

California Energy Commission

DOCKETED

11-AFC-4

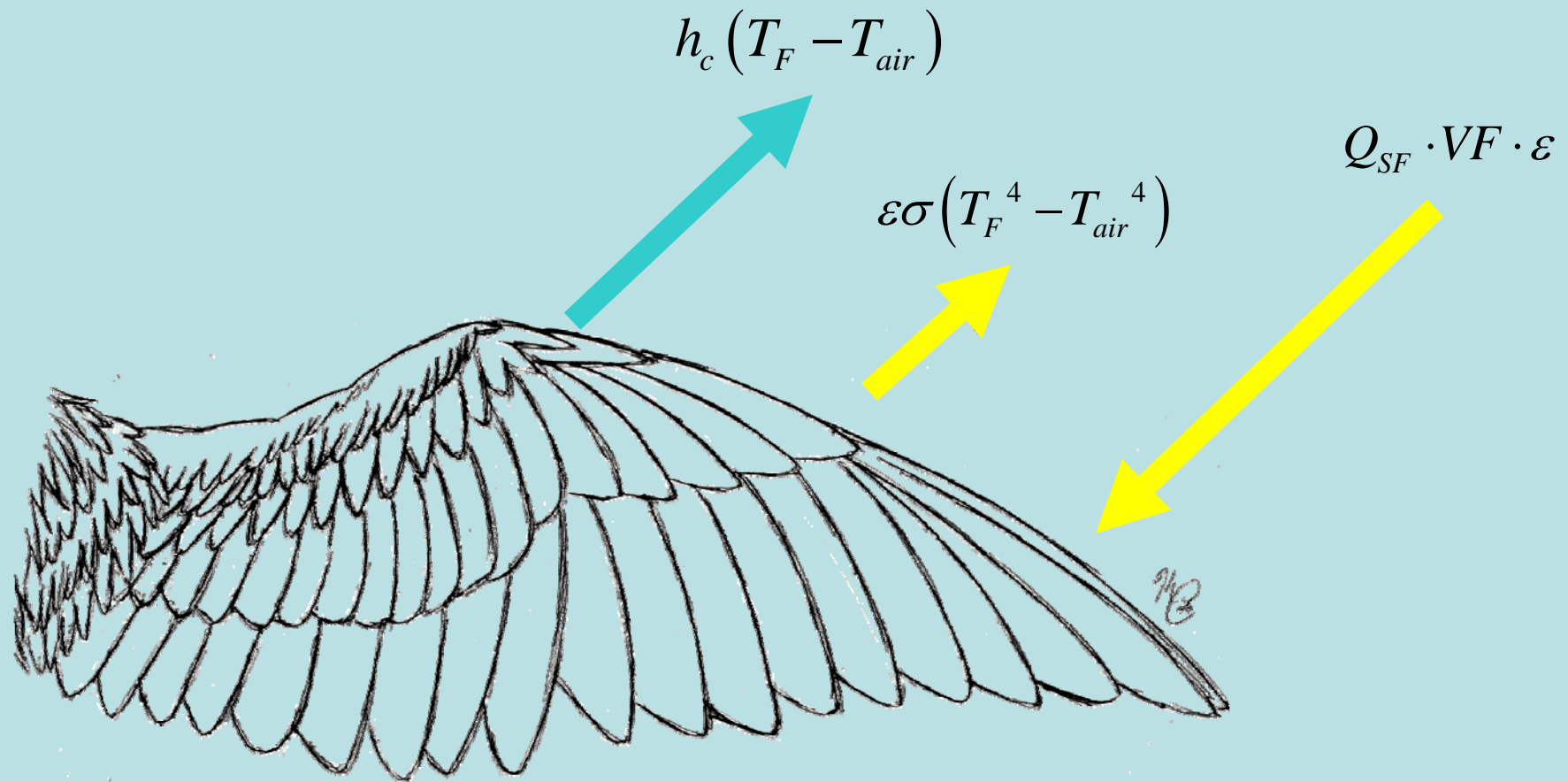
TN # 68786

DEC. 05 2012

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PSA equations for heating and cooling



Solving for solar flux that heats feather to 160 C

Solar Flux = Radiant Losses + Convective Losses

$$Q_{SF} \cdot VF \cdot \varepsilon = \varepsilon \sigma (T_F^4 - T_{air}^4) + h_c (T_F - T_{air})$$

$$Q_{SF}^{MAX} = \frac{\varepsilon \sigma \left((160 + 273)^4 - T_{air}^4 \right) + h_c (160 - T_{air})}{VF \cdot \varepsilon}$$

Parameters used in the PSA

View Factor $VF = 1$

$$h_c = \frac{k_{air}}{L} Nu = 0.664 \frac{k_{air}}{L} \sqrt{Re} \sqrt[3]{Pr} \cong 28.5$$

$$T_{air} = 49C$$

$$\varepsilon = 0.95$$

$$Q_{SF}^{MAX} \cong 4.7 \text{ kW/m}^2$$

Absorptivity of feathers

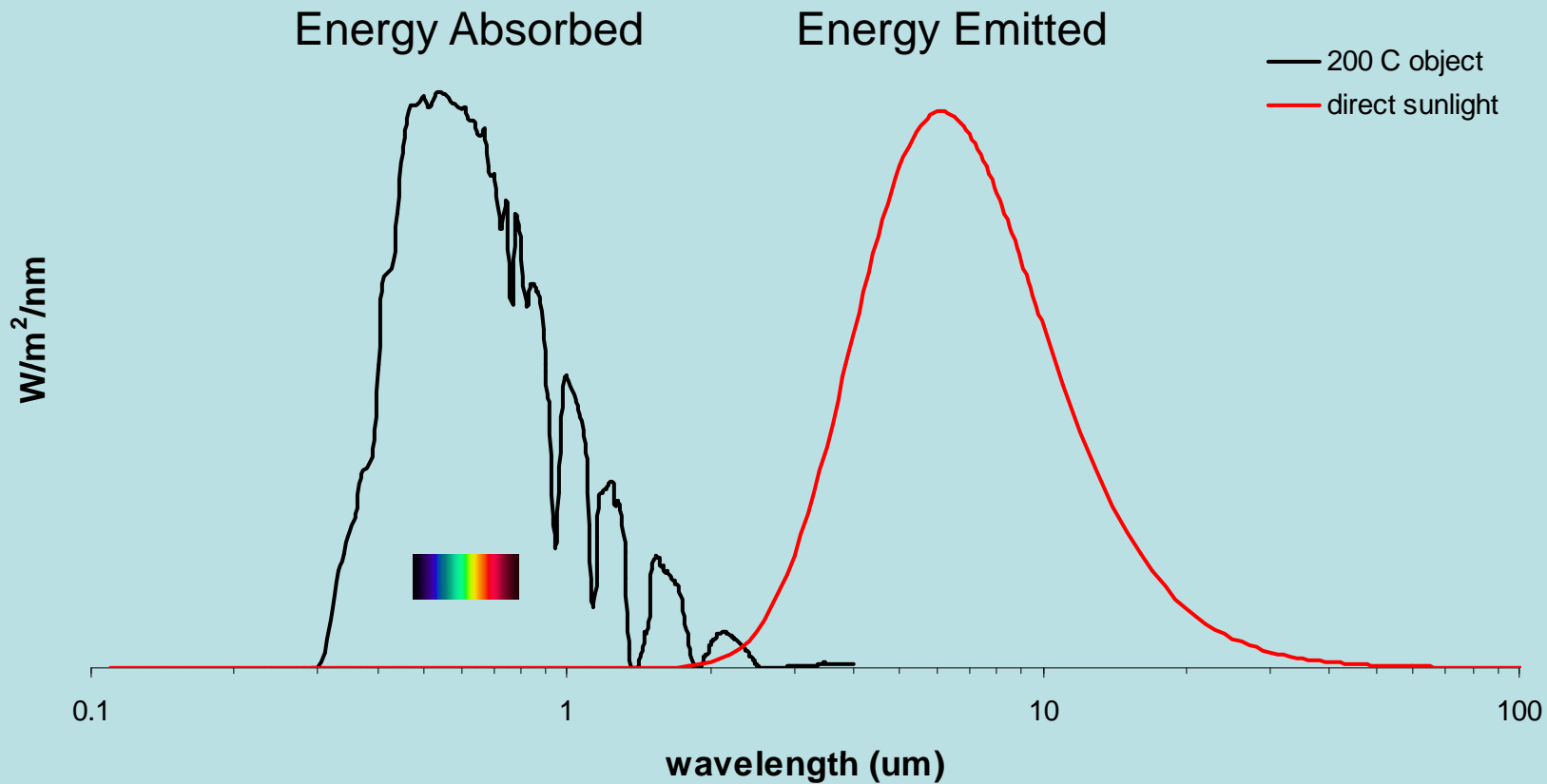
$$Q_{SF} \cdot VF \cdot \varepsilon$$

$$Q_{SF} \cdot VF \cdot \alpha$$

does $\alpha = \varepsilon$?

$$\alpha(\lambda) = \varepsilon(\lambda)$$

Spectra of sun and feather heated to 200 C



nearly all < 2um

nearly all > 2um

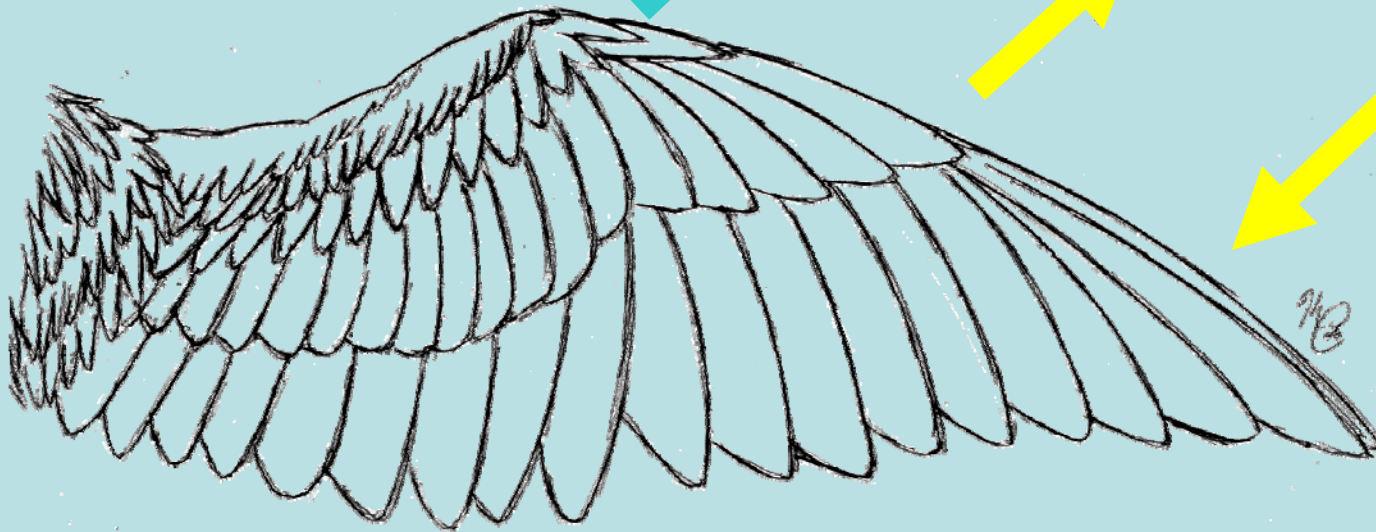
$$\alpha \neq \varepsilon$$

First correction of equations

$$h_c (T_F - T_{air})$$

$$\varepsilon \sigma (T_F^4 - T_{air}^4)$$

$$Q_{SF} \cdot VF \cdot \alpha_{sol}$$



Results after first correction

kW/m²

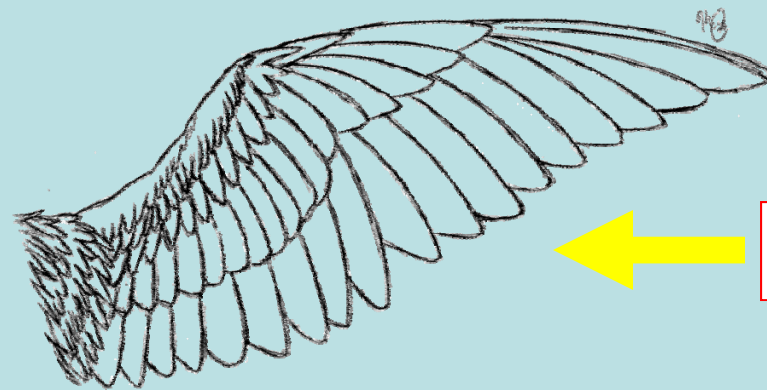
| α_{sol} | Absorptivity correction | | | | |
|----------------|-------------------------|--|--|--|--|
| 0.95 | 4.7 From PSA | | | | |
| 0.65 | 6.9 | | | | |
| 0.75 | 6.0 | | | | |
| 0.85 | 5.3 | | | | |

View Factor



← (VF = 1)

versus



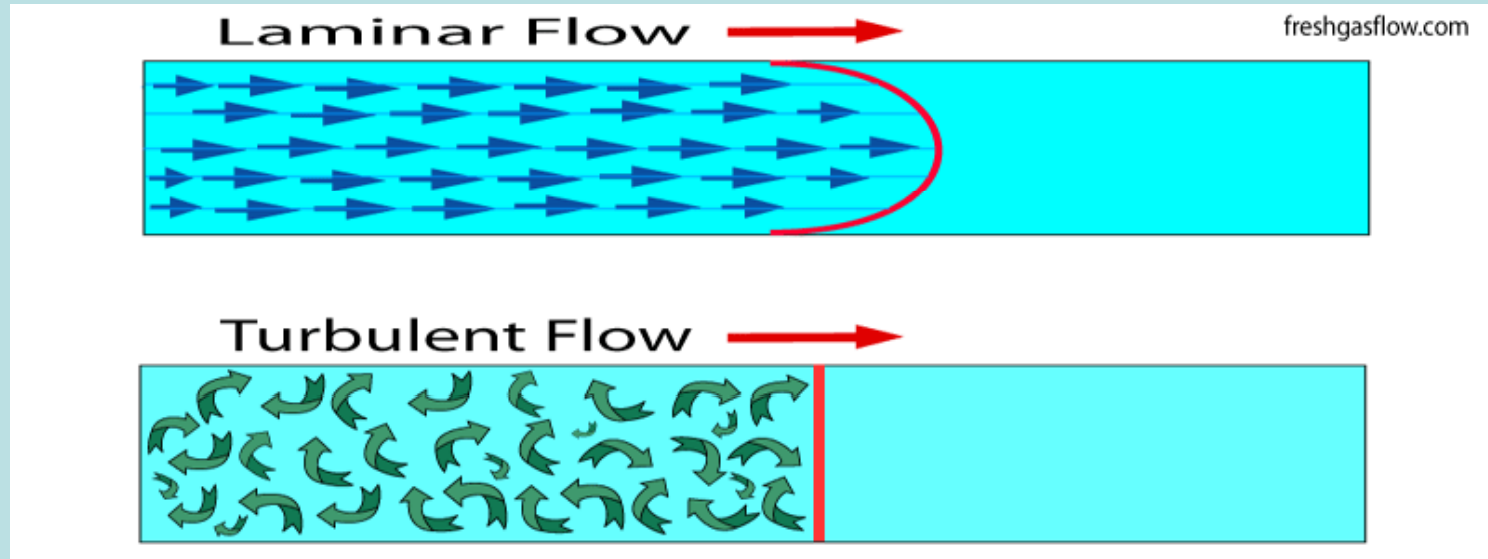
← (VF = 0.342)

Results after second correction

kW/m²

| α_{sol} | Absorptivity correction | View Factor VF = 0.342 | | | |
|----------------|-------------------------|---------------------------|--|--|--|
| 0.95 | 4.7 From PSA | 14 | | | |
| 0.65 | 6.9 | 20 | | | |
| 0.75 | 6.0 | 17 | | | |
| 0.85 | 5.3 | 15 | | | |

Heat Transfer Coefficient h_c



$$h_c = \frac{k_{air}}{L} Nu = 0.664 \frac{k_{air}}{L} \sqrt{Re} \sqrt[3]{Pr} \cong 28.5$$

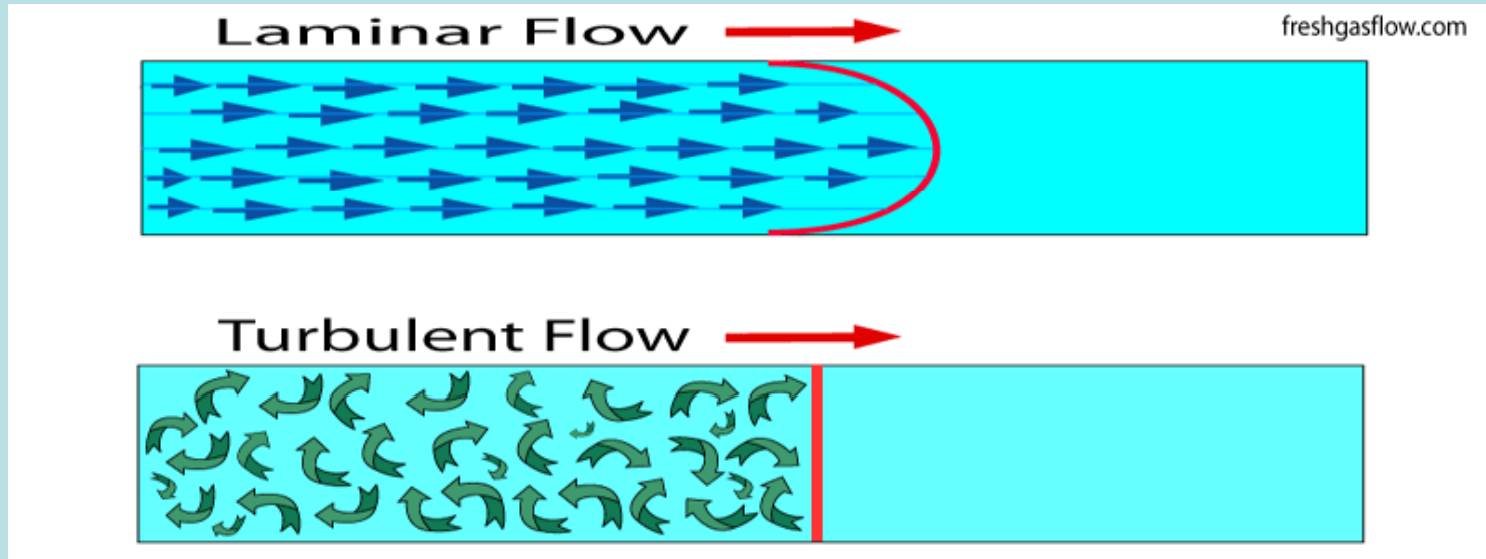
Laminar

versus

$$h_c = \frac{k_{air}}{L} Nu = 0.0592 \frac{k_{air}}{L} (Re)^{4/5} \sqrt[3]{Pr} \cong 71.8$$

Turbulent

Heat Transfer Coefficient h_c



$$h_c = \frac{k_{air}}{L} Nu = 0.664 \frac{k_{air}}{L} \sqrt{Re} \sqrt[3]{Pr} \cong 28.5$$

versus

$$h_c = \frac{k_{air}}{L} Nu = 0.0592 \frac{k_{air}}{L} (Re)^{4/5} \sqrt[3]{Pr} \cong 71.8$$

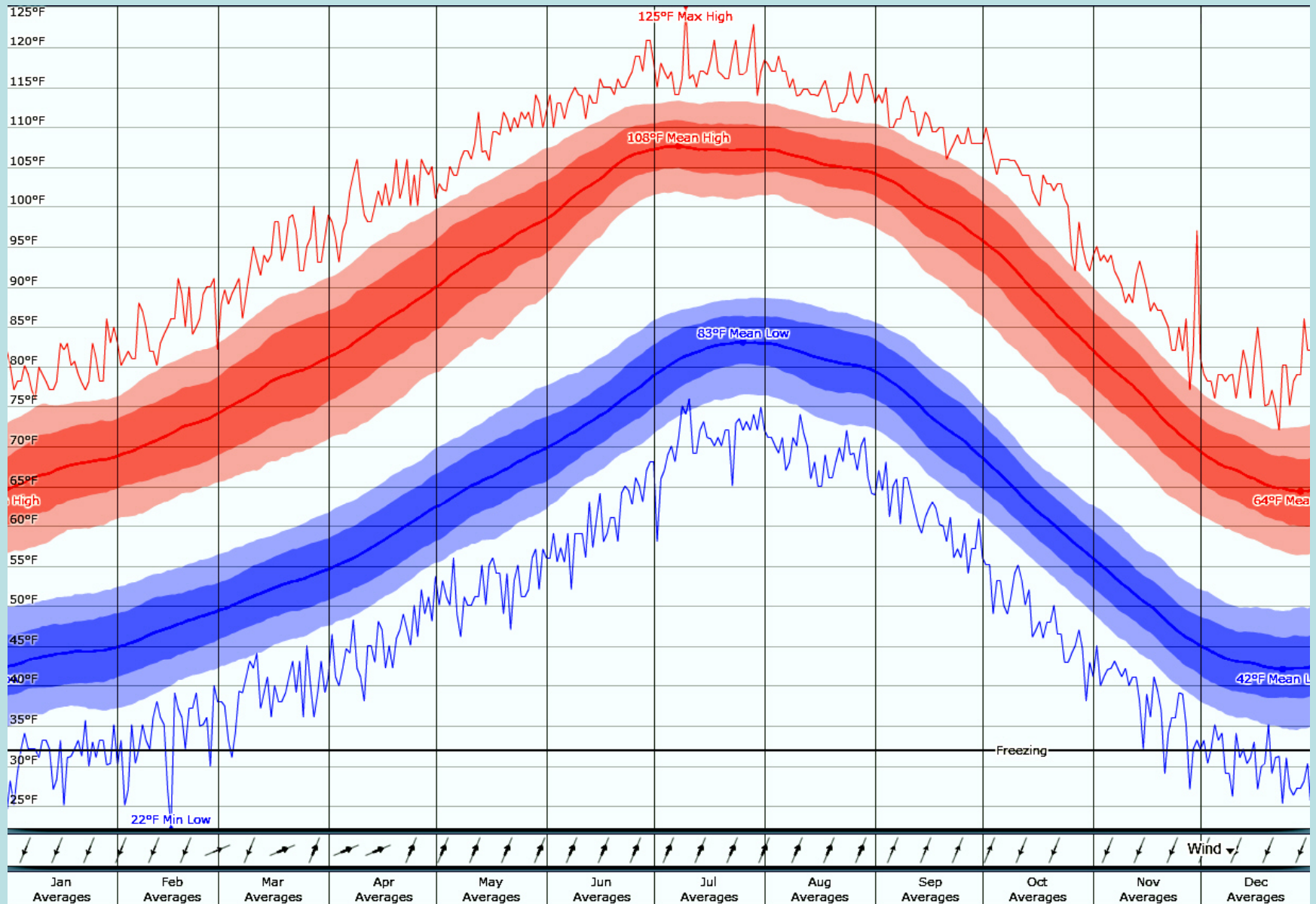
$Re = \sim 68,000$ --- Turbulent flow

Results after third correction

kW/m²

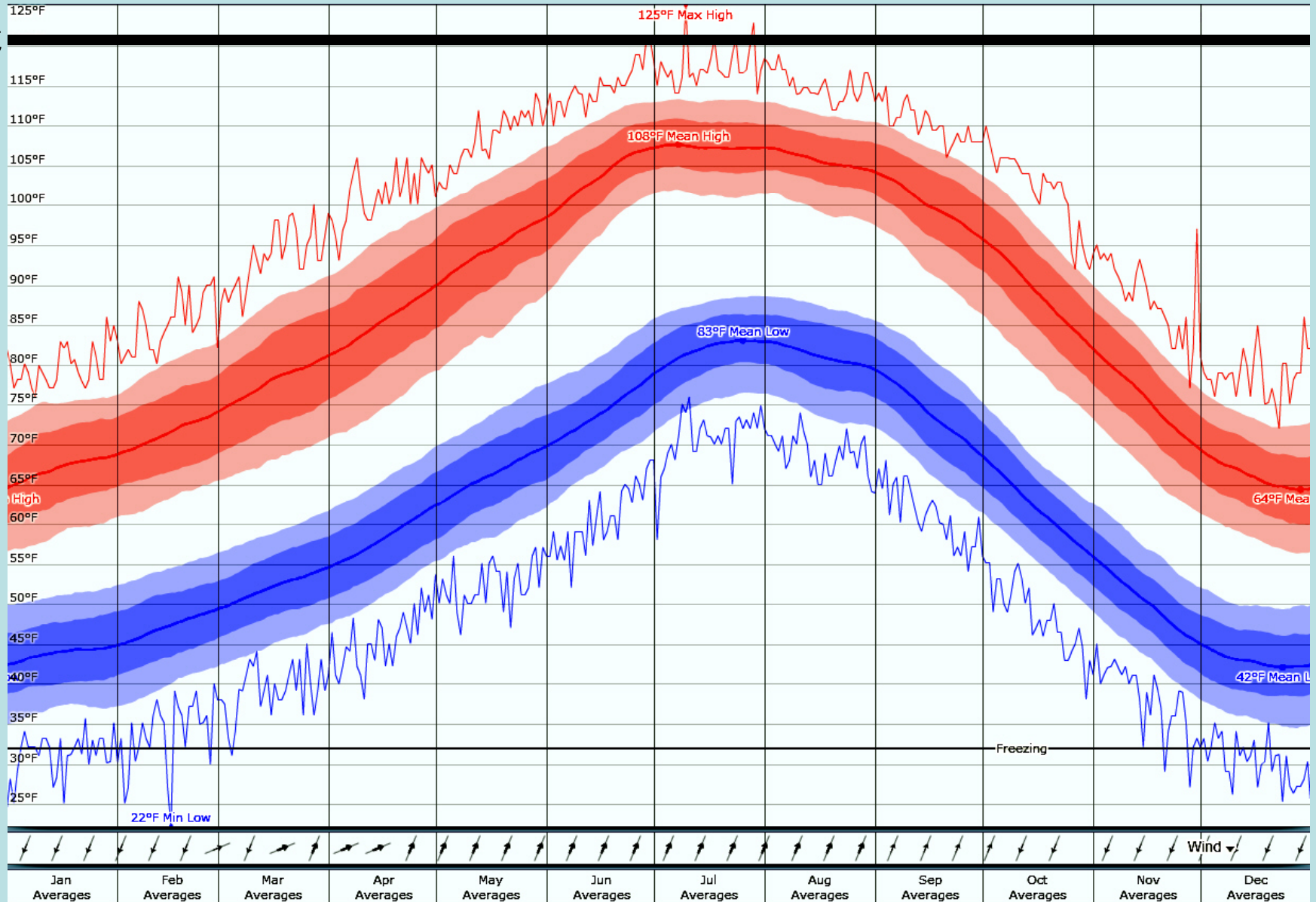
| α_{sol} | Absorptivity correction | View Factor VF = 0.342 | Heat Xfer Coef. $H_c = 71.8$ | | |
|----------------|-------------------------|---------------------------|---------------------------------|--|--|
| 0.95 | 4.7 From PSA | 14 | 29 | | |
| 0.65 | 6.9 | 20 | 42 | | |
| 0.75 | 6.0 | 17 | 36 | | |
| 0.85 | 5.3 | 15 | 32 | | |

T_{air} = 49 C?

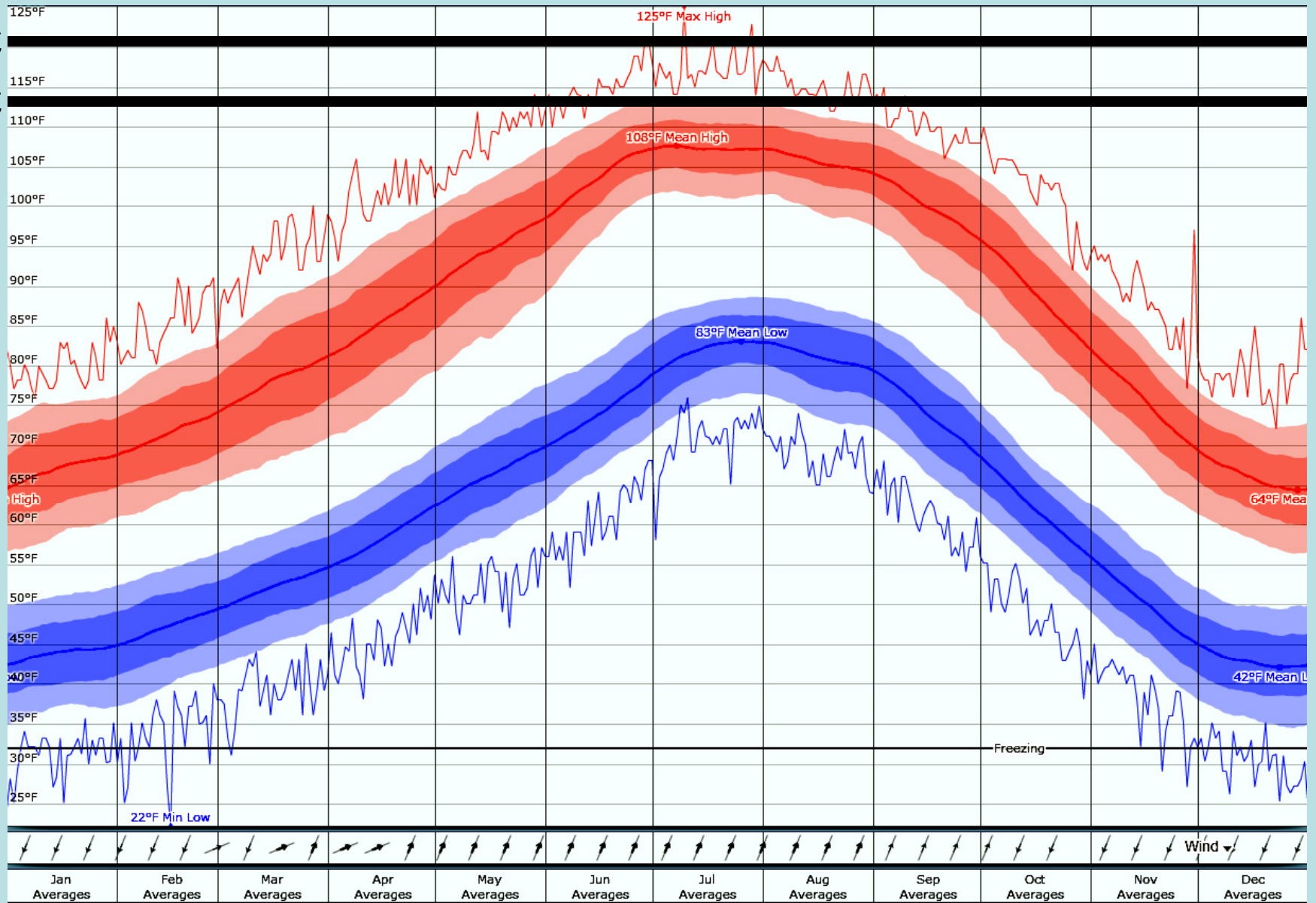


T_{air} = 49 C?

49 C



49 C
45 C



Results after fourth correction

kW/m²

| α_{sol} | Absorptivity correction | View Factor VF = 0.342 | Heat Xfer Coef. $H_c = 71.8$ | Ambient Air $T_{air} = 45\text{ C}$ | |
|----------------|-------------------------|---------------------------|---------------------------------|--|--|
| 0.95 | 4.7 From PSA | 14 | 29 | 29 | |
| 0.65 | 6.9 | 20 | 42 | 43 | |
| 0.75 | 6.0 | 17 | 36 | 37 | |
| 0.85 | 5.3 | 15 | 32 | 33 | |

Radiative heat loss

$$h_c (T_F - T_{air})$$

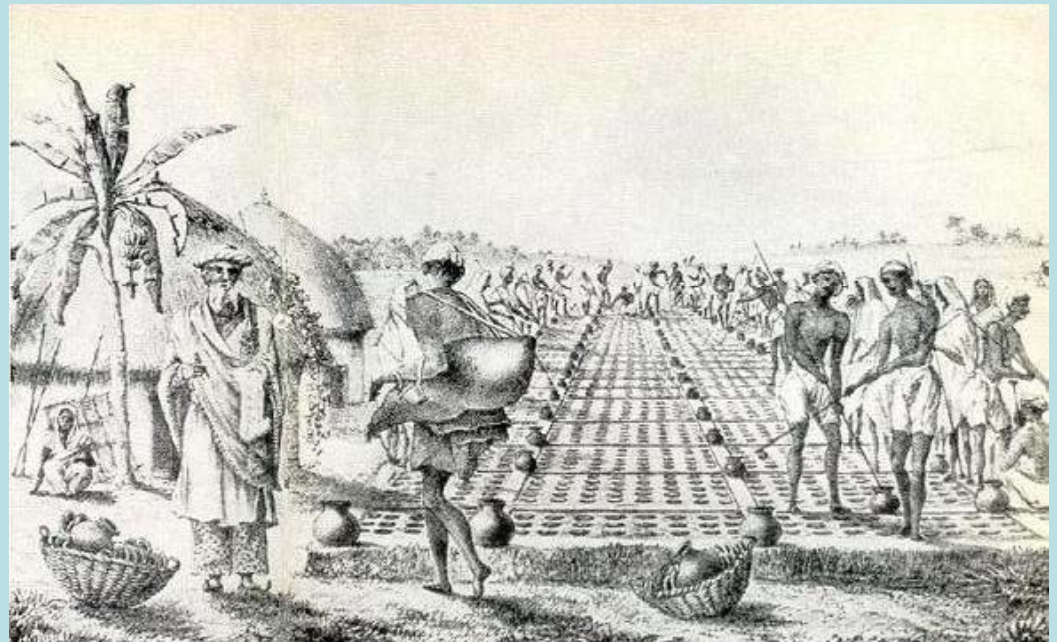
$$\varepsilon\sigma (T_F^4 - T_{air}^4)$$

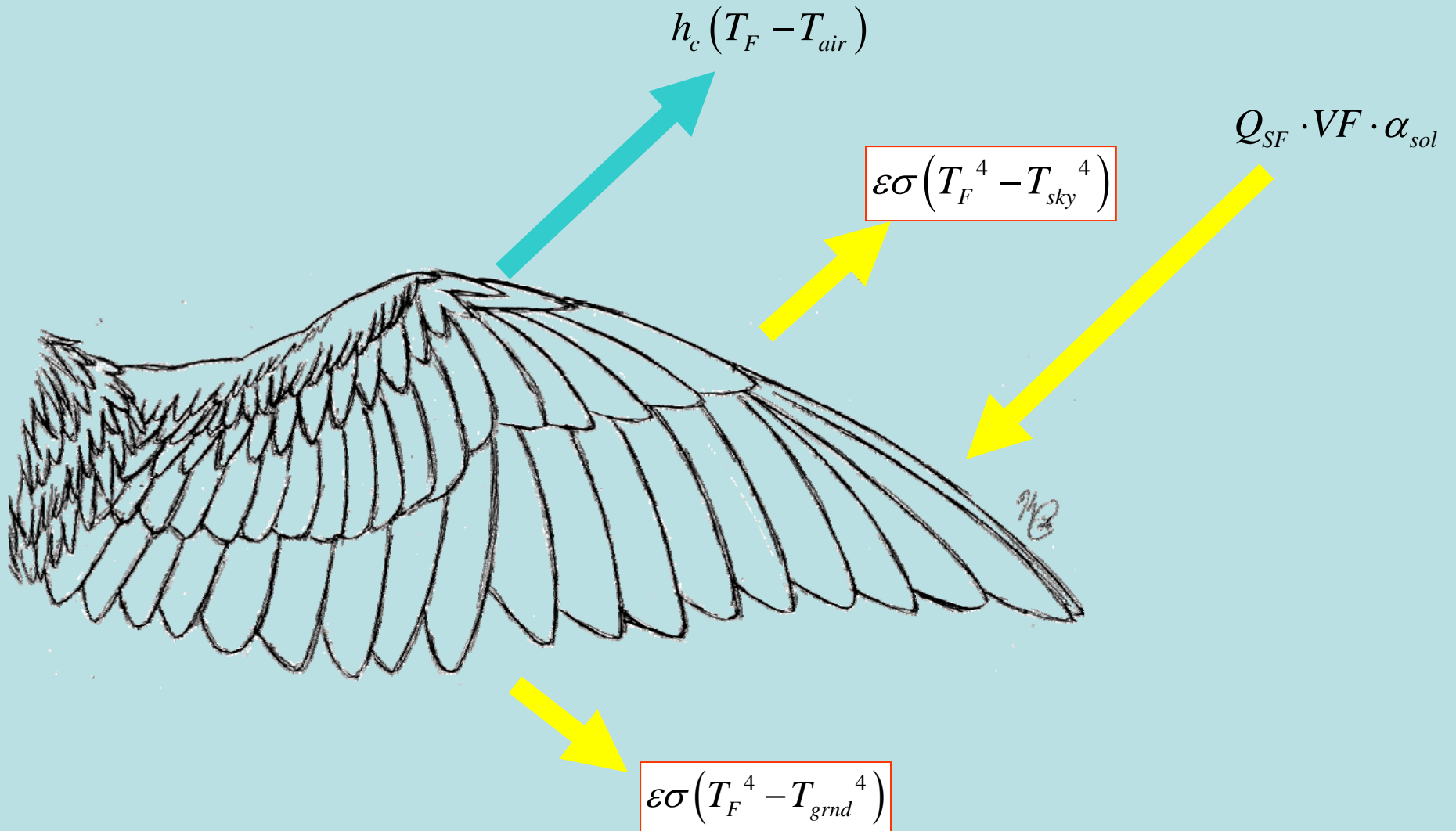
$$Q_{SF} \cdot VF \cdot \alpha_{sol}$$





Radiative temperature versus Air temperature




$$h_c (T_F - T_{air})$$

$$\varepsilon\sigma (T_F^4 - T_{sky}^4)$$

$$Q_{SF} \cdot VF \cdot \alpha_{sol}$$

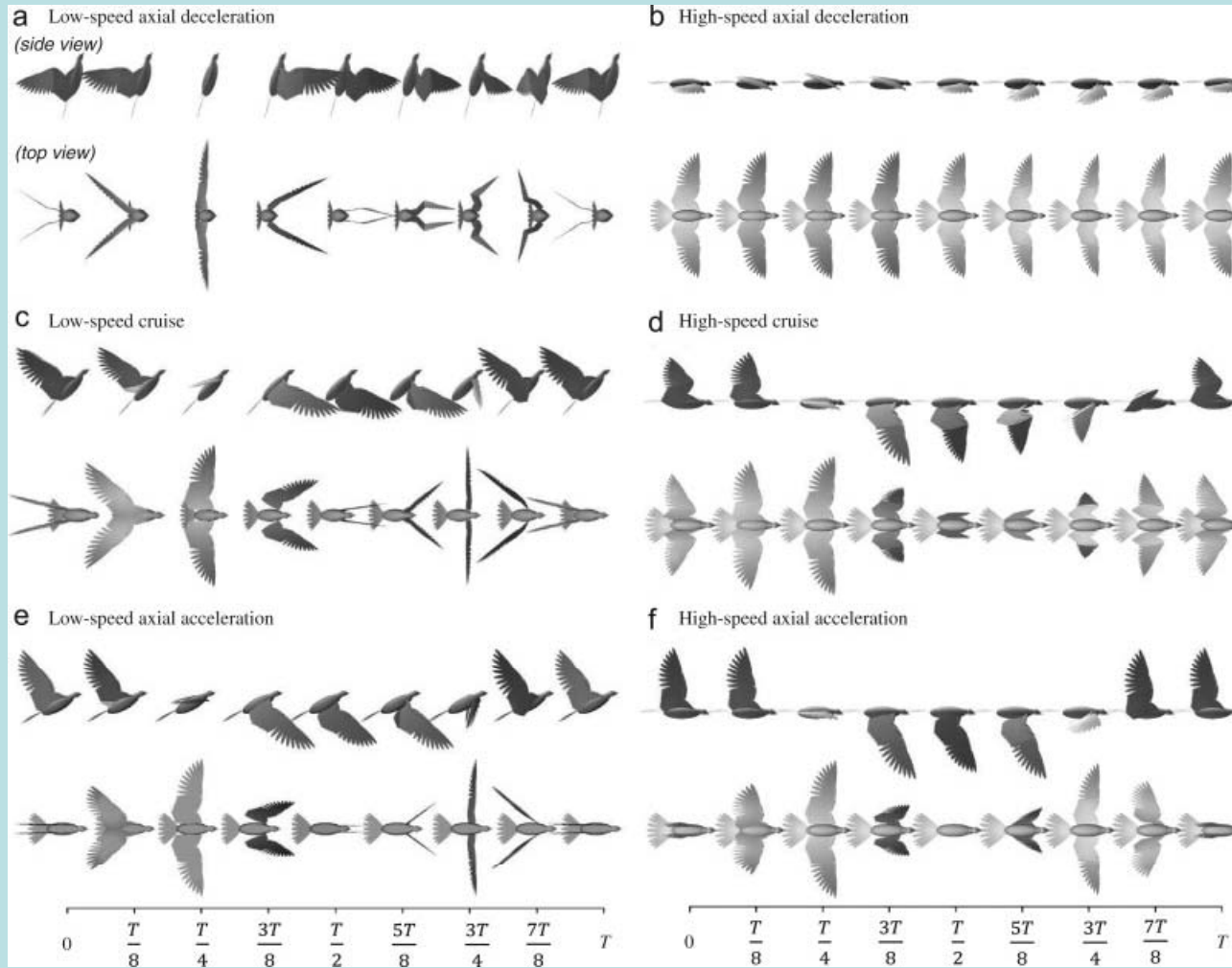
$$\varepsilon\sigma (T_F^4 - T_{grnd}^4)$$

Results after fourth correction

kW/m²

| α_{sol} | Absorptivity correction | View Factor VF = 0.342 | Heat Xfer Coef. $H_c = 71.8$ | Ambient Air $T_{air} = 45\text{ C}$ | $T_{sky} = 0\text{ C}$ $T_{grnd} = 45$ |
|----------------|-------------------------|---------------------------|---------------------------------|--|---|
| 0.95 | 4.7 From PSA | 14 | 29 | 29 | 34 |
| 0.65 | 6.9 | 20 | 42 | 43 | 50 |
| 0.75 | 6.0 | 17 | 36 | 37 | 44 |
| 0.85 | 5.3 | 15 | 32 | 33 | 39 |

Wings Flap!





Conclusions

- Equations presented in the PSA are incorrect.
- Revised analysis presented here represents a reasonable, yet very conservative lower bound for flux effects.
- Wing flapping may significantly effect the heat transfer coefficient further reducing potential for flux effects.

STATE OF CALIFORNIA

Energy Resources Conservation
and Development Commission

APPLICATION FOR CERTIFICATION)
for the RIO MESA SOLAR ELECTRIC) Docket No. 11-AFC-04
GENERATING FACILITY)
_____)

PROOF OF SERVICE

I, Karen A. Mitchell, declare that on December 5, 2012, I served the attached *December 5 2012 CEC Workshop Presentation by Dr. Sonke Johnsen* via electronic and U.S. mail to all parties on the attached service list.

I declare under the penalty of perjury that the foregoing is true and correct.



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11-AFC-04

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