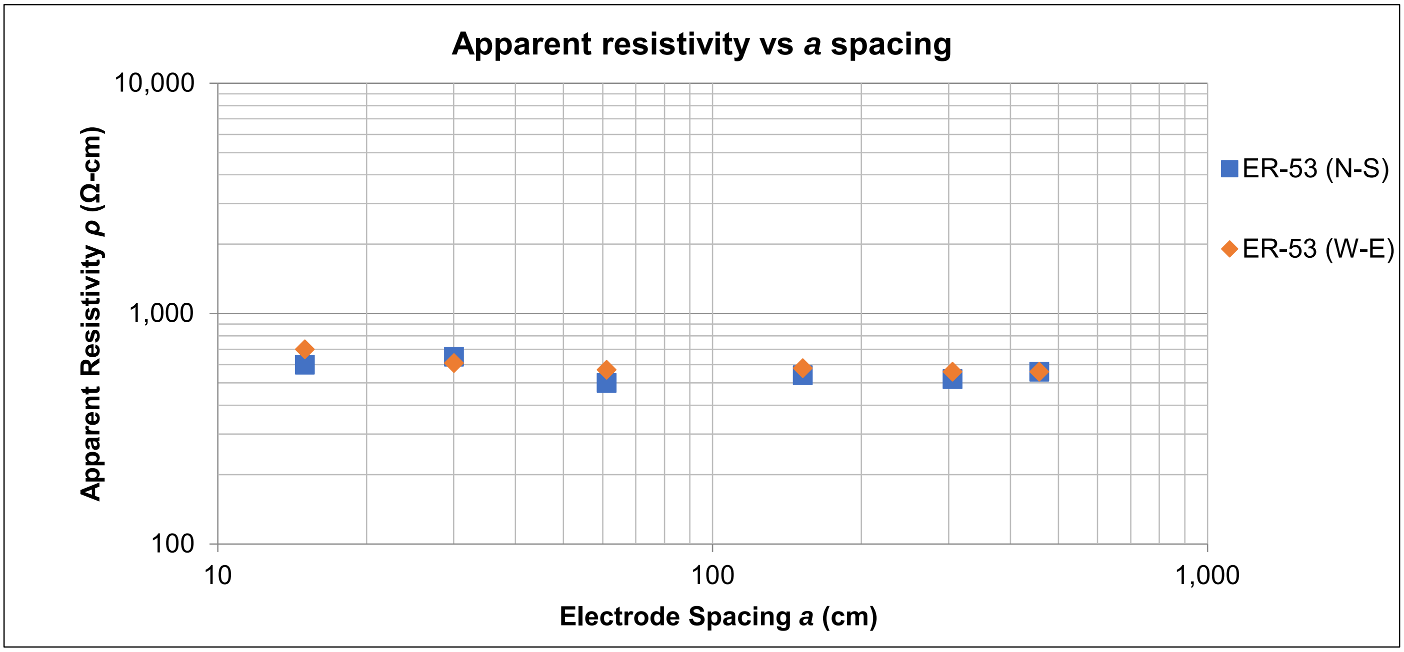
Method Wenner 4-pin ASTM G57-06 (2012); IEEE 81-2012

Notes & Conflicts Arrays oriented N-S and W-E with a common midpoint.

Apparent resistivity ρ is calculated as :

$$\rho = \frac{4\pi a R}{1 + \frac{2a}{\sqrt{a^2 + 4b^2}} - \frac{a}{\sqrt{a^2 + b^2}}}$$

Electrode Spacing *a*		Electrode Depth *b*		ER-53 (N-S)		ER-53 (W-E)	
(feet)	(centimeters)	(inches)	(centimeters)	Measured Resistance *R*	Apparent Resistivity ρ	Measured Resistance *R*	Apparent Resistivity ρ
				Ω	(Ω-cm)	Ω	(Ω-cm)
0.5	15	1	3	5.943	600	7.009	700
1	30	1	3	3.404	650	3.166	610
2	61	2	5	1.285	500	1.464	570
5	152	6	15	0.5527	540	0.5956	580
10	305	12	30	0.2682	520	0.2895	560
15	457	12	30	0.1928	560	0.1929	560



FIELD ELECTRICAL RESISTIVITY DATA SHEET

Darden Solar Facility ■ Cantua Creek, Fresno County, California
October 13, 2023 ■ Terracon Project No. 60225172

NORCAL GEOPHYSICAL CONSULTANTS INC.
A Terracon COMPANY

Array Loc. **ER-54** (36.475684°N, 120.221251°W)

Instrument L&R Instruments - Ultra Mini Res

Weather Partly cloudy, high of 48°F.

Serial # SN-214U

Ground Cond. Fallow field.

Cal. Check 2/14/2023

Tested By H. Philson

Test Date February 23, 2023

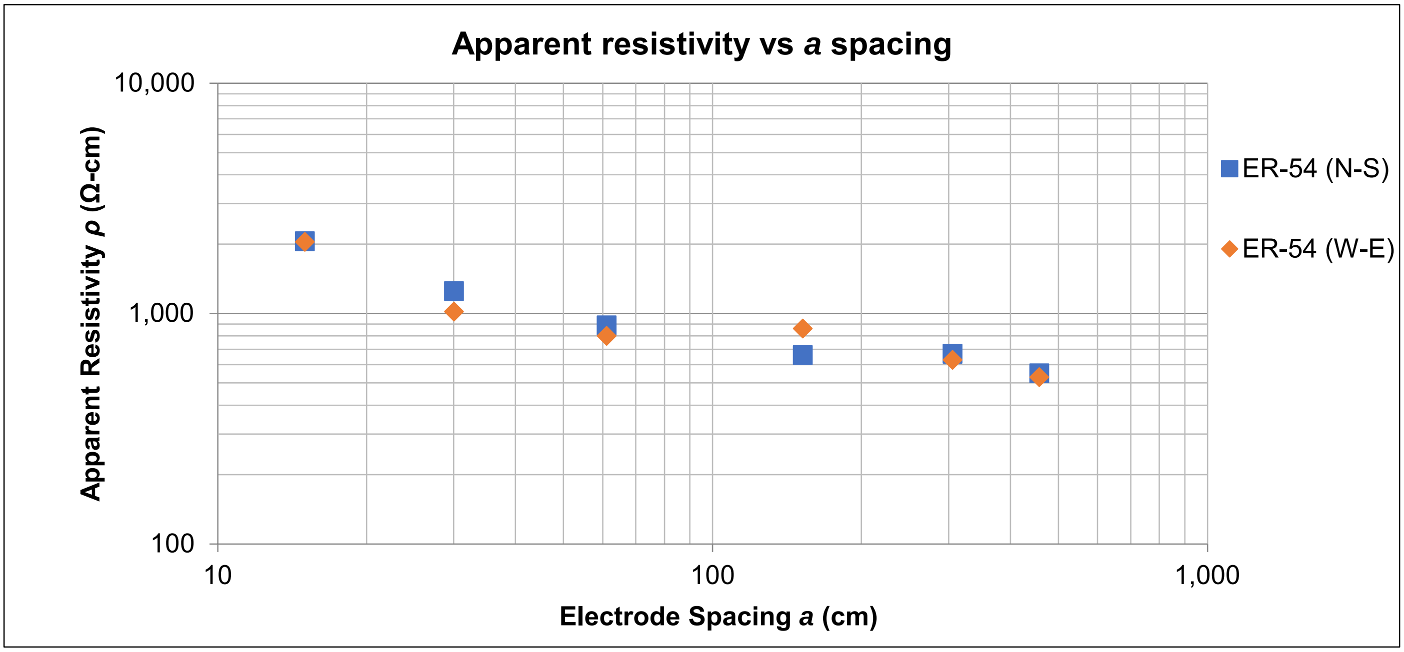
Method Wenner 4-pin ASTM G57-06 (2012); IEEE 81-2012

Notes & Conflicts Arrays oriented N-S and W-E with a common midpoint.

Apparent resistivity ρ is calculated as :

$$\rho = \frac{4\pi a R}{1 + \frac{2a}{\sqrt{a^2 + 4b^2}} - \frac{a}{\sqrt{a^2 + b^2}}}$$

Electrode Spacing *a*		**Electrode Depth *b***		**ER-54 (N-S)**		**ER-54 (W-E)**	
(feet)	(centimeters)	(inches)	(centimeters)	Measured Resistance *R*	Apparent Resistivity *ρ*	Measured Resistance *R*	Apparent Resistivity *ρ*
				Ω	(Ω-cm)	Ω	(Ω-cm)
0.5	15	1	3	20.50	2060	20.40	2050
1	30	1	3	6.532	1250	5.322	1020
2	61	2	5	2.302	890	2.075	800
5	152	6	15	0.6764	660	0.8896	860
10	305	12	30	0.3426	670	0.3231	630
15	457	12	30	0.1918	550	0.1831	530



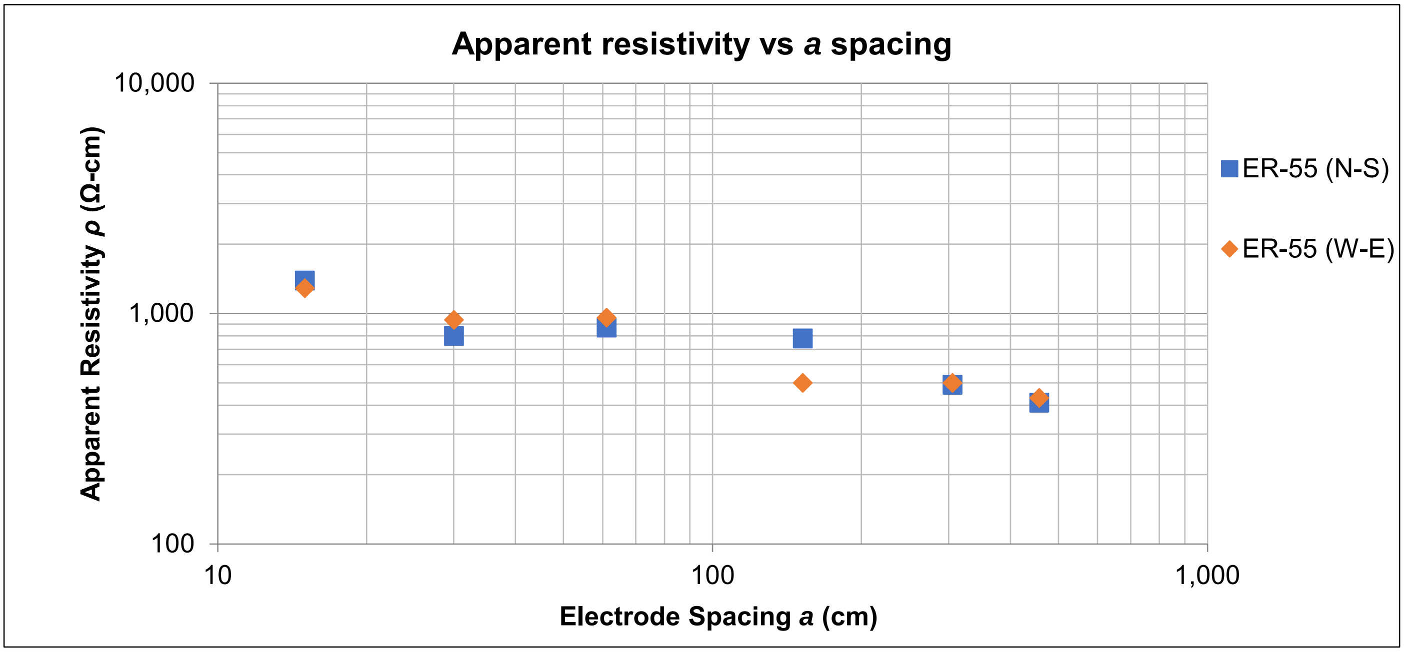
Array Loc. **ER-55** (36.475488°N, 120.211207°W)

Instrument	L&R Instruments - Ultra Mini Res	**Weather**	Partly cloudy, high of 48°F.
Serial #	SN-214U	**Ground Cond.**	Fallow field.
Cal. Check	2/14/2023	**Tested By**	H. Philson
Test Date	February 23, 2023	**Method**	Wenner 4-pin ASTM G57-06 (2012); IEEE 81-2012

Notes & Conflicts Arrays oriented N-S and W-E with a common midpoint.

Apparent resistivity ρ is calculated as : $\rho = \dfrac{4\pi a R}{1 + \dfrac{2a}{\sqrt{a^2 + 4b^2}} - \dfrac{a}{\sqrt{a^2 + b^2}}}$

Electrode Spacing *a*		Electrode Depth *b*		ER-55 (N-S)		ER-55 (W-E)	
(feet)	(centimeters)	(inches)	(centimeters)	Measured Resistance *R*	Apparent Resistivity *ρ*	Measured Resistance *R*	Apparent Resistivity *ρ*
				Ω	(Ω-cm)	Ω	(Ω-cm)
0.5	15	1	3	13.85	1390	12.86	1290
1	30	1	3	4.175	800	4.906	940
2	61	2	5	2.234	870	2.488	960
5	152	6	15	0.8081	780	0.5198	500
10	305	12	30	0.2515	490	0.2589	500
15	457	12	30	0.1415	410	0.1471	430



FIELD ELECTRICAL RESISTIVITY DATA SHEET

Darden Solar Facility ■ Cantua Creek, Fresno County, California
October 13, 2023 ■ Terracon Project No. 60225172

NORCAL GEOPHYSICAL CONSULTANTS INC.
A Terracon COMPANY

Array Loc. **ER-56** (36.473420°N, 120.202797°W)

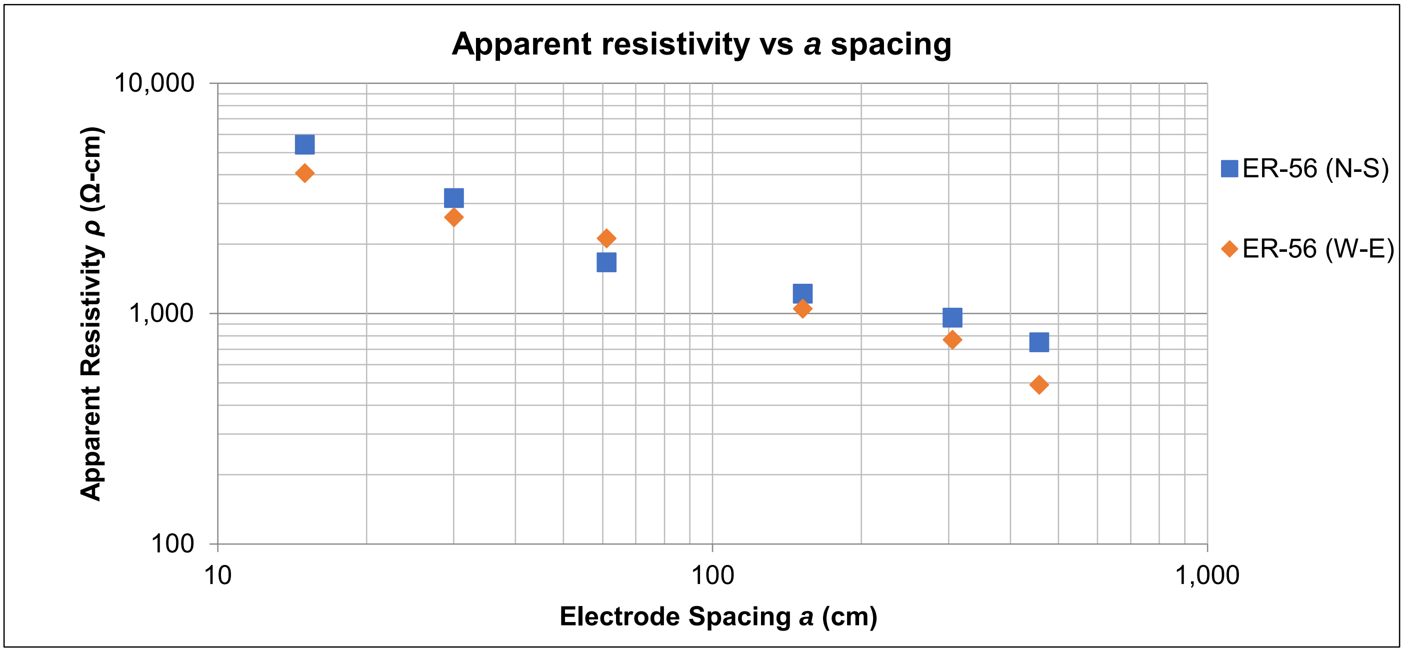
Instrument	AGI SuperSting R1	**Weather**	Sunny, High 62°F.
Serial #	SP0303161	**Ground Cond.**	Vegetated, silty, sandy soil
Cal. Check	4/8/2022	**Tested By**	T. Black
Test Date	February 17, 2023	**Method**	Wenner 4-pin ASTM G57-06 (2012); IEEE 81-2012

Notes & Conflicts Arrays oriented N-S and W-E with a common midpoint.

Apparent resistivity ρ is calculated as :

$$\rho = \frac{4\pi aR}{1 + \frac{2a}{\sqrt{a^2 + 4b^2}} - \frac{a}{\sqrt{a^2 + b^2}}}$$

Electrode Spacing a		**Electrode Depth b**		**ER-56 (N-S)**		**ER-56 (W-E)**	
(feet)	(centimeters)	(inches)	(centimeters)	Measured Resistance R	Apparent Resistivity ρ	Measured Resistance R	Apparent Resistivity ρ
				Ω	(Ω-cm)	Ω	(Ω-cm)
0.5	15	1	3	53.71	5400	40.53	4070
1	30	1	3	16.530	3170	13.660	2620
2	61	2	5	4.307	1670	5.461	2120
5	152	6	15	1.261	1220	1.082	1050
10	305	12	30	0.4951	960	0.3965	770
15	457	12	30	0.2591	750	0.1680	490



NORCAL GEOPHYSICAL CONSULTANTS INC.
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FIELD ELECTRICAL RESISTIVITY DATA SHEET

Darden Solar Facility ■ Cantua Creek, Fresno County, California
October 13, 2023 ■ Terracon Project No. 60225172

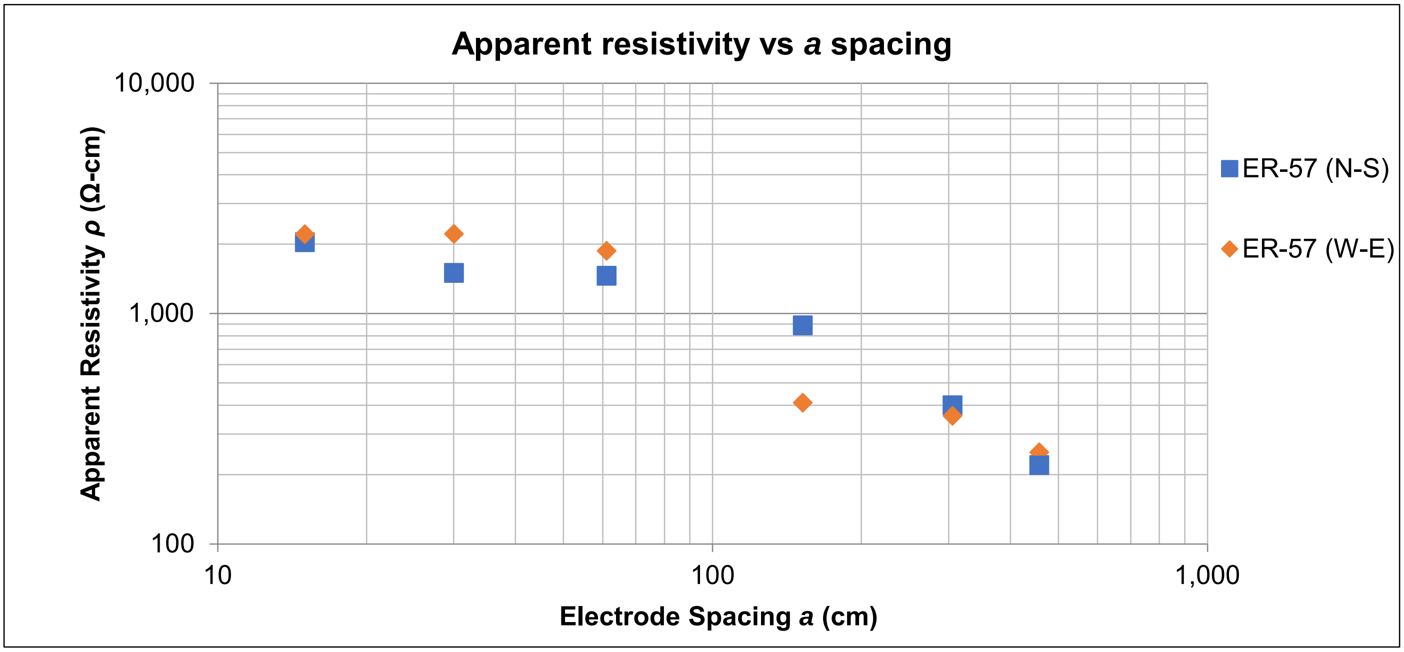
Array Loc. **ER-57** (36.477529°N, 120.194971°W)

Instrument	AGI SuperSting R1	**Weather**	Partly cloudy, High 48°F.
Serial #	SP0303161	**Ground Cond.**	Vegetated, silty, sandy soil
Cal. Check	4/8/2022	**Tested By**	T. Black
Test Date	February 23, 2023	**Method**	Wenner 4-pin ASTM G57-06 (2012); IEEE 81-2012

Notes & Conflicts Arrays oriented N-S and W-E with a common midpoint.

Apparent resistivity ρ is calculated as :
$$\rho = \frac{4\pi a R}{1 + \frac{2a}{\sqrt{a^2 + 4b^2}} - \frac{a}{\sqrt{a^2 + b^2}}}$$

Electrode Spacing *a*		**Electrode Depth *b***		**ER-57 (N-S)**		**ER-57 (W-E)**	
(feet)	(centimeters)	(inches)	(centimeters)	Measured Resistance *R* Ω	Apparent Resistivity *ρ* (Ω-cm)	Measured Resistance *R* Ω	Apparent Resistivity *ρ* (Ω-cm)
0.5	15	1	3	20.32	2040	21.98	2210
1	30	1	3	7.842	1500	11.570	2220
2	61	2	5	3.775	1460	4.827	1870
5	152	6	15	0.9194	890	0.4226	410
10	305	12	30	0.2063	400	0.1833	360
15	457	12	30	0.0759	220	0.0867	250



FIELD ELECTRICAL RESISTIVITY DATA SHEET

Darden Solar Facility ■ Cantua Creek, Fresno County, California

October 13, 2023 ■ Terracon Project No. 60225172

NORCAL GEOPHYSICAL CONSULTANTS INC.
A Terracon COMPANY

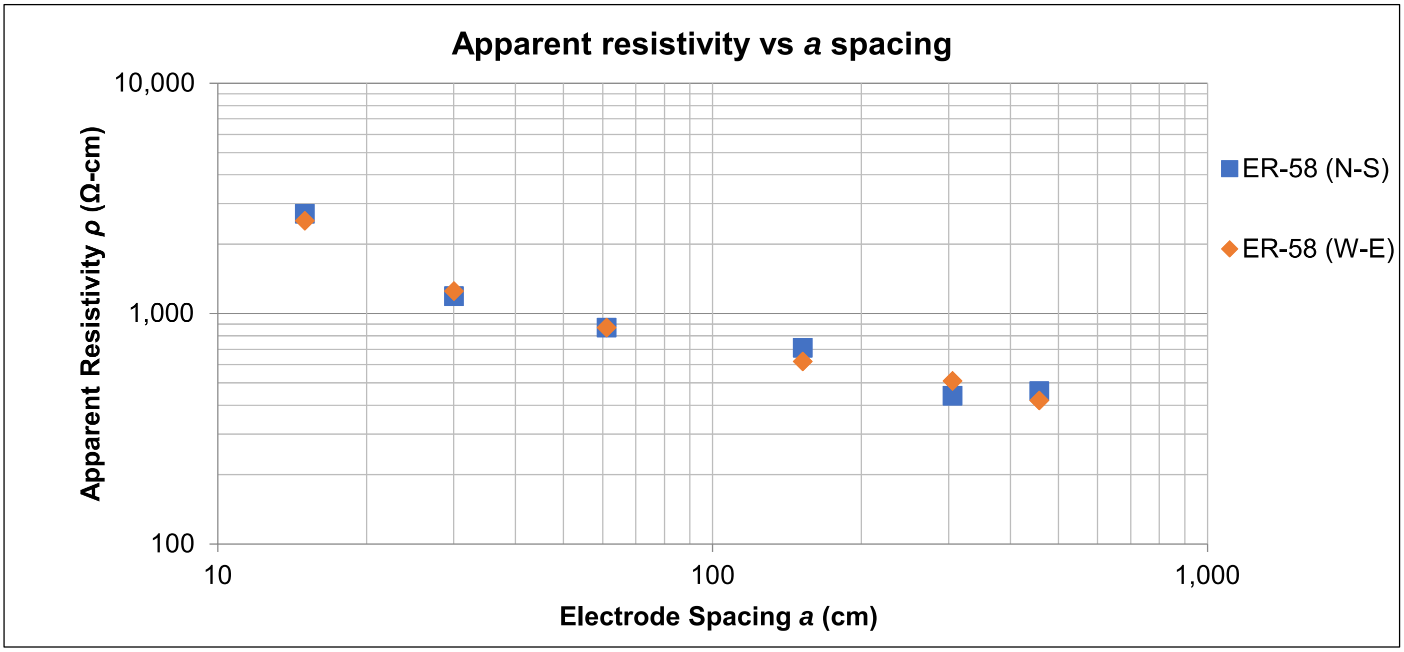
Array Loc. **ER-58** (36.469909°N, 120.218445°W)

Instrument	AGI SuperSting R1	**Weather**	Sunny, High 60°F.
Serial #	SP0303161	**Ground Cond.**	Silty, sandy soil
Cal. Check	4/8/2022	**Tested By**	T. Black
Test Date	February 17, 2023	**Method**	Wenner 4-pin ASTM G57-06 (2012); IEEE 81-2012

Notes & Conflicts Arrays oriented N-S and W-E with a common midpoint.

Apparent resistivity ρ is calculated as : $\rho = \dfrac{4\pi a R}{1 + \dfrac{2a}{\sqrt{a^2 + 4b^2}} - \dfrac{a}{\sqrt{a^2 + b^2}}}$

Electrode Spacing *a*		**Electrode Depth *b***		**ER-58 (N-S)**		**ER-58 (W-E)**	
(feet)	(centimeters)	(inches)	(centimeters)	Measured Resistance *R* Ω	Apparent Resistivity *ρ* (Ω-cm)	Measured Resistance *R* Ω	Apparent Resistivity *ρ* (Ω-cm)
0.5	15	1	3	26.96	2710	25.21	2530
1	30	1	3	6.193	1190	6.517	1250
2	61	2	5	2.247	870	2.233	870
5	152	6	15	0.7269	710	0.6365	620
10	305	12	30	0.2257	440	0.2640	510
15	457	12	30	0.1593	460	0.1458	420



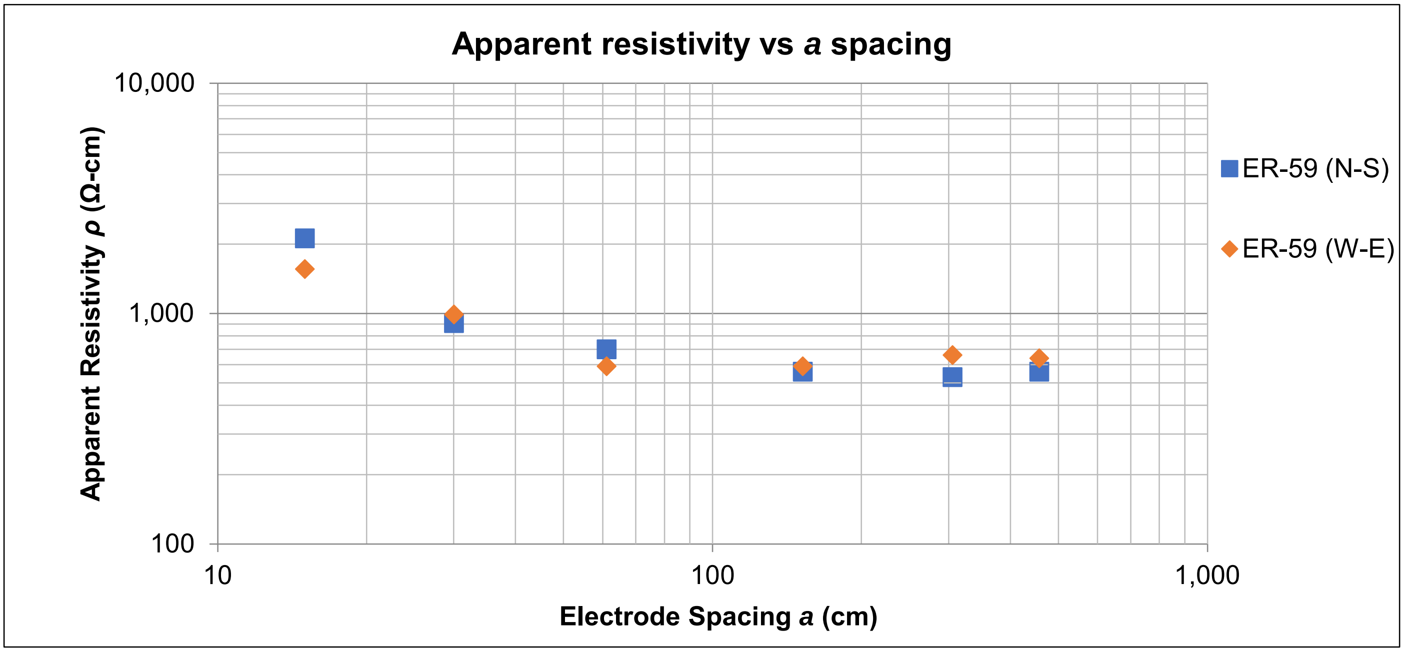
FIELD ELECTRICAL RESISTIVITY DATA SHEET

Darden Solar Facility ■ Cantua Creek, Fresno County, California
October 13, 2023 ■ Terracon Project No. 60225172

Array Loc.	**ER-59** (36.469253°N, 120.229117°W)		
Instrument	AGI SuperSting R1	**Weather**	Sunny, High 52°F.
Serial #	SP0303161	**Ground Cond.**	Silty, sandy soil
Cal. Check	4/8/2022	**Tested By**	T. Black
Test Date	February 15, 2023	**Method**	Wenner 4-pin ASTM G57-06 (2012); IEEE 81-2012
Notes & Conflicts	Arrays oriented N-S and W-E with a common midpoint.		

Apparent resistivity ρ is calculated as : $\rho = \dfrac{4\pi a R}{1 + \dfrac{2a}{\sqrt{a^2 + 4b^2}} - \dfrac{a}{\sqrt{a^2 + b^2}}}$

Electrode Spacing *a*		**Electrode Depth *b***		**ER-59 (N-S)**		**ER-59 (W-E)**	
(feet)	(centimeters)	(inches)	(centimeters)	Measured Resistance *R*	Apparent Resistivity ρ	Measured Resistance *R*	Apparent Resistivity ρ
				Ω	(Ω-cm)	Ω	(Ω-cm)
0.5	15	1	3	21.08	2120	15.56	1560
1	30	1	3	4.735	910	5.184	990
2	61	2	5	1.793	700	1.509	590
5	152	6	15	0.5817	560	0.6103	590
10	305	12	30	0.2739	530	0.3381	660
15	457	12	30	0.1936	560	0.2210	640



FIELD ELECTRICAL RESISTIVITY DATA SHEET

Darden Solar Facility ■ Cantua Creek, Fresno County, California
October 13, 2023 ■ Terracon Project No. 60225172

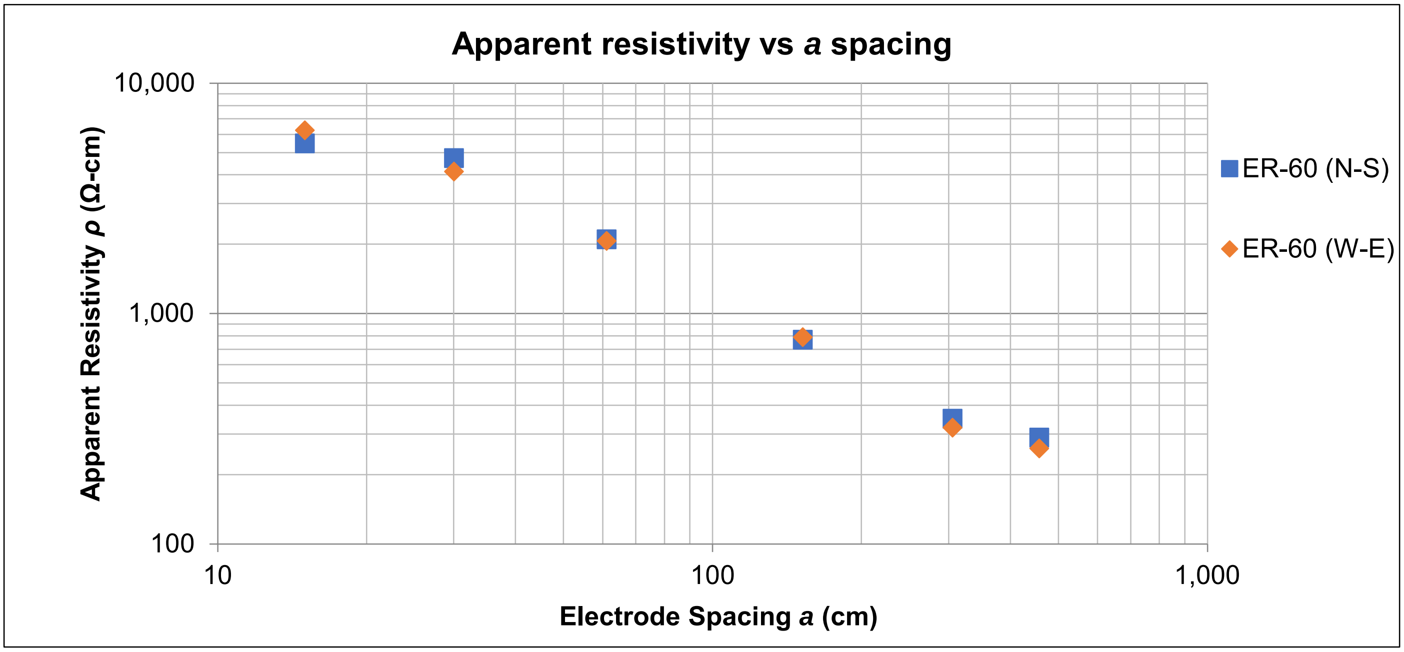
Array Loc. **ER-60** (36.468116°N, 120.212817°W)

Instrument	AGI SuperSting R1	**Weather**	Sunny, High 60°F.
Serial #	SP0303161	**Ground Cond.**	Silty, sandy soil
Cal. Check	4/8/2022	**Tested By**	T. Black
Test Date	February 17, 2023	**Method**	Wenner 4-pin ASTM G57-06 (2012); IEEE 81-2012

Notes & Conflicts Arrays oriented N-S and W-E with a common midpoint.

Apparent resistivity ρ is calculated as : $\rho = \dfrac{4\pi aR}{1 + \dfrac{2a}{\sqrt{a^2+4b^2}} - \dfrac{a}{\sqrt{a^2+b^2}}}$

Electrode Spacing *a*		**Electrode Depth *b***		**ER-60 (N-S)**		**ER-60 (W-E)**	
(feet)	(centimeters)	(inches)	(centimeters)	Measured Resistance *R* Ω	Apparent Resistivity *ρ* (Ω-cm)	Measured Resistance *R* Ω	Apparent Resistivity *ρ* (Ω-cm)
0.5	15	1	3	54.49	5470	62.08	6240
1	30	1	3	24.67	4730	21.58	4140
2	61	2	5	5.419	2100	5.331	2070
5	152	6	15	0.7970	770	0.8184	790
10	305	12	30	0.1818	350	0.1630	320
15	457	12	30	0.1011	290	0.0884	260



FIELD ELECTRICAL RESISTIVITY DATA SHEET

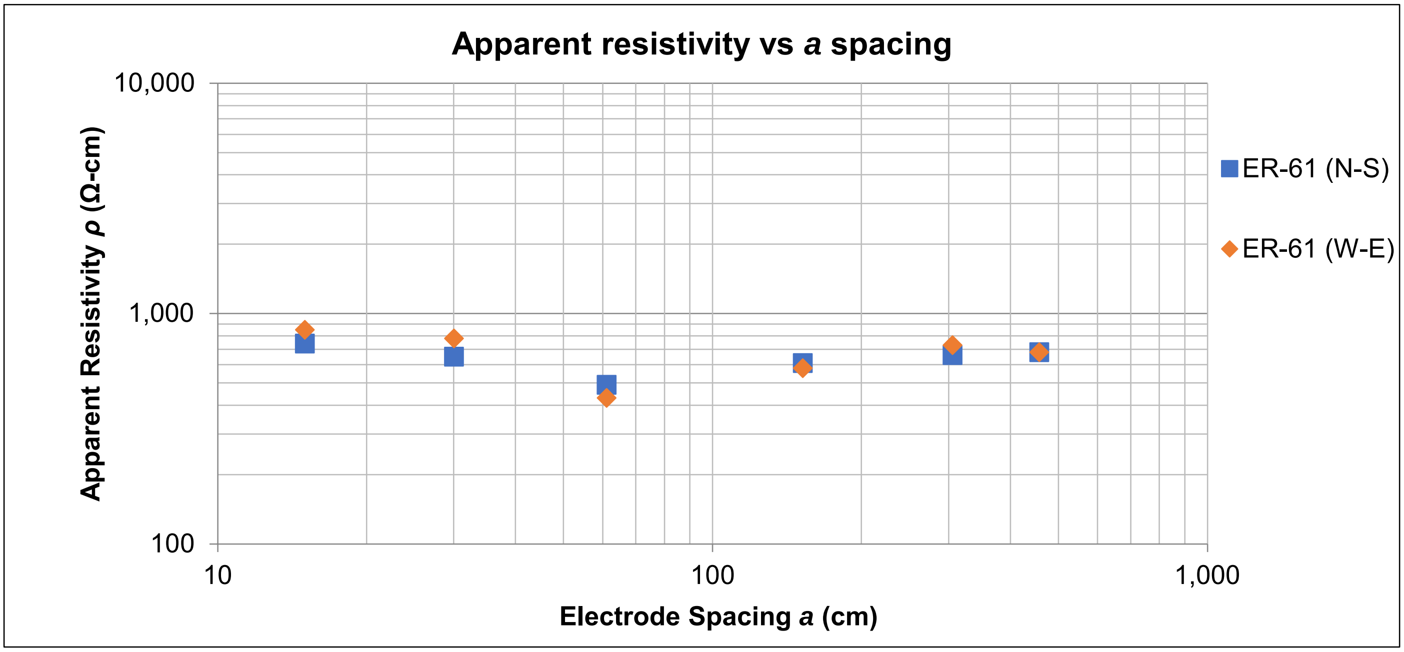
Darden Solar Facility ■ Cantua Creek, Fresno County, California
October 13, 2023 ■ Terracon Project No. 60225172

NORCAL GEOPHYSICAL CONSULTANTS INC.
A Terracon COMPANY

Array Loc.	**ER-61** (36.464005°N, 120.22514°W)		
Instrument	AGI SuperSting R1	**Weather**	Sunny, High 52°F.
Serial #	SP0303161	**Ground Cond.**	Silty, sandy soil
Cal. Check	4/8/2022	**Tested By**	T. Black
Test Date	February 15, 2023	**Method**	Wenner 4-pin ASTM G57-06 (2012); IEEE 81-2012
Notes & Conflicts	Arrays oriented N-S and W-E with a common midpoint.		

Apparent resistivity ρ is calculated as : $$\rho = \frac{4\pi a R}{1 + \frac{2a}{\sqrt{a^2 + 4b^2}} - \frac{a}{\sqrt{a^2 + b^2}}}$$

Electrode Spacing *a*		**Electrode Depth *b***		**ER-61 (N-S)**		**ER-61 (W-E)**	
(feet)	(centimeters)	(inches)	(centimeters)	Measured Resistance *R*	Apparent Resistivity *ρ*	Measured Resistance *R*	Apparent Resistivity *ρ*
				Ω	(Ω-cm)	Ω	(Ω-cm)
0.5	15	1	3	7.380	740	8.496	850
1	30	1	3	3.366	650	4.043	780
2	61	2	5	1.258	490	1.112	430
5	152	6	15	0.6245	610	0.6018	580
10	305	12	30	0.3381	660	0.3734	730
15	457	12	30	0.2359	680	0.2363	680



FIELD ELECTRICAL RESISTIVITY DATA SHEET

Darden Solar Facility ■ Cantua Creek, Fresno County, California
October 13, 2023 ■ Terracon Project No. 60225172

Array Loc. **ER-62** (36.458598°N, 120.227410°W)

Instrument AGI SuperSting R1 **Weather** Sunny, High 52°F.

Serial # SP0303161 **Ground Cond.** Silty, sandy soil

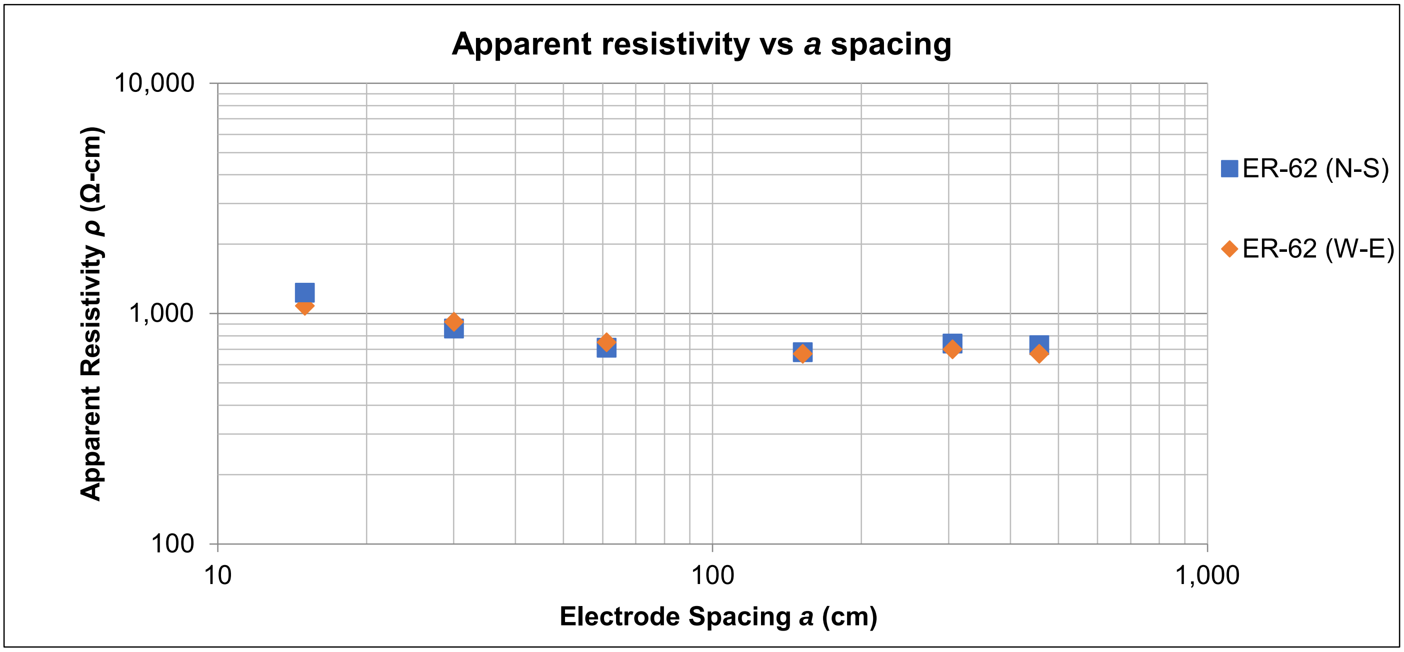
Cal. Check 4/8/2022 **Tested By** T. Black

Test Date February 15, 2023 **Method** Wenner 4-pin ASTM G57-06 (2012); IEEE 81-2012

Notes & Conflicts Arrays oriented N-S and W-E with a common midpoint.

Apparent resistivity ρ is calculated as :
$$\rho = \frac{4\pi a R}{1 + \frac{2a}{\sqrt{a^2 + 4b^2}} - \frac{a}{\sqrt{a^2 + b^2}}}$$

Electrode Spacing *a*		**Electrode Depth *b***		**ER-62 (N-S)**		**ER-62 (W-E)**	
(feet)	(centimeters)	(inches)	(centimeters)	Measured Resistance *R*	Apparent Resistivity *ρ*	Measured Resistance *R*	Apparent Resistivity *ρ*
				Ω	(Ω-cm)	Ω	(Ω-cm)
0.5	15	1	3	12.21	1230	10.72	1080
1	30	1	3	4.460	860	4.811	920
2	61	2	5	1.832	710	1.927	750
5	152	6	15	0.7028	680	0.6934	670
10	305	12	30	0.3810	740	0.3594	700
15	457	12	30	0.2526	730	0.2322	670



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GEOPHYSICAL CONSULTANTS INC.
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FIELD ELECTRICAL RESISTIVITY DATA SHEET

Darden Solar Facility ■ Cantua Creek, Fresno County, California
October 13, 2023 ■ Terracon Project No. 60225172

Array Loc. **ER-63** (36.461791°N, 120.216267°W)

Instrument AGI SuperSting R1

Serial # SP0303161

Cal. Check 4/8/2022

Test Date February 17, 2023

Weather Sunny, High 60°F.

Ground Cond. Silty, sandy soil

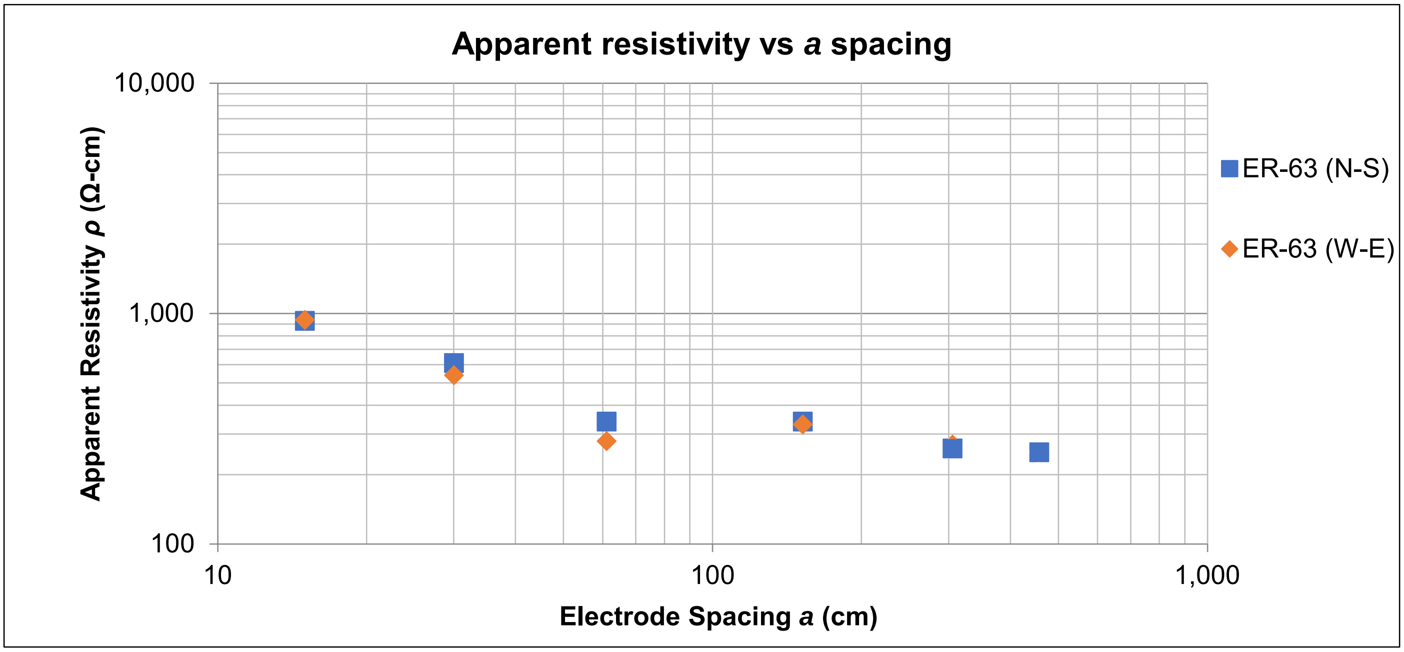
Tested By T. Black

Method Wenner 4-pin ASTM G57-06 (2012); IEEE 81-2012

Notes & Conflicts Arrays oriented N-S and W-E with a common midpoint.

Apparent resistivity ρ is calculated as : $\rho = \dfrac{4\pi a R}{1 + \dfrac{2a}{\sqrt{a^2 + 4b^2}} - \dfrac{a}{\sqrt{a^2 + b^2}}}$

Electrode Spacing *a*		Electrode Depth *b*		ER-63 (N-S)		ER-63 (W-E)	
(feet)	(centimeters)	(inches)	(centimeters)	Measured Resistance *R*	Apparent Resistivity *ρ*	Measured Resistance *R*	Apparent Resistivity *ρ*
				Ω	(Ω-cm)	Ω	(Ω-cm)
0.5	15	1	3	9.241	930	9.373	940
1	30	1	3	3.199	610	2.832	540
2	61	2	5	0.867	340	0.734	280
5	152	6	15	0.3525	340	0.3444	330
10	305	12	30	0.1338	260	0.1382	270
15	457	12	30	0.0873	250	0.0863	250



FIELD ELECTRICAL RESISTIVITY DATA SHEET

Darden Solar Facility ■ Cantua Creek, Fresno County, California
October 13, 2023 ■ Terracon Project No. 60225172

Array Loc. **ER-64** (36.454832°N, 120.212869°W)

Instrument AGI SuperSting R1

Weather Sunny, High 60°F.

Serial # SP0303161

Ground Cond. Silty, sandy soil

Cal. Check 4/8/2022

Tested By T. Black

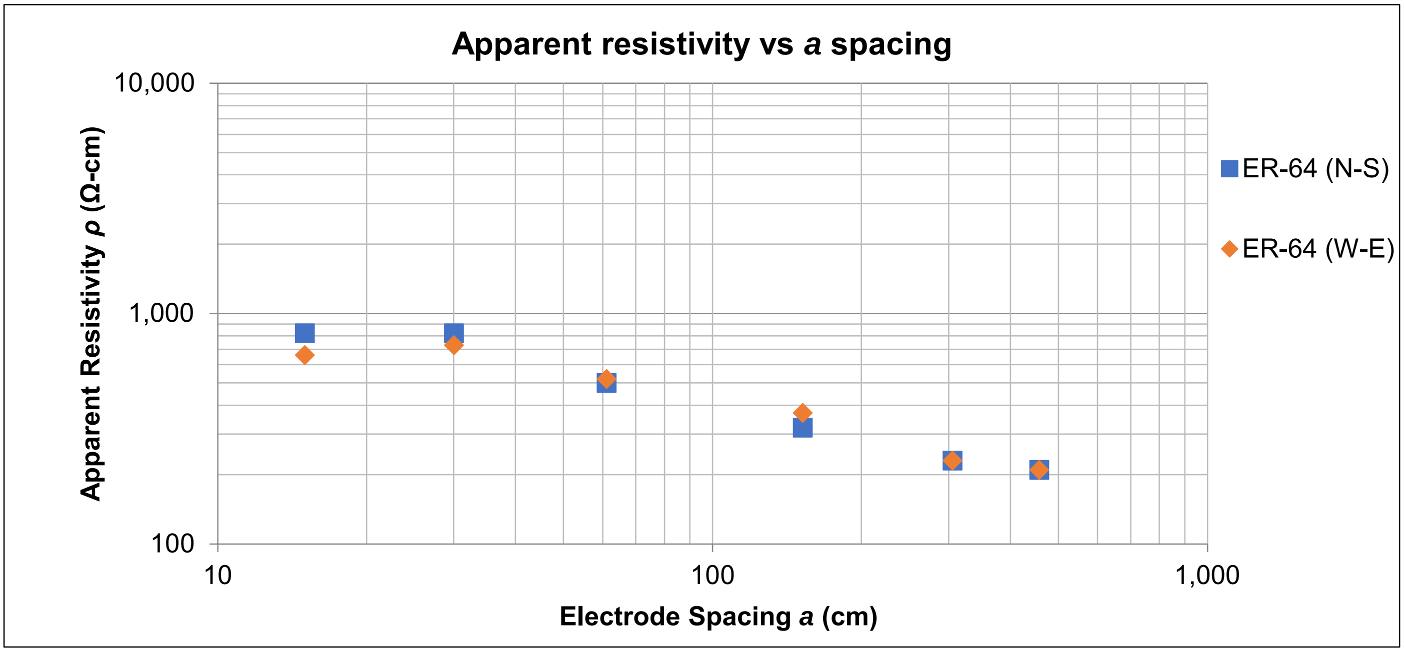
Test Date February 16, 2023

Method Wenner 4-pin ASTM G57-06 (2012); IEEE 81-2012

Notes & Conflicts Arrays oriented N-S and W-E with a common midpoint.

Apparent resistivity ρ is calculated as : $$\rho = \frac{4\pi a R}{1 + \frac{2a}{\sqrt{a^2 + 4b^2}} - \frac{a}{\sqrt{a^2 + b^2}}}$$

Electrode Spacing *a*		**Electrode Depth *b***		**ER-64 (N-S)**		**ER-64 (W-E)**	
(feet)	(centimeters)	(inches)	(centimeters)	Measured Resistance *R*	Apparent Resistivity *ρ*	Measured Resistance *R*	Apparent Resistivity *ρ*
				Ω	(Ω-cm)	Ω	(Ω-cm)
0.5	15	1	3	8.169	820	6.599	660
1	30	1	3	4.290	820	3.827	730
2	61	2	5	1.295	500	1.335	520
5	152	6	15	0.3330	320	0.3860	370
10	305	12	30	0.1195	230	0.1191	230
15	457	12	30	0.0739	210	0.0713	210



FIELD ELECTRICAL RESISTIVITY DATA SHEET

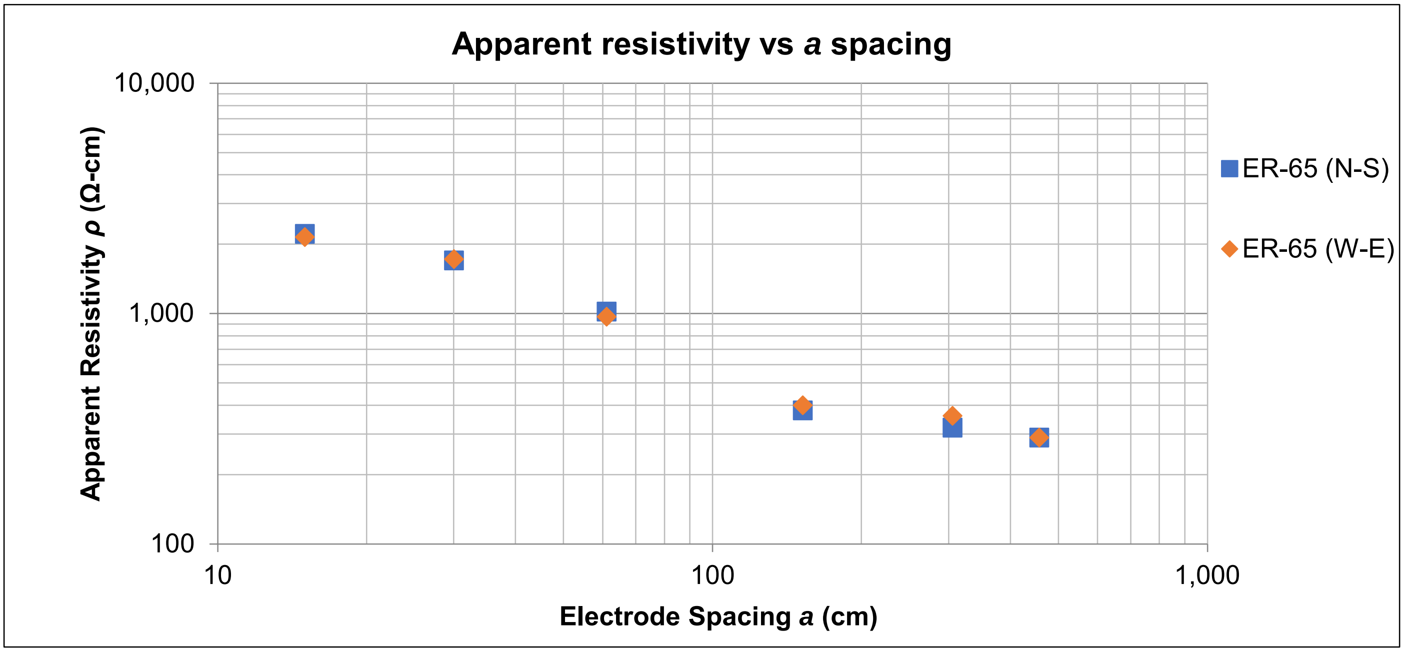
Darden Solar Facility ■ Cantua Creek, Fresno County, California
October 13, 2023 ■ Terracon Project No. 60225172

NORCAL GEOPHYSICAL CONSULTANTS INC.
A Terracon COMPANY

Array Loc.	**ER-65** (36.449303°N, 120.214889°W)		
Instrument	AGI SuperSting R1	**Weather**	Sunny, High 60°F.
Serial #	SP0303161	**Ground Cond.**	Silty, sandy soil
Cal. Check	4/8/2022	**Tested By**	T. Black
Test Date	February 16, 2023	**Method**	Wenner 4-pin ASTM G57-06 (2012); IEEE 81-2012
Notes & Conflicts	Arrays oriented N-S and W-E with a common midpoint.		

Apparent resistivity ρ is calculated as : $$\rho = \frac{4\pi a R}{1 + \frac{2a}{\sqrt{a^2 + 4b^2}} - \frac{a}{\sqrt{a^2 + b^2}}}$$

Electrode Spacing *a*		**Electrode Depth *b***		**ER-65 (N-S)**		**ER-65 (W-E)**	
(feet)	(centimeters)	(inches)	(centimeters)	Measured Resistance *R*	Apparent Resistivity *ρ*	Measured Resistance *R*	Apparent Resistivity *ρ*
				Ω	(Ω-cm)	Ω	(Ω-cm)
0.5	15	1	3	22.05	2220	21.43	2150
1	30	1	3	8.886	1700	8.953	1720
2	61	2	5	2.624	1020	2.506	970
5	152	6	15	0.3920	380	0.4104	400
10	305	12	30	0.1645	320	0.1838	360
15	457	12	30	0.0990	290	0.0999	290



FIELD ELECTRICAL RESISTIVITY DATA SHEET
Darden Solar Facility ■ Cantua Creek, Fresno County, California
October 13, 2023 ■ Terracon Project No. 60225172

NORCAL GEOPHYSICAL CONSULTANTS INC.
A Terracon COMPANY

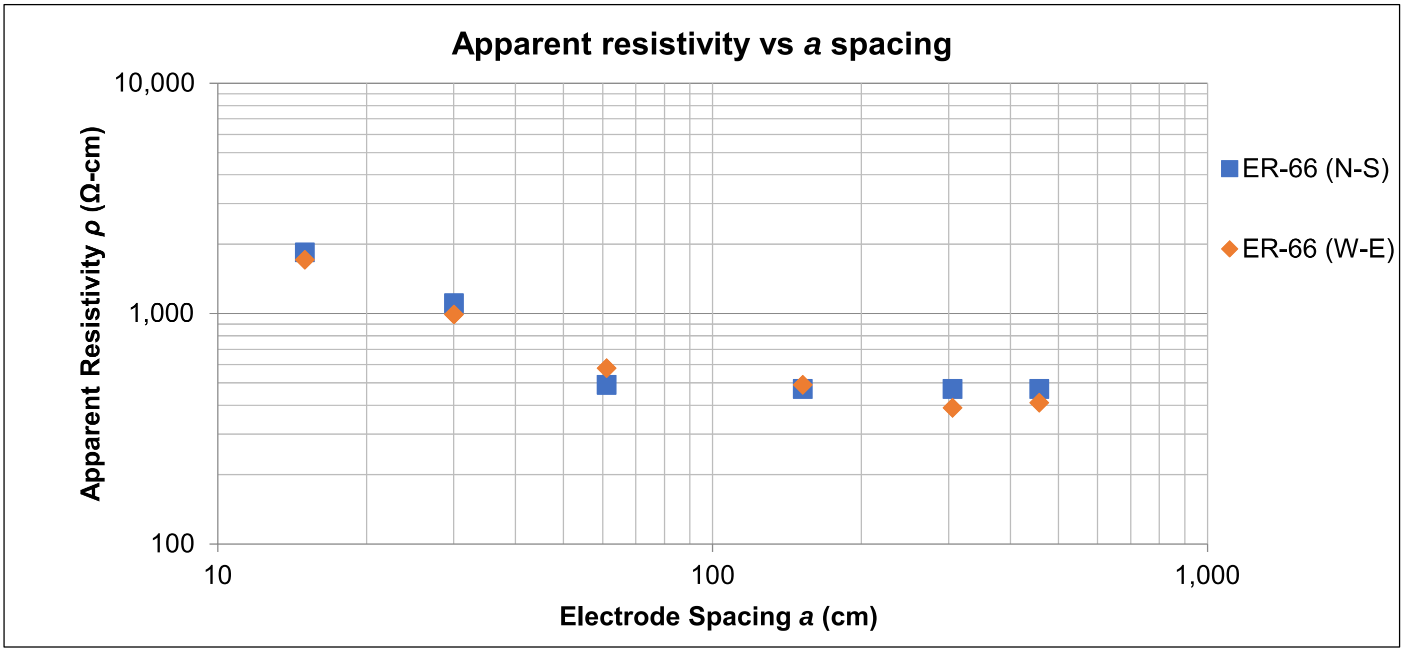
Array Loc. **ER-66** (36.446119°N, 120.220368°W)

Instrument	AGI SuperSting R1	**Weather**	Sunny, High 60°F.
Serial #	SP0303161	**Ground Cond.**	Silty, sandy soil
Cal. Check	4/8/2022	**Tested By**	T. Black
Test Date	February 16, 2023	**Method**	Wenner 4-pin ASTM G57-06 (2012); IEEE 81-2012

Notes & Conflicts Arrays oriented N-S and W-E with a common midpoint.

Apparent resistivity ρ is calculated as : $\rho = \dfrac{4\pi aR}{1 + \dfrac{2a}{\sqrt{a^2 + 4b^2}} - \dfrac{a}{\sqrt{a^2 + b^2}}}$

Electrode Spacing *a*		**Electrode Depth *b***		**ER-66 (N-S)**		**ER-66 (W-E)**	
(feet)	(centimeters)	(inches)	(centimeters)	Measured Resistance *R* Ω	Apparent Resistivity *ρ* (Ω-cm)	Measured Resistance *R* Ω	Apparent Resistivity *ρ* (Ω-cm)
0.5	15	1	3	18.35	1840	17.02	1710
1	30	1	3	5.773	1110	5.183	990
2	61	2	5	1.270	490	1.485	580
5	152	6	15	0.4869	470	0.5059	490
10	305	12	30	0.2421	470	0.2012	390
15	457	12	30	0.1629	470	0.1412	410



FIELD ELECTRICAL RESISTIVITY DATA SHEET

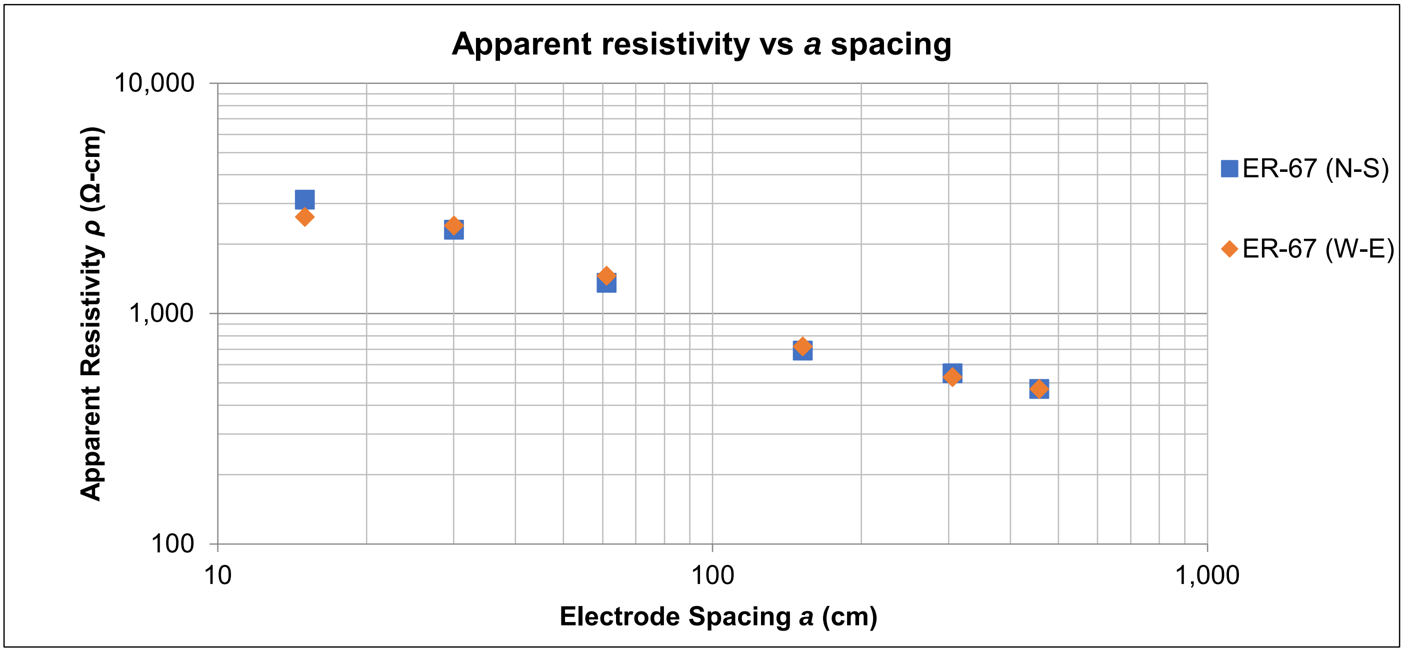
Darden Solar Facility ■ Cantua Creek, Fresno County, California
October 13, 2023 ■ Terracon Project No. 60225172

Array Loc.	**ER-67** (36.444453°N, 120.228263°W)		
Instrument	AGI SuperSting R1	**Weather**	Sunny, High 60°F.
Serial #	SP0303161	**Ground Cond.**	Silty, sandy soil
Cal. Check	4/8/2022	**Tested By**	T. Black
Test Date	February 16, 2023	**Method**	Wenner 4-pin ASTM G57-06 (2012); IEEE 81-2012
Notes & Conflicts	Arrays oriented N-S and W-E with a common midpoint.		

Apparent resistivity ρ is calculated as :

$$\rho = \frac{4\pi a R}{1 + \frac{2a}{\sqrt{a^2 + 4b^2}} - \frac{a}{\sqrt{a^2 + b^2}}}$$

Electrode Spacing *a*		**Electrode Depth *b***		**ER-67 (N-S)**		**ER-67 (W-E)**	
(feet)	(centimeters)	(inches)	(centimeters)	Measured Resistance *R*	Apparent Resistivity *ρ*	Measured Resistance *R*	Apparent Resistivity *ρ*
				Ω	(Ω-cm)	Ω	(Ω-cm)
0.5	15	1	3	31.07	3120	26.20	2630
1	30	1	3	12.070	2310	12.580	2410
2	61	2	5	3.515	1360	3.772	1460
5	152	6	15	0.7094	690	0.7421	720
10	305	12	30	0.2801	550	0.2703	530
15	457	12	30	0.1615	470	0.1621	470



FIELD ELECTRICAL RESISTIVITY DATA SHEET

Darden Solar Facility ■ Cantua Creek, Fresno County, California
October 13, 2023 ■ Terracon Project No. 60225172

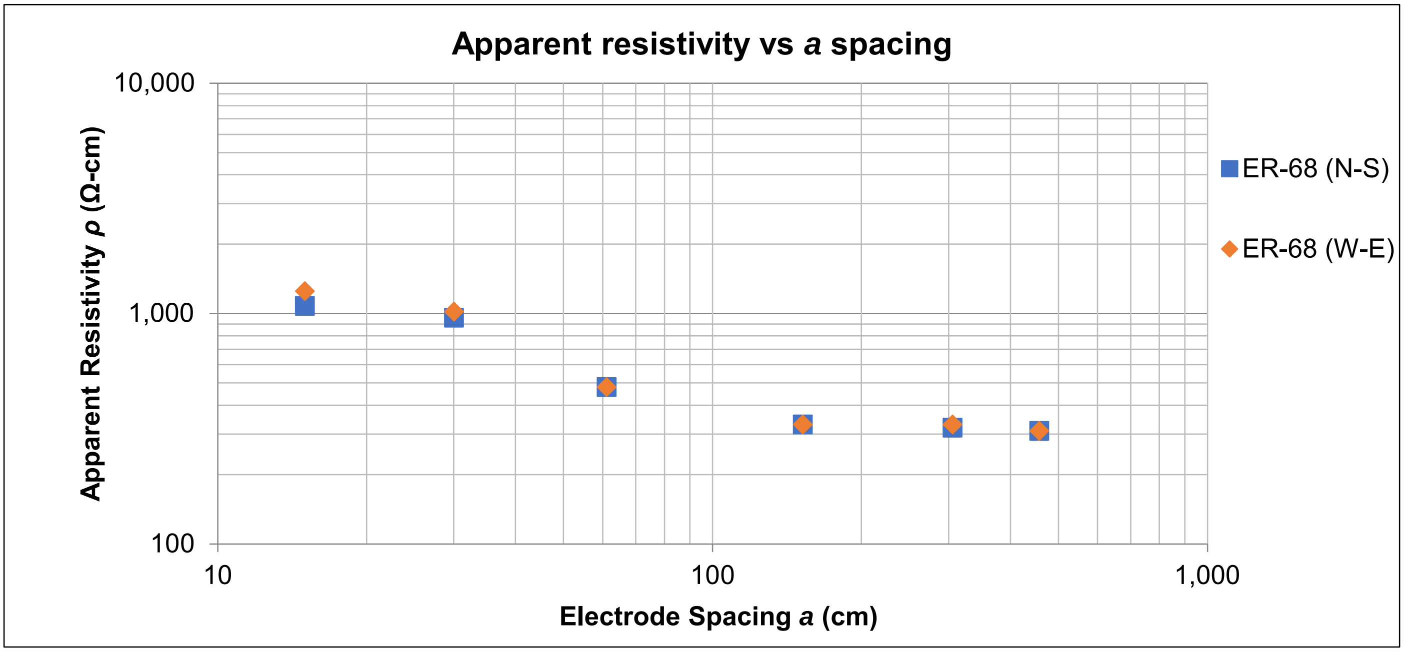
NORCAL GEOPHYSICAL CONSULTANTS INC.
A Terracon COMPANY

Array Loc.	**ER-68** (36.448120°N, 120.227466°W)		
Instrument	AGI SuperSting R1	**Weather**	Sunny, High 52°F.
Serial #	SP0303161	**Ground Cond.**	Silty, sandy soil
Cal. Check	4/8/2022	**Tested By**	T. Black
Test Date	February 15, 2023	**Method**	Wenner 4-pin ASTM G57-06 (2012); IEEE 81-2012
Notes & Conflicts	Arrays oriented N-S and W-E with a common midpoint.		

Apparent resistivity ρ is calculated as :

$$\rho = \frac{4\pi a R}{1 + \frac{2a}{\sqrt{a^2 + 4b^2}} - \frac{a}{\sqrt{a^2 + b^2}}}$$

Electrode Spacing *a*		**Electrode Depth *b***		**ER-68 (N-S)**		**ER-68 (W-E)**	
(feet)	(centimeters)	(inches)	(centimeters)	Measured Resistance *R*	Apparent Resistivity *ρ*	Measured Resistance *R*	Apparent Resistivity *ρ*
				Ω	(Ω-cm)	Ω	(Ω-cm)
0.5	15	1	3	10.78	1080	12.40	1250
1	30	1	3	4.985	960	5.294	1020
2	61	2	5	1.249	480	1.226	480
5	152	6	15	0.3423	330	0.3362	330
10	305	12	30	0.1636	320	0.1684	330
15	457	12	30	0.1081	310	0.1068	310



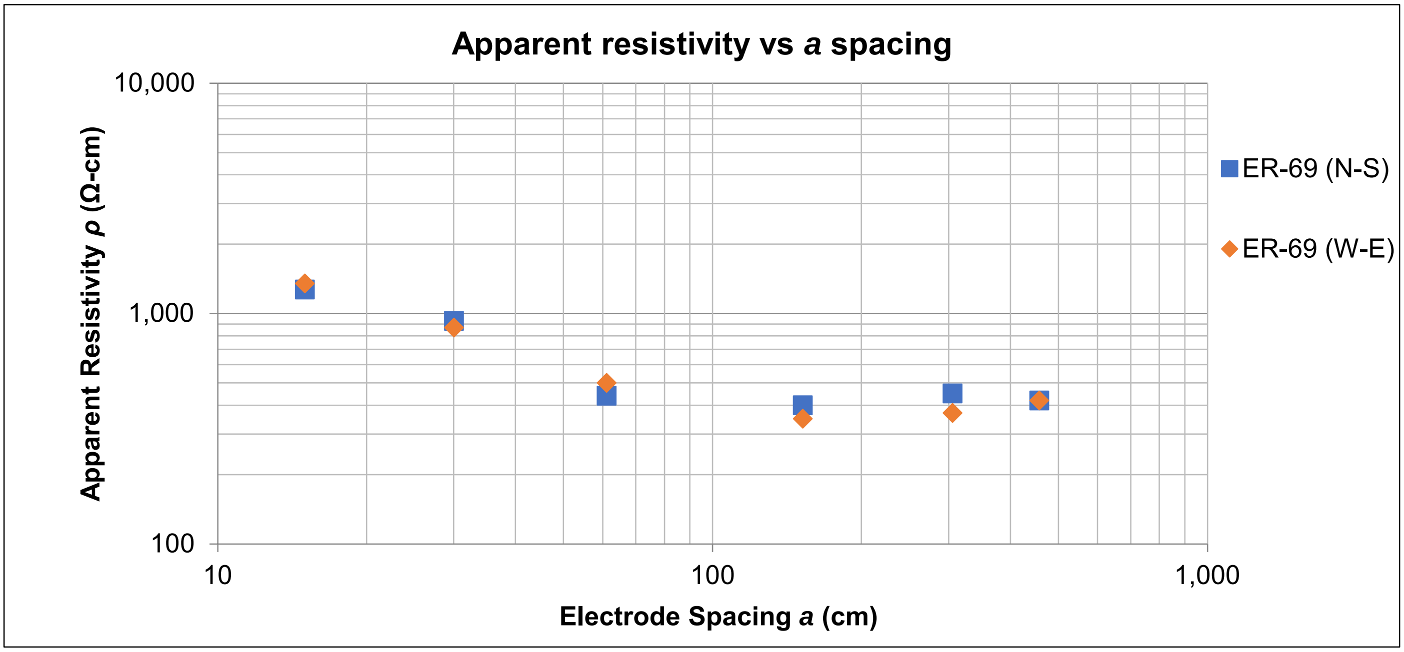
FIELD ELECTRICAL RESISTIVITY DATA SHEET

Darden Solar Facility ■ Cantua Creek, Fresno County, California
October 13, 2023 ■ Terracon Project No. 60225172

Array Loc.	**ER-69** (36.4454317°N, 120.2219715°W)		
Instrument	AGI SuperSting R1	**Weather**	Sunny, High 60°F.
Serial #	SP0303161	**Ground Cond.**	Silty, sandy soil
Cal. Check	4/8/2022	**Tested By**	T. Black
Test Date	February 16, 2023	**Method**	Wenner 4-pin ASTM G57-06 (2012); IEEE 81-2012
Notes & Conflicts	Arrays oriented N-S and W-E with a common midpoint.		

Apparent resistivity ρ is calculated as : $$\rho = \frac{4\pi a R}{1 + \frac{2a}{\sqrt{a^2 + 4b^2}} - \frac{a}{\sqrt{a^2 + b^2}}}$$

Electrode Spacing *a*		**Electrode Depth *b***		**ER-69 (N-S)**		**ER-69 (W-E)**	
(feet)	(centimeters)	(inches)	(centimeters)	Measured Resistance *R*	Apparent Resistivity *ρ*	Measured Resistance *R*	Apparent Resistivity *ρ*
				Ω	(Ω-cm)	Ω	(Ω-cm)
0.5	15	1	3	12.64	1270	13.41	1350
1	30	1	3	4.854	930	4.513	870
2	61	2	5	1.122	440	1.285	500
5	152	6	15	0.4125	400	0.3586	350
10	305	12	30	0.2311	450	0.1910	370
15	457	12	30	0.1468	420	0.1456	420



FIELD ELECTRICAL RESISTIVITY DATA SHEET

Darden Solar Facility ■ Cantua Creek, Fresno County, California
October 13, 2023 ■ Terracon Project No. 60225172

NORCAL GEOPHYSICAL CONSULTANTS INC.
A Terracon COMPANY

Array Loc. **ER-70** (36.468895°N, 120.179723°W)

Instrument AGI SuperSting R1

Weather Sunny, High 70°F.

Serial # SP0303161

Ground Cond. Silty, sandy soil

Cal. Check 4/8/2022

Tested By T. Black

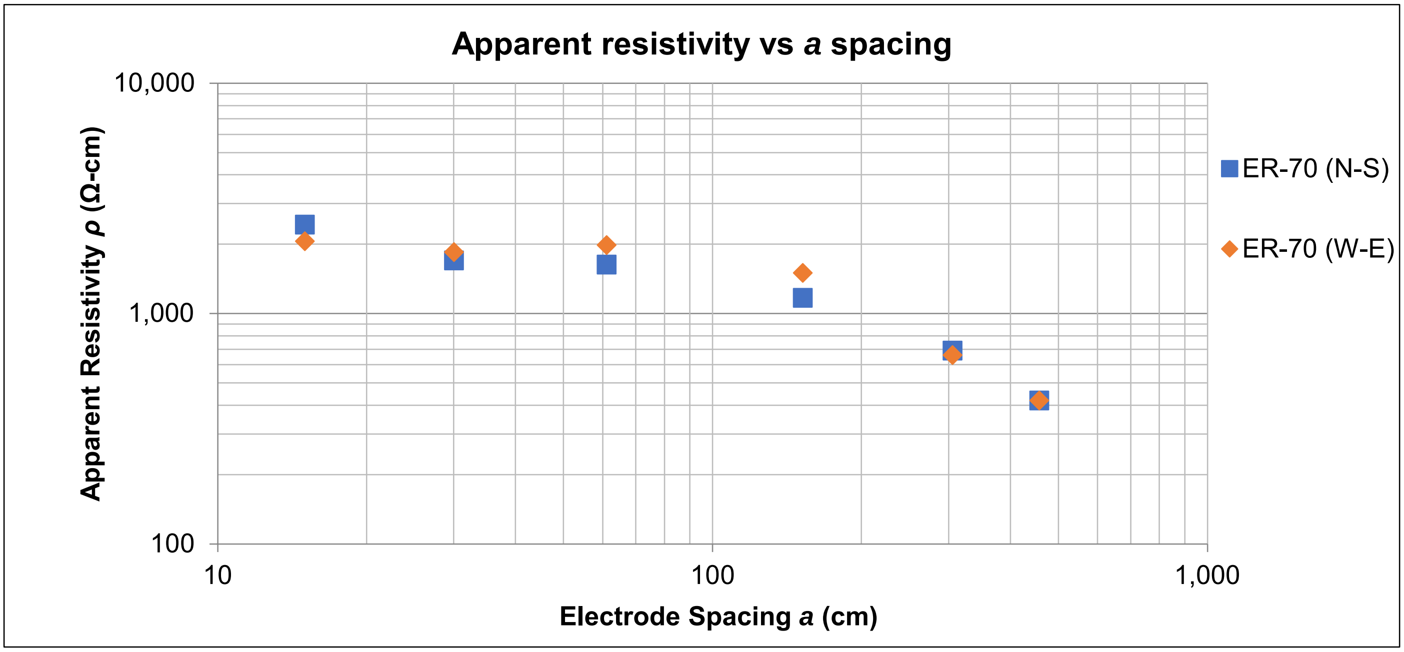
Test Date February 21, 2023

Method Wenner 4-pin ASTM G57-06 (2012); IEEE 81-2012

Notes & Conflicts Arrays oriented N-S and W-E with a common midpoint.

Apparent resistivity ρ is calculated as :
$$\rho = \frac{4\pi a R}{1 + \frac{2a}{\sqrt{a^2 + 4b^2}} - \frac{a}{\sqrt{a^2 + b^2}}}$$

Electrode Spacing *a*		**Electrode Depth *b***		**ER-70 (N-S)**		**ER-70 (W-E)**	
(feet)	(centimeters)	(inches)	(centimeters)	Measured Resistance *R*	Apparent Resistivity *ρ*	Measured Resistance *R*	Apparent Resistivity *ρ*
				Ω	(Ω-cm)	Ω	(Ω-cm)
0.5	15	1	3	24.16	2430	20.52	2060
1	30	1	3	8.878	1700	9.628	1850
2	61	2	5	4.196	1630	5.105	1980
5	152	6	15	1.2010	1170	1.5460	1500
10	305	12	30	0.3531	690	0.3402	660
15	457	12	30	0.1441	420	0.1462	420



FIELD ELECTRICAL RESISTIVITY DATA SHEET

Darden Solar Facility ■ Cantua Creek, Fresno County, California
October 13, 2023 ■ Terracon Project No. 60225172

NORCAL GEOPHYSICAL CONSULTANTS INC.
A Terracon COMPANY

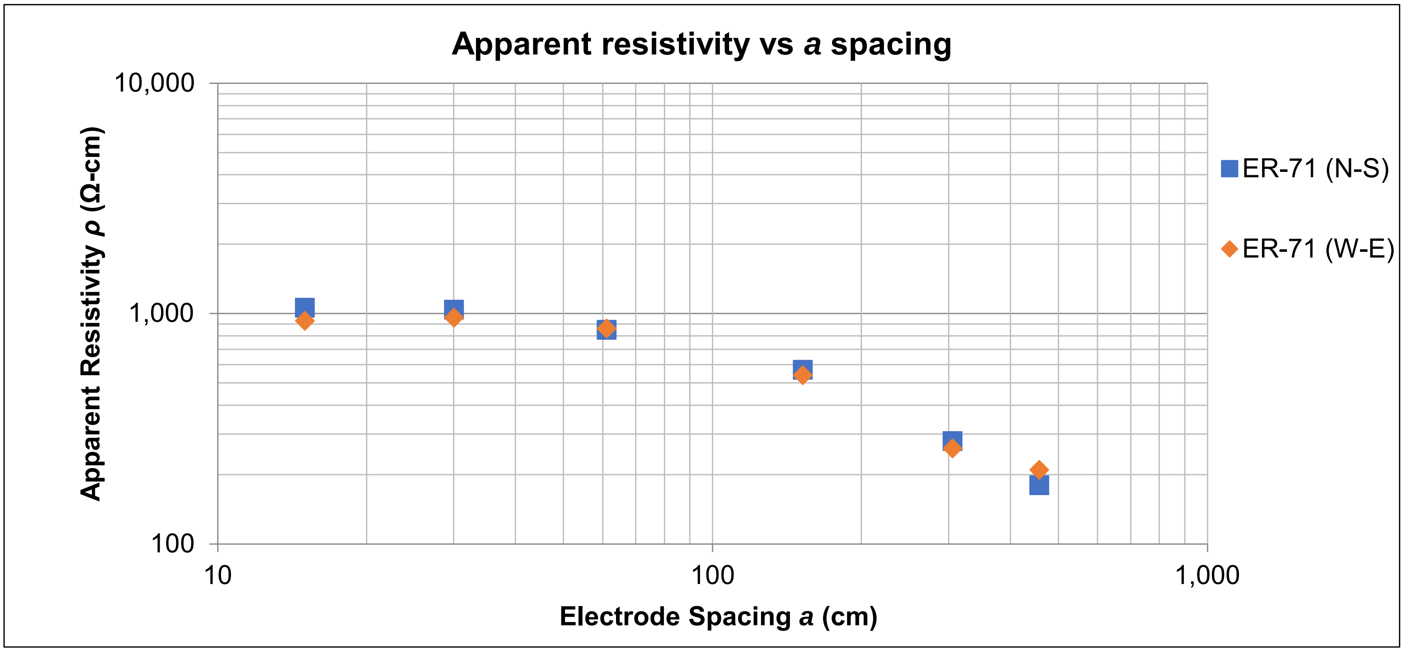
Array Loc. **ER-71** (36.463204°N, 120.192419°W)

Instrument	AGI SuperSting R1	**Weather**	Sunny, High 62°F.
Serial #	SP0303161	**Ground Cond.**	Silty, sandy soil
Cal. Check	4/8/2022	**Tested By**	T. Black
Test Date	February 17, 2023	**Method**	Wenner 4-pin ASTM G57-06 (2012); IEEE 81-2012

Notes & Conflicts Arrays oriented N-S and W-E with a common midpoint.

Apparent resistivity ρ is calculated as : $\rho = \dfrac{4\pi a R}{1 + \dfrac{2a}{\sqrt{a^2 + 4b^2}} - \dfrac{a}{\sqrt{a^2 + b^2}}}$

Electrode Spacing *a*		**Electrode Depth *b***		**ER-71 (N-S)**		**ER-71 (W-E)**	
(feet)	(centimeters)	(inches)	(centimeters)	Measured Resistance *R*	Apparent Resistivity *ρ*	Measured Resistance *R*	Apparent Resistivity *ρ*
				Ω	(Ω-cm)	Ω	(Ω-cm)
0.5	15	1	3	10.57	1060	9.232	930
1	30	1	3	5.445	1040	4.982	960
2	61	2	5	2.187	850	2.210	860
5	152	6	15	0.5860	570	0.5525	540
10	305	12	30	0.1414	280	0.1319	260
15	457	12	30	0.0638	180	0.0727	210



FIELD ELECTRICAL RESISTIVITY DATA SHEET

Darden Solar Facility ■ Cantua Creek, Fresno County, California
October 13, 2023 ■ Terracon Project No. 60225172

NORCAL GEOPHYSICAL CONSULTANTS INC.
A Terracon COMPANY

Array Loc. **ER-72** (36.469323°N, 120.185189°W)

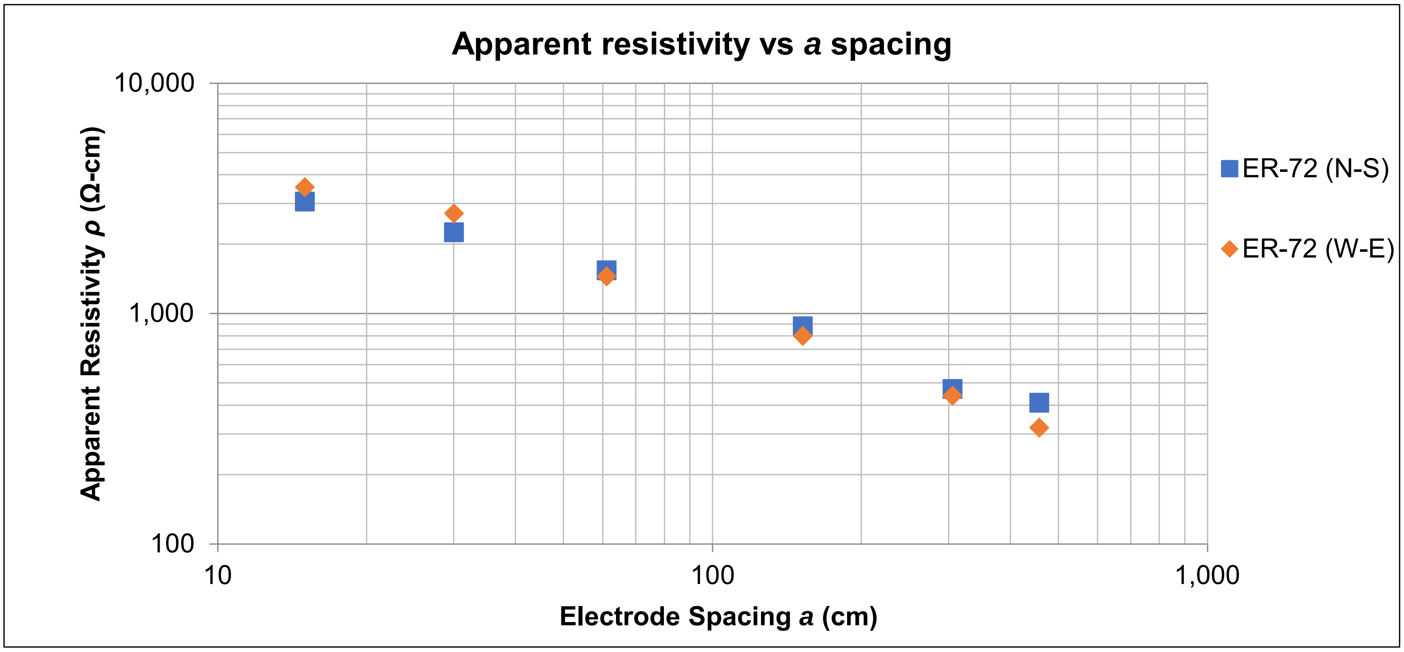
Instrument	AGI SuperSting R1	**Weather**	Sunny, High 70°F.
Serial #	SP0303161	**Ground Cond.**	Silty, sandy soil
Cal. Check	4/8/2022	**Tested By**	T. Black
Test Date	February 21, 2023	**Method**	Wenner 4-pin ASTM G57-06 (2012); IEEE 81-2012

Notes & Conflicts Arrays oriented N-S and W-E with a common midpoint.

Apparent resistivity ρ is calculated as :

$$\rho = \frac{4\pi a R}{1 + \frac{2a}{\sqrt{a^2 + 4b^2}} - \frac{a}{\sqrt{a^2 + b^2}}}$$

Electrode Spacing *a*		**Electrode Depth *b***		**ER-72 (N-S)**		**ER-72 (W-E)**	
(feet)	(centimeters)	(inches)	(centimeters)	Measured Resistance *R* Ω	Apparent Resistivity *ρ* (Ω-cm)	Measured Resistance *R* Ω	Apparent Resistivity *ρ* (Ω-cm)
0.5	15	1	3	30.43	3060	35.23	3540
1	30	1	3	11.75	2250	14.19	2720
2	61	2	5	3.966	1540	3.745	1450
5	152	6	15	0.9059	880	0.8263	800
10	305	12	30	0.2413	470	0.2243	440
15	457	12	30	0.1431	410	0.1097	320



FIELD ELECTRICAL RESISTIVITY DATA SHEET

Darden Solar Facility ■ Cantua Creek, Fresno County, California
October 13, 2023 ■ Terracon Project No. 60225172

NORCAL GEOPHYSICAL CONSULTANTS INC.
A Terracon COMPANY

Array Loc. **ER-73** (36.461605°N, 120.186377°W)

Instrument AGI SuperSting R1

Weather Sunny, High 50°F.

Serial # SP0303161

Ground Cond. Silty, sandy soil

Cal. Check 4/8/2022

Tested By T. Black

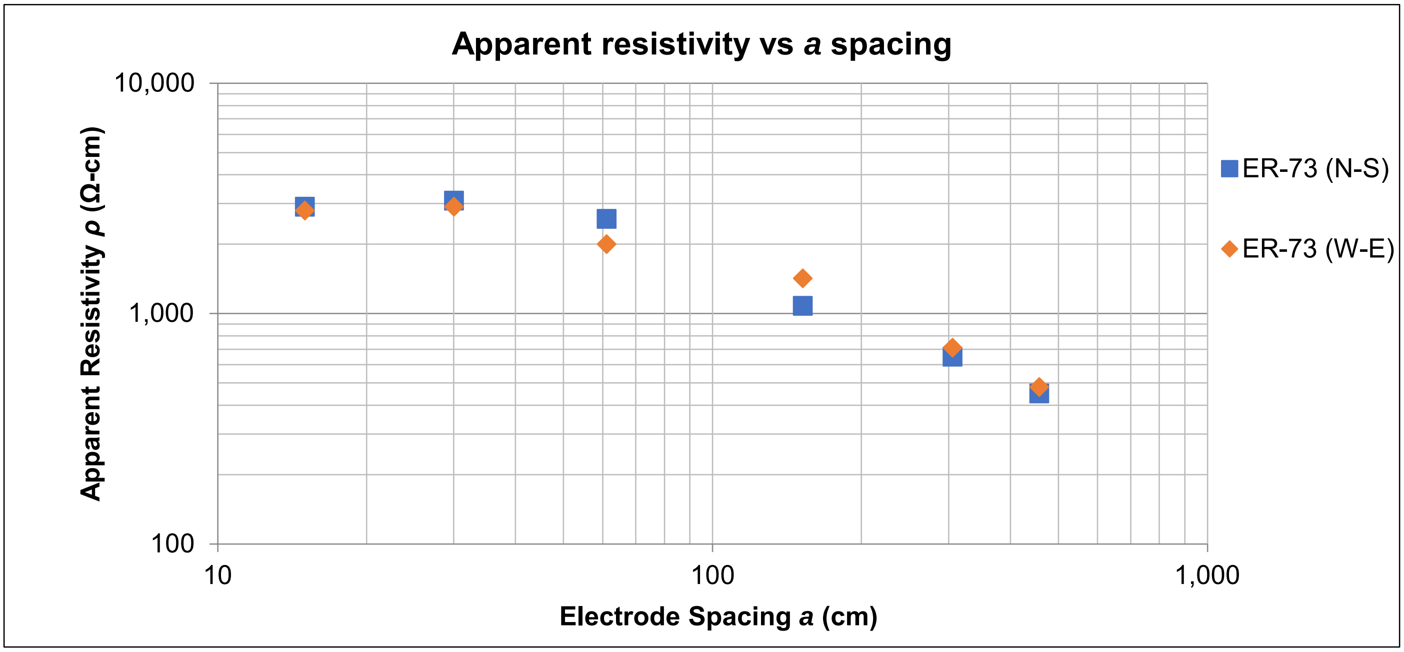
Test Date February 22, 2023

Method Wenner 4-pin ASTM G57-06 (2012); IEEE 81-2012

Notes & Conflicts Arrays oriented N-S and W-E with a common midpoint.

Apparent resistivity ρ is calculated as : $$\rho = \frac{4\pi a R}{1 + \frac{2a}{\sqrt{a^2 + 4b^2}} - \frac{a}{\sqrt{a^2 + b^2}}}$$

Electrode Spacing *a*		**Electrode Depth *b***		**ER-73 (N-S)**		**ER-73 (W-E)**	
(feet)	(centimeters)	(inches)	(centimeters)	Measured Resistance *R*	Apparent Resistivity *ρ*	Measured Resistance *R*	Apparent Resistivity *ρ*
				Ω	(Ω-cm)	Ω	(Ω-cm)
0.5	15	1	3	29.00	2910	27.92	2800
1	30	1	3	16.10	3090	15.20	2910
2	61	2	5	6.658	2580	5.164	2000
5	152	6	15	1.1100	1080	1.4590	1420
10	305	12	30	0.3345	650	0.3629	710
15	457	12	30	0.1556	450	0.1652	480



FIELD ELECTRICAL RESISTIVITY DATA SHEET

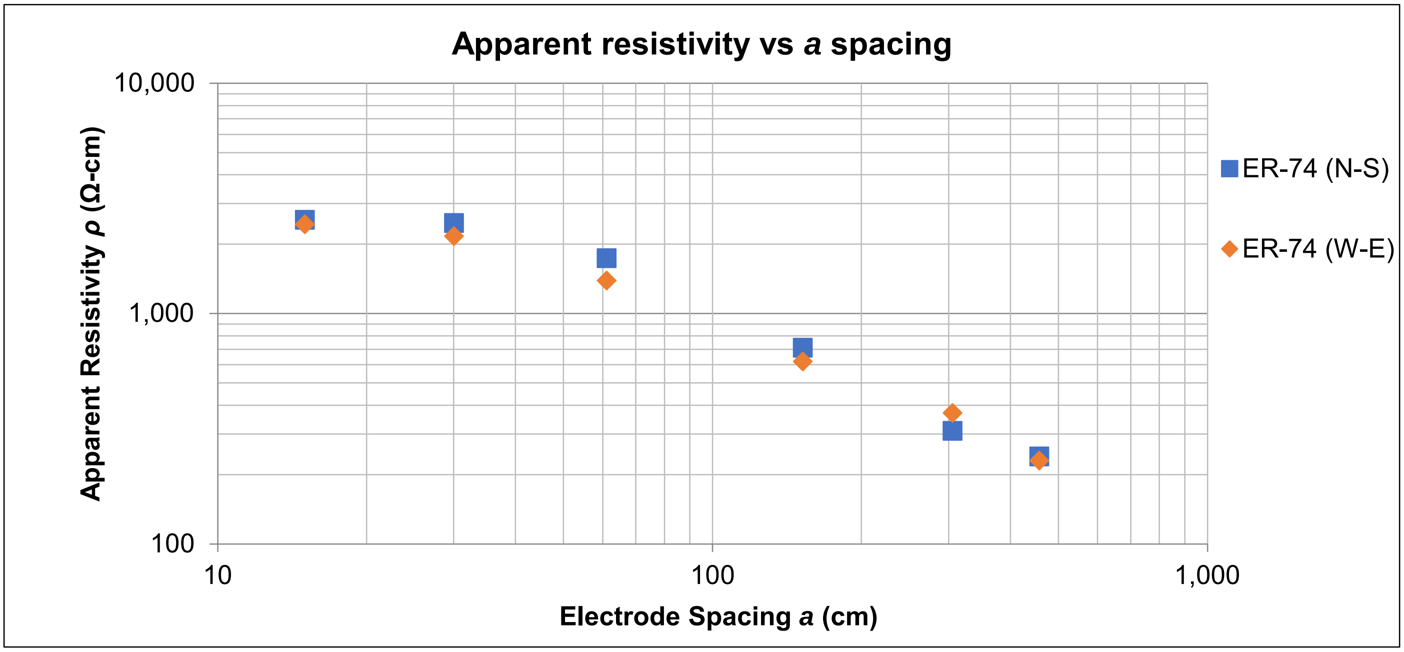
Darden Solar Facility ■ Cantua Creek, Fresno County, California
October 13, 2023 ■ Terracon Project No. 60225172

Array Loc.	**ER-74** (36.459094°N, 120.192568°W)		
Instrument	AGI SuperSting R1	**Weather**	Sunny, High 62°F.
Serial #	SP0303161	**Ground Cond.**	Silty, sandy soil
Cal. Check	4/8/2022	**Tested By**	T. Black
Test Date	February 17, 2023	**Method**	Wenner 4-pin ASTM G57-06 (2012); IEEE 81-2012
Notes & Conflicts	Arrays oriented N-S and W-E with a common midpoint.		

Apparent resistivity ρ is calculated as :

$$\rho = \frac{4\pi a R}{1 + \frac{2a}{\sqrt{a^2 + 4b^2}} - \frac{a}{\sqrt{a^2 + b^2}}}$$

Electrode Spacing *a*		**Electrode Depth *b***		**ER-74 (N-S)**		**ER-74 (W-E)**	
(feet)	(centimeters)	(inches)	(centimeters)	Measured Resistance *R*	Apparent Resistivity *ρ*	Measured Resistance *R*	Apparent Resistivity *ρ*
				Ω	(Ω-cm)	Ω	(Ω-cm)
0.5	15	1	3	25.42	2550	24.29	2440
1	30	1	3	12.90	2470	11.32	2170
2	61	2	5	4.488	1740	3.582	1390
5	152	6	15	0.7362	710	0.6374	620
10	305	12	30	0.1583	310	0.1876	370
15	457	12	30	0.0841	240	0.0798	230



FIELD ELECTRICAL RESISTIVITY DATA SHEET

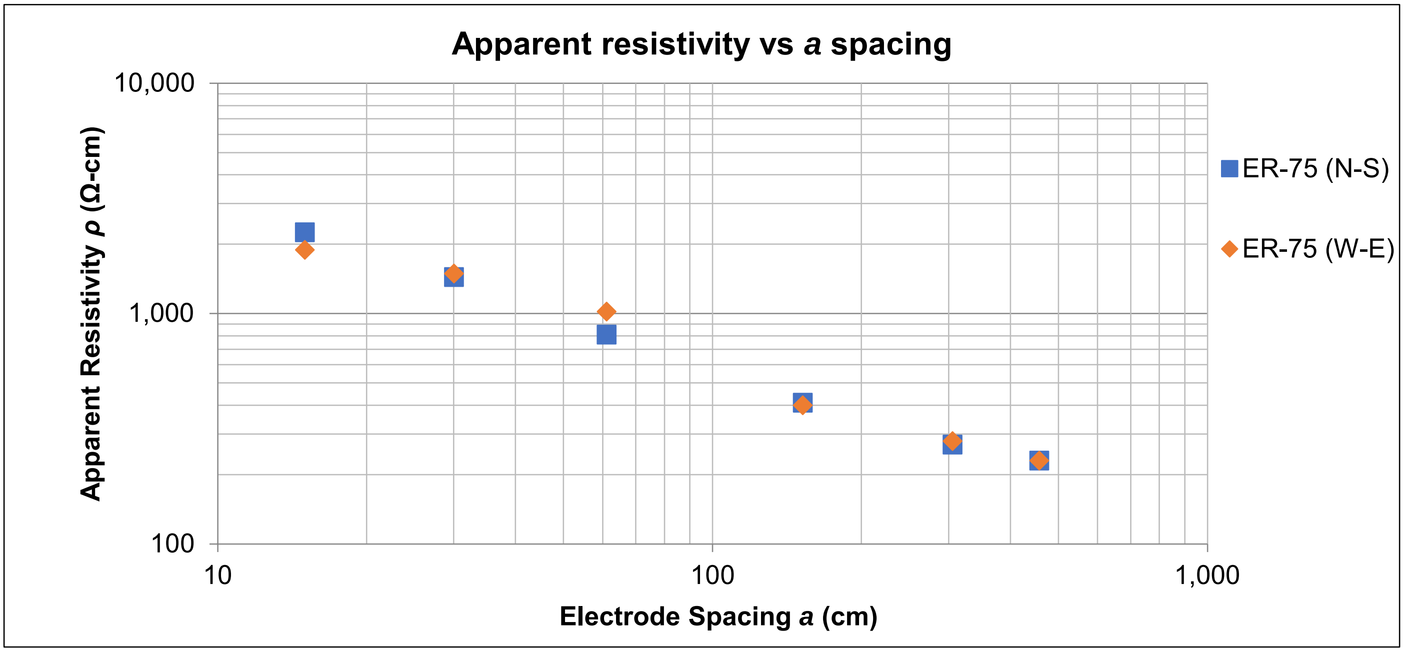
Darden Solar Facility ■ Cantua Creek, Fresno County, California
October 13, 2023 ■ Terracon Project No. 60225172

Array Loc.	**ER-75** (36.459191°N, 120.180378°W)		
Instrument	AGI SuperSting R1	**Weather**	Sunny, High 49°F.
Serial #	SP0303161	**Ground Cond.**	Silty, sandy soil
Cal. Check	4/8/2022	**Tested By**	T. Black
Test Date	February 22, 2023	**Method**	Wenner 4-pin ASTM G57-06 (2012); IEEE 81-2012
Notes & Conflicts	Arrays oriented N-S and W-E with a common midpoint.		

Apparent resistivity ρ is calculated as :

$$\rho = \frac{4\pi a R}{1 + \frac{2a}{\sqrt{a^2 + 4b^2}} - \frac{a}{\sqrt{a^2 + b^2}}}$$

Electrode Spacing *a*		**Electrode Depth *b***		**ER-75 (N-S)**		**ER-75 (W-E)**	
(feet)	(centimeters)	(inches)	(centimeters)	Measured Resistance *R*	Apparent Resistivity *ρ*	Measured Resistance *R*	Apparent Resistivity *ρ*
				Ω	(Ω-cm)	Ω	(Ω-cm)
0.5	15	1	3	22.40	2250	18.80	1890
1	30	1	3	7.514	1440	7.763	1490
2	61	2	5	2.081	810	2.621	1020
5	152	6	15	0.4264	410	0.4138	400
10	305	12	30	0.1365	270	0.1424	280
15	457	12	30	0.0810	230	0.0802	230



FIELD ELECTRICAL RESISTIVITY DATA SHEET

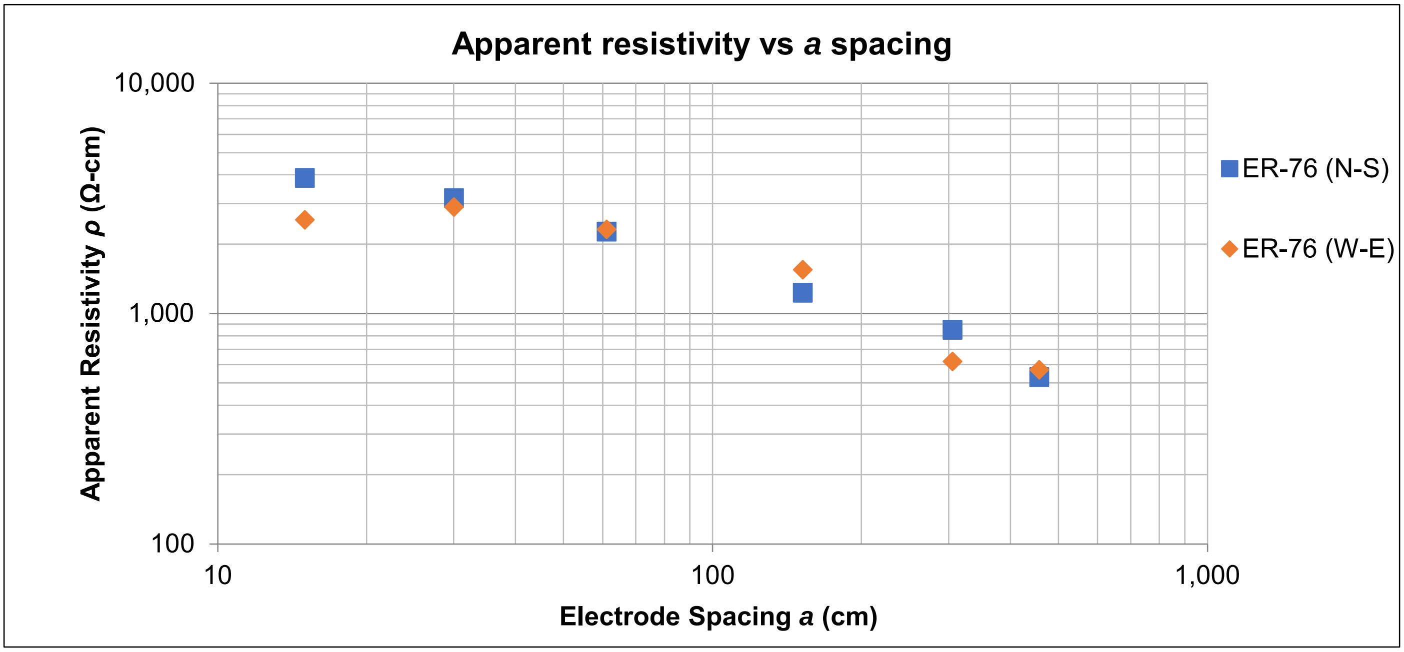
Darden Solar Facility ■ Cantua Creek, Fresno County, California
October 13, 2023 ■ Terracon Project No. 60225172

Array Loc.	**ER-76** (36.472277°N, 120.187083°W)		
Instrument	AGI SuperSting R1	**Weather**	Sunny, High 70°F.
Serial #	SP0303161	**Ground Cond.**	Silty, sandy soil
Cal. Check	4/8/2022	**Tested By**	T. Black
Test Date	February 21, 2023	**Method**	Wenner 4-pin ASTM G57-06 (2012); IEEE 81-2012
Notes & Conflicts	Arrays oriented N-S and W-E with a common midpoint.		

Apparent resistivity ρ is calculated as :

$$\rho = \frac{4\pi a R}{1 + \frac{2a}{\sqrt{a^2 + 4b^2}} - \frac{a}{\sqrt{a^2 + b^2}}}$$

Electrode Spacing *a*		**Electrode Depth *b***		**ER-76 (N-S)**		**ER-76 (W-E)**	
(feet)	(centimeters)	(inches)	(centimeters)	Measured Resistance *R*	Apparent Resistivity *ρ*	Measured Resistance *R*	Apparent Resistivity *ρ*
				Ω	(Ω-cm)	Ω	(Ω-cm)
0.5	15	1	3	38.65	3880	25.36	2550
1	30	1	3	16.53	3170	15.11	2900
2	61	2	5	5.864	2270	5.993	2320
5	152	6	15	1.262	1230	1.596	1550
10	305	12	30	0.4366	850	0.3195	620
15	457	12	30	0.1832	530	0.1972	570



FIELD ELECTRICAL RESISTIVITY DATA SHEET

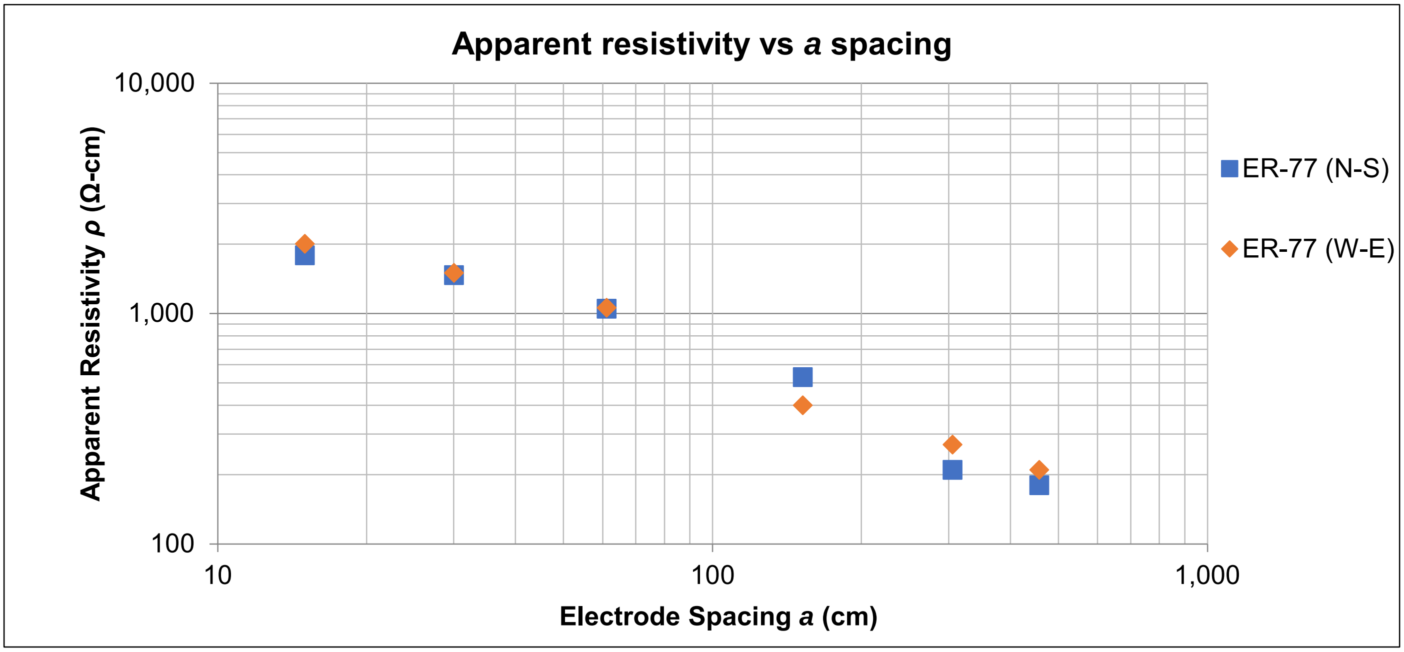
Darden Solar Facility ■ Cantua Creek, Fresno County, California
October 13, 2023 ■ Terracon Project No. 60225172

Array Loc. **ER-77** (36.467465°N, 120.192971°W)
Instrument AGI SuperSting R1 **Weather** Sunny, High 62°F.
Serial # SP0303161 **Ground Cond.** Silty, sandy soil
Cal. Check 4/8/2022 **Tested By** T. Black
Test Date February 17, 2023 **Method** Wenner 4-pin ASTM G57-06 (2012); IEEE 81-2012
Notes & Conflicts Arrays oriented N-S and W-E with a common midpoint.

Apparent resistivity ρ is calculated as :

$$\rho = \frac{4\pi aR}{1 + \frac{2a}{\sqrt{a^2 + 4b^2}} - \frac{a}{\sqrt{a^2 + b^2}}}$$

Electrode Spacing *a*		**Electrode Depth *b***		**ER-77 (N-S)**		**ER-77 (W-E)**	
(feet)	(centimeters)	(inches)	(centimeters)	Measured Resistance *R*	Apparent Resistivity *ρ*	Measured Resistance *R*	Apparent Resistivity *ρ*
				Ω	(Ω-cm)	Ω	(Ω-cm)
0.5	15	1	3	17.78	1790	19.98	2010
1	30	1	3	7.649	1470	7.805	1500
2	61	2	5	2.699	1050	2.743	1060
5	152	6	15	0.5444	530	0.4072	400
10	305	12	30	0.1053	210	0.1382	270
15	457	12	30	0.0627	180	0.0729	210



FIELD ELECTRICAL RESISTIVITY DATA SHEET

Darden Solar Facility ■ Cantua Creek, Fresno County, California
October 13, 2023 ■ Terracon Project No. 60225172

NORCAL GEOPHYSICAL CONSULTANTS INC.
A Terracon COMPANY

Array Loc. **ER-78** (36.445939°N, 120.158669°W)

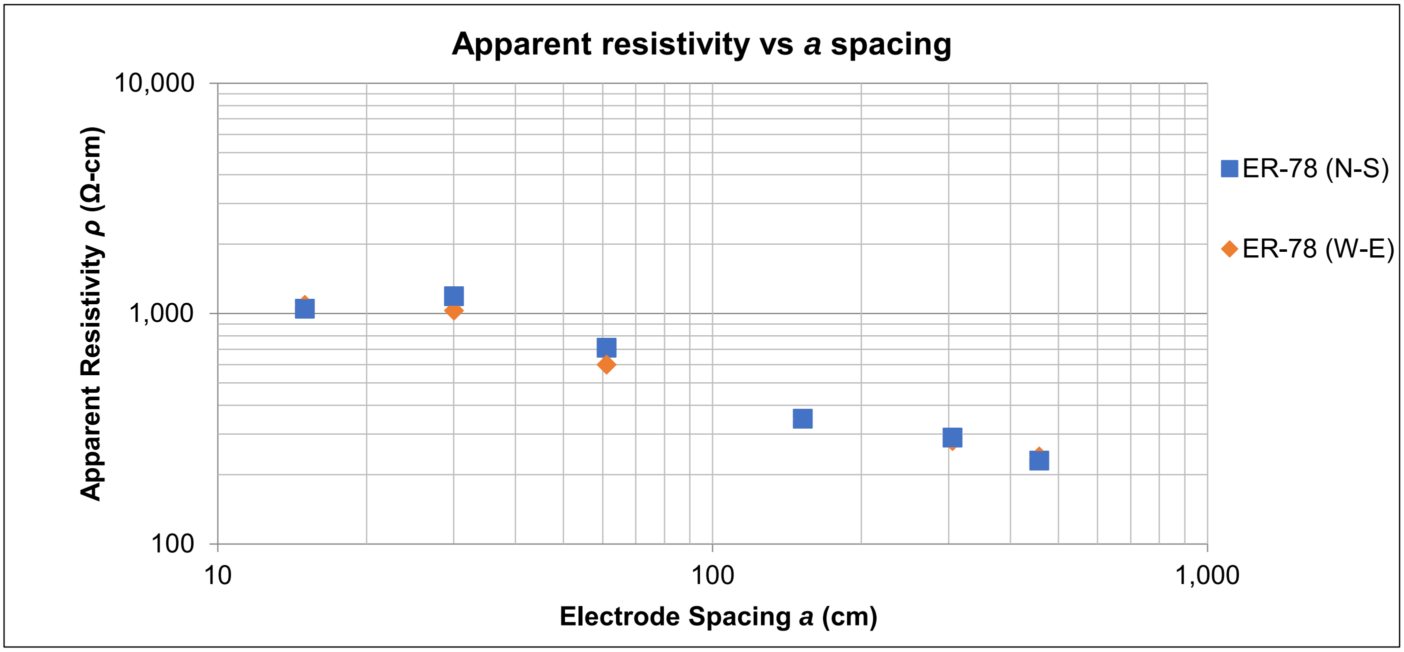
Instrument	AGI SuperSting R1	**Weather**	Partly cloudy, light rain, High 49°F.
Serial #	SP0303161	**Ground Cond.**	Vegetated, silty, sandy soil
Cal. Check	4/8/2022	**Tested By**	T. Black
Test Date	February 22, 2023	**Method**	Wenner 4-pin ASTM G57-06 (2012); IEEE 81-2012

Notes & Conflicts Arrays oriented N-S and W-E with a common midpoint.

Apparent resistivity ρ is calculated as :

$$\rho = \frac{4\pi a R}{1 + \frac{2a}{\sqrt{a^2 + 4b^2}} - \frac{a}{\sqrt{a^2 + b^2}}}$$

Electrode Spacing *a*		**Electrode Depth *b***		**ER-78 (N-S)**		**ER-78 (W-E)**	
(feet)	(centimeters)	(inches)	(centimeters)	Measured Resistance *R*	Apparent Resistivity *ρ*	Measured Resistance *R*	Apparent Resistivity *ρ*
				Ω	(Ω-cm)	Ω	(Ω-cm)
0.5	15	1	3	10.50	1050	10.87	1090
1	30	1	3	6.188	1190	5.348	1030
2	61	2	5	1.819	710	1.560	600
5	152	6	15	0.3651	350	0.3601	350
10	305	12	30	0.1465	290	0.1441	280
15	457	12	30	0.0805	230	0.0830	240



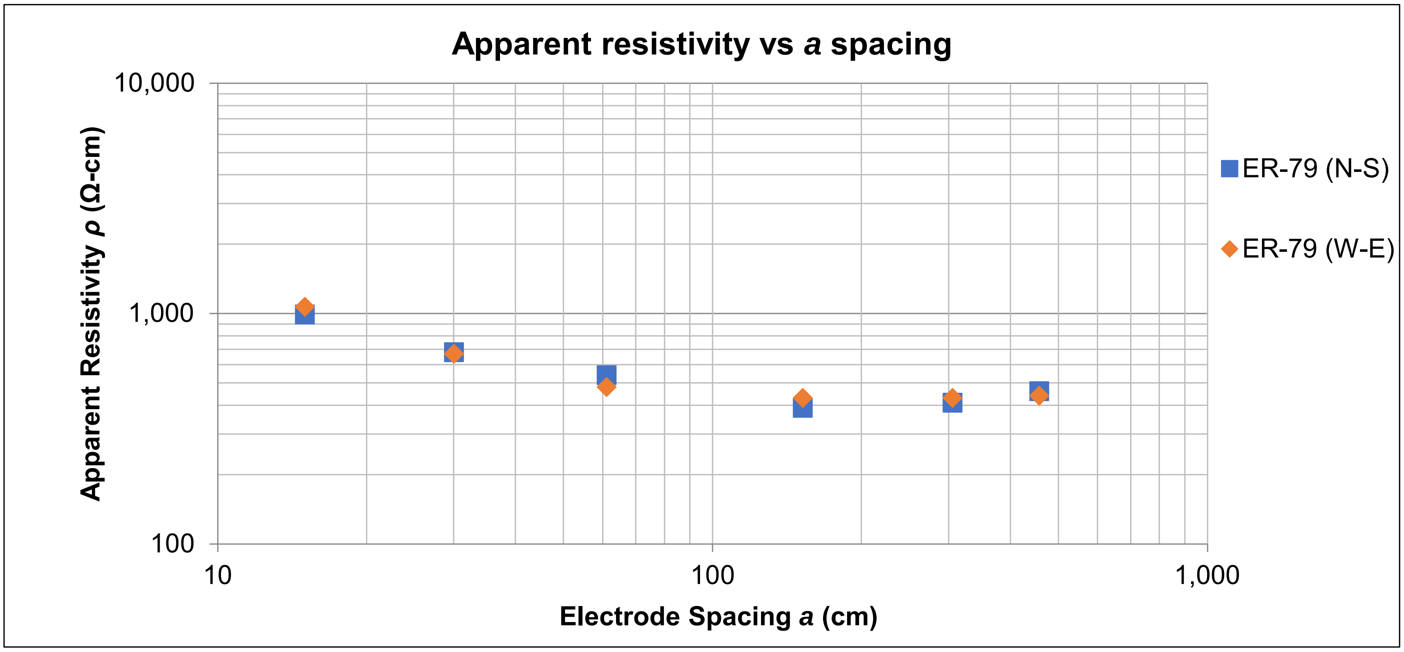
FIELD ELECTRICAL RESISTIVITY DATA SHEET

Darden Solar Facility ■ Cantua Creek, Fresno County, California
October 13, 2023 ■ Terracon Project No. 60225172

Array Loc.	**ER-79** (36.446117°N, 120.167139°W)		
Instrument	AGI SuperSting R1	**Weather**	Partly cloudy, light rain, High 49°F.
Serial #	SP0303161	**Ground Cond.**	Vegetated, silty, sandy soil
Cal. Check	4/8/2022	**Tested By**	T. Black
Test Date	February 22, 2023	**Method**	Wenner 4-pin ASTM G57-06 (2012); IEEE 81-2012
Notes & Conflicts	Arrays oriented N-S and W-E with a common midpoint.		

Apparent resistivity ρ is calculated as : $$\rho = \frac{4\pi a R}{1 + \frac{2a}{\sqrt{a^2 + 4b^2}} - \frac{a}{\sqrt{a^2 + b^2}}}$$

Electrode Spacing *a*		**Electrode Depth *b***		**ER-79 (N-S)**		**ER-79 (W-E)**	
(feet)	(centimeters)	(inches)	(centimeters)	Measured Resistance *R*	Apparent Resistivity *ρ*	Measured Resistance *R*	Apparent Resistivity *ρ*
				Ω	(Ω-cm)	Ω	(Ω-cm)
0.5	15	1	3	9.892	990	10.66	1070
1	30	1	3	3.525	680	3.500	670
2	61	2	5	1.389	540	1.229	480
5	152	6	15	0.3965	390	0.4442	430
10	305	12	30	0.2099	410	0.2202	430
15	457	12	30	0.1596	460	0.1508	440



FIELD ELECTRICAL RESISTIVITY DATA SHEET

Darden Solar Facility ■ Cantua Creek, Fresno County, California
October 13, 2023 ■ Terracon Project No. 60225172

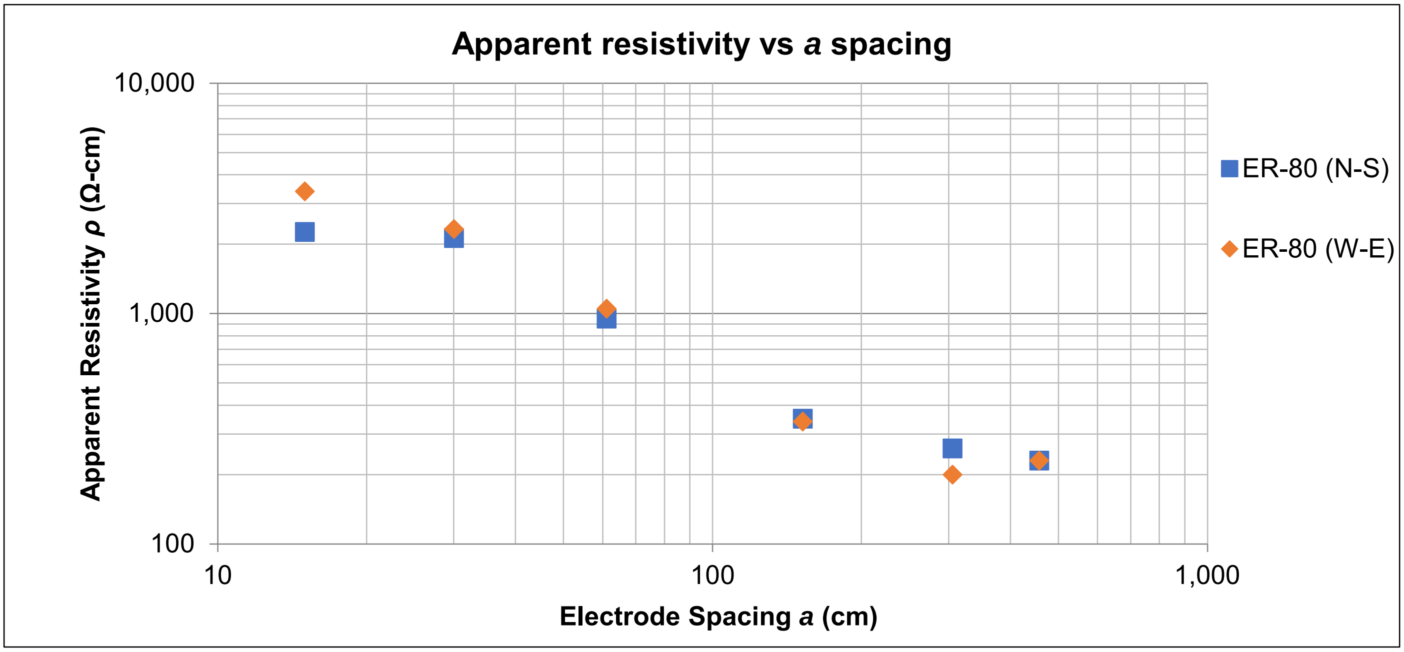
Array Loc. **ER-80** (36.448450°N, 120.175964°W)

Instrument	AGI SuperSting R1	**Weather**	Partly cloudy, light rain, High 49°F.
Serial #	SP0303161	**Ground Cond.**	Vegetated, silty, sandy soil
Cal. Check	4/8/2022	**Tested By**	T. Black
Test Date	February 22, 2023	**Method**	Wenner 4-pin ASTM G57-06 (2012); IEEE 81-2012

Notes & Conflicts Arrays oriented N-S and W-E with a common midpoint.

Apparent resistivity ρ is calculated as : $\rho = \dfrac{4\pi a R}{1 + \dfrac{2a}{\sqrt{a^2 + 4b^2}} - \dfrac{a}{\sqrt{a^2 + b^2}}}$

Electrode Spacing *a*		Electrode Depth *b*		ER-80 (N-S)		ER-80 (W-E)	
(feet)	(centimeters)	(inches)	(centimeters)	Measured Resistance *R*	Apparent Resistivity *ρ*	Measured Resistance *R*	Apparent Resistivity *ρ*
				Ω	(Ω-cm)	Ω	(Ω-cm)
0.5	15	1	3	22.49	2260	33.78	3390
1	30	1	3	11.09	2130	12.15	2330
2	61	2	5	2.451	950	2.717	1050
5	152	6	15	0.3595	350	0.3500	340
10	305	12	30	0.1314	260	0.1038	200
15	457	12	30	0.0798	230	0.0794	230



FIELD ELECTRICAL RESISTIVITY DATA SHEET

Darden Solar Facility ■ Cantua Creek, Fresno County, California
October 13, 2023 ■ Terracon Project No. 60225172

NORCAL GEOPHYSICAL CONSULTANTS INC. A Terracon COMPANY

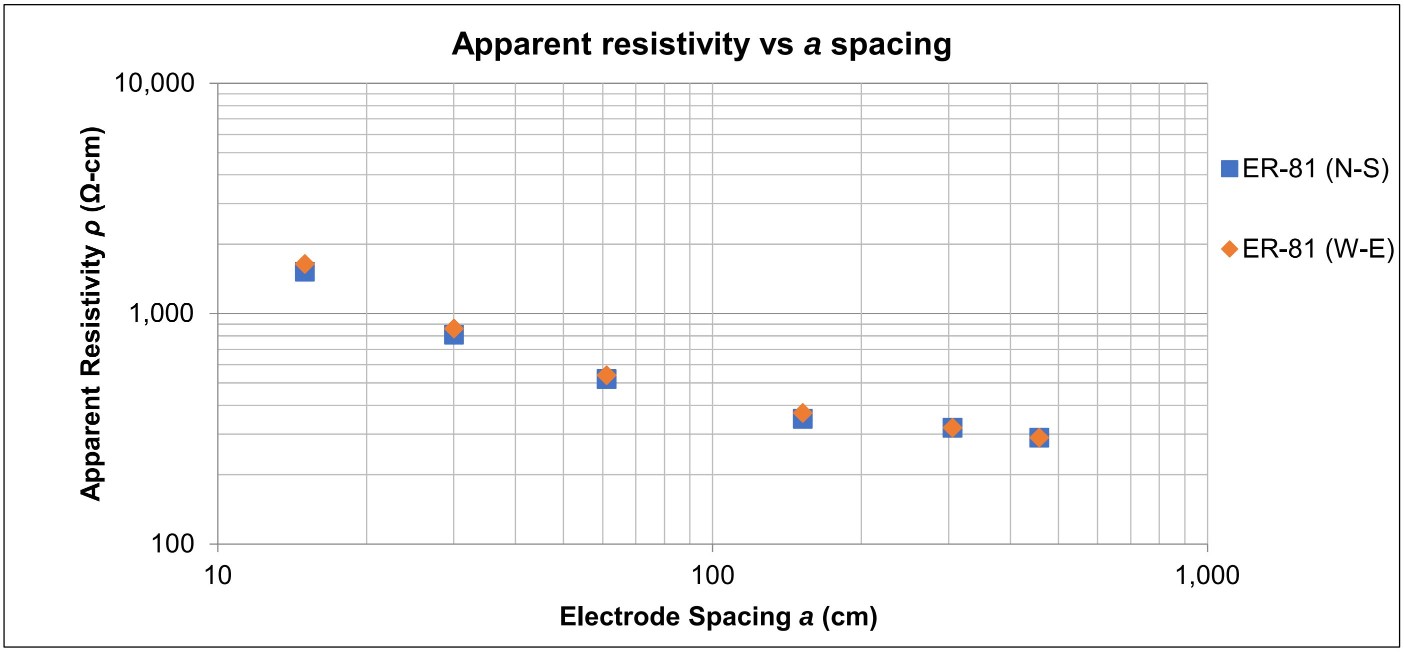
Array Loc. **ER-81** (36.452106°N, 120.162634°W)

Instrument	AGI SuperSting R1	**Weather**	Partly cloudy, light rain, High 49°F.
Serial #	SP0303161	**Ground Cond.**	Vegetated, silty, sandy soil
Cal. Check	4/8/2022	**Tested By**	T. Black
Test Date	February 22, 2023	**Method**	Wenner 4-pin ASTM G57-06 (2012); IEEE 81-2012

Notes & Conflicts Arrays oriented N-S and W-E with a common midpoint.

Apparent resistivity ρ is calculated as : $\rho = \dfrac{4\pi a R}{1 + \dfrac{2a}{\sqrt{a^2 + 4b^2}} - \dfrac{a}{\sqrt{a^2 + b^2}}}$

Electrode Spacing *a*		**Electrode Depth *b***		**ER-81 (N-S)**		**ER-81 (W-E)**	
(feet)	(centimeters)	(inches)	(centimeters)	Measured Resistance *R* Ω	Apparent Resistivity *ρ* (Ω-cm)	Measured Resistance *R* Ω	Apparent Resistivity *ρ* (Ω-cm)
0.5	15	1	3	15.16	1520	16.35	1640
1	30	1	3	4.250	810	4.486	860
2	61	2	5	1.345	520	1.401	540
5	152	6	15	0.3645	350	0.3828	370
10	305	12	30	0.1667	320	0.1663	320
15	457	12	30	0.1005	290	0.1011	290



FIELD ELECTRICAL RESISTIVITY DATA SHEET

Darden Solar Facility ■ Cantua Creek, Fresno County, California
October 13, 2023 ■ Terracon Project No. 60225172

NORCAL GEOPHYSICAL CONSULTANTS INC. A Terracon COMPANY

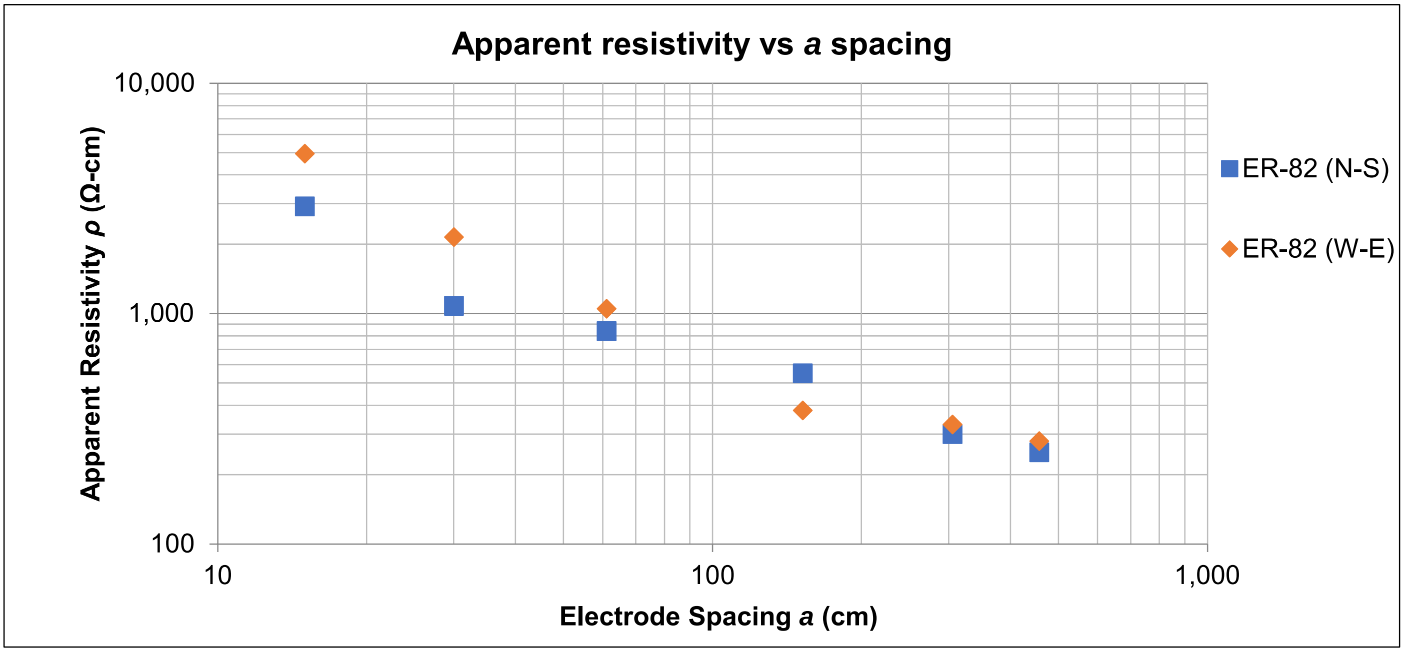
Array Loc. **ER-82** (36.455384°N, 120.178378°W)

Instrument	AGI SuperSting R1	**Weather**	Sunny, High 49°F.
Serial #	SP0303161	**Ground Cond.**	Vegetated, silty, sandy soil
Cal. Check	4/8/2022	**Tested By**	T. Black
Test Date	February 22, 2023	**Method**	Wenner 4-pin ASTM G57-06 (2012); IEEE 81-2012

Notes & Conflicts Arrays oriented N-S and W-E with a common midpoint.

Apparent resistivity ρ is calculated as : $\rho = \dfrac{4\pi a R}{1 + \dfrac{2a}{\sqrt{a^2 + 4b^2}} - \dfrac{a}{\sqrt{a^2 + b^2}}}$

Electrode Spacing *a*		**Electrode Depth *b***		**ER-82 (N-S)**		**ER-82 (W-E)**	
(feet)	(centimeters)	(inches)	(centimeters)	Measured Resistance *R* Ω	Apparent Resistivity *ρ* (Ω-cm)	Measured Resistance *R* Ω	Apparent Resistivity *ρ* (Ω-cm)
0.5	15	1	3	29.10	2920	49.13	4940
1	30	1	3	5.621	1080	11.230	2150
2	61	2	5	2.154	840	2.703	1050
5	152	6	15	0.5616	550	0.3883	380
10	305	12	30	0.1552	300	0.1675	330
15	457	12	30	0.0869	250	0.0955	280



FIELD ELECTRICAL RESISTIVITY DATA SHEET

Darden Solar Facility ■ Cantua Creek, Fresno County, California
October 13, 2023 ■ Terracon Project No. 60225172

Array Loc. **ER-83** (36.452572°N, 120.170337°W)

Instrument AGI SuperSting R1

Weather Sunny, High 49°F.

Serial # SP0303161

Ground Cond. Vegetated, silty, sandy soil

Cal. Check 4/8/2022

Tested By T. Black

Test Date February 22, 2023

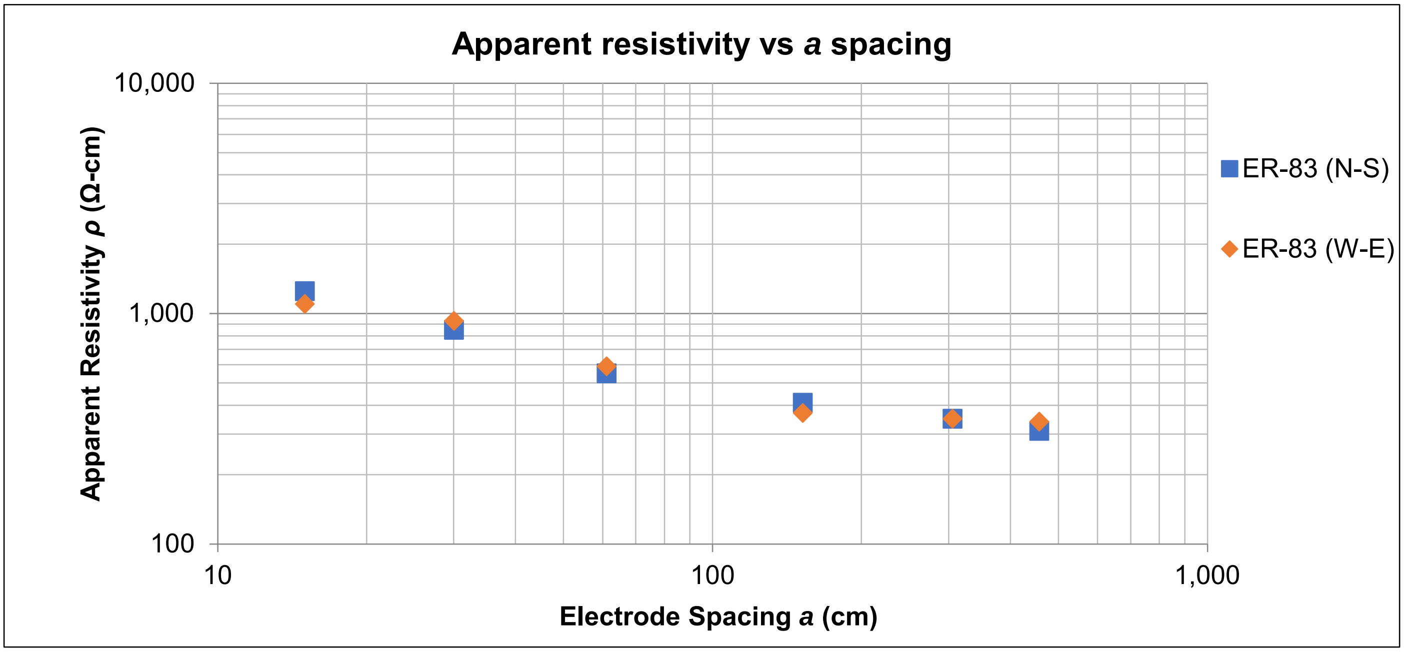
Method Wenner 4-pin ASTM G57-06 (2012); IEEE 81-2012

Notes & Conflicts Arrays oriented N-S and W-E with a common midpoint.

Apparent resistivity ρ is calculated as :

$$\rho = \frac{4\pi a R}{1 + \frac{2a}{\sqrt{a^2 + 4b^2}} - \frac{a}{\sqrt{a^2 + b^2}}}$$

Electrode Spacing *a*		**Electrode Depth *b***		**ER-83 (N-S)**		**ER-83 (W-E)**	
(feet)	(centimeters)	(inches)	(centimeters)	Measured Resistance *R*	Apparent Resistivity *ρ*	Measured Resistance *R*	Apparent Resistivity *ρ*
				Ω	(Ω-cm)	Ω	(Ω-cm)
0.5	15	1	3	12.46	1250	10.92	1100
1	30	1	3	4.441	850	4.836	930
2	61	2	5	1.417	550	1.525	590
5	152	6	15	0.4171	410	0.3785	370
10	305	12	30	0.1814	350	0.1806	350
15	457	12	30	0.1085	310	0.1158	340



FIELD ELECTRICAL RESISTIVITY DATA SHEET

Darden Solar Facility ■ Cantua Creek, Fresno County, California
October 13, 2023 ■ Terracon Project No. 60225172

NORCAL GEOPHYSICAL CONSULTANTS INC.
A Terracon COMPANY

Array Loc. **ER-84** (36.457902°N, 120.157854°W)

Instrument AGI SuperSting R1

Weather Partly cloudy, High 48°F.

Serial # SP0303161

Ground Cond. Vegetated, silty, sandy soil

Cal. Check 4/8/2022

Tested By T. Black

Test Date February 23, 2023

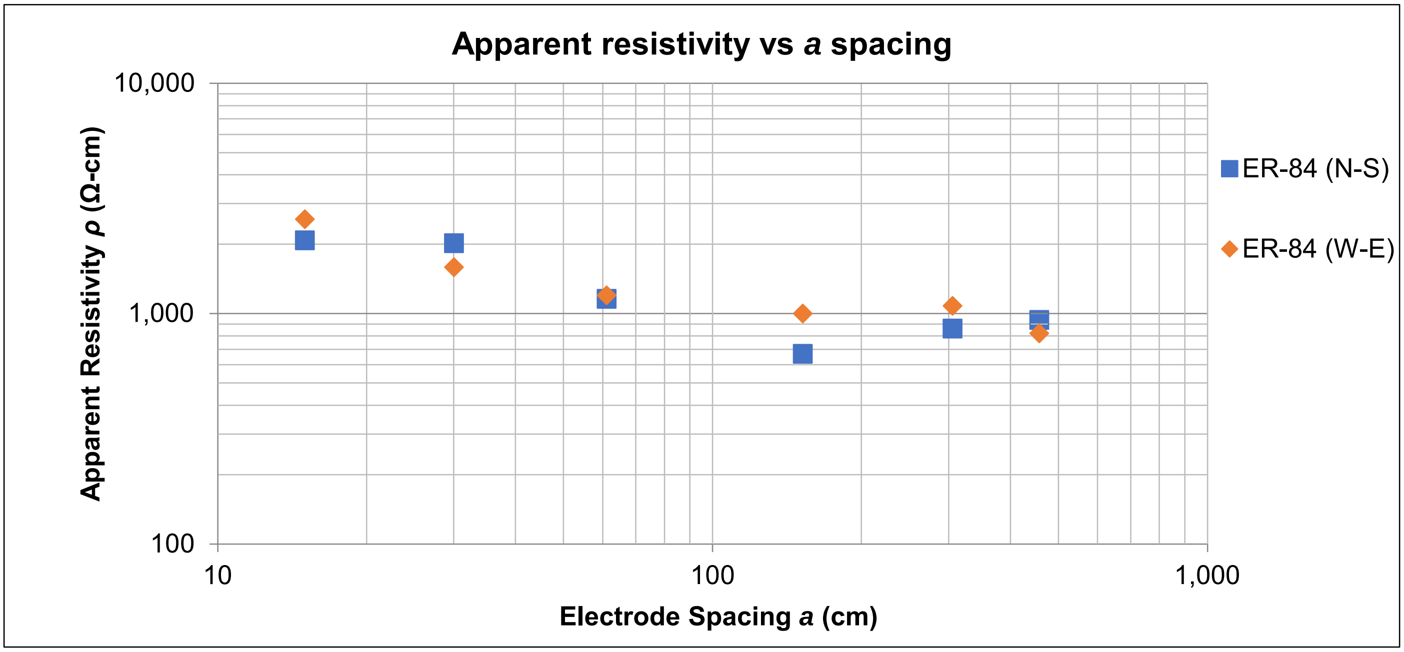
Method Wenner 4-pin ASTM G57-06 (2012); IEEE 81-2012

Notes & Conflicts Arrays oriented N-S and W-E with a common midpoint.

Apparent resistivity ρ is calculated as :

$$\rho = \frac{4\pi a R}{1 + \frac{2a}{\sqrt{a^2 + 4b^2}} - \frac{a}{\sqrt{a^2 + b^2}}}$$

Electrode Spacing *a*		**Electrode Depth *b***		**ER-84 (N-S)**		**ER-84 (W-E)**	
(feet)	(centimeters)	(inches)	(centimeters)	Measured Resistance *R*	Apparent Resistivity *ρ*	Measured Resistance *R*	Apparent Resistivity *ρ*
				Ω	(Ω-cm)	Ω	(Ω-cm)
0.5	15	1	3	20.69	2080	25.60	2570
1	30	1	3	10.560	2020	8.284	1590
2	61	2	5	2.987	1160	3.100	1200
5	152	6	15	0.6863	670	1.0330	1000
10	305	12	30	0.4389	860	0.5538	1080
15	457	12	30	0.3254	940	0.2843	820



FIELD ELECTRICAL RESISTIVITY DATA SHEET

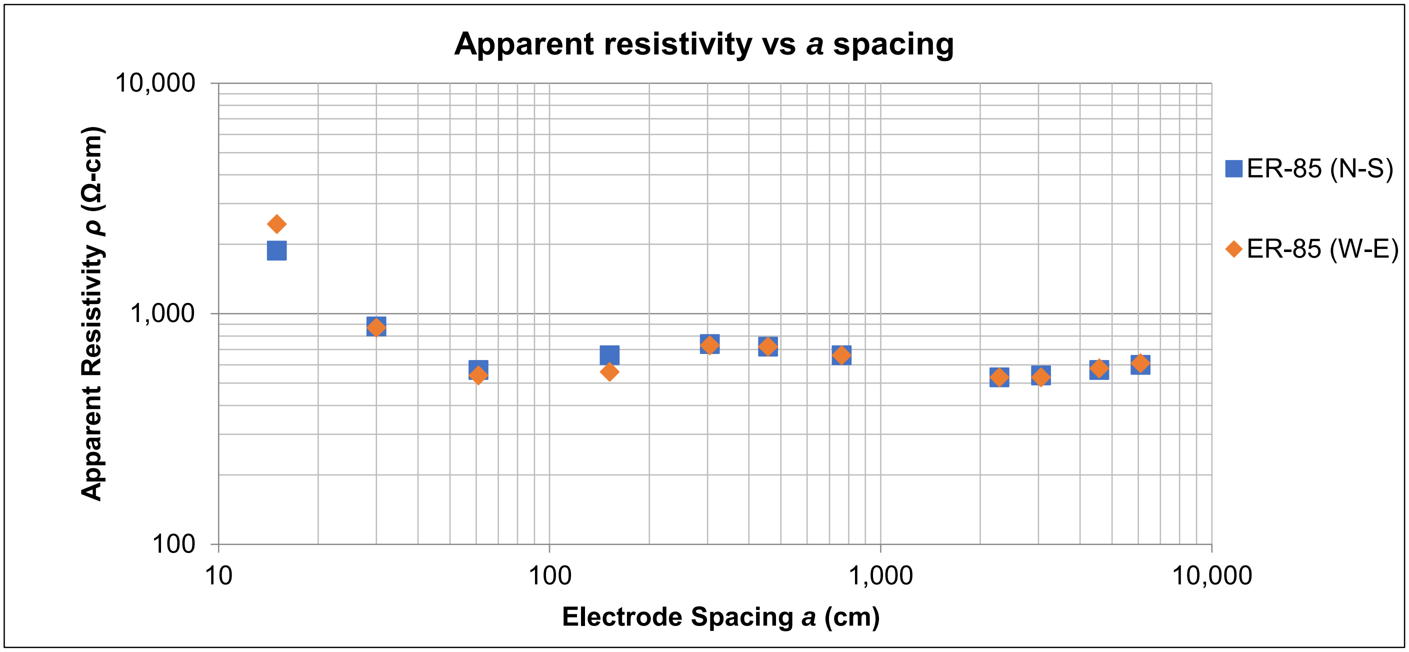
Darden Solar Facility ■ Cantua Creek, Fresno County, California
October 13, 2023 ■ Terracon Project No. 60225172

NORCAL GEOPHYSICAL CONSULTANTS INC.
A Terracon COMPANY

Array Loc.	**ER-85** (36.448840°N, 120.246522°W), BESS Area		
Instrument	AGI SuperSting R1	**Weather**	Clear, high of 60°F.
Serial #	SP0303161	**Ground Cond.**	Fallow field.
Cal. Check	4/8/2022	**Tested By**	H. Philson
Test Date	February 16, 2023	**Method**	Wenner 4-pin ASTM G57-06 (2012); IEEE 81-2012
Notes & Conflicts	Arrays oriented N-S and W-E with a common midpoint.		

Apparent resistivity ρ is calculated as : $\rho = \dfrac{4\pi a R}{1 + \dfrac{2a}{\sqrt{a^2 + 4b^2}} - \dfrac{a}{\sqrt{a^2 + b^2}}}$

Electrode Spacing *a*		Electrode Depth *b*		ER-85 (N-S)		ER-85 (W-E)	
(feet)	(centimeters)	(inches)	(centimeters)	Measured Resistance *R*	Apparent Resistivity *ρ*	Measured Resistance *R*	Apparent Resistivity *ρ*
				Ω	(Ω-cm)	Ω	(Ω-cm)
0.5	15	1	3	18.69	1880	24.43	2450
1	30	1	3	4.598	880	4.532	870
2	61	2	5	1.461	570	1.390	540
5	152	6	15	0.6816	660	0.5779	560
10	305	12	30	0.3802	740	0.3724	730
15	457	12	30	0.2475	720	0.2493	720
25	762	12	30	0.1377	660	0.1378	660
75	2286	12	30	0.03709	530	0.03676	530
100	3048	12	30	0.02835	540	0.02774	530
150	4572	12	30	0.01976	570	0.02006	580
200	6096	12	30	0.01579	600	0.01597	610



FIELD ELECTRICAL RESISTIVITY DATA SHEET

Darden Solar Facility ■ Cantua Creek, Fresno County, California
October 13, 2023 ■ Terracon Project No. 60225172

NORCAL GEOPHYSICAL CONSULTANTS INC. A Terracon COMPANY

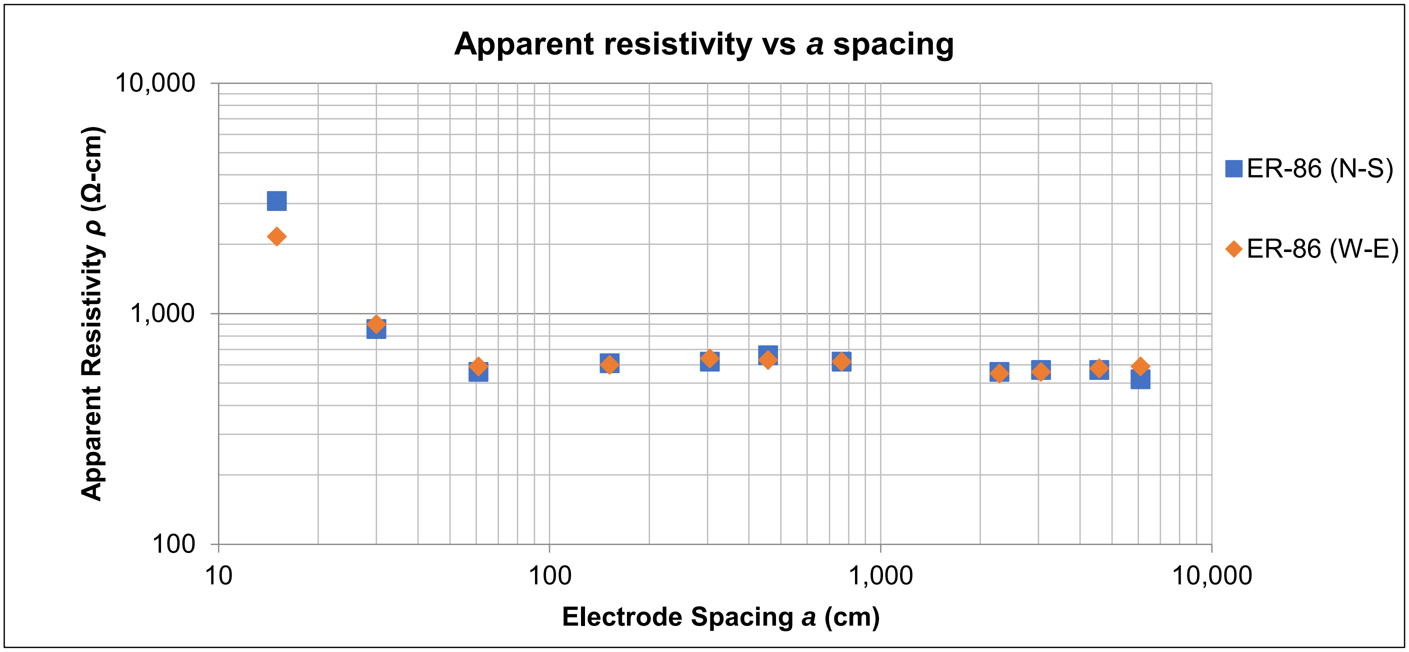
Array Loc. **ER-86** (36.444543°N, 120.245979°W), Substation Area

Instrument	AGI SuperSting R1	**Weather**	Clear, high of 60°F.
Serial #	SP0303161	**Ground Cond.**	Fallow field.
Cal. Check	4/8/2022	**Tested By**	H. Philson
Test Date	February 16, 2023	**Method**	Wenner 4-pin ASTM G57-06 (2012); IEEE 81-2012

Notes & Conflicts Arrays oriented N-S and W-E with a common midpoint.

Apparent resistivity ρ is calculated as :
$$\rho = \frac{4\pi a R}{1 + \frac{2a}{\sqrt{a^2 + 4b^2}} - \frac{a}{\sqrt{a^2 + b^2}}}$$

Electrode Spacing *a*		**Electrode Depth *b***		**ER-86 (N-S)**		**ER-86 (W-E)**	
(feet)	(centimeters)	(inches)	(centimeters)	Measured Resistance *R* Ω	Apparent Resistivity ρ (Ω-cm)	Measured Resistance *R* Ω	Apparent Resistivity ρ (Ω-cm)
0.5	15	1	3	30.69	3080	21.52	2160
1	30	1	3	4.462	860	4.678	900
2	61	2	5	1.443	560	1.512	590
5	152	6	15	0.6253	610	0.6199	600
10	305	12	30	0.3171	620	0.3285	640
15	457	12	30	0.2266	660	0.2173	630
25	762	12	30	0.1299	620	0.1295	620
75	2286	12	30	0.03903	560	0.03857	550
100	3048	12	30	0.02991	570	0.02903	560
150	4572	12	30	0.01986	570	0.02034	580
200	6096	12	30	0.01359	520	0.01542	590



FIELD ELECTRICAL RESISTIVITY DATA SHEET

Darden Solar Facility ■ Cantua Creek, Fresno County, California
October 13, 2023 ■ Terracon Project No. 60225172

NORCAL GEOPHYSICAL CONSULTANTS INC. A Terracon COMPANY

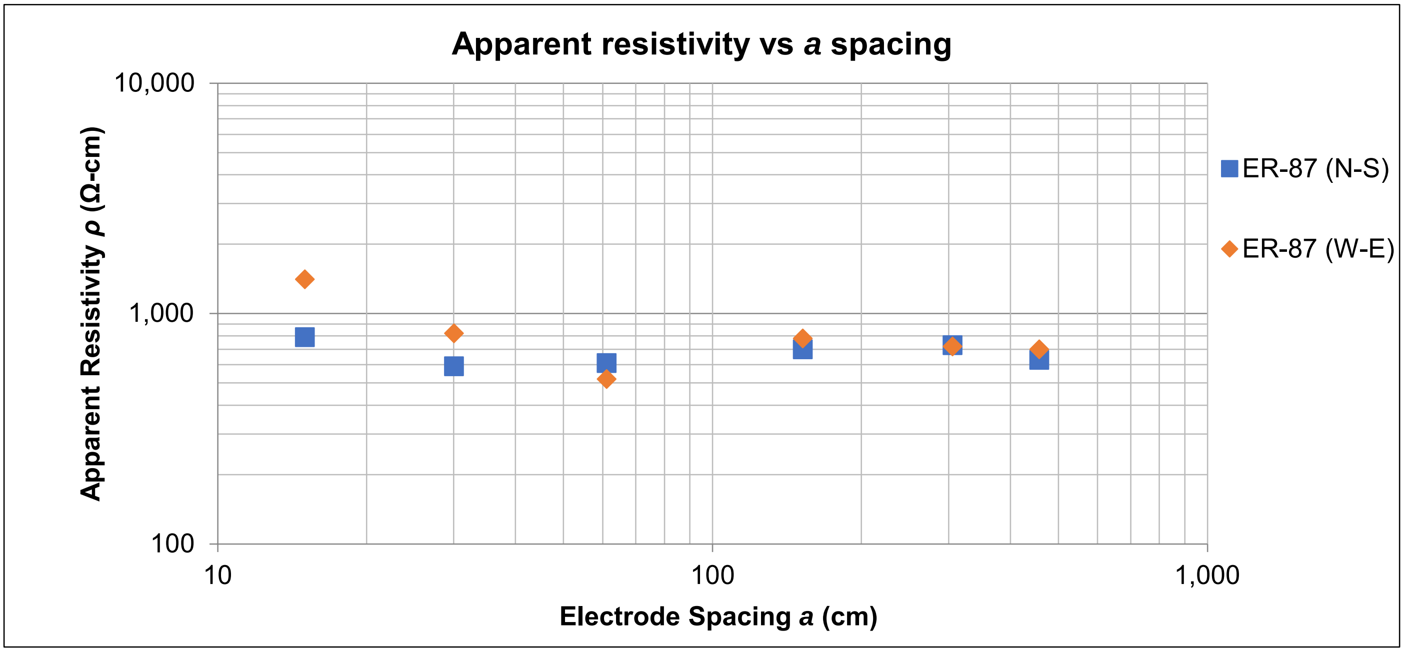
Array Loc. **ER-87** (36.451378°N, 120.243444°W)

Instrument	L&R Instruments - Ultra Mini Res	**Weather**	Clear, high of 51°F.
Serial #	SN-214U	**Ground Cond.**	Fallow field.
Cal. Check	2/14/2023	**Tested By**	H. Philson
Test Date	February 22, 2023	**Method**	Wenner 4-pin ASTM G57-06 (2012); IEEE 81-2012

Notes & Conflicts Arrays oriented N-S and W-E with a common midpoint.

Apparent resistivity ρ is calculated as : $\rho = \dfrac{4\pi a R}{1 + \dfrac{2a}{\sqrt{a^2 + 4b^2}} - \dfrac{a}{\sqrt{a^2 + b^2}}}$

Electrode Spacing *a*		**Electrode Depth *b***		**ER-87 (N-S)**		**ER-87 (W-E)**	
(feet)	(centimeters)	(inches)	(centimeters)	Measured Resistance *R*	Apparent Resistivity *ρ*	Measured Resistance *R*	Apparent Resistivity *ρ*
				Ω	(Ω-cm)	Ω	(Ω-cm)
0.5	15	1	3	7.86	790	14.07	1410
1	30	1	3	3.086	590	4.291	820
2	61	2	5	1.567	610	1.347	520
5	152	6	15	0.7208	700	0.7988	780
10	305	12	30	0.3742	730	0.3685	720
15	457	12	30	0.2161	630	0.2415	700



FIELD ELECTRICAL RESISTIVITY DATA SHEET

Darden Solar Facility ■ Cantua Creek, Fresno County, California
October 13, 2023 ■ Terracon Project No. 60225172

Array Loc. **ER-88** (36.442617°N, 120.239192°W)

Instrument L&R Instruments - Ultra Mini Res

Weather Clear, high of 51°F.

Serial # SN-214U

Ground Cond. Fallow field.

Cal. Check 2/14/2023

Tested By H. Philson

Test Date February 22, 2023

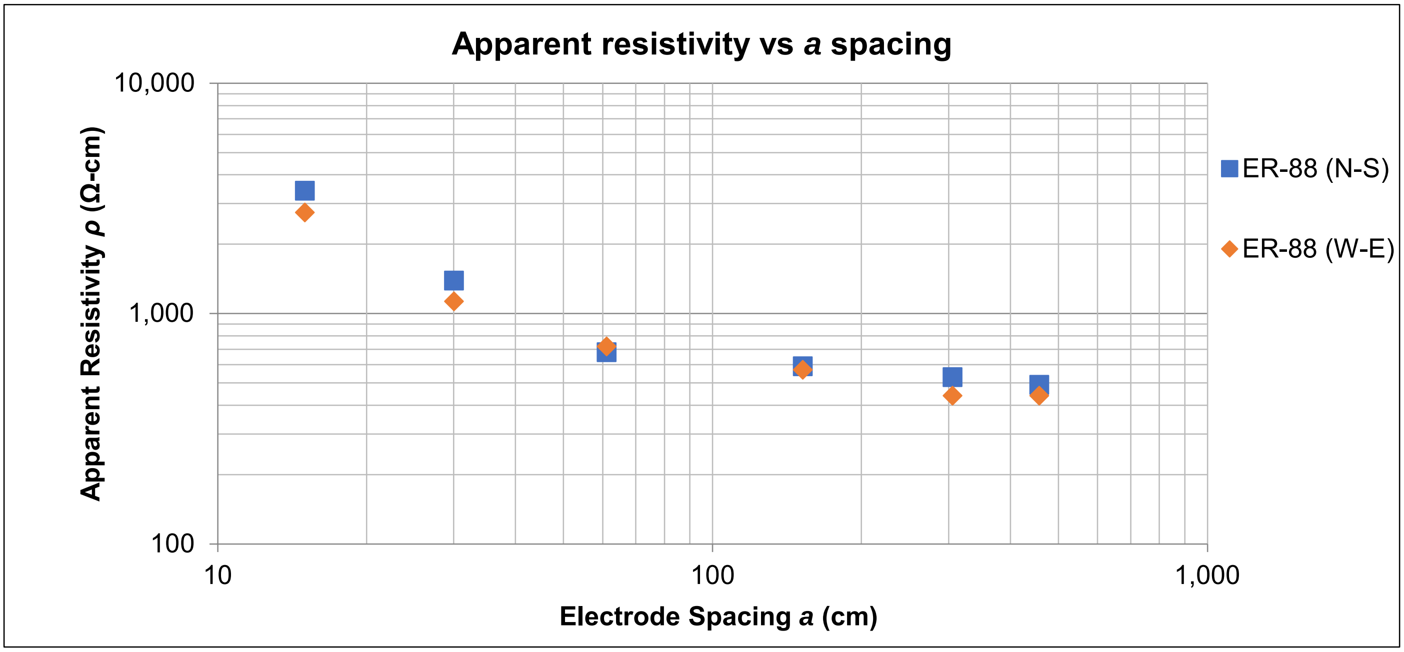
Method Wenner 4-pin ASTM G57-06 (2012); IEEE 81-2012

Notes & Conflicts Arrays oriented N-S and W-E with a common midpoint.

Apparent resistivity ρ is calculated as :

$$\rho = \frac{4\pi a R}{1 + \dfrac{2a}{\sqrt{a^2 + 4b^2}} - \dfrac{a}{\sqrt{a^2 + b^2}}}$$

Electrode Spacing *a*		**Electrode Depth *b***		**ER-88 (N-S)**		**ER-88 (W-E)**	
(feet)	(centimeters)	(inches)	(centimeters)	Measured Resistance *R*	Apparent Resistivity *ρ*	Measured Resistance *R*	Apparent Resistivity *ρ*
				Ω	(Ω-cm)	Ω	(Ω-cm)
0.5	15	1	3	33.90	3410	27.40	2750
1	30	1	3	7.272	1390	5.911	1130
2	61	2	5	1.764	680	1.865	720
5	152	6	15	0.6075	590	0.5902	570
10	305	12	30	0.2727	530	0.2261	440
15	457	12	30	0.1691	490	0.1518	440



FIELD ELECTRICAL RESISTIVITY DATA SHEET

Darden Solar Facility ■ Cantua Creek, Fresno County, California
October 13, 2023 ■ Terracon Project No. 60225172

Array Loc. **ER-89** (36.438839°N, 120.243618°W)

Instrument L&R Instruments - Ultra Mini Res

Serial # SN-214U

Cal. Check 2/14/2023

Test Date February 22, 2023

Weather Clear, high of 51°F.

Ground Cond. Fallow field.

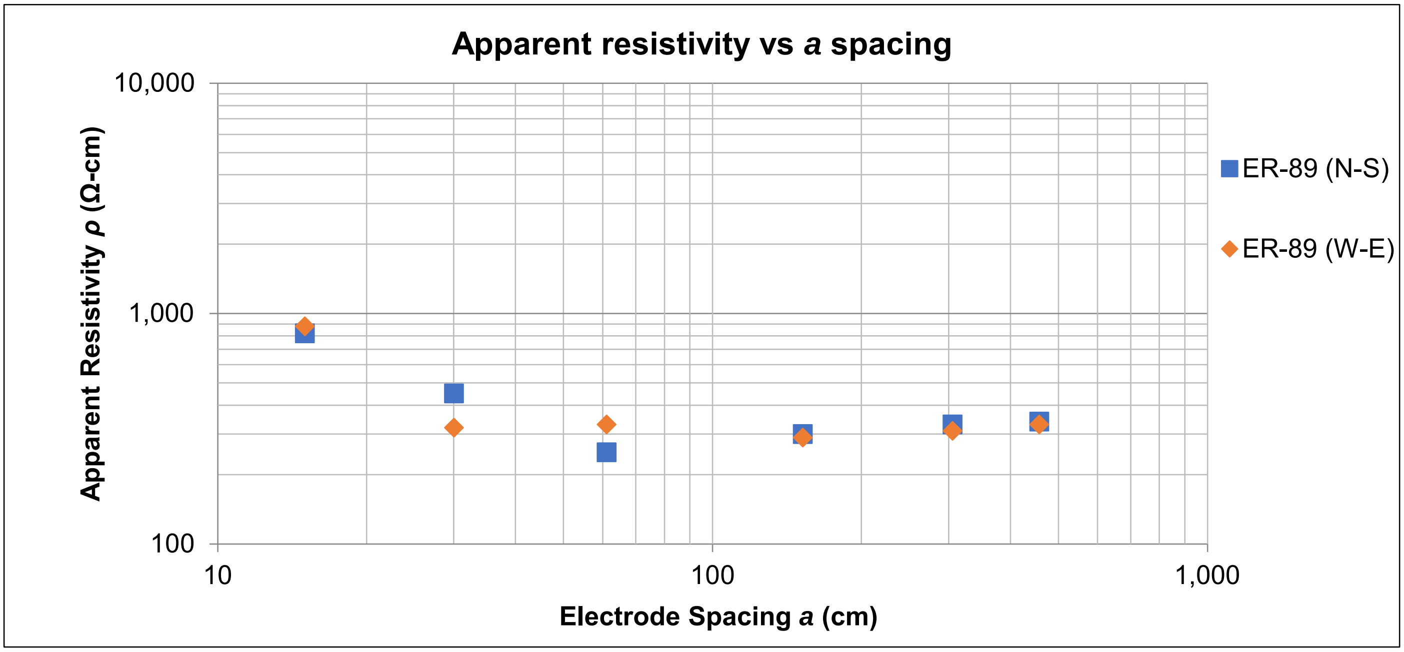
Tested By H. Philson

Method Wenner 4-pin ASTM G57-06 (2012); IEEE 81-2012

Notes & Conflicts Arrays oriented N-S and W-E with a common midpoint.

Apparent resistivity ρ is calculated as : $\rho = \dfrac{4\pi a R}{1 + \dfrac{2a}{\sqrt{a^2 + 4b^2}} - \dfrac{a}{\sqrt{a^2 + b^2}}}$

Electrode Spacing *a*		**Electrode Depth *b***		**ER-89 (N-S)**		**ER-89 (W-E)**	
(feet)	(centimeters)	(inches)	(centimeters)	Measured Resistance *R*	Apparent Resistivity *ρ*	Measured Resistance *R*	Apparent Resistivity *ρ*
				Ω	(Ω-cm)	Ω	(Ω-cm)
0.5	15	1	3	8.19	820	8.71	880
1	30	1	3	2.327	450	1.675	320
2	61	2	5	0.6408	250	0.8548	330
5	152	6	15	0.3042	300	0.2995	290
10	305	12	30	0.1699	330	0.1575	310
15	457	12	30	0.1172	340	0.1137	330



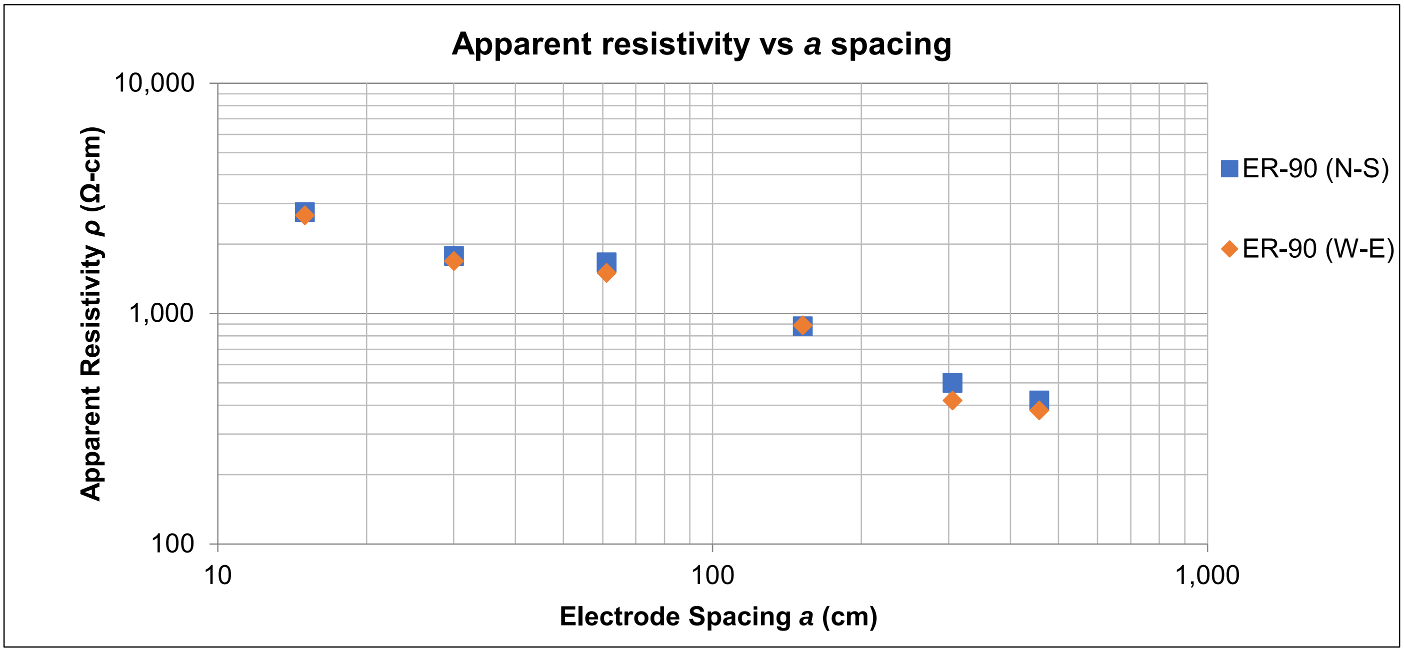
FIELD ELECTRICAL RESISTIVITY DATA SHEET

Darden Solar Facility ■ Cantua Creek, Fresno County, California
October 13, 2023 ■ Terracon Project No. 60225172

Array Loc.	**ER-90** (36.439630°N, 120.234036°W)		
Instrument	L&R Instruments - Ultra Mini Res	**Weather**	Clear, high of 51°F.
Serial #	SN-214U	**Ground Cond.**	Fallow field.
Cal. Check	2/14/2023	**Tested By**	H. Philson
Test Date	February 22, 2023	**Method**	Wenner 4-pin ASTM G57-06 (2012); IEEE 81-2012
Notes & Conflicts	Arrays oriented N-S and W-E with a common midpoint.		

Apparent resistivity ρ is calculated as : $$\rho = \frac{4\pi a R}{1 + \frac{2a}{\sqrt{a^2 + 4b^2}} - \frac{a}{\sqrt{a^2 + b^2}}}$$

Electrode Spacing *a*		**Electrode Depth *b***		**ER-90 (N-S)**		**ER-90 (W-E)**	
(feet)	(centimeters)	(inches)	(centimeters)	Measured Resistance *R*	Apparent Resistivity *ρ*	Measured Resistance *R*	Apparent Resistivity *ρ*
				Ω	(Ω-cm)	Ω	(Ω-cm)
0.5	15	1	3	27.50	2760	26.60	2670
1	30	1	3	9.268	1780	8.794	1690
2	61	2	5	4.319	1670	3.868	1500
5	152	6	15	0.9105	880	0.9195	890
10	305	12	30	0.2558	500	0.2133	420
15	457	12	30	0.1456	420	0.1305	380



Apparent resistivity vs *a* spacing

FIELD ELECTRICAL RESISTIVITY DATA SHEET

Darden Solar Facility ■ Cantua Creek, Fresno County, California
October 13, 2023 ■ Terracon Project No. 60225172

NORCAL GEOPHYSICAL CONSULTANTS INC.
A Terracon COMPANY

Array Loc. **ER-91** (36.435413°N, 120.236050°W)

Instrument L&R Instruments - Ultra Mini Res

Weather Clear, high of 51°F.

Serial # SN-214U

Ground Cond. Fallow field.

Cal. Check 2/14/2023

Tested By H. Philson

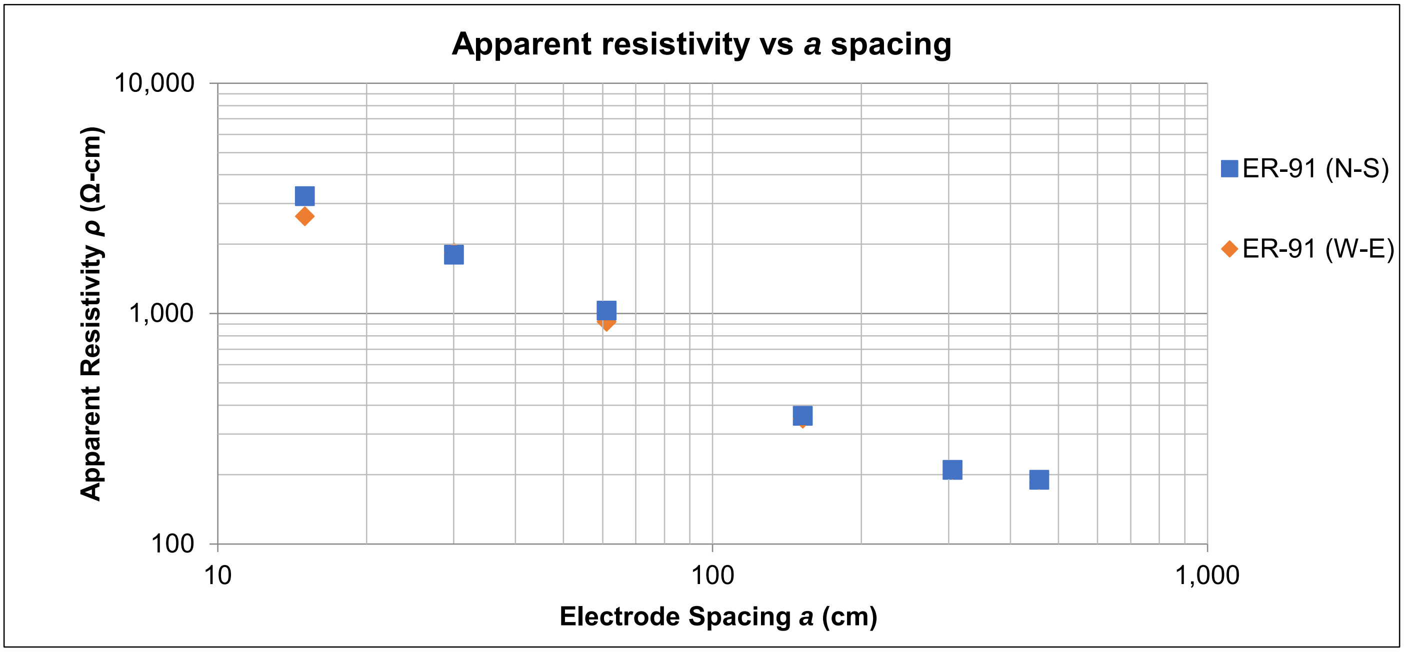
Test Date February 22, 2023

Method Wenner 4-pin ASTM G57-06 (2012); IEEE 81-2012

Notes & Conflicts Arrays oriented N-S and W-E with a common midpoint.

Apparent resistivity ρ is calculated as : $\rho = \dfrac{4\pi a R}{1 + \dfrac{2a}{\sqrt{a^2 + 4b^2}} - \dfrac{a}{\sqrt{a^2 + b^2}}}$

Electrode Spacing *a*		Electrode Depth *b*		ER-91 (N-S)		ER-91 (W-E)	
(feet)	(centimeters)	(inches)	(centimeters)	Measured Resistance *R*	Apparent Resistivity *ρ*	Measured Resistance *R*	Apparent Resistivity *ρ*
				Ω	(Ω-cm)	Ω	(Ω-cm)
0.5	15	1	3	32.20	3230	26.30	2640
1	30	1	3	9.392	1800	9.603	1840
2	61	2	5	2.652	1030	2.366	920
5	152	6	15	0.3687	360	0.3564	350
10	305	12	30	0.1059	210	0.1074	210
15	457	12	30	0.0645	190	0.0653	190



FIELD ELECTRICAL RESISTIVITY DATA SHEET

Darden Solar Facility ■ Cantua Creek, Fresno County, California
October 13, 2023 ■ Terracon Project No. 60225172

NORCAL GEOPHYSICAL CONSULTANTS INC.
A Terracon COMPANY

Array Loc. **ER-92** (36.431848°N, 120.233114°W)

Instrument L&R Instruments - Ultra Mini Res

Weather Clear, high of 51°F.

Serial # SN-214U

Ground Cond. Fallow field.

Cal. Check 2/14/2023

Tested By H. Philson

Test Date February 22, 2023

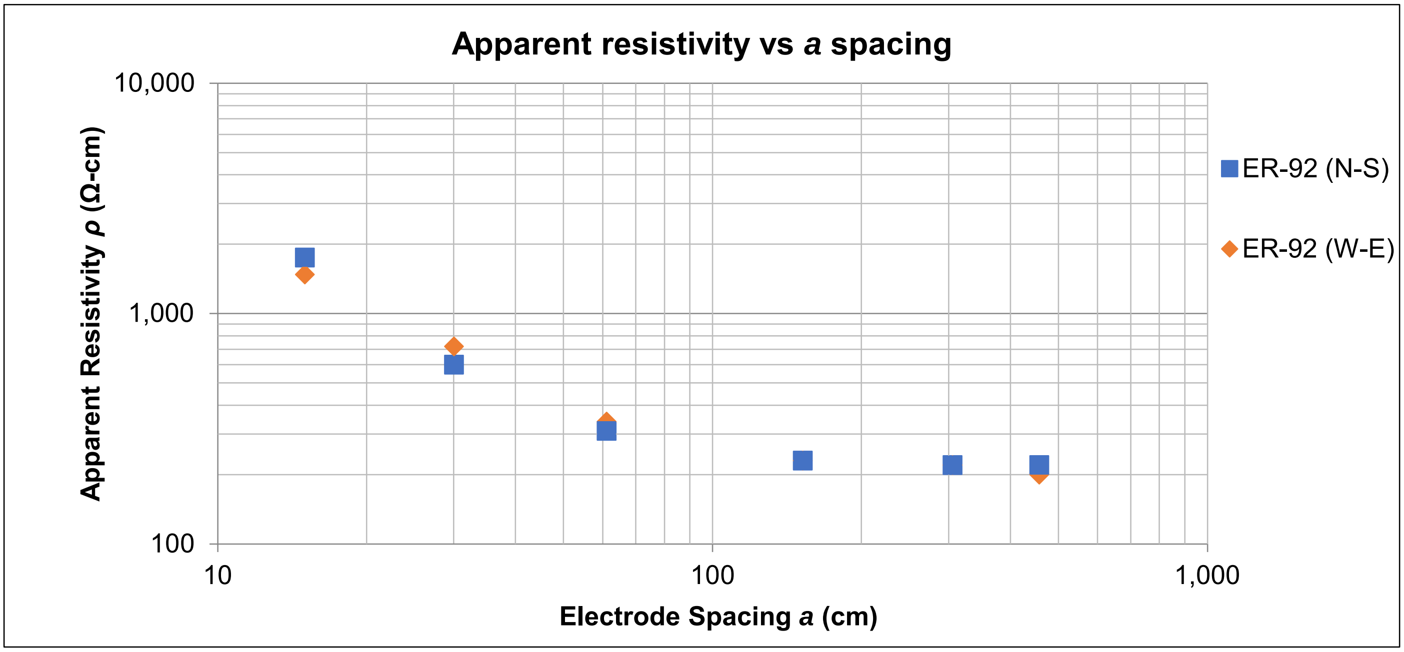
Method Wenner 4-pin ASTM G57-06 (2012); IEEE 81-2012

Notes & Conflicts Arrays oriented N-S and W-E with a common midpoint.

Apparent resistivity ρ is calculated as :

$$\rho = \frac{4\pi a R}{1 + \dfrac{2a}{\sqrt{a^2 + 4b^2}} - \dfrac{a}{\sqrt{a^2 + b^2}}}$$

Electrode Spacing *a*		**Electrode Depth *b***		**ER-92 (N-S)**		**ER-92 (W-E)**	
(feet)	(centimeters)	(inches)	(centimeters)	Measured Resistance *R* Ω	Apparent Resistivity *ρ* (Ω-cm)	Measured Resistance *R* Ω	Apparent Resistivity *ρ* (Ω-cm)
0.5	15	1	3	17.47	1750	14.71	1480
1	30	1	3	3.147	600	3.757	720
2	61	2	5	0.796	310	0.875	340
5	152	6	15	0.2419	230	0.2345	230
10	305	12	30	0.1125	220	0.1124	220
15	457	12	30	0.0749	220	0.0691	200



FIELD ELECTRICAL RESISTIVITY DATA SHEET

Darden Solar Facility ■ Cantua Creek, Fresno County, California
October 13, 2023 ■ Terracon Project No. 60225172

NORCAL GEOPHYSICAL CONSULTANTS INC.
A Terracon COMPANY

Array Loc. **ER-93** (36.448045°N, 120.239967°W)

Instrument L&R Instruments - Ultra Mini Res

Weather Clear, high of 100°F.

Serial # SN-214U

Ground Cond. Fallow field.

Cal. Check 2/14/2023

Tested By M. Yoni

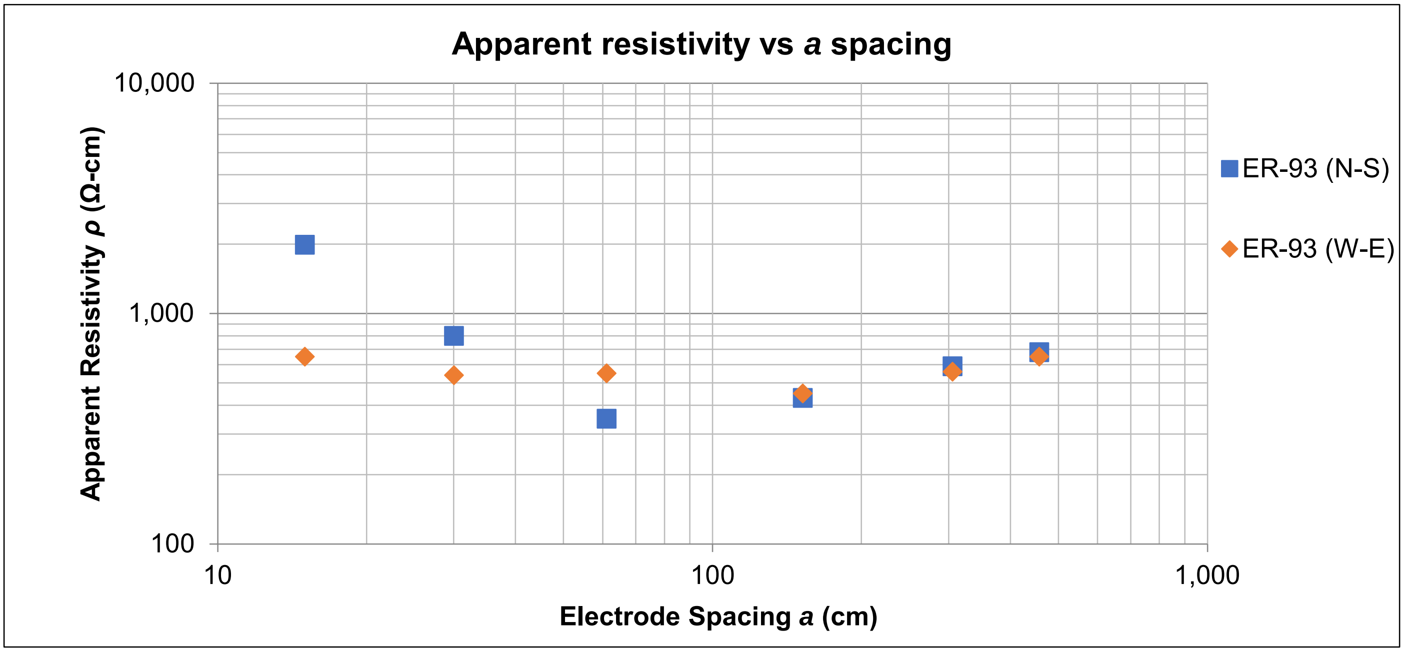
Test Date August 3, 2023

Method Wenner 4-pin ASTM G57-06 (2012); IEEE 81-2012

Notes & Conflicts Arrays oriented N-S and W-E with a common midpoint.

Apparent resistivity ρ is calculated as : $\rho = \dfrac{4\pi aR}{1 + \dfrac{2a}{\sqrt{a^2 + 4b^2}} - \dfrac{a}{\sqrt{a^2 + b^2}}}$

Electrode Spacing *a*		**Electrode Depth *b***		**ER-93 (N-S)**		**ER-93 (W-E)**	
(feet)	(centimeters)	(inches)	(centimeters)	Measured Resistance *R*	Apparent Resistivity *ρ*	Measured Resistance *R*	Apparent Resistivity *ρ*
				Ω	(Ω-cm)	Ω	(Ω-cm)
0.5	15	2	5	18.13	1990	5.87	650
1	30	2	5	4.04	800	2.75	540
2	61	2	5	0.906	350	1.419	550
5	152	3	8	0.445	430	0.465	450
10	305	3	8	0.305	590	0.293	560
15	457	3	8	0.236	680	0.227	650



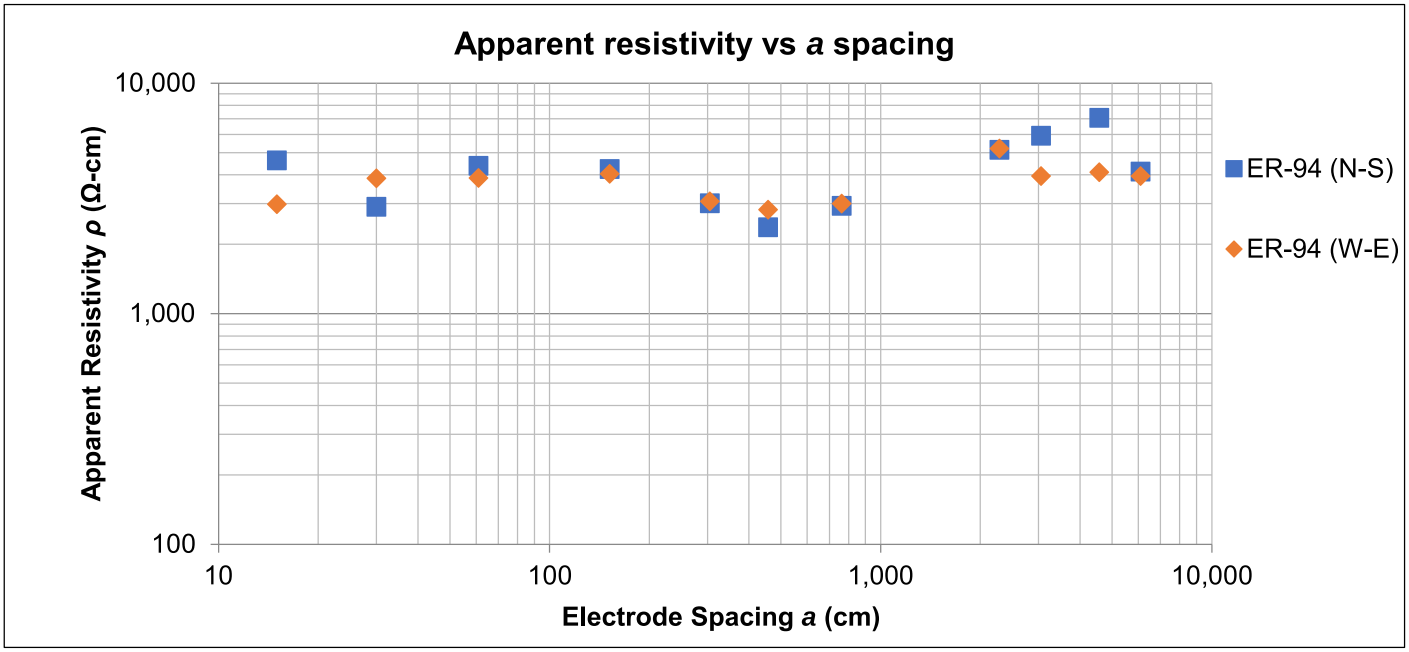
FIELD ELECTRICAL RESISTIVITY DATA SHEET

Darden Solar Facility ■ Cantua Creek, Fresno County, California
October 13, 2023 ■ Terracon Project No. 60225172

Array Loc.	**ER-94** (36.426712°N, 120.396495°W), Substation Area		
Instrument	L&R Instruments - Ultra Mini Res	**Weather**	Clear, high of 100°F.
Serial #	SN-214U	**Ground Cond.**	Fallow field.
Cal. Check	2/14/2023	**Tested By**	M. Yoni/ G. Alexa
Test Date	August 3, 2023	**Method**	Wenner 4-pin ASTM G57-06 (2012); IEEE 81-2012
Notes & Conflicts	Arrays oriented N-S and W-E with a common midpoint.		

Apparent resistivity ρ is calculated as :
$$\rho = \frac{4\pi a R}{1 + \frac{2a}{\sqrt{a^2 + 4b^2}} - \frac{a}{\sqrt{a^2 + b^2}}}$$

Electrode Spacing *a*		**Electrode Depth *b***		**ER-94 (N-S)**		**ER-94 (W-E)**	
(feet)	(centimeters)	(inches)	(centimeters)	Measured Resistance *R* Ω	Apparent Resistivity *ρ* (Ω-cm)	Measured Resistance *R* Ω	Apparent Resistivity *ρ* (Ω-cm)
0.5	15	2	5	42.10	4630	27.20	2990
1	30	2	5	14.75	2910	19.60	3870
2	61	2	5	11.31	4380	10.01	3880
5	152	3	8	4.42	4240	4.21	4040
10	305	3	8	1.57	3010	1.60	3070
15	457	3	8	0.825	2370	0.986	2830
25	762	4	10	0.614	2940	0.626	3000
75	2286	6	15	0.358	5140	0.362	5200
100	3048	6	15	0.309	5920	0.207	3960
150	4572	6	15	0.246	7070	0.143	4110
200	6096	6	15	0.108	4140	0.103	3950



FIELD ELECTRICAL RESISTIVITY DATA SHEET

Darden Solar Facility ■ Cantua Creek, Fresno County, California
October 13, 2023 ■ Terracon Project No. 60225172

NORCAL GEOPHYSICAL CONSULTANTS INC.
A Terracon COMPANY

Array Loc. **ER-95** (36.426620°N, 120.401000°W), Switchyard Area

Instrument L&R Instruments - Ultra Mini Res

Weather Clear, high of 100°F.

Serial # SN-214U

Ground Cond. Fallow field.

Cal. Check 2/14/2023

Tested By M. Yoni/ G. Alexa

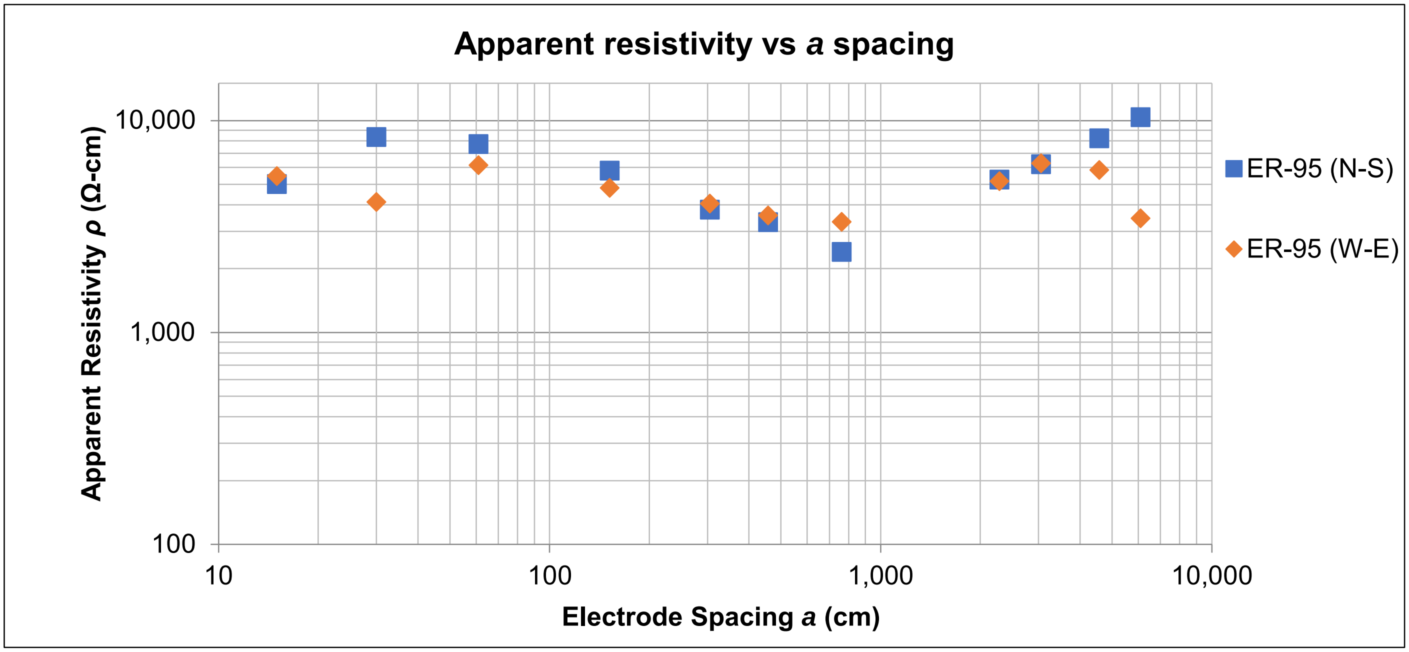
Test Date August 3, 2023

Method Wenner 4-pin ASTM G57-06 (2012); IEEE 81-2012

Notes & Conflicts Arrays oriented N-S and W-E with a common midpoint.

Apparent resistivity ρ is calculated as :
$$\rho = \frac{4\pi a R}{1 + \frac{2a}{\sqrt{a^2 + 4b^2}} - \frac{a}{\sqrt{a^2 + b^2}}}$$

Electrode Spacing *a*		**Electrode Depth *b***		**ER-95 (N-S)**		**ER-95 (W-E)**	
(feet)	(centimeters)	(inches)	(centimeters)	Measured Resistance *R*	Apparent Resistivity *ρ*	Measured Resistance *R*	Apparent Resistivity *ρ*
				Ω	(Ω-cm)	Ω	(Ω-cm)
0.5	15	2	5	45.60	5010	49.70	5460
1	30	2	5	42.30	8340	20.90	4120
2	61	2	5	20.00	7750	15.90	6160
5	152	3	8	6.04	5790	5.00	4800
10	305	3	8	1.97	3790	2.12	4060
15	457	3	8	1.15	3310	1.24	3570
25	762	4	10	0.502	2400	0.696	3330
75	2286	6	15	0.367	5270	0.360	5170
100	3048	6	15	0.325	6220	0.328	6280
150	4572	6	15	0.287	8240	0.203	5830
200	6096	6	15	0.271	10380	0.090	3450



Test Pile Driving Data

Contents:

Pile Location Procedures

The test locations were established in the field by using a hand-held GPS (accurate to about 20 feet) and existing site features as reference points. The mapped test locations should be considered accurate only to the degree implied by the means and methods used to define them.

Test Pile Details

Terracon provided the steel piles to the job site. The piles were driven to facilitate performing tension (pull-out), lateral, and compression tests. The bare steel sections have the following properties[1]:

Parameter	W6x9
Depth	5.900 in
Flange Width, b_f	3.940 in
Flange Thickness, t_f	0.215 in
Web Thickness, t_w	0.170 in
Moment of Inertia, I_x	16.40 in^4
Section Area, A	2.68 in^2
Young's Modulus, E_s	29,000 ksi
Yield Stress, F_y	50 ksi
Hot Dip Galvanization	None

Test Pile Installation

The test piles consisted of wide-flange, bare steel W6x9 sections. A group of three test piles were installed at each of the ninety-one (91) test locations. The pile identification system for each location begins with "PLT" and is followed by the number corresponding to the test pile group location and a letter identifying the pile. "A" and "B" piles were installed to approximate depths of 5 to 10 feet below existing site grades (bgs) and utilized for axial tension and lateral testing. "C" piles were installed to the same depth as the shortest embedded pile (5 to 7 feet) at that particular location and utilized for compression testing.

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[1] American Institute of Steel Construction (AISC), *"Steel Construction Manual – Fourteenth Edition"* February 2012.

Terracon subcontracted Sunstall, Inc. to install W-section steel piles for the pile load tests. Gayk HRE equipment with a hydraulic attachment was utilized for installation. All piles were driven within an approximate total drive time ranging between 7 and 104 second. The time rate of installation was recorded with a stopwatch. The total time required to advance each pile to its specified embedment depth was recorded and is summarized in the attached tables.

Pile Load Test Locations

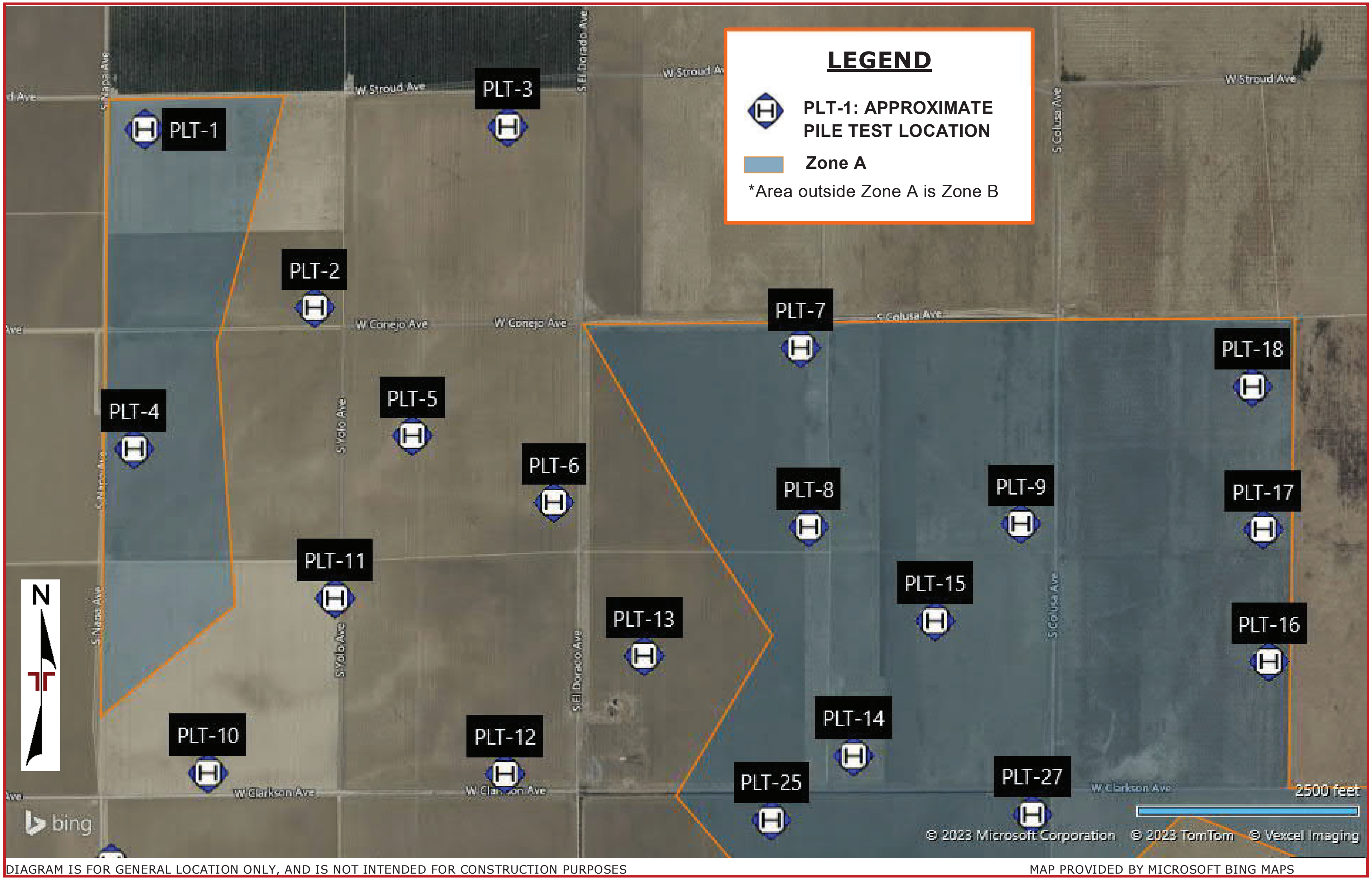

DIAGRAM IS FOR GENERAL LOCATION ONLY, AND IS NOT INTENDED FOR CONSTRUCTION PURPOSES

MAP PROVIDED BY MICROSOFT BING MAPS

Pile Load Test Locations

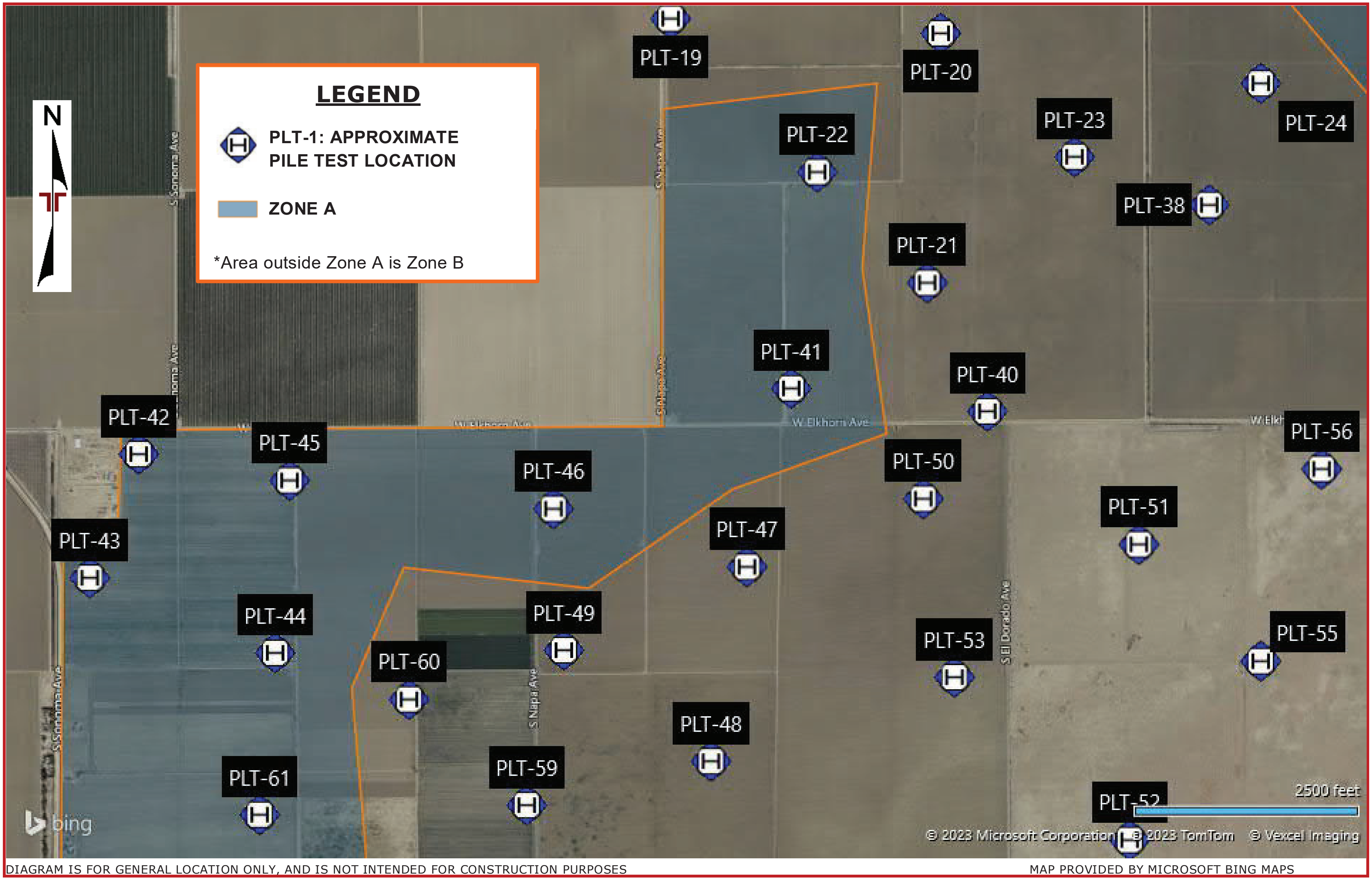

DIAGRAM IS FOR GENERAL LOCATION ONLY, AND IS NOT INTENDED FOR CONSTRUCTION PURPOSES

MAP PROVIDED BY MICROSOFT BING MAPS

Pile Load Test Locations

DIAGRAM IS FOR GENERAL LOCATION ONLY, AND IS NOT INTENDED FOR CONSTRUCTION PURPOSES

MAP PROVIDED BY MICROSOFT BING MAPS

Pile Load Test Locations

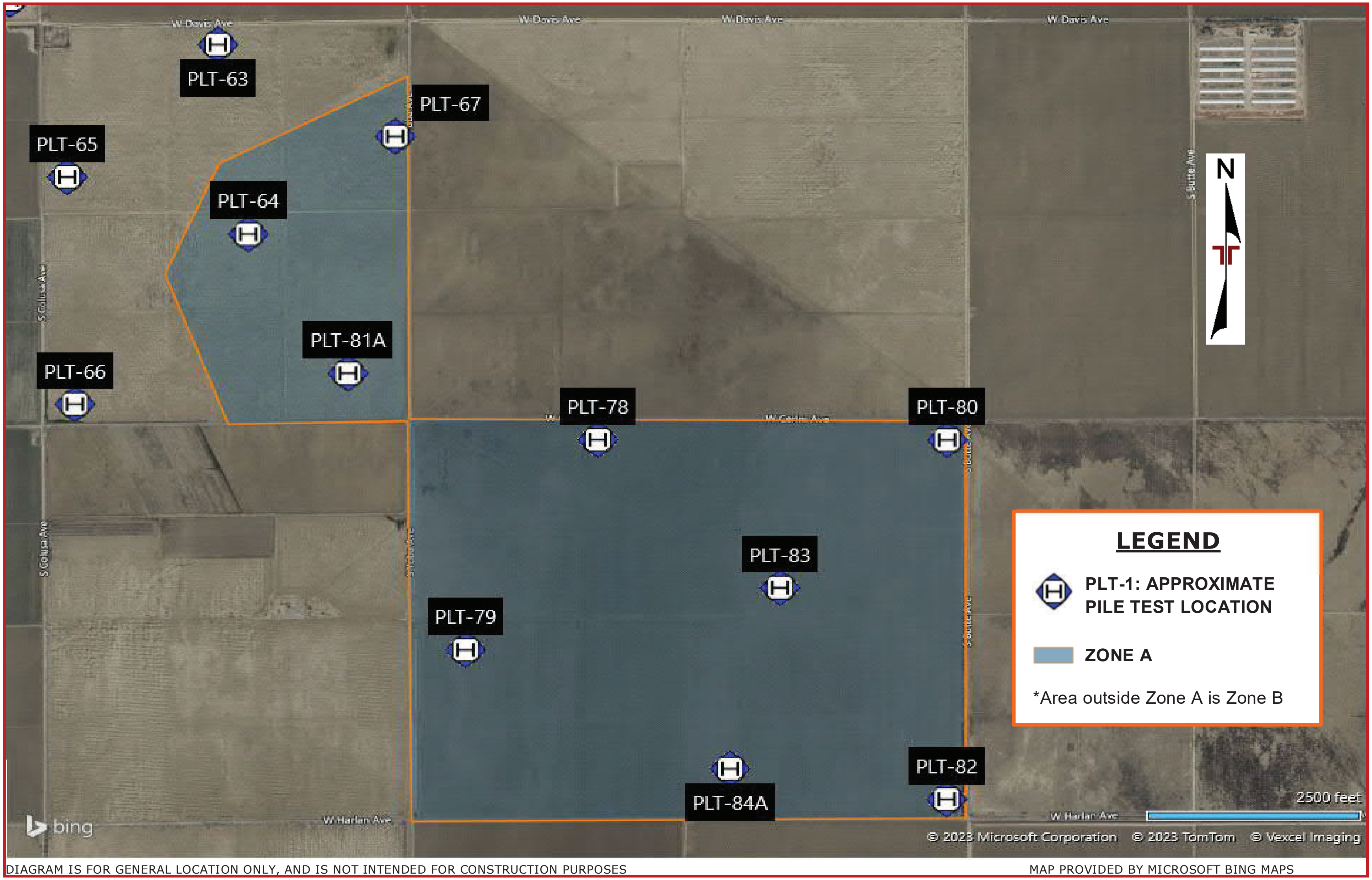

DIAGRAM IS FOR GENERAL LOCATION ONLY, AND IS NOT INTENDED FOR CONSTRUCTION PURPOSES

MAP PROVIDED BY MICROSOFT BING MAPS

Pile Load Test Locations

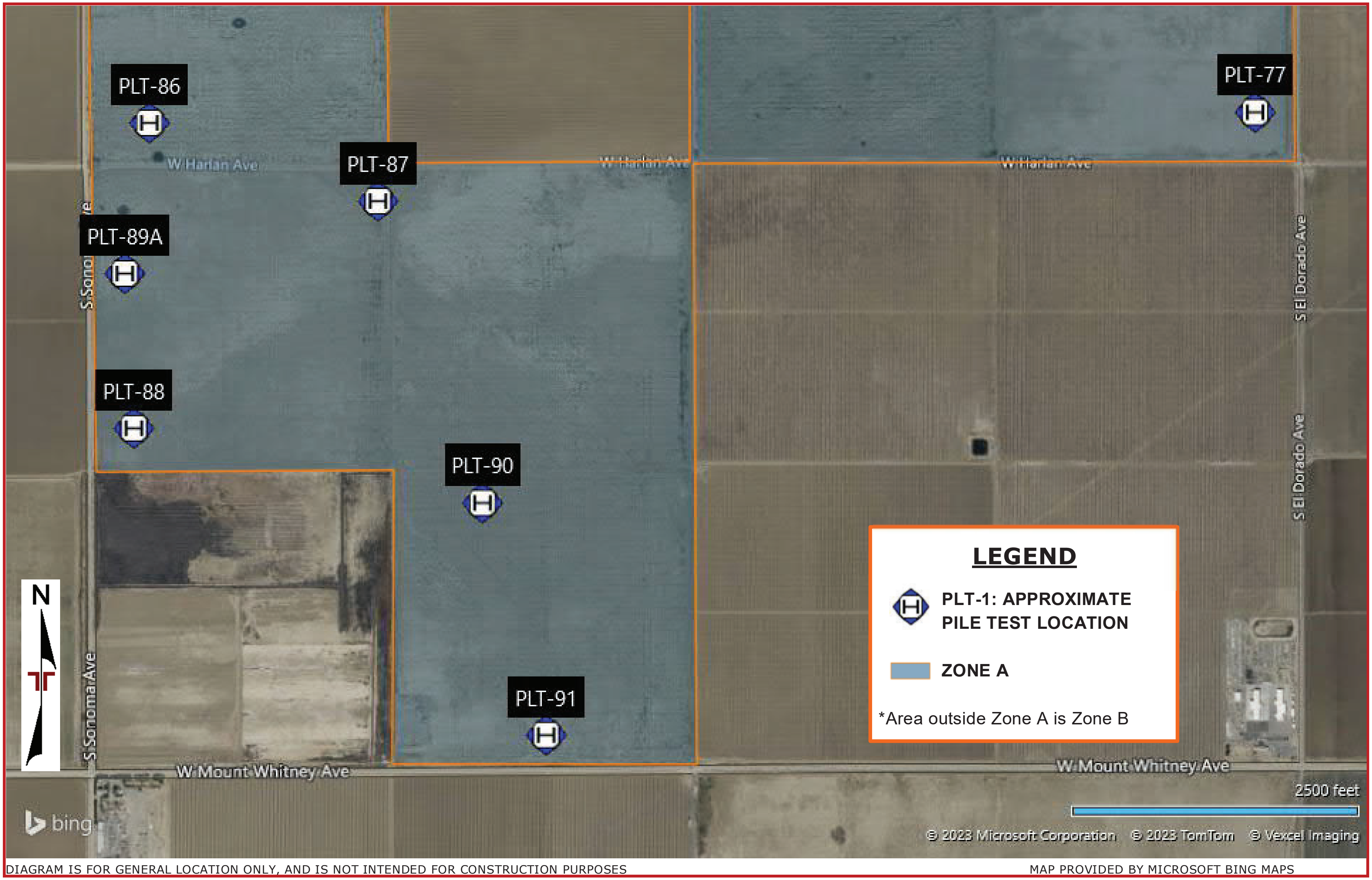

DIAGRAM IS FOR GENERAL LOCATION ONLY, AND IS NOT INTENDED FOR CONSTRUCTION PURPOSES

MAP PROVIDED BY MICROSOFT BING MAPS

Pile Embedment Drive Time: Darden Solar - 60225172

Pile Location	Pile Size	Pile	Pile Length, ft	Embed Depth, ft	Drive Time (s)	Feet (ft)									
						1	2	3	4	5	6	7	8	9	10
						Seconds									
PLT-1	W6x9	A	7	5	8	1	1	2	2	2					
	W6x9	B	10	8	24	1	2	2	2	2	3	5	7		
	W6x9	C	7	5	8	1	1	2	2	2					
PLT-2	W6x9	A	8	6	20	1	2	3	4	5	5				
	W6x9	B	11	9	57	2	2	4	4	5	6	9	11	14	
	W6x9	C	8	6	15	1	2	2	3	3	4				
PLT-3	W6x9	A	9	7	40	1	3	5	6	6	10	9			
	W6x9	B	12	10	103	1	2	5	7	9	11	12	19	19	18
	W6x9	C	9	7	36	1	3	2	3	7	9	11			
PLT-4	W6x9	A	7	5	7	1	1	1	2	2					
	W6x9	B	10	8	15	1	2	1	1	2	2	3	3		
	W6x9	C	7	5	7	1	1	1	2	2					
PLT-5	W6x9	A	8	6	14	1	1	2	3	3	4				
	W6x9	B	11	9	47	1	2	2	3	3	6	9	11	10	
	W6x9	C	8	6	20	2	1	3	3	6	5				
PLT-6	W6x9	A	9	7	22	1	1	2	3	4	5	6			
	W6x9	B	12	10	40	1	2	2	3	3	4	5	6	7	7
	W6x9	C	9	7	19	1	1	3	4	4	3	3			
PLT-7	W6x9	A	7	5	11	1	2	1	3	4					
	W6x9	B	10	8	26	1	2	2	3	4	4	4	6		
	W6x9	C	7	5	11	1	1	2	3	4					
PLT-8	W6x9	A	8	6	16	1	1	2	4	4	4				
	W6x9	B	11	9	34	1	2	1	4	4	2	4	7	9	
	W6x9	C	8	6	27	1	2	3	6	7	8				
PLT-9	W6x9	A	9	7	43	1	2	4	8	9	9	10			
	W6x9	B	12	10	79	1	3	4	7	9	10	10	10	11	14
	W6x9	C	9	7	43	1	2	4	7	8	10	11			
PLT-10	W6x9	A	7	5	12	1	2	2	3	4					
	W6x9	B	10	8	29	1	2	2	3	4	5	6	6		
	W6x9	C	7	5	11	1	2	2	3	3					
PLT-11	W6x9	A	8	6	8	1	1	1	1	2	2				
	W6x9	B	11	9	18	1	2	1	1	1	2	3	3	4	
	W6x9	C	8	6	7	1	1	1	1	1	2				
PLT-12	W6x9	A	9	7	38	1	2	3	5	6	10	11			
	W6x9	B	12	10	74	1	2	3	3	4	5	8	15	16	17
	W6x9	C	9	7	31	1	2	3	5	4	6	10			
PLT-13	W6x9	A	7	5	17	1	2	4	4	6					
	W6x9	B	10	8	48	1	3	4	5	6	8	10	11		
	W6x9	C	7	5	11	1	1	3	2	4					
PLT-14	W6x9	A	8	6	30	1	2	2	8	8	9				
	W6x9	B	11	9	42	1	2	7	7	6	5	5	4	5	
	W6x9	C	8	6	34	1	2	3	8	10	10				
PLT-15	W6x9	A	9	7	27	1	2	3	5	5	5	6			
	W6x9	B	12	10	61	1	2	2	5	5	6	7	8	10	15
	W6x9	C	9	7	28	1	2	3	6	5	5	6			
PLT-16	W6x9	A	7	5	13	1	1	2	3	6					
	W6x9	B	10	8	70	1	2	4	6	10	17	14	16		
	W6x9	C	7	5	15	1	2	2	4	6					
PLT-17	W6x9	A	8	6	20	1	3	2	5	4	5				
	W6x9	B	11	9	50	1	2	2	5	5	5	8	11	11	
	W6x9	C	8	6	27	1	2	2	6	7	9				

Pile Embedment Drive Time: Darden Solar - 60225172

Pile Location	Pile Size	Pile	Pile Length, ft	Embed Depth, ft	Drive Time (s)	Feet (ft)									
						1	2	3	4	5	6	7	8	9	10
						Seconds									
PLT-18	W6x9	A	9	7	45	1	3	5	6	7	11	12			
	W6x9	B	12	10	90	1	2	3	5	8	10	12	16	16	17
	W6x9	C	9	7	42	1	2	3	6	7	10	13			
PLT-19	W6x9	A	7	5	10	1	2	3	2	2					
	W6x9	B	10	8	21	1	2	2	2	3	4	3	4		
	W6x9	C	7	5	7	1	2	1	2	1					
PLT-20	W6x9	A	8	6	24	1	2	4	6	5	6				
	W6x9	B	11	9	64	1	3	4	6	8	9	10	11	12	
	W6x9	C	8	6	15	1	2	3	3	2	4				
PLT-21	W6x9	A	9	7	30	1	2	5	6	6	5	5			
	W6x9	B	12	10	60	1	2	5	7	5	5	5	6	10	14
	W6x9	C	9	7	28	1	2	3	4	5	6	7			
PLT-22	W6x9	A	7	5	13	1	2	3	3	4					
	W6x9	B	10	8	25	1	2	2	4	4	3	4	5		
	W6x9	C	7	5	14	1	3	4	3	3					
PLT-23	W6x9	A	8	6	17	1	2	3	2	2	7				
	W6x9	B	11	9	41	1	2	4	3	3	5	11	12		
	W6x9	C	8	6	27	1	3	2	6	8	7				
PLT-24	W6x9	A	9	7	29	1	2	4	5	5	5	7			
	W6x9	B	12	10	51	1	3	4	6	5	5	5	9	9	4
	W6x9	C	9	7	31	1	1	4	6	6	6	7			
PLT-25	W6x9	A	7	5	15	1	2	3	4	5					
	W6x9	B	10	8	39	1	2	3	6	6	7	7	7		
	W6x9	C	7	5	13	1	2	2	3	5					
PLT-26	W6x9	A	8	6	17	1	2	2	3	5	4				
	W6x9	B	11	9	85	1	2	4	7	9	9	12	16	25	
	W6x9	C	8	6	15	1	3	2	2	3	4				
PLT-27	W6x9	A	9	7	41	1	2	2	4	10	12	10			
	W6x9	B	12	10	82	1	2	2	5	8	10	11	12	14	17
	W6x9	C	9	7	37	1	2	2	5	6	9	12			
PLT-28	W6x9	A	7	5	19	1	1	4	5	8					
	W6x9	B	10	8	55	1	2	4	6	8	10	12	12		
	W6x9	C	7	5	21	1	2	4	6	8					
PLT-29	W6x9	A	8	6	33	1	1	4	8	9	10				
	W6x9	B	11	9	68	1	2	3	7	7	11	12	12	13	
	W6x9	C	8	6	37	1	3	4	6	9	14				
PLT-30	W6x9	A	9	7	32	1	2	3	4	5	7	10			
	W6x9	B	12	10	65	1	2	2	2	3	6	9	13	13	14
	W6x9	C	9	7	29	1	2	3	3	4	6	10			
PLT-31	W6x9	A	7	5	15	1	3	3	4	4					
	W6x9	B	10	8	84	4	7	7	10	11	13	15	17		
	W6x9	C	7	5	23	1	3	3	6	10					
PLT-32	W6x9	A	8	6	33	1	3	5	6	8	10				
	W6x9	B	11	9	69	1	3	4	7	8	10	11	12	13	
	W6x9	C	8	6	29	1	2	4	6	7	9				
PLT-33	W6x9	A	9	7	30	1	2	3	4	4	6	10			
	W6x9	B	12	10	66	1	2	4	5	6	7	8	12	14	7
	W6x9	C	9	7	52	1	3	3	6	8	13	18			
PLT-34	W6x9	A	7	5	18	1	2	4	5	6					
	W6x9	B	10	8	60	1	2	6	7	8	10	11	15		
	W6x9	C	7	5	18	1	1	3	5	8					
PLT-35	W6x9	A	8	6	25	1	2	3	5	5	9				
	W6x9	B	11	9	69	1	1	4	5	7	10	12	13	16	
	W6x9	C	8	6	25	1	2	4	3	6	9				

Pile Embedment Drive Time: Darden Solar - 60225172

Pile Location	Pile Size	Pile	Pile Length, ft	Embed Depth, ft	Drive Time (s)	Feet (ft)									
						1	2	3	4	5	6	7	8	9	10
						Seconds									
PLT-36	W6x9	A	9	7	58	1	2	7	11	10	13	14			
	W6x9	B	12	10	91	1	2	6	9	10	11	13	13	10	16
	W6x9	C	9	7	58	1	2	3	8	11	14	19			
PLT-37	W6x9	A	7	5	23	1	3	5	6	8					
	W6x9	B	10	8	57	1	2	5	6	9	10	10	14		
	W6x9	C	7	5	22	1	3	4	6	8					
PLT-38	W6x9	A	8	6	26	1	3	5	4	6	7				
	W6x9	B	11	9	52	1	3	5	5	4	5	7	10	12	
	W6x9	C	8	6	33	1	3	6	7	7	9				
PLT-39	W6x9	A	9	7	24	Push	Push	1	4	4	7	8			
	W6x9	B	12	10	50	Push	2	4	4	4	5	7	7	7	10
	W6x9	C	9	7	31	Push	2	3	3	4	6	13			
PLT-40	W6x9	A	7	5	16	1	2	3	5	5					
	W6x9	B	10	8	53	1	3	5	7	7	8	9	13		
	W6x9	C	7	5	24	1	4	4	7	8					
PLT-41	W6x9	A	8	6	18	1	3	3	3	4	4				
	W6x9	B	11	9	37	1	3	4	4	4	5	5	5	6	
	W6x9	C	8	6	24	1	3	5	5	5	5				
PLT-42	W6x9	A	9	7	22	1	1	3	5	4	4	4			
	W6x9	B	12	10	38	1	2	2	4	4	4	5	5	5	6
	W6x9	C	9	7	22	1	1	3	4	4	4	5			
PLT-43	W6x9	A	7	5	20	1	1	4	6	8					
	W6x9	B	10	8	59	1	3	5	7	8	10	11	14		
	W6x9	C	7	5	22	1	3	5	6	7					
PLT-44	W6x9	A	8	6	23	1	2	4	5	6	5				
	W6x9	B	11	9	34	1	3	4	4	4	4	5	5	4	
	W6x9	C	8	6	22	1	3	4	5	5	4				
PLT-45	W6x9	A	9	7	23	1	1	3	4	5	5	4			
	W6x9	B	12	10	32	1	2	2	5	5	4	4	3	3	3
	W6x9	C	9	7	21	1	2	4	3	4	3	4			
PLT-46	W6x9	A	7	5	18	1	3	4	5	5					
	W6x9	B	10	8	34	1	3	4	5	5	5	6	5		
	W6x9	C	7	5	15	1	2	3	4	5					
PLT-47	W6x9	A	8	6	34	1	3	5	7	8	10				
	W6x9	B	11	9	74	1	4	7	8	10	10	10	12	12	
	W6x9	C	8	6	29	1	3	5	6	7	7				
PLT-48	W6x9	A	9	7	38	1	2	5	7	7	7	9			
	W6x9	B	12	10	79	1	2	6	6	6	8	7	12	14	17
	W6x9	C	9	7	38	1	2	4	7	7	8	9			
PLT-49	W6x9	A	7	5	27	1	3	6	7	10					
	W6x9	B	10	8	46	1	2	4	6	7	7	9	10		
	W6x9	C	7	5	22	1	4	5	6	6					
PLT-50	W6x9	A	8	6	35	1	2	5	8	9	10				
	W6x9	B	11	9	52	1	2	4	6	7	7	8	8	9	
	W6x9	C	8	6	19	1	2	2	4	5	5				
PLT-51	W6x9	A	9	7	41	Push	3	6	7	4	8	13			
	W6x9	B	12	10	86	Push	7	7	6	7	8	10	12	15	14
	W6x9	C	9	7	43	Push	3	6	7	6	7	14			
PLT-52	W6x9	A	7	5	22	1	3	5	6	7					
	W6x9	B	10	8	36	1	2	4	6	5	6	6	6		
	W6x9	C	7	5	21	1	3	4	7	6					
PLT-53	W6x9	A	8	6	25	1	2	4	6	6	6				
	W6x9	B	11	9	55	1	2	4	7	5	4	7	9	16	
	W6x9	C	8	6	30	1	3	5	7	7	7				

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Pile Location	Pile Size	Pile	Pile Length, ft	Embed Depth, ft	Drive Time (s)	Feet (ft)									
						1	2	3	4	5	6	7	8	9	10
						Seconds									
PLT-54	W6x9	A	9	7	37	1	2	5	4	5	8	12			
	W6x9	B	12	10	70	1	2	5	5	4	7	9	9	12	16
	W6x9	C	9	7	33	1	2	4	4	4	7	11			
PLT-55	W6x9	A	7	5	29	1	3	6	9	10					
	W6x9	B	10	8	65	1	3	7	9	9	11	12	13		
	W6x9	C	7	5	27	1	5	5	7	9					
PLT-56	W6x9	A	8	6	32	1	2	4	6	8	11				
	W6x9	B	11	9	90	1	2	4	8	9	11	16	19	20	
	W6x9	C	8	6	31	1	2	5	7	7	9				
PLT-57	W6x9	A	9	7	28	1	2	4	5	7	5	4			
	W6x9	B	12	10	42	1	2	4	5	5	4	5	5	5	6
	W6x9	C	9	7	31	1	1	4	5	7	6	7			
PLT-58	W6x9	A	7	5	19	1	2	5	6	5					
	W6x9	B	10	8	49	1	2	4	6	6	8	9	13		
	W6x9	C	7	5	22	1	2	5	7	7					
PLT-59	W6x9	A	8	6	35	1	3	4	7	10	10				
	W6x9	B	11	9	67	1	3	5	6	7	10	10	13	12	
	W6x9	C	8	6	32	1	3	5	5	8	10				
PLT-60	W6x9	A	9	7	44	1	2	5	4	8	11	13			
	W6x9	B	12	10	100	1	2	7	9	12	13	14	15	14	13
	W6x9	C	9	7	53	1	3	7	8	9	11	14			
PLT-61	W6x9	A	7	5	29	1	6	7	7	8					
	W6x9	B	10	8	58	1	3	6	8	7	9	10	14		
	W6x9	C	7	5	19	1	2	3	6	7					
PLT-62	W6x9	A	8	6	23	1	2	4	5	6	5				
	W6x9	B	11	9	48	1	2	4	5	6	7	7	8	8	
	W6x9	C	8	6	22	1	2	4	5	5	5				
PLT-63	W6x9	A	9	7	27	1	2	2	3	4	7	8			
	W6x9	B	12	10	59	1	1	2	3	5	7	9	10	11	10
	W6x9	C	9	7	30	1	2	3	3	4	8	9			
PLT-64	W6x9	A	7	5	18	1	2	4	5	6					
	W6x9	B	10	8	53	1	3	5	5	6	9	11	13		
	W6x9	C	7	5	19	1	2	3	6	7					
PLT-65	W6x9	A	8	6	33	1	3	6	7	7	9				
	W6x9	B	11	9	83	1	3	5	8	8	10	14	16	18	
	W6x9	C	8	6	34	1	2	5	7	9	10				
PLT-66	W6x9	A	9	7	28	1	2	3	4	3	6	9			
	W6x9	B	12	10	55	1	1	3	5	5	6	7	8	10	9
	W6x9	C	9	7	25	1	1	3	3	4	5	8			
PLT-67	W6x9	A	7	5	15	1	1	2	4	7					
	W6x9	B	10	8	47	1	2	4	5	6	9	10	10		
	W6x9	C	7	5	23	1	3	5	7	7					
PLT-68	W6x9	A	8	6	17	1	2	2	4	4	4				
	W6x9	B	11	9	33	1	2	2	2	4	4	5	6	7	
	W6x9	C	8	6	23	1	2	5	5	5	5				
PLT-69	W6x9	A	9	7	36	1	2	2	4	6	9	12			
	W6x9	B	12	10	69	1	2	3	5	6	8	9	11	11	13
	W6x9	C	9	7	34	1	2	3	5	6	8	9			
PLT-70	W6x9	A	7	5	12	1	2	3	3	3					
	W6x9	B	10	8	22	1	1	3	3	2	3	3	6		
	W6x9	C	7	5	9	1	1	3	2	2					
PLT-71	W6x9	A	8	6	28	1	1	4	7	8	7				
	W6x9	B	11	9	37	1	1	4	7	5	4	4	5	6	
	W6x9	C	8	6	25	1	2	4	6	7	5				

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Pile Location	Pile Size	Pile	Pile Length, ft	Embed Depth, ft	Drive Time (s)	Feet (ft)									
						1	2	3	4	5	6	7	8	9	10
						Seconds									
PLT-72	W6x9	A	9	7	20	1	2	2	2	3	5	5			
	W6x9	B	12	10	37	1	1	1	2	4	6	4	5	6	7
	W6x9	C	9	7	20	1	1	2	2	3	6	5			
PLT-73	W6x9	A	7	5	19	1	3	5	4	6					
	W6x9	B	10	8	43	1	3	4	5	6	7	9	8		
	W6x9	C	7	5	15	1	2	3	4	5					
PLT-74	W6x9	A	8	6	19	1	1	2	4	5	6				
	W6x9	B	11	9	51	1	1	3	5	7	7	8	9	10	
	W6x9	C	8	6	26	1	2	4	5	7	7				
PLT-75	W6x9	A	9	7	26	1	2	4	4	3	4	8			
	W6x9	B	12	10	49	1	2	4	4	3	5	5	8	9	8
	W6x9	C	9	7	26	1	3	4	3	3	6	6			
PLT-76	W6x9	A	7	5	21	1	3	4	6	7					
	W6x9	B	10	8	51	1	2	4	7	8	9	9	11		
	W6x9	C	7	5	27	1	3	5	8	10					
PLT-77	W6x9	A	8	6	50	1	4	6	9	12	18				
	W6x9	B	11	9	93	1	3	7	8	12	15	16	14	17	
	W6x9	C	8	6	52	1	4	6	10	14	17				
PLT-78	W6x9	A	9	7	36	1	2	4	4	6	7	12			
	W6x9	B	12	10	53	1	2	4	3	4	6	6	7	9	11
	W6x9	C	9	7	26	1	2	4	4	4	5	6			
PLT-79	W6x9	A	7	5	33	1	3	6	11	12					
	W6x9	B	10	8	67	2	5	6	10	10	11	11	12		
	W6x9	C	7	5	20	1	1	4	6	8					
PLT-80	W6x9	A	8	6	29	1	4	4	6	6	8				
	W6x9	B	11	9	35	1	2	3	4	4	5	5	5	6	
	W6x9	C	8	6	25	1	3	4	5	5	7				
PLT-81	W6x9	A	9	7	40	1	1	6	8	7	7	10			
	W6x9	B	12	10	104	1	3	7	10	10	11	13	16	16	17
	W6x9	C	9	7	35	1	1	5	6	7	7	8			
PLT-82	W6x9	A	7	5	18	1	3	3	5	6					
	W6x9	B	10	8	33	1	2	4	5	5	5	5	6		
	W6x9	C	7	5	16	1	2	3	5	5					
PLT-83	W6x9	A	8	6	27	1	2	4	5	7	8				
	W6x9	B	11	9	62	1	2	5	7	7	9	9	9	13	
	W6x9	C	8	6	27	1	1	5	6	7	7				
PLT-84	W6x9	A	9	7	26	1	2	3	4	5	5	6			
	W6x9	B	12	10	49	1	1	4	4	5	5	4	5	6	14
	W6x9	C	9	7	22	1	1	4	5	3	4	4			
PLT-85	W6x9	A	7	5	10	1	1	2	3	3					
	W6x9	B	10	8	16	1	1	1	3	2	3	2	3		
	W6x9	C	7	5	14	1	2	3	3	5					
PLT-86	W6x9	A	8	6	15	1	2	4	2	3	3				
	W6x9	B	11	9	30	1	2	3	3	3	3	4	5	6	
	W6x9	C	8	6	21	1	3	3	3	4	7				
PLT-87	W6x9	A	9	7	29	1	2	4	4	5	6	7			
	W6x9	B	10	8	42	1	2	3	6	5	8	8	9		
	W6x9	C	9	7	26	1	1	3	4	5	6	6			
PLT-88	W6x9	A	7	5	17	1	1	3	5	7					
	W6x9	B	10	8	36	1	1	3	4	6	6	7	8		
	W6x9	C	7	5	17	1	1	3	6	6					
PLT-89	W6x9	A	7	5	21	1	2	4	5	9					
	W6x9	B	8	6	21	1	1	3	4	6	6				
	W6x9	C	7	5	14	1	1	3	3	6					

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Pile Location	Pile Size	Pile	Pile Length, ft	Embed Depth, ft	Drive Time (s)	Feet (ft)									
						1	2	3	4	5	6	7	8	9	10
						Seconds									
PLT-90	W6x9	A	9	7	26	1	1	2	3	4	7	8			
	W6x9	B	10	8	36	1	2	3	4	3	6	7	10		
	W6x9	C	9	7	32	1	1	3	4	5	7	11			
PLT-91	W6x9	A	7	5	17	1	2	3	5	6					
	W6x9	B	10	8	32	1	1	3	4	6	6	5	6		
	W6x9	C	7	5	14	1	1	3	3	6					