

| <b>DOCKETED</b>         |                                                                                  |
|-------------------------|----------------------------------------------------------------------------------|
| <b>Docket Number:</b>   | 21-AFC-02                                                                        |
| <b>Project Title:</b>   | Willow Rock Energy Storage Center                                                |
| <b>TN #:</b>            | 265110                                                                           |
| <b>Document Title:</b>  | Willow Rock CURE Data Request 2 Response, Attachment DR136-1_Part 2_Appendix A-2 |
| <b>Description:</b>     | Resubmission of files previously submitted through Kiteworks                     |
| <b>Filer:</b>           | Kathryn Stevens                                                                  |
| <b>Organization:</b>    | WSP USA Inc.                                                                     |
| <b>Submitter Role:</b>  | Applicant Consultant                                                             |
| <b>Submission Date:</b> | 7/29/2025 8:38:32 PM                                                             |
| <b>Docketed Date:</b>   | 7/30/2025                                                                        |



CLIENT: Lane Power & Energy Solutions  
PROJECT: Hydrostor Zevsar  
PROJECT LOCATION: Rosamod, CA

SURFACE ELEVATION (ft): 2556.7  
NORTHING: 2154809.152  
EASTING: 6514431.756

PROJECT No: 951-20  
DATE: 8/5/2023 - 10/21/2023  
DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities          |                        | Sampling & In Situ Testing |                |       |                                                            |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|--------------------------|------------------------|----------------------------|----------------|-------|------------------------------------------------------------|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments                                 |
| 455                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 0     | UCS = 1,475                                                |
| 2105                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 56    | PL(A) = 621                                                |
| 450                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                                            |
| 2110                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 0     |                                                            |
| 445                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                                            |
| 2115                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 27    | ITS = 1,258<br>PL(A) = 912<br>SLK = Type I<br>UCS = 19,550 |
| 440                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                                            |
| 2120                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                                            |
| 435                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 25    |                                                            |
| 2125                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                                            |
| 430                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                                            |
| 2130                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 88             | 32    |                                                            |
| 425                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                                            |
| 2134                | CORE LOSS                   |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                                            |

BORING TYPE: HQ3  
HOLE DEPTH (ft): 3014.7  
REMARKS: \_\_\_\_\_

DRILLER: CruX  
WATER OBSERVATIONS: 711 ft.

LOGGED BY: Chris Messenger  
CASING: HW to 171 ft.

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                  |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|----------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type ___) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)       |
| W                                 | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)       |

(Continued Next Page)



CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2556.7

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2154809.152

DATE: 8/5/2023 - 10/21/2023

PROJECT LOCATION: Rosamod, CA

EASTING: 6514431.756

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities          |                        | Sampling & In Situ Testing |                |       |                            |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|--------------------------|------------------------|----------------------------|----------------|-------|----------------------------|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments |
| 2135.4              |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 420                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 2140                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 415                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 2145                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 410                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 2150                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 405                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 2155                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 400                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 2160                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 395                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 2165                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 390                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |

BORING TYPE: HQ3

DRILLER: Crux

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 3014.7

WATER OBSERVATIONS: 711 ft.

CASING: HW to 171 ft.

REMARKS: \_\_\_\_\_

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                         |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|-----------------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type <u>  </u> ) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)              |
| WL                                | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)              |

(Continued Next Page)



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PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2154809.152

DATE: 8/5/2023 - 10/21/2023

PROJECT LOCATION: Rosamod, CA

EASTING: 6514431.756

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities                                                |                        | Sampling & In Situ Testing |                |       |                            |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|----------------------------------------------------------------|------------------------|----------------------------|----------------|-------|----------------------------|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear                                       | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments |
| 385                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                                |                        |                            |                |       |                            |
| 2175                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                                |                        | C                          | 100            | 0     | ITS = 600<br>PL(A) = 349   |
| 360                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                                |                        | C                          | 100            | 31    |                            |
| 2180                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                                |                        |                            |                |       |                            |
| 2182                | CORE LOSS                   |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                                |                        |                            |                |       |                            |
| 2183                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2183' to 2187':<br>Rubble                                 |                        | C                          | 56             | 0     |                            |
| 2185                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                                |                        | C                          | 100            | 0     |                            |
| 370                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                                |                        |                            |                |       | SLK = Type II              |
| 2190                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2188.4' to 2189.3':<br>90° Planar smooth                  |                        | C                          | 100            | 19    | UCS = 3,583                |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2190': 67° Undulating<br>smooth                                |                        |                            |                |       |                            |
| 365                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2192.15' to 2193':<br>49°-51°-78° Undulating<br>rough     |                        |                            |                |       | ITS = 478                  |
| 2195                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2193.5': 61° Undulating<br>rough                               |                        |                            |                |       | PL(A) = 190                |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2193.6' to 2196':<br>Rubble                               |                        | C                          | 100            | 31    |                            |
| 360                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2196.5' to 2197':<br>(3) 17°-21°-39°<br>Undulating rough  |                        |                            |                |       |                            |
| 2200                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2197' to 2198':<br>Rubble                                 |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2198.6' to 2199.3':<br>S. undulating stepped<br>rough 81° |                        | C                          | 100            | 0     |                            |
| 355                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2199.3' to 2207':<br>Rubble, 90° stress                   |                        |                            |                |       |                            |

BORING TYPE: HQ3

DRILLER: Crux

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 3014.7

WATER OBSERVATIONS: 711 ft.

CASING: HW to 171 ft.

REMARKS: \_\_\_\_\_

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                    |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|------------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type _____) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)         |
| L                                 | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)         |

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**SURFACE ELEVATION (ft):** 2556.7

**PROJECT No:** 951-20

**PROJECT:** Hydrostor Zevsar

**NORTHING:** 2154809.152

**DATE:** 8/5/2023 - 10/21/2023

**PROJECT LOCATION:** Rosamod, CA

**EASTING:** 6514431.756

DIP/AZIMUTH: -90 /

[illegible]

**BORING TYPE:** HQ3

**DRILLER:** Crux

**LOGGED BY:** Chris Messenger

HOLE DEPTH (ft): 3014.7

**WATER OBSERVATIONS:** 711 ft.

**CASING:** HW to 171 ft.

REMARKS:

| SAMPLING & IN SITU TESTING LEGEND |               |        |                                                  |
|-----------------------------------|---------------|--------|--------------------------------------------------|
| C                                 | Core drilling | ITS    | Indirect tensile strength (Brazilian) test (psi) |
| W                                 | Water seep    | SLK    | Slake durability test (Type _____)               |
| W                                 | Water level   | TRI    | Triaxial stress test (psi)                       |
|                                   |               | PLA(I) | Point load axial test (s(50) (psi)               |
|                                   |               | PL(D)  | Point load diametral test (s(50) (psi)           |
|                                   |               | UCS    | Uniaxial stress test (psi)                       |

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| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata                                                                                                                                 | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities          |                        | Sampling & In Situ Testing |                |       |                            |
|---------------------|-------------------------------------------------------------------------------------------------------------------------------------------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|--------------------------|------------------------|----------------------------|----------------|-------|----------------------------|
|                     |                                                                                                                                                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments |
| 2241                | QTZ MONZONITE, light gray to white, phaneritic, massive, with K-Na-Ca rich feldspar, quartz, hornblende, and biotite, trace muscovite, chlorite, and pyrite |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 315                 |                                                                                                                                                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 2245                |                                                                                                                                                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 310                 |                                                                                                                                                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 2250                |                                                                                                                                                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 305                 |                                                                                                                                                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 2255                |                                                                                                                                                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 300                 |                                                                                                                                                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 2260                |                                                                                                                                                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 295                 |                                                                                                                                                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 2265                |                                                                                                                                                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 290                 |                                                                                                                                                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 2270                |                                                                                                                                                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 285                 |                                                                                                                                                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |

**BORING TYPE:** HQ3  
**HOLE DEPTH (ft):** 3014.7  
**REMARKS:**

**DRILLER:** Crux  
**WATER OBSERVATIONS:** 711 ft.

**LOGGED BY:** Chris Messenger  
**CASING:** HW to 171 ft.

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                  |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|----------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type ___) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)       |
| WL                                | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)       |

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| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities          |                        | Sampling & In Situ Testing |                |       |                                                            |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|--------------------------|------------------------|----------------------------|----------------|-------|------------------------------------------------------------|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments                                 |
| 280                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       | ITS = 816                                                  |
| 2280                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 54    | SLK = Type I                                               |
| 275                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       | UCS = 19,470                                               |
| 2285                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                                            |
| 270                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 27    |                                                            |
| 2290                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                                            |
| 265                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 43    |                                                            |
| 2295                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                                            |
| 260                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                                            |
| 2298.8              | CORE LOSS                   |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 19             | 0     |                                                            |
| 2300                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                                            |
| 255                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                                            |
| 2305                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                                            |
| 2306.0              |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 75    | ITS = 1,393<br>PL(A) = 695<br>SLK = Type I<br>UCS = 15,069 |
| 250                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                                            |

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**HOLE DEPTH (ft):** 3014.7  
**REMARKS:**

**DRILLER:** Crux  
**WATER OBSERVATIONS:** 711 ft.

**LOGGED BY:** Chris Messenger  
**CASING:** HW to 171 ft.

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                  |
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| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type ___) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)       |
| W                                 | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)       |

(Continued Next Page)

**CLIENT:** Lane Power & Energy Solutions

**SURFACE ELEVATION (ft):** 2556.7

**PROJECT No:** 951-20

**PROJECT:** Hydrostor Zevsar

**NORTHING:** 2154809.152

**DATE:** 8/5/2023 - 10/21/2023

**PROJECT LOCATION:** Rosamod, CA

**EASTING:** 6514431.756

DIP/AZIMUTH: -90 /

[illegible]

**BORING TYPE:** HQ3

**DRILLER:** Crux

**LOGGED BY:** Chris Messenger

**HOLE DEPTH (ft):** 3014.7

WATER OBSERVATIONS: 711 ft.

**CASING:** HW to 171 ft.

REMARKS:

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |
|-----------------------------------|---------------|-------|--------------------------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) |
| W                                 | Water seep    | PL(A) | Point load axial test 1s(50) (psi)               |
| W                                 | Water level   | PL(D) | Point load diametral test 1s(50) (psi)           |
|                                   |               | SLK   | Slake durability test (Type _____)               |
|                                   |               | TRI   | Triaxial stress test (psi)                       |
|                                   |               | UCS   | Uniaxial stress test (psi)                       |

(Continued Next Page)



CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2556.7

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2154809.152

DATE: 8/5/2023 - 10/21/2023

PROJECT LOCATION: Rosamod, CA

EASTING: 6514431.756

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities                                       |                        | Sampling & In Situ Testing |                |       |                                              |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|-------------------------------------------------------|------------------------|----------------------------|----------------|-------|----------------------------------------------|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear                              | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments                   |
| 210                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | (7) Undulating rough                                  |                        |                            |                |       |                                              |
| 2350                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2347': 42°                                            |                        |                            |                |       |                                              |
| 205                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2349' to 2350': (3)<br>20°-24° Planar smooth     |                        | C                          | 100            | 73    | ITS = 1,265<br>PL(A) = 1,014<br>UCS = 18,181 |
| 2355                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2350' to 2359':<br>61°-74° Planar smooth<br>Ca+2 |                        |                            |                |       |                                              |
| 200                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2354.3': 7° Undulating<br>rough, K feldspar           |                        |                            |                |       |                                              |
| 2360                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2357': 79° S. undulating<br>rough                     |                        | C                          | 100            | 10    | SLK = Type I                                 |
| 195                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2361.9': 45° Planar<br>smooth                         |                        |                            |                |       |                                              |
| 2365                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2362.2' to 2367.6':<br>Stepped 38°-42° wedge     |                        |                            |                |       |                                              |
| 190                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2363.3' to 2366':<br>90° Planar smooth S.        |                        |                            |                |       |                                              |
| 2369                | PEGMATITE DIKE              |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2369.2': Planar smooth                                |                        | C                          | 94             | 74    |                                              |
| 2369.8              | CORE LOSS                   |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                       |                        |                            |                |       |                                              |
| 2370                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                       |                        |                            |                |       |                                              |
| 185                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2372.1': 2° Planar<br>smooth                          |                        | C                          | 100            | 51    |                                              |
| 2375                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2372.9': 3° Planar<br>smooth                          |                        |                            |                |       |                                              |
| 180                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2375' to 2375.45':<br>84° Undulating rough       |                        |                            |                |       |                                              |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2375.9': 80° Undulating<br>rough                      |                        |                            |                |       |                                              |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2378': 49° Undulating<br>smooth                       |                        |                            |                |       |                                              |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2379': 38° Planar<br>smooth                           |                        | C                          | 100            | 54    |                                              |

BORING TYPE: HQ3

DRILLER: Crux

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 3014.7

WATER OBSERVATIONS: 711 ft.

CASING: HW to 171 ft.

REMARKS: \_\_\_\_\_

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                    |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|------------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type _____) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)         |
| WL                                | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)         |

(Continued Next Page)



**CLIENT:** Lane Power & Energy Solutions  
**PROJECT:** Hydrostor Zevsar  
**PROJECT LOCATION:** Rosamod, CA

**SURFACE ELEVATION (ft):** 2556.7  
**NORTHING:** 2154809.152  
**EASTING:** 6514431.756

**PROJECT No:** 951-20  
**DATE:** 8/5/2023 - 10/21/2023  
**DIP/AZIMUTH:** -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities          |                        | Sampling & In Situ Testing |                |       |                               |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|--------------------------|------------------------|----------------------------|----------------|-------|-------------------------------|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments    |
| 175                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                               |
| 2385                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       | ITS = 1,521<br>UCS = 17,945   |
| 170                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                               |
| 2390                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 31    | PL(A) = 1,180<br>SLK = Type I |
| 165                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                               |
| 2395                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                               |
| 160                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                               |
| 2400                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 90    |                               |
| 155                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                               |
| 2405                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                               |
| 150                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                               |
| 2410                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 0     |                               |
| 145                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       | ITS = 491<br>UCS = 15,661     |

**BORING TYPE:** HQ3  
**HOLE DEPTH (ft):** 3014.7  
**REMARKS:**

**DRILLER:** Crux  
**WATER OBSERVATIONS:** 711 ft.

**LOGGED BY:** Chris Messenger  
**CASING:** HW to 171 ft.

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                  |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|----------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type ___) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)       |
| WL                                | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)       |

(Continued Next Page)



CLIENT: Lane Power & Energy Solutions  
PROJECT: Hydrostor Zevsar  
PROJECT LOCATION: Rosamod, CA

SURFACE ELEVATION (ft): 2556.7  
NORTHING: 2154809.152  
EASTING: 6514431.756

PROJECT No: 951-20  
DATE: 8/5/2023 - 10/21/2023  
DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities          |                        | Sampling & In Situ Testing |                |       |                            |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|--------------------------|------------------------|----------------------------|----------------|-------|----------------------------|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments |
| 140                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| -2420               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| -2425               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| -2430               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| -2435               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| -2440               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| -2445               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |

BORING TYPE: HQ3  
HOLE DEPTH (ft): 3014.7  
REMARKS:

DRILLER: Crux  
WATER OBSERVATIONS: 711 ft.

LOGGED BY: Chris Messenger  
CASING: HW to 171 ft.

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                         |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|-----------------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type <u>  </u> ) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)              |
| W                                 | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)              |

(Continued Next Page)





**CLIENT:** Lane Power & Energy Solutions  
**PROJECT:** Hydrostor Zevsar  
**PROJECT LOCATION:** Rosamod, CA

**SURFACE ELEVATION (ft):** 2556.7  
**NORTHING:** 2154809.152  
**EASTING:** 6514431.756

**PROJECT No:** 951-20  
**DATE:** 8/5/2023 - 10/21/2023  
**DIP/AZIMUTH:** -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata                             | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities                                           |                        | Sampling & In Situ Testing |                |       |                                              |
|---------------------|---------------------------------------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|-----------------------------------------------------------|------------------------|----------------------------|----------------|-------|----------------------------------------------|
|                     |                                                         | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear                                  | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments                   |
| 105                 |                                                         |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                           |                        |                            |                |       | PL(A) = 161<br>SLK = Type I                  |
| 2455                |                                                         |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | -2454.9': 49° Planar smooth                               |                        |                            |                |       |                                              |
| 100                 |                                                         |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2456' to 2458':<br>90°-45° S. planar smooth          |                        |                            |                |       |                                              |
| 2460                |                                                         |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | -2458.3': 47° Undulating smooth                           |                        | C                          | 100            | 46    | UCS = 7,179                                  |
| 95                  |                                                         |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2460' to 2461':<br>Rubble, 90° stepped rough         |                        |                            |                |       |                                              |
| 2465                |                                                         |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | -2462.1': 71° Undulating rough                            |                        | C                          | 100            | 45    |                                              |
| 90                  |                                                         |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2463' to 2463.1':<br>27°-49° Undulating rough        |                        |                            |                |       |                                              |
| 2470                |                                                         |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2464' to 2466':<br>Stepped 90° S. rough              |                        |                            |                |       | TRI = 30,236<br>TRI = 37,313<br>TRI = 32,387 |
| 85                  |                                                         |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                           |                        |                            |                |       |                                              |
| 2473                | QTZ MONZONITE, light gray to white, phaneritic, massive |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                           |                        |                            |                |       |                                              |
| 2475                |                                                         |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2474' to 2476':<br>Rubble                            |                        |                            |                |       |                                              |
| 80                  |                                                         |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2476.1' to 2477':<br>69° Planar smooth               |                        | C                          | 100            | 12    | PL(A) = 1,220                                |
| 2480                |                                                         |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2479.8' to 2481':<br>(4) 61° Undulating rough        |                        |                            |                |       |                                              |
| 75                  |                                                         |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2481' to 2496':<br>Multiple 74°-90° undulating rough |                        | C                          | 100            | 13    |                                              |

**BORING TYPE:** HQ3  
**HOLE DEPTH (ft):** 3014.7  
**REMARKS:**

**DRILLER:** Crux  
**WATER OBSERVATIONS:** 711 ft.

**LOGGED BY:** Chris Messenger  
**CASING:** HW to 171 ft.

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                               |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|-------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type ) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)    |
| W                                 | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)    |

(Continued Next Page)





CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2556.7

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2154809.152

DATE: 8/5/2023 - 10/21/2023

PROJECT LOCATION: Rosamod, CA

EASTING: 6514431.756

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities          |                        | Sampling & In Situ Testing |                |       |                            |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|--------------------------|------------------------|----------------------------|----------------|-------|----------------------------|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments |
| 70                  |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 2490                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 2490.5              | CORE LOSS                   |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 2490.5              |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 65                  |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 2495                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 2496                | QTZ MONZONITE               |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 60                  |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 2500                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 55                  |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 2505                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 50                  |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 2510                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 45                  |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 2515                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 40                  |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |

BORING TYPE: HQ3

DRILLER: Crux

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 3014.7

WATER OBSERVATIONS: 711 ft.

CASING: HW to 171 ft.

REMARKS: \_\_\_\_\_

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                   |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|-----------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type ____) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)        |
| WL                                | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)        |

(Continued Next Page)



**Agapito Associates, Inc.**  
**ENGINEERS & GEOLOGISTS**

PAGE 73 OF 87

DIP/AZIMUTH: -90 /

**BORING TYPE:** HQ3  
**HOLE DEPTH (ft):** 3014.7  
**REMARKS:** \_\_\_\_\_

**DRILLER:** Crux  
**WATER OBSERVATIONS:** 711 ft.

**LOGGED BY:** Chris Messenger  
**CASING:** HW to 171 ft.

(Continued Next Page)



**CLIENT:** Lane Power & Energy Solutions  
**PROJECT:** Hydrostor Zevsar  
**PROJECT LOCATION:** Rosamod, CA

**SURFACE ELEVATION (ft):** 2556.7  
**NORTHING:** 2154809.152  
**EASTING:** 6514431.756

**PROJECT No:** 951-20  
**DATE:** 8/5/2023 - 10/21/2023  
**DIP/AZIMUTH:** -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities                                                                |                        | Sampling & In Situ Testing |                |       |                            |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|--------------------------------------------------------------------------------|------------------------|----------------------------|----------------|-------|----------------------------|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear                                                       | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments |
| 0                   |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                                                |                        |                            |                |       |                            |
| -2560               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2556.4' to 2559.4':<br>(7) 40°-60° Stress<br>fracture undulating<br>rough |                        | C                          | 100            | 16    | ITS = 1,640                |
| -2565               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2561' to 2565': 90°<br>Undulating rough                                   |                        |                            |                |       | SLK = Type I               |
| -2570               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2567' to 2570': (8)<br>32°-49° Undulating<br>rough                        |                        | C                          | 100            | 14    |                            |
| -2575               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2571' to 2572': 90°<br>Planar smooth                                      |                        |                            |                |       |                            |
| -2580               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2572.6' to 2574':<br>90° Stepped smooth                                   |                        |                            |                |       |                            |
| -2585               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | -2575.3': 46° Planar<br>smooth                                                 |                        | C                          | 100            | 33    | UCS = 19,333               |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | -2577.8': 32° Planar<br>rough                                                  |                        |                            |                |       | PL(A) = 1,342              |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | -2578.7': 45° Stepped<br>smooth                                                |                        |                            |                |       | ITS = 1,232                |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2579.9' to 2580.5':<br>(2) 47° Planar smooth                              |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2581' to 2586':<br>Rubble                                                 |                        | C                          | 100            | 0     |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | -2587.2': 32° Planar<br>smooth                                                 |                        | C                          | 100            | 13    |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | -2587.5': 41° Planar<br>smooth                                                 |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | -2587.8': 67° Planar                                                           |                        |                            |                |       |                            |

**BORING TYPE:** HQ3  
**HOLE DEPTH (ft):** 3014.7  
**REMARKS:** \_\_\_\_\_

**DRILLER:** Crux  
**WATER OBSERVATIONS:** 711 ft.

**LOGGED BY:** Chris Messenger  
**CASING:** HW to 171 ft.

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                   |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|-----------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type ____) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)        |
| WL                                | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)        |

(Continued Next Page)



CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2556.7

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2154809.152

DATE: 8/5/2023 - 10/21/2023

PROJECT LOCATION: Rosamod, CA

EASTING: 6514431.756

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities                                                   |                        | Sampling & In Situ Testing |                |       |                            |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|-------------------------------------------------------------------|------------------------|----------------------------|----------------|-------|----------------------------|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear                                          | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments |
| -35                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | smooth                                                            |                        |                            |                |       |                            |
| -2595               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2588.6' to 2592':<br>80°-90° Vertical S.<br>undulating rough |                        | C                          | 100            | 6     |                            |
| -40                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2592.9' to 2593.5':<br>90° S. undulating planar<br>smooth    |                        |                            |                |       |                            |
| -2600               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2594' to 2596':<br>90°-78° S. undulating<br>rough            |                        |                            |                |       |                            |
| -45                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2596' to 2597':<br>Rubble                                    |                        |                            |                |       |                            |
| -2605               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2599.4': Planar irregular<br>smooth                               |                        | C                          | 100            | 20    |                            |
| -50                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2600' to 2600.7':<br>0° Planar smooth                        |                        |                            |                |       |                            |
| -2610               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2601.5': 74° Planar<br>smooth                                     |                        |                            |                |       |                            |
| -55                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2603.6': 8° Undulating<br>smooth                                  |                        |                            |                |       |                            |
| -2615               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2606' to 2607':<br>Rubble                                    |                        |                            |                |       |                            |
| -60                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2609' to 2610.8':<br>Rubble                                  |                        | C                          | 100            | 100   |                            |
| -2620               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2613.4': 7° Planar<br>smooth                                      |                        |                            |                |       |                            |
| -65                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2613.7': 89° Planar<br>smooth                                     |                        | C                          | 100            | 23    |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2617.9': Planar irregular                                         |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2618.7' to 2620':<br>Rubble                                  |                        | C                          | 100            | 10    |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2621' to 2623':<br>Rubble                                    |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2623.1' to 2625.6':<br>Multiple 90° S. 42° (2)<br>20° smooth |                        |                            |                |       |                            |

PL(A) = 214  
UCS = 3,493  
SLK = Type II

BORING TYPE: HQ3

DRILLER: Crux

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 3014.7

WATER OBSERVATIONS: 711 ft.

CASING: HW to 171 ft.

REMARKS: \_\_\_\_\_

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                  |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|----------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type ___) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)       |
| W                                 | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)       |

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CLIENT: Lane Power & Energy Solutions  
PROJECT: Hydrostor Zevsar  
PROJECT LOCATION: Rosamod, CA

SURFACE ELEVATION (ft): 2556.7  
NORTHING: 2154809.152  
EASTING: 6514431.756

PROJECT No: 951-20  
DATE: 8/5/2023 - 10/21/2023  
DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities                                                      |                        | Sampling & In Situ Testing |                |       |                              |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|----------------------------------------------------------------------|------------------------|----------------------------|----------------|-------|------------------------------|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear                                             | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments   |
| -70                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2626.4' to 2629':<br>Rubble                                     |                        | C                          | 100            | 0     | PL(A) = 441                  |
| -2630               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2629.35': 7° Planar<br>smooth                                        |                        | C                          | 100            | 19    |                              |
| -75                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2629.65': 13° Planar<br>smooth                                       |                        |                            |                |       |                              |
| -2635               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2629.85': 32° Planar<br>smooth                                       |                        |                            |                |       |                              |
| -80                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2630': 22° Planar rough                                              |                        |                            |                |       |                              |
| -2640               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2630.25' to 2631':<br>79° Planar smooth                         |                        |                            |                |       | SLK = Type I<br>UCS = 22,748 |
| -85                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2631.45': 22° Planar<br>smooth                                       |                        |                            |                |       |                              |
| -2645               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2632.9' to 2633.7':<br>90° Undulating rough                     |                        | C                          | 100            | 18    |                              |
| -90                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2634.1': 22° Planar<br>smooth                                        |                        |                            |                |       |                              |
| -2650               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2635' to 2636': (2)<br>38° Planar smooth                        |                        |                            |                |       |                              |
| -95                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2636.5' to 2639':<br>90° Undulating rough,<br>healed and open K |                        |                            |                |       | ITS = 1,535<br>PL(A) = 913   |
| -2655               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2640': 42° Planar<br>smooth                                          |                        |                            |                |       |                              |
| -100                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2641' to 2642.2':<br>(3) 0° Planar smooth                       |                        |                            |                |       |                              |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2644.72' to 2646':<br>Rubble                                    |                        |                            |                |       |                              |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2646.1' to 2648':<br>(4) 0° Planar smooth/<br>rubble            |                        |                            |                |       |                              |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2646.9' to 2652.2':<br>(6) 50°-67° Planar<br>smooth             |                        | C                          | 100            | 13    | ITS = 1,535<br>PL(A) = 913   |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2652.5' to 2653.7':<br>90° S. planar smooth,<br>mineralized     |                        |                            |                |       |                              |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2654': 3° Planar smooth                                              |                        | C                          | 100            | 25    |                              |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2654.9': 3° Planar<br>smooth                                         |                        |                            |                |       |                              |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2655' to 2656.4':<br>Rubble                                     |                        |                            |                |       |                              |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2657': 71° Undulating<br>smooth                                      |                        |                            |                |       | ITS = 1,535<br>PL(A) = 913   |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2658' to 2659.6':<br>Multiple 90° undulating                    |                        | C                          | 100            | 48    |                              |

BORING TYPE: HQ3  
HOLE DEPTH (ft): 3014.7  
REMARKS: \_\_\_\_\_

DRILLER: Crux  
WATER OBSERVATIONS: 711 ft.

LOGGED BY: Chris Messenger  
CASING: HW to 171 ft.

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                    |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|------------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type _____) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)         |
| W                                 | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)         |

(Continued Next Page)



**CLIENT:** Lane Power & Energy Solutions  
**PROJECT:** Hydrostor Zevsar  
**PROJECT LOCATION:** Rosamod, CA

**SURFACE ELEVATION (ft):** 2556.7  
**NORTHING:** 2154809.152  
**EASTING:** 6514431.756

**PROJECT No:** 951-20  
**DATE:** 8/5/2023 - 10/21/2023  
**DIP/AZIMUTH:** -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities                                                        |                        | Sampling & In Situ Testing |                |       |                             |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|------------------------------------------------------------------------|------------------------|----------------------------|----------------|-------|-----------------------------|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear                                               | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments  |
| -105'               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | Fractures                                                              |                        |                            |                |       |                             |
| -2665               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2660' to 2661':<br>Rubble                                         |                        |                            |                |       |                             |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2661.5': 67° Planar<br>smooth                                          |                        |                            |                |       |                             |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2664' to 2666': (3)<br>50°-60° Planar smooth                      |                        | C                          | 100            | 65    |                             |
| -2670               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2667': 57° Planar<br>smooth                                            |                        |                            |                |       |                             |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2668.5': 66° Undulating<br>smooth                                      |                        |                            |                |       |                             |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2670': 69° Planar<br>smooth/ undulating                                |                        |                            |                |       |                             |
| -2675               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2671' to 2690': (4)<br>60°-70° Planar smooth                      |                        |                            |                |       |                             |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2671.1' to 2672':<br>(3) 38° Planar smooth                        |                        |                            |                |       |                             |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2672.6' to 2673.8':<br>Rubble                                     |                        | C                          | 100            | 43    | SLK = Type I                |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2674.45': 26° Planar<br>smooth                                         |                        |                            |                |       |                             |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2675.9': Planar smooth                                                 |                        |                            |                |       |                             |
| -2680               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2677': 22° Planar<br>smooth                                            |                        |                            |                |       | ITS = 1,405<br>UCS = 22,096 |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2678.7' to 2679':<br>(3) 20°-26° Planar<br>smooth                 |                        | C                          | 100            | 53    |                             |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2680' to 2681':<br>Rubble                                         |                        |                            |                |       |                             |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2681.1' to 2682':<br>90° S. undulating<br>smooth                  |                        |                            |                |       |                             |
| -2685               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2683': 81° Undulating<br>smooth                                        |                        |                            |                |       | PL(A) = 655<br>TRI = 29,762 |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2684': 31° Planar<br>smooth                                            |                        |                            |                |       |                             |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2685.3': 38° Planar<br>smooth                                          |                        |                            |                |       |                             |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2686.5': 13° Planar<br>smooth                                          |                        | C                          | 100            | 44    | TRI = 38,095                |
| -2690               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2687.7': 45° Planar<br>smooth                                          |                        |                            |                |       |                             |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2689': 31° Undulating<br>smooth                                        |                        |                            |                |       |                             |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2691' to 2696': (8)<br>45° Undulating, (7)<br>0°-10° Planar rough |                        |                            |                |       |                             |

**BORING TYPE:** HQ3  
**HOLE DEPTH (ft):** 3014.7  
**REMARKS:**

**DRILLER:** Crux  
**WATER OBSERVATIONS:** 711 ft.

**LOGGED BY:** Chris Messenger  
**CASING:** HW to 171 ft.

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                               |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|-------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type ) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)    |
| W                                 | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)    |

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**CLIENT:** Lane Power & Energy Solutions  
**PROJECT:** Hydrostor Zevsar  
**PROJECT LOCATION:** Rosamod, CA

**SURFACE ELEVATION (ft):** 2556.7  
**NORTHING:** 2154809.152  
**EASTING:** 6514431.756

**PROJECT No:** 951-20  
**DATE:** 8/5/2023 - 10/21/2023  
**DIP/AZIMUTH:** -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities          |                        | Sampling & In Situ Testing |                |       |                                             |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|--------------------------|------------------------|----------------------------|----------------|-------|---------------------------------------------|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments                  |
| -140                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       | IRI = 29,827                                |
| -145                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 17    |                                             |
| -2700               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 14    |                                             |
| -145                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 43    | UCS = 1,014                                 |
| -2705               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 24    |                                             |
| -150                | 2707                        |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       | ITS = 1,481                                 |
| -150                | QTZ MONZONITE               |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                             |
| -2710               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 12    |                                             |
| -155                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 0     |                                             |
| -2715               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 0     |                                             |
| -160                | 2718                        |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 0     | SLK = Type I                                |
| -160                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 53    |                                             |
| -2720               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       | PL(A) = 1,170                               |
| -165                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                             |
| -2725               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 36    | TRI = 17,136<br>TRI = 24,185<br>UCS = 6,744 |
| -170                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                             |

**BORING TYPE:** HQ3  
**HOLE DEPTH (ft):** 3014.7  
**REMARKS:**

**DRILLER:** Crux  
**WATER OBSERVATIONS:** 711 ft.

**LOGGED BY:** Chris Messenger  
**CASING:** HW to 171 ft.

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                  |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|----------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type ___) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)       |
| WL                                | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)       |





**CLIENT:** Lane Power & Energy Solutions  
**PROJECT:** Hydrostor Zevsar  
**PROJECT LOCATION:** Rosamod, CA

**SURFACE ELEVATION (ft):** 2556.7  
**NORTHING:** 2154809.152  
**EASTING:** 6514431.756

**PROJECT No:** 951-20  
**DATE:** 8/5/2023 - 10/21/2023  
**DIP/AZIMUTH:** -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities                                                               |                        | Sampling & In Situ Testing |                |       |                            |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|-------------------------------------------------------------------------------|------------------------|----------------------------|----------------|-------|----------------------------|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear                                                      | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments |
| -175                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | Rubble                                                                        |                        | C                          | 100            | 10    | ITS = 1,053<br>UCS = 8,318 |
| -2735               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2729.4' to 2736':<br>(13) 60°-90° Undulating<br>planar smooth J.         |                        |                            |                |       |                            |
| -180                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2736.1' to 2740':<br>90° Vertical and 79°<br>stepped undulating<br>rough |                        | C                          | 100            | 19    |                            |
| -2740               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2741' to 2742.7':<br>Rubble                                              |                        |                            |                |       | PL(A) = 75                 |
| -185                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                                               |                        | C                          | 100            | 18    |                            |
| -2745               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2746' to 2752':<br>20°-45° and 90°<br>Undulating                         |                        | C                          | 100            | 13    |                            |
| -190                | DIABASE                     |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                                               |                        |                            |                |       | SLK = Type I               |
| -2750               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2751': 69°-74°<br>Undulating smooth                                           |                        |                            |                |       |                            |
| -195                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2753': 90° Stepped<br>smooth                                                  |                        | C                          | 100            | 31    |                            |
| -2755               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2754' to 2755': 90°<br>Healed                                            |                        |                            |                |       | ITS = 542                  |
| -200                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2756' to 2757':<br>Rubble                                                |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2758': 47° Undulating<br>smooth                                               |                        |                            |                |       |                            |
| -2760               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2759' to 2760': 90°<br>S. planar rough                                   |                        | C                          | 100            | 35    |                            |
| -205                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2760': 42° Planar<br>smooth                                                   |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2761' to 2763':<br>Rubble                                                |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2763.1' to 2765':<br>90°-0° Stepped rough                                |                        |                            |                |       |                            |

**BORING TYPE:** HQ3  
**HOLE DEPTH (ft):** 3014.7  
**REMARKS:**

**DRILLER:** Crux  
**WATER OBSERVATIONS:** 711 ft.

**LOGGED BY:** Chris Messenger  
**CASING:** HW to 171 ft.

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                  |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|----------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type ___) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)       |
| W                                 | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)       |

(Continued Next Page)





CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2556.7

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2154809.152

DATE: 8/5/2023 - 10/21/2023

PROJECT LOCATION: Rosamod, CA

EASTING: 6514431.756

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata                       | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities          |                        | Sampling & In Situ Testing |                |       |                            |
|---------------------|---------------------------------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|--------------------------|------------------------|----------------------------|----------------|-------|----------------------------|
|                     |                                                   | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments |
| 2768<br>-210        | QTZ MONZONITE, light gray,<br>phaneritic, massive |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| -2770               |                                                   |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 33    |                            |
| -2775               |                                                   |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 35    |                            |
| -2780               |                                                   |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 0     |                            |
| -2785               |                                                   |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 39    | TRI = 2,732                |
| -2790               |                                                   |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 34    |                            |
| -2795               |                                                   |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 46    |                            |
| -2800               |                                                   |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       | SLK = Type II              |

BORING TYPE: HQ3

DRILLER: CruX

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 3014.7

WATER OBSERVATIONS: 711 ft.

CASING: HW to 171 ft.

REMARKS: \_\_\_\_\_

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                 |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|---------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type II) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)      |
| WL                                | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)      |

(Continued Next Page)



CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2556.7

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2154809.152

DATE: 8/5/2023 - 10/21/2023

PROJECT LOCATION: Rosamod, CA

EASTING: 6514431.756

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata               | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities          |                        | Sampling & In Situ Testing |                |       |                            |
|---------------------|-------------------------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|--------------------------|------------------------|----------------------------|----------------|-------|----------------------------|
|                     |                                           | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments |
| -245                |                                           |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| -2805               |                                           |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 12    |                            |
| -2810               |                                           |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| -2811               | From 2811' to 2826': Chlorite and epidote |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 97             | 23    |                            |
| -2815               |                                           |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| -2815.4             | CORE LOSS                                 |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| -2815.6             |                                           |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| -2820               |                                           |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 27    |                            |
| -2825               |                                           |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 23    |                            |
| -2830               |                                           |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 26    |                            |
| -2835               |                                           |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| -2840               |                                           |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 12    |                            |

BORING TYPE: HQ3

DRILLER: Crux

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 3014.7

WATER OBSERVATIONS: 711 ft.

CASING: HW to 171 ft.

REMARKS: \_\_\_\_\_

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                  |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|----------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type ___) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)       |
| WL                                | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)       |

(Continued Next Page)

**CLIENT:** Lane Power & Energy Solutions

**SURFACE ELEVATION (ft):** 2556.7

**PROJECT No:** 951-20

**PROJECT:** Hydrostor Zevsar

**NORTHING:** 2154809.152

**DATE:** 8/5/2023 - 10/21/2023

**PROJECT LOCATION:** Rosamod, CA

**EASTING:** 6514431.756

DIP/AZIMUTH: -90 /

| EL    | DEPTH<br>(ft) | Description<br>of<br>Strata                                                                                                                                                                                 | Degree of Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture Spacing<br>(ft) |      |      |      | Discontinuities |                          | Sampling & In Situ Testing |               |                |       |
|-------|---------------|-------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|----------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|--------------------------|------|------|------|-----------------|--------------------------|----------------------------|---------------|----------------|-------|
|       |               |                                                                                                                                                                                                             | Fr                   | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       | 0.05                     | 0.25 | 0.50 | 2.50 | 5.00            | B - Bedding<br>S - Shear | J - Joint<br>F- Fault      | Type          | Core<br>Rec. % | RQD % |
| -280' |               | From 2841' to 2861': Calcite, chlorite, and epidote present<br><br>QTZ MONZONITE, light gray to white, phaneritic, with biotite, K-Na-Ca feldspar, and quartz, trace epidote, chlorite, pyrite, and calcite |                      |    |    |    |    |                |               |      |          |      |           |         |       |                          |      |      |      | C               | 100                      | 15                         | PL(A) = 1,033 |                |       |
| -2840 | 2841'         |                                                                                                                                                                                                             |                      |    |    |    |    |                |               |      |          |      |           |         |       |                          |      |      |      | C               | 100                      | 9                          |               |                |       |
| -285' |               |                                                                                                                                                                                                             |                      |    |    |    |    |                |               |      |          |      |           |         |       |                          |      |      |      |                 |                          |                            |               |                |       |
| -2845 |               |                                                                                                                                                                                                             |                      |    |    |    |    |                |               |      |          |      |           |         |       |                          |      |      |      |                 |                          |                            |               |                |       |
| -290' |               |                                                                                                                                                                                                             |                      |    |    |    |    |                |               |      |          |      |           |         |       |                          |      |      |      |                 |                          |                            |               |                |       |
| -2850 |               |                                                                                                                                                                                                             |                      |    |    |    |    |                |               |      |          |      |           |         |       |                          |      |      |      |                 | C                        | 100                        | 22            | PL(A) = 828    |       |
| -295' |               |                                                                                                                                                                                                             |                      |    |    |    |    |                |               |      |          |      |           |         |       |                          |      |      |      |                 |                          |                            |               |                |       |
| -2855 |               |                                                                                                                                                                                                             |                      |    |    |    |    |                |               |      |          |      |           |         |       |                          |      |      |      |                 |                          |                            |               |                |       |
| -300' |               |                                                                                                                                                                                                             |                      |    |    |    |    |                |               |      |          |      |           |         |       |                          |      |      |      |                 | C                        | 100                        | 0             | SLK = Type II  |       |
| -2860 |               |                                                                                                                                                                                                             |                      |    |    |    |    |                |               |      |          |      |           |         |       |                          |      |      |      |                 |                          |                            |               |                |       |
| -305' |               |                                                                                                                                                                                                             |                      |    |    |    |    |                |               |      |          |      |           |         |       |                          |      |      |      | C               | 100                      | 26                         |               |                |       |
| -2865 |               |                                                                                                                                                                                                             |                      |    |    |    |    |                |               |      |          |      |           |         |       |                          |      |      |      |                 |                          |                            |               |                |       |
| -310' |               |                                                                                                                                                                                                             |                      |    |    |    |    |                |               |      |          |      |           |         |       |                          |      |      |      | C               | 100                      | 36                         |               |                |       |

**BORING TYPE:** HQ3

**DRILLER:** Crux

**LOGGED BY:** Chris Messenger

HOLE DEPTH (ft): 3014.7

WATER OBSERVATIONS: 711 ft.

**CASING:** HW to 171 ft.

REMARKS:

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |
|-----------------------------------|---------------|-------|--------------------------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               |
| W                                 | Water level   | PL(D) | Point load diametral test Is(50) (psi)           |
|                                   |               | SLK   | Slake durability test (Type _____)               |
|                                   |               | TRI   | Triaxial stress test (psi)                       |
|                                   |               | UCS   | Uniaxial stress test (psi)                       |

(Continued Next Page)



Agapito Associates, Inc.  
ENGINEERS & GEOLOGISTS

**ZEV-CH-03-23**

PAGE 83 OF 87

**CLIENT:** Lane Power & Energy Solutions  
**PROJECT:** Hydrostor Zevsar  
**PROJECT LOCATION:** Rosamod, CA

**SURFACE ELEVATION (ft):** 2556.7  
**NORTHING:** 2154809.152  
**EASTING:** 6514431.756

**PROJECT No:** 951-20  
**DATE:** 8/5/2023 - 10/21/2023  
**DIP/azimuth:** -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration<br><br>Fr<br>SA<br>MA<br>HA<br>CA | Graphic<br>Log | Rock Strength |      |          |      |           | Water | Fracture<br>Spacing<br>(ft)          | Discontinuities                                                          | Sampling & In Situ Testing                         |                |       | Test Results<br>& Comments |
|---------------------|-----------------------------|-----------------------------------------------------------|----------------|---------------|------|----------|------|-----------|-------|--------------------------------------|--------------------------------------------------------------------------|----------------------------------------------------|----------------|-------|----------------------------|
|                     |                             |                                                           |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard |       |                                      |                                                                          | Type                                               | Core<br>Rec. % | RQD % |                            |
|                     |                             |                                                           |                |               |      |          |      |           |       | 0.05<br>0.25<br>0.50<br>2.50<br>5.00 |                                                                          |                                                    |                |       |                            |
|                     |                             |                                                           |                |               |      |          |      |           |       |                                      | rough                                                                    | B - Bedding<br>S - Shear<br>J - Joint<br>F - Fault |                |       |                            |
|                     |                             |                                                           |                |               |      |          |      |           |       |                                      | 2868.5': J.                                                              |                                                    |                |       |                            |
|                     |                             |                                                           |                |               |      |          |      |           |       |                                      | 2869.9': 20° Planar<br>smooth                                            |                                                    |                |       |                            |
|                     |                             |                                                           |                |               |      |          |      |           |       |                                      | From 2870' to 2870.5':<br>Multiple J.                                    |                                                    |                |       |                            |
|                     |                             |                                                           |                |               |      |          |      |           |       |                                      | 2870.8': 7° Planar<br>smooth                                             |                                                    |                |       |                            |
|                     |                             |                                                           |                |               |      |          |      |           |       |                                      | 2870.9': 10° Undulating<br>smooth                                        | C                                                  | 100            | 59    | UCS = 1,345                |
|                     |                             |                                                           |                |               |      |          |      |           |       |                                      | From 2871' to 2871.5': J.                                                |                                                    |                |       |                            |
|                     |                             |                                                           |                |               |      |          |      |           |       |                                      | From 2872' to 2874':<br>Multiple fractures                               |                                                    |                |       |                            |
|                     |                             |                                                           |                |               |      |          |      |           |       |                                      | From 2874.1' to 2874.8':<br>High K feldspar veining,<br>healed fractures |                                                    |                |       | PL(A) = 35<br>UCS = 1,426  |
|                     |                             |                                                           |                |               |      |          |      |           |       |                                      | 2874.8': 75° Stepped<br>rough                                            |                                                    |                |       |                            |
|                     |                             |                                                           |                |               |      |          |      |           |       |                                      | 2877.8': Planar rough                                                    |                                                    |                |       |                            |
|                     |                             |                                                           |                |               |      |          |      |           |       |                                      | 2878.6': 35° Stepped<br>slickenside                                      |                                                    |                |       |                            |
|                     |                             |                                                           |                |               |      |          |      |           |       |                                      | From 2880' to 2881':<br>Multiple J.                                      |                                                    |                |       |                            |
|                     |                             |                                                           |                |               |      |          |      |           |       |                                      | 2881.1': Planar smooth                                                   | C                                                  | 100            | 29    |                            |
|                     |                             |                                                           |                |               |      |          |      |           |       |                                      | From 2882' to 2883.6':<br>Rubble                                         |                                                    |                |       |                            |
|                     |                             |                                                           |                |               |      |          |      |           |       |                                      | 2884': Planar rough                                                      |                                                    |                |       |                            |
|                     |                             |                                                           |                |               |      |          |      |           |       |                                      | 2884.6': 50° Undulating<br>rough                                         |                                                    |                |       |                            |
|                     |                             |                                                           |                |               |      |          |      |           |       |                                      | From 2884.7' to 2884.9':<br>Rubble                                       |                                                    |                |       |                            |
|                     |                             |                                                           |                |               |      |          |      |           |       |                                      | 2885': 90° S. fracture                                                   |                                                    |                |       |                            |
|                     |                             |                                                           |                |               |      |          |      |           |       |                                      | 2886.6': Planar rough                                                    |                                                    |                |       |                            |
|                     |                             |                                                           |                |               |      |          |      |           |       |                                      | 2886.9': 70° Planar<br>rough                                             |                                                    |                |       |                            |
|                     |                             |                                                           |                |               |      |          |      |           |       |                                      | From 2887' to 2888':<br>Multiple fractures                               |                                                    |                |       |                            |
|                     |                             |                                                           |                |               |      |          |      |           |       |                                      | 2888.5': Planar rough                                                    | C                                                  | 93             | 9     |                            |
|                     |                             |                                                           |                |               |      |          |      |           |       |                                      | From 2889.4' to 2891':<br>Multiple fractures                             |                                                    |                |       |                            |
|                     |                             |                                                           |                |               |      |          |      |           |       |                                      | From 2891.5' to 2891.9':<br>Rubble                                       |                                                    |                |       |                            |
|                     |                             |                                                           |                |               |      |          |      |           |       |                                      | 2892.6': J.                                                              |                                                    |                |       |                            |
|                     |                             |                                                           |                |               |      |          |      |           |       |                                      | 2893.4': 45° Undulating<br>rough                                         |                                                    |                |       |                            |
|                     |                             |                                                           |                |               |      |          |      |           |       |                                      | From 2893.7' to 2901':<br>Multiple fractures planar,<br>S., J., rubble   | C                                                  | 100            | 32    |                            |
|                     |                             |                                                           |                |               |      |          |      |           |       |                                      | 2901.7': Planar smooth                                                   |                                                    |                |       |                            |
|                     |                             |                                                           |                |               |      |          |      |           |       |                                      | 2901.9': 90° S.                                                          |                                                    |                |       |                            |

**BORING TYPE:** HQ3  
**HOLE DEPTH (ft):** 3014.7

**DRILLER:** Cux  
**WATER OBSERVATIONS:** 711 ft.

**LOGGED BY:** Chris Messenger  
**CASING:** HW to 171 ft.

**REMARKS:**

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                          |
|-----------------------------------|---------------|-------|------------------------------------------|
| C                                 | Core drilling | ITS   | Stress durability test (Type <u>  </u> ) |
| W                                 | Water seep    | PL(A) | Point load axial test (lbf/psi)          |
| W                                 | Water level   | PL(D) | Point load diametral test (lbf/psi)      |
|                                   |               | TR    | Triaxial stress test (psi)               |
|                                   |               | UCS   | Uniaxial stress test (psi)               |

(Continued Next Page)



PAGE 84 OF 87

**PROJECT:** Hydrostor Zevsar

SURFACE ELEVATION (ft): 2556.7  
NORTHING: 2154809.152  
EASTING: 6514431.756

PROJECT No: 951-20  
DATE: 8/5/2023 - 10/21/2023  
DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata                                                                                                                              | Degree of<br>Alteration<br><br>Fr<br>SA<br>MA<br>HA<br>CA | Graphic<br>Log | Rock Strength |      |                          |      |           |                | Water | Fracture<br>Spacing<br>(ft) | Discontinuities                       |                        |      | Sampling & In Situ Testing |       |  | Test Results<br>& Comments |
|---------------------|----------------------------------------------------------------------------------------------------------------------------------------------------------|-----------------------------------------------------------|----------------|---------------|------|--------------------------|------|-----------|----------------|-------|-----------------------------|---------------------------------------|------------------------|------|----------------------------|-------|--|----------------------------|
|                     |                                                                                                                                                          |                                                           |                | Very Soft     | Soft | Med-Hard                 | Hard | Very Hard | Ex Hard        |       |                             | B - Bedding<br>S - Shear<br>F - Fault | J - Joint<br>I - Fault | Type | Core<br>Rec. %             | RQD % |  |                            |
| 2935                | QTZ MONZONITE, light gray to white, porphyritic, plagioclase, massive, with biotite, rich Na-Ca K feldspar, trace chlorite, epidote, calcite, and quartz |                                                           |                |               |      | 2928.3: CORE LOSS        |      |           | SLK = Type III |       |                             |                                       |                        |      |                            |       |  |                            |
| 2930                |                                                                                                                                                          |                                                           |                |               |      | 2928.3: J.               | C    | 95        |                |       |                             |                                       |                        |      |                            |       |  | 28                         |
| 2928.3              |                                                                                                                                                          |                                                           |                |               |      | 2928.3: Planar rough     | C    | 100       |                |       |                             |                                       |                        |      |                            |       |  | 20                         |
| 2928.3              |                                                                                                                                                          |                                                           |                |               |      | 2928.3: Undulating rough |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              |                                                                                                                                                          |                                                           |                |               |      | 2928.3: Planar rough     |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              |                                                                                                                                                          |                                                           |                |               |      | 2928.3: Undulating rough |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              |                                                                                                                                                          |                                                           |                |               |      | 2928.3: Planar rough     |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              |                                                                                                                                                          |                                                           |                |               |      | 2928.3: Planar rough     | C    | 100       |                |       |                             |                                       |                        |      |                            |       |  | 19                         |
| 2928.3              |                                                                                                                                                          |                                                           |                |               |      | 2928.3: Undulating rough |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              |                                                                                                                                                          |                                                           |                |               |      | 2928.3: Planar rough     |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     | C                                                         | 100            | 25            |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     | C                                                         | 100            | 20            |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     | C                                                         | 100            | 19            |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     | C                                                         | 100            | 20            |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     | C                                                         | 100            | 20            |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     | C                                                         | 100            | 20            |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     | C                                                         | 100            | 20            |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     | C                                                         | 100            | 20            |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     | C                                                         | 100            | 20            |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     | C                                                         | 100            | 20            |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     | C                                                         | 100            | 20            |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     | C                                                         | 100            | 20            |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     | C                                                         | 100            | 20            |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     | C                                                         | 100            | 20            |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     | C                                                         | 100            | 20            |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     | C                                                         | 100            | 20            |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     | C                                                         | 100            | 20            |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     | C                                                         | 100            | 20            |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     | C                                                         | 100            | 20            |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     | C                                                         | 100            | 20            |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     | C                                                         | 100            | 20            |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     | C                                                         | 100            | 20            |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     | C                                                         | 100            | 20            |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     | C                                                         | 100            | 20            |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     | C                                                         | 100            | 20            |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     | C                                                         | 100            | 20            |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     | C                                                         | 100            | 20            |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     | C                                                         | 100            | 20            |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     | C                                                         | 100            | 20            |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     | C                                                         | 100            | 20            |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     | C                                                         | 100            | 20            |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     | C                                                         | 100            | 20            |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     | C                                                         | 100            | 20            |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     | C                                                         | 100            | 20            |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     | C                                                         | 100            | 20            |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     | C                                                         | 100            | 20            |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     | C                                                         | 100            | 20            |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     | C                                                         | 100            | 20            |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     | C                                                         | 100            | 20            |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     | C                                                         | 100            | 20            |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     | C                                                         | 100            | 20            |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     | C                                                         | 100            | 20            |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     | C                                                         | 100            | 20            |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     | C                                                         | 100            | 20            |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     | C                                                         | 100            | 20            |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     | C                                                         | 100            | 20            |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     | C                                                         | 100            | 20            |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     | C                                                         | 100            | 20            |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     | C                                                         | 100            | 20            |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     | C                                                         | 100            | 20            |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     | C                                                         | 100            | 20            |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     | C                                                         | 100            | 20            |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     | C                                                         | 100            | 20            |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     | C                                                         | 100            | 20            |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     | C                                                         | 100            | 20            |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     | C                                                         | 100            | 20            |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     | C                                                         | 100            | 20            |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     | C                                                         | 100            | 20            |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     | C                                                         | 100            | 20            |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     | C                                                         | 100            | 20            |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     | C                                                         | 100            | 20            |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     | C                                                         | 100            | 20            |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Planar rough                                                                                                                                     |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |
| 2928.3              | 2928.3: Undulating rough                                                                                                                                 |                                                           |                |               |      |                          |      |           |                |       |                             |                                       |                        |      |                            |       |  |                            |

**DRILLER:** Crux

**LOGGED BY:** Chris Messenger

**WATER OBSERVATIONS:** 711 ft.

**CASING:** HW to 171 ft..

**SAMPLING & IN SITU TESTING LEGEND**

| Slake durability test (Type — | Triaxial stress test (psi) | Uniaxial stress test (psi) |
|-------------------------------|----------------------------|----------------------------|
| 1                             | 100                        | 100                        |
| 2                             | 100                        | 100                        |
| 3                             | 100                        | 100                        |
| 4                             | 100                        | 100                        |
| 5                             | 100                        | 100                        |
| 6                             | 100                        | 100                        |
| 7                             | 100                        | 100                        |
| 8                             | 100                        | 100                        |
| 9                             | 100                        | 100                        |
| 10                            | 100                        | 100                        |
| 11                            | 100                        | 100                        |
| 12                            | 100                        | 100                        |
| 13                            | 100                        | 100                        |
| 14                            | 100                        | 100                        |
| 15                            | 100                        | 100                        |
| 16                            | 100                        | 100                        |
| 17                            | 100                        | 100                        |
| 18                            | 100                        | 100                        |
| 19                            | 100                        | 100                        |
| 20                            | 100                        | 100                        |
| 21                            | 100                        | 100                        |
| 22                            | 100                        | 100                        |
| 23                            | 100                        | 100                        |
| 24                            | 100                        | 100                        |
| 25                            | 100                        | 100                        |
| 26                            | 100                        | 100                        |
| 27                            | 100                        | 100                        |
| 28                            | 100                        | 100                        |
| 29                            | 100                        | 100                        |
| 30                            | 100                        | 100                        |
| 31                            | 100                        | 100                        |
| 32                            | 100                        | 100                        |
| 33                            | 100                        | 100                        |
| 34                            | 100                        | 100                        |
| 35                            | 100                        | 100                        |
| 36                            | 100                        | 100                        |
| 37                            | 100                        | 100                        |
| 38                            | 100                        | 100                        |
| 39                            | 100                        | 100                        |
| 40                            | 100                        | 100                        |
| 41                            | 100                        | 100                        |
| 42                            | 100                        | 100                        |
| 43                            | 100                        | 100                        |
| 44                            | 100                        | 100                        |
| 45                            | 100                        | 100                        |
| 46                            | 100                        | 100                        |
| 47                            | 100                        | 100                        |
| 48                            | 100                        | 100                        |
| 49                            | 100                        | 100                        |
| 50                            | 100                        | 100                        |
| 51                            | 100                        | 100                        |
| 52                            | 100                        | 100                        |
| 53                            | 100                        | 100                        |
| 54                            | 100                        | 100                        |
| 55                            | 100                        | 100                        |
| 56                            | 100                        | 100                        |
| 57                            | 100                        | 100                        |
| 58                            | 100                        | 100                        |
| 59                            | 100                        | 100                        |
| 60                            | 100                        | 100                        |
| 61                            | 100                        | 100                        |
| 62                            | 100                        | 100                        |
| 63                            | 100                        | 100                        |
| 64                            | 100                        | 100                        |
| 65                            | 100                        | 100                        |
| 66                            | 100                        | 100                        |
| 67                            | 100                        | 100                        |
| 68                            | 100                        | 100                        |
| 69                            | 100                        | 100                        |
| 70                            | 100                        | 100                        |
| 71                            | 100                        | 100                        |
| 72                            | 100                        | 100                        |
| 73                            | 100                        | 100                        |
| 74                            | 100                        | 100                        |
| 75                            | 100                        | 100                        |
| 76                            | 100                        | 100                        |
| 77                            | 100                        | 100                        |
| 78                            | 100                        | 100                        |
| 79                            | 100                        | 100                        |
| 80                            | 100                        | 100                        |
| 81                            | 100                        | 100                        |
| 82                            | 100                        | 100                        |
| 83                            | 100                        | 100                        |
| 84                            | 100                        | 100                        |
| 85                            | 100                        | 100                        |
| 86                            | 100                        | 100                        |
| 87                            | 100                        | 100                        |
| 88                            | 100                        | 100                        |
| 89                            | 100                        | 100                        |
| 90                            | 100                        | 100                        |
| 91                            | 100                        | 100                        |
| 92                            | 100                        | 100                        |
| 93                            | 100                        | 100                        |
| 94                            | 100                        | 100                        |
| 95                            | 100                        | 100                        |
| 96                            | 100                        | 100                        |
| 97                            | 100                        | 100                        |
| 98                            | 100                        | 100                        |
| 99                            | 100                        | 100                        |
| 100                           | 100                        | 100                        |

(Continued Next Page)

**CLIENT:** Lane Power & Energy Solutions

**SURFACE ELEVATION (ft):** 2556.7

**PROJECT No:** 951-20

**PROJECT:** Hydrostor Zevsar

**NORTHING:** 2154809.152

**DATE:** 8/5/2023 - 10/21/2023

**PROJECT LOCATION:** Rosamod, CA

**EASTING:** 6514431.756

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata                                                                                                                                | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) |                                    |                            | Discontinuities                             |                        | Sampling & In Situ Testing |                |             |                            |
|---------------------|------------------------------------------------------------------------------------------------------------------------------------------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|------------------------------------|----------------------------|---------------------------------------------|------------------------|----------------------------|----------------|-------------|----------------------------|
|                     |                                                                                                                                                            |                         |    |    |    |    |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             |                                    |                            | B - Bedding<br>S - Shear                    | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD %       | Test Results<br>& Comments |
|                     |                                                                                                                                                            | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       | 0.05                        | 0.25                               | 0.50                       | 2.50                                        | 5.00                   |                            |                |             |                            |
| -385'               | QTZ MONZONITE, light gray to white, porphyritic, phaneritic, massive, with biotite, plagioclase feldspar, and quartz, trace chlorite, epidote, and calcite |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                    | 2934.5': 25° Planar smooth |                                             |                        |                            | PL(A) = 565    |             |                            |
|                     |                                                                                                                                                            |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                    |                            | 2934.9': 30° Undulating rough               |                        |                            |                |             |                            |
| -2945               |                                                                                                                                                            |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                    |                            | From 2935' to 2935.2': 90° S.               |                        |                            |                | UCS = 9,375 |                            |
|                     |                                                                                                                                                            |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                    |                            | From 2936' to 2936.5': Rubble               |                        |                            |                |             |                            |
| -390'               |                                                                                                                                                            |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                    |                            | From 2937' to 2939': Rubble                 | C                      | 100                        | 49             | ITS = 1,485 |                            |
|                     |                                                                                                                                                            |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                    |                            | 2939.5': 65° Undulating rough               |                        |                            |                |             |                            |
| -2950               |                                                                                                                                                            |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                    |                            | 2940': 20° Planar smooth                    |                        |                            |                | PL(A) = 308 |                            |
|                     |                                                                                                                                                            |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                    |                            | From 2940.1' to 2941': Multiple breaks      |                        |                            |                |             |                            |
| -395'               |                                                                                                                                                            |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                    |                            | 2941.8': 25° Planar rough                   |                        |                            |                |             |                            |
|                     |                                                                                                                                                            |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                    |                            | 2942.5': 70° Planar rough                   |                        |                            |                |             |                            |
| -2955               |                                                                                                                                                            |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                    |                            | 2943.2': 65° Planar smooth                  |                        |                            |                |             |                            |
|                     |                                                                                                                                                            |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                    |                            | From 2944' to 2945': J.                     |                        |                            |                |             |                            |
| -400'               |                                                                                                                                                            |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                    |                            | 2945.1': Planar rough                       | C                      | 100                        | 35             |             |                            |
|                     |                                                                                                                                                            |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                    |                            | 2947.2': Planar rough                       |                        |                            |                |             |                            |
| -2960               |                                                                                                                                                            |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                    |                            | 2947.4': 60° Planar smooth and J.           |                        |                            |                |             |                            |
|                     |                                                                                                                                                            |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                    |                            | 2948': 35° Planar rough                     |                        |                            |                |             |                            |
| -405'               |                                                                                                                                                            |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                    |                            | 2948.6': 50° Planar rough, slightly stepped |                        |                            |                |             |                            |
|                     |                                                                                                                                                            |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                    |                            | 2949.3': Planar rough                       | C                      | 100                        | 59             |             |                            |
| -2965               |                                                                                                                                                            |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                    |                            | 2950': 55° Undulating rough                 |                        |                            |                |             |                            |
|                     |                                                                                                                                                            |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                    |                            | From 2950.3' to 2951': Rubble               |                        |                            |                |             |                            |
| -410'               | 2968                                                                                                                                                       |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2951.8': 50° Undulating rough      |                            |                                             |                        |                            |                |             |                            |
|                     |                                                                                                                                                            |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2952.3': Planar smooth             |                            |                                             |                        |                            |                |             |                            |
| -2970               |                                                                                                                                                            |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2952.6': J.                        |                            |                                             |                        |                            |                |             |                            |
|                     |                                                                                                                                                            |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2952.8': 40° Undulating            | C                          | 100                                         | 15                     |                            |                |             |                            |
| -415'               |                                                                                                                                                            |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2953': Planar rough                |                            |                                             |                        |                            |                |             |                            |
|                     |                                                                                                                                                            |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2953.6': Planar rough              |                            |                                             |                        |                            |                |             |                            |
|                     |                                                                                                                                                            |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2953.9': 50° Planar rough          |                            |                                             |                        |                            |                |             |                            |
|                     |                                                                                                                                                            |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2954.2': 35° Planar rough          |                            |                                             |                        |                            |                |             |                            |
|                     |                                                                                                                                                            |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2954.9': 35° Planar rough          | C                          | 100                                         | 0                      |                            |                |             |                            |
|                     |                                                                                                                                                            |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2955.3' to 2956': Multiple J. |                            |                                             |                        |                            |                |             |                            |

**BORING TYPE:** HQ3

**DRILLER:** Crux

**LOGGED BY:** Chris Messenger

**HOLE DEPTH (ft):** 3014.7

WATER OBSERVATIONS: 711 ft.

**CASING:** HW to 171 ft.

REMARKS:

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |
|-----------------------------------|---------------|-------|--------------------------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) |
| W                                 | Water seep    | PL(A) | Point load axial test 1s(50) (psi)               |
| W                                 | Water level   | PL(D) | Point load diametral test 1s(50) (psi)           |
|                                   |               | SLK   | Slake durability test (Type _____)               |
|                                   |               | TRI   | Triaxial stress test (psi)                       |
|                                   |               | UCS   | Uniaxial stress test (psi)                       |

(Continued Next Page)



CLIENT: Lane Power & Energy Solutions  
PROJECT: Hydrostor Zevsar  
PROJECT LOCATION: Rosamod, CA

SURFACE ELEVATION (ft): 2556.7  
NORTHING: 2154809.152  
EASTING: 6514431.756

PROJECT No: 951-20  
DATE: 8/5/2023 - 10/21/2023  
DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities                                                    |                        | Sampling & In Situ Testing |                |       |                              |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|--------------------------------------------------------------------|------------------------|----------------------------|----------------|-------|------------------------------|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear                                           | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments   |
| -420                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2956.5': Planar rough                                              |                        |                            |                |       | SLK = Type I<br>UCS = 15,773 |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2956.8': J.                                                        |                        |                            |                |       |                              |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2957.8': 60° Undulating rough                                      |                        |                            |                |       |                              |
| -2980               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2958' to 2961': Multiple 60° fractures, 20°-30° planar smooth |                        | C                          | 100            | 13    |                              |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2968.8' to 2969.1': Multiple J.                               |                        |                            |                |       |                              |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2969.6': 30° Undulating rough                                      |                        | C                          | 100            | 14    |                              |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2969.7': 30° Undulating rough                                      |                        |                            |                |       |                              |
| -2985               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2970' to 2972.4': Rubble                                      |                        |                            |                |       |                              |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2972.7': 79° S.                                                    |                        |                            |                |       |                              |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2973': Multiple fractures                                          |                        |                            |                |       |                              |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2973.1' to 2974': Multiple J., 55° planar rough               |                        |                            |                |       |                              |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2974.5' to 2976': Rubble                                      |                        |                            |                |       |                              |
| -2990               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2976.1' to 2976.8': Rubble                                    |                        | C                          | 100            | 31    |                              |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2977': 20° Planar smooth                                           |                        |                            |                |       |                              |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2977.1' to 2977.5': Rubble                                    |                        |                            |                |       |                              |
| -2995               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2977.8': 50° Undulating rough                                      |                        | C                          | 100            | 20    |                              |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2978.3': 25° Planar smooth                                         |                        |                            |                |       |                              |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2978.7': 40° Planar smooth                                         |                        |                            |                |       |                              |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2979' to 2981': Rubble                                        |                        |                            |                |       |                              |
| -3000               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2981.9': 60° Planar rough                                          |                        |                            |                |       |                              |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2982.2': Planar rough                                              |                        |                            |                |       |                              |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2982.5' to 2983': Rubble                                      |                        | C                          | 100            | 0     |                              |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2983' to 2991': Rubble                                        |                        | C                          | 100            | 8     |                              |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2983.5': 30° Planar rough                                          |                        |                            |                |       |                              |
| -3005               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2991.1' to 2993': Rubble                                      |                        |                            |                |       |                              |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2993.1': 40° Undulating slickenside                                |                        | C                          | 100            | 25    |                              |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2994': J.                                                          |                        |                            |                |       |                              |
| -450                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2994.1' to 2995': Rubble                                      |                        |                            |                |       |                              |

BORING TYPE: HQ3  
HOLE DEPTH (ft): 3014.7  
REMARKS: \_\_\_\_\_

DRILLER: Crux  
WATER OBSERVATIONS: 711 ft.

LOGGED BY: Chris Messenger  
CASING: HW to 171 ft.

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                   |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|-----------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type ____) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)        |
| W                                 | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)        |

(Continued Next Page)



CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2556.7

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2154809.152

DATE: 8/5/2023 - 10/21/2023

PROJECT LOCATION: Rosamod, CA

EASTING: 6514431.756

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) |                        |      |                | Discontinuities |                            | Sampling & In Situ Testing |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |    |
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|                     |                             |                         |    |    |    |    |                | Rock Strength |      |          |      |           |         |       |                             |                        |      |                |                 |                            | Sampling & In Situ Testing |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |    |
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       | B - Bedding<br>S - Shear    | J - Joint<br>F - Fault | Type | Core<br>Rec. % | RQD %           | Test Results<br>& Comments |                            |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |    |
| -455'               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                        |      |                |                 |                            |                            |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | </ |

Bottom of borehole at 3014.7 feet.

BORING TYPE: HQ3

DRILLER: Crux

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 3014.7

WATER OBSERVATIONS: 711 ft.

CASING: HW to 171 ft.

REMARKS: \_\_\_\_\_

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                    |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|------------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type _____) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)         |
| W                                 | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)         |





CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2542.7

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2153909.161

DATE: 1/23/2024 - 3/21/2024

PROJECT LOCATION: Rosamod, CA

EASTING: 6515965.764

DIP/AZIMUTH: -90 /

| EL | DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities          |                        | Sampling & In Situ Testing |                |       |                            |
|----|---------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|--------------------------|------------------------|----------------------------|----------------|-------|----------------------------|
|    |               |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments |
|    | 0             | Well Casing                 |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
|    | 5             |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
|    | 10            |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
|    | 15            |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
|    | 20            |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
|    | 25            |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
|    | 30            |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |

BORING TYPE: HQ3

DRILLER: CruX

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 2581

WATER OBSERVATIONS: 241 ft, 811 ft, 2336 ft.

CASING: HW to 76 ft.

REMARKS: \_\_\_\_\_

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                         |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|-----------------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type <u>  </u> ) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)              |
| WL                                | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)              |



CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2542.7

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2153909.161

DATE: 1/23/2024 - 3/21/2024

PROJECT LOCATION: Rosamod, CA

EASTING: 6515965.764

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities          |                        | Sampling & In Situ Testing |                |       |                            |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|--------------------------|------------------------|----------------------------|----------------|-------|----------------------------|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments |
| 2505<br>40          |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 2500<br>45          |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 2495<br>50          |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 2490<br>55          |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 2485<br>60          |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 2480<br>65          |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 2475                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |

BORING TYPE: HQ3

DRILLER: CruX

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 2581

WATER OBSERVATIONS: 241 ft, 811 ft, 2336 ft.

CASING: HW to 76 ft.

REMARKS: \_\_\_\_\_

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                         |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|-----------------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type <u>  </u> ) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)              |
| WL                                | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)              |



CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2542.7

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2153909.161

DATE: 1/23/2024 - 3/21/2024

PROJECT LOCATION: Rosamod, CA

EASTING: 6515965.764

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log                                                                      | Rock Strength |          |          |           |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities          |                       | Sampling & In Situ Testing |                |       |                            |  |
|---------------------|-----------------------------|-------------------------|----|----|----|----|-------------------------------------------------------------------------------------|---------------|----------|----------|-----------|-----------|---------|-------|-----------------------------|--------------------------|-----------------------|----------------------------|----------------|-------|----------------------------|--|
|                     |                             |                         |    |    |    |    |                                                                                     | Very Soft     | Soft     | Med-Hard | Hard      | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear | J - Joint<br>F- Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments |  |
|                     |                             | Fr                      | SA | MA | HA | CA | Very Soft                                                                           | Soft          | Med-Hard | Hard     | Very Hard | Ex Hard   | 0.05    | 0.25  | 0.50                        | 2.50                     | 5.00                  |                            |                |       |                            |  |
| 2470                |                             |                         |    |    |    |    |                                                                                     |               |          |          |           |           |         |       |                             |                          |                       |                            |                |       |                            |  |
| 75                  |                             |                         |    |    |    |    |                                                                                     |               |          |          |           |           |         |       |                             |                          |                       |                            |                |       |                            |  |
| 76                  | QTZ MONZONITE               |                         |    |    |    |    |    |               |          |          |           |           |         |       |                             |                          |                       |                            | C              | 0     | 11                         |  |
| 80                  | CORE LOSS                   |                         |    |    |    |    |                                                                                     |               |          |          |           |           |         |       |                             |                          |                       |                            |                |       |                            |  |
| 85                  |                             |                         |    |    |    |    |                                                                                     |               |          |          |           |           |         |       |                             |                          |                       |                            |                |       |                            |  |
| 90                  |                             |                         |    |    |    |    |                                                                                     |               |          |          |           |           |         |       |                             |                          |                       |                            | C              | 0     | 6                          |  |
| 95                  |                             |                         |    |    |    |    |                                                                                     |               |          |          |           |           |         |       |                             |                          |                       |                            |                |       |                            |  |
| 97.9                |                             |                         |    |    |    |    |  |               |          |          |           |           |         |       |                             |                          |                       |                            | C              | 31    | 0                          |  |
| 101                 | CORE LOSS                   |                         |    |    |    |    |                                                                                     |               |          |          |           |           |         |       |                             |                          |                       |                            |                |       |                            |  |
| 2440                |                             |                         |    |    |    |    |                                                                                     |               |          |          |           |           |         |       |                             |                          |                       |                            |                |       |                            |  |

BORING TYPE: HQ3

DRILLER: Crux

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 2581

WATER OBSERVATIONS: 241 ft, 811 ft, 2336 ft.

CASING: HW to 76 ft.

REMARKS: \_\_\_\_\_

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                         |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|-----------------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type <u>  </u> ) |
|                                   | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)              |
|                                   | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)              |

(Continued Next Page)

**CLIENT:** Lane Power & Energy Solutions

**SURFACE ELEVATION (ft):** 2542.7

**PROJECT No:** 951-20

**PROJECT:** Hydrostor Zevsar

**NORTHING:** 2153909.161

**DATE:** 1/23/2024 - 3/21/2024

**PROJECT LOCATION:** Rosamod, CA

**EASTING:** 6515965.764

DIP/AZIMUTH: -90 /

| EL     | DEPTH<br>(ft) | Description<br>of<br>Strata                                                                                                                     | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) |      |      | Discontinuities |                                                                                                                                                                                                                                                                                                                                                             | Sampling & In Situ Testing |                       |      |                |       |                            |  |  |  |
|--------|---------------|-------------------------------------------------------------------------------------------------------------------------------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|------|------|-----------------|-------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|----------------------------|-----------------------|------|----------------|-------|----------------------------|--|--|--|
|        |               |                                                                                                                                                 | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       | 0.05                        | 0.25 | 0.50 | 2.50            | 5.00                                                                                                                                                                                                                                                                                                                                                        | B - Bedding<br>S - Shear   | J - Joint<br>F- Fault | Type | Core<br>Rec. % | RQD % | Test Results<br>& Comments |  |  |  |
| '2435' | -110          | QTZ MONZONITE, light gray to white, phaneritic, biotite rich, with hornblende and K-Na feldspar, trace amounts of epidote, pyrite, and chlorite |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |      |                 | <p>From 116' to 120': (6) 0° - 2° Planar breaks</p> <p>~121.3': 38° Filled with altered biotite</p> <p>From 123' to 127': (10) 10° - 22° Planar smooth</p> <p>From 131' to 134': (13) 5° - 15° Irregular undulating smooth</p> <p>~136.5': 17° Planar smooth</p> <p>~137.6': Reverse angle wedge 45° - 38° undulating rough</p> <p>From 138.5' to 140':</p> |                            |                       | C    | 15             | 9     |                            |  |  |  |
| '2430' |               |                                                                                                                                                 |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |      |                 |                                                                                                                                                                                                                                                                                                                                                             |                            |                       |      |                |       |                            |  |  |  |
| 114.5  |               |                                                                                                                                                 |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |      |                 |                                                                                                                                                                                                                                                                                                                                                             |                            |                       |      |                |       |                            |  |  |  |
| -115   |               |                                                                                                                                                 |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |      |                 |                                                                                                                                                                                                                                                                                                                                                             |                            |                       |      |                |       |                            |  |  |  |
| '2425' | -120          |                                                                                                                                                 |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |      |                 |                                                                                                                                                                                                                                                                                                                                                             |                            |                       |      |                |       |                            |  |  |  |
| '2420' | -125          |                                                                                                                                                 |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |      |                 |                                                                                                                                                                                                                                                                                                                                                             |                            |                       |      |                |       |                            |  |  |  |
| '2415' | -130          |                                                                                                                                                 |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |      |                 |                                                                                                                                                                                                                                                                                                                                                             |                            |                       |      |                |       |                            |  |  |  |
| '2410' | -135          |                                                                                                                                                 |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |      |                 |                                                                                                                                                                                                                                                                                                                                                             |                            |                       |      |                |       |                            |  |  |  |
| '2405' |               |                                                                                                                                                 |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |      |                 |                                                                                                                                                                                                                                                                                                                                                             |                            |                       |      |                |       |                            |  |  |  |

**BORING TYPE:** HQ3

**DRILLER:** Crux

**LOGGED BY:** Chris Messenger

**HOLE DEPTH (ft):** 2581

**WATER OBSERVATIONS:** 241 ft, 811 ft, 2336 ft.

**CASING:** HW to 76 ft.

REMARKS:

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |
|-----------------------------------|---------------|-------|--------------------------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               |
| W                                 | Water level   | PL(D) | Point load diametral test Is(50) (psi)           |
|                                   |               | SLK   | Slake durability test (Type _____)               |
|                                   |               | TRI   | Triaxial stress test (psi)                       |
|                                   |               | UCS   | Uniaxial stress test (psi)                       |

(Continued Next Page)



CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2542.7

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2153909.161

DATE: 1/23/2024 - 3/21/2024

PROJECT LOCATION: Rosamod, CA

EASTING: 6515965.764

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata            | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities          |                        | Sampling & In Situ Testing |                |       |                            |
|---------------------|----------------------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|--------------------------|------------------------|----------------------------|----------------|-------|----------------------------|
|                     |                                        | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments |
| 2400                |                                        |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 145                 |                                        |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 2395                |                                        |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 150                 |                                        |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 2390                |                                        |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 154                 | PEGMATITE DIKE                         |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 155                 |                                        |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 157                 |                                        |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 2385                |                                        |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 160                 |                                        |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 2380                | From 162.75' to 163': Chlorite veining |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 165                 |                                        |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 2375                |                                        |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 170                 |                                        |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 2370                |                                        |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |

BORING TYPE: HQ3

DRILLER: Crux

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 2581

WATER OBSERVATIONS: 241 ft, 811 ft, 2336 ft.

CASING: HW to 76 ft.

REMARKS: \_\_\_\_\_

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                    |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|------------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type _____) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)         |
| WL                                | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)         |

(Continued Next Page)



CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2542.7

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2153909.161

DATE: 1/23/2024 - 3/21/2024

PROJECT LOCATION: Rosamod, CA

EASTING: 6515965.764

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities          |                        | Sampling & In Situ Testing |                |       |                            |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|--------------------------|------------------------|----------------------------|----------------|-------|----------------------------|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments |
| 2365                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 180                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 2360                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 185                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 2355                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 190                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 2350                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 195                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 2345                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 200                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 2340                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 205                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 2335                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |

BORING TYPE: HQ3

DRILLER: Crux

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 2581

WATER OBSERVATIONS: 241 ft, 811 ft, 2336 ft.

CASING: HW to 76 ft.

REMARKS: \_\_\_\_\_

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                         |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|-----------------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type <u>  </u> ) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)              |
| WL                                | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)              |

(Continued Next Page)



CLIENT: Lane Power & Energy Solutions  
PROJECT: Hydrostor Zevsar  
PROJECT LOCATION: Rosamod, CA

SURFACE ELEVATION (ft): 2542.7  
NORTHING: 2153909.161  
EASTING: 6515965.764

PROJECT No: 951-20  
DATE: 1/23/2024 - 3/21/2024  
DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities          |                        | Sampling & In Situ Testing |                |       |                            |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|--------------------------|------------------------|----------------------------|----------------|-------|----------------------------|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments |
| 2330                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 215                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 2325                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 220                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 55    |                            |
| 2320                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 225                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 2315                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 58    |                            |
| 230                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 2310                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 235                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 2305                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 77    |                            |
| 240                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 2300                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |

BORING TYPE: HQ3  
HOLE DEPTH (ft): 2581  
REMARKS: \_\_\_\_\_

DRILLER: Crux  
WATER OBSERVATIONS: 241 ft, 811 ft, 2336 ft.

LOGGED BY: Chris Messenger  
CASING: HW to 76 ft.

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                  |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|----------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type ___) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)       |
| WL                                | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)       |



CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2542.7

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2153909.161

DATE: 1/23/2024 - 3/21/2024

PROJECT LOCATION: Rosamod, CA

EASTING: 6515965.764

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities          |                       | Sampling & In Situ Testing |                |       |                            |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|--------------------------|-----------------------|----------------------------|----------------|-------|----------------------------|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear | J - Joint<br>F- Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments |
| 2295                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |
| 250                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |
| 2290                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |
| 255                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |
| 2285                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |
| 260                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |
| 2280                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |
| 265                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |
| 2275                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |
| 270                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |
| 2270                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |
| 275                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |
| 2265                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |

BORING TYPE: HQ3

DRILLER: CruX

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 2581

WATER OBSERVATIONS: 241 ft, 811 ft, 2336 ft.

CASING: HW to 76 ft.

REMARKS: \_\_\_\_\_

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                  |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|----------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type ___) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)       |
| WL                                | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)       |

(Continued Next Page)





CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2542.7

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2153909.161

DATE: 1/23/2024 - 3/21/2024

PROJECT LOCATION: Rosamod, CA

EASTING: 6515965.764

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities          |                       | Sampling & In Situ Testing |                |       |                            |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|--------------------------|-----------------------|----------------------------|----------------|-------|----------------------------|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear | J - Joint<br>F- Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments |
| 2260                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |
| 285                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |
| 286                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |
| 286.5               | CORE LOSS                   |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |
| 2255                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       | C                          | 95             | 52    |                            |
| 290                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |
| 2250                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       | C                          | 100            | 52    |                            |
| 295                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |
| 2245                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |
| 300                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |
| 2240                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |
| 305                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |
| 2235                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       | C                          | 100            | 45    |                            |
| 310                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |
| 2230                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |

BORING TYPE: HQ3

DRILLER: CruX

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 2581

WATER OBSERVATIONS: 241 ft, 811 ft, 2336 ft.

CASING: HW to 76 ft.

REMARKS: \_\_\_\_\_

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                         |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|-----------------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type <u>  </u> ) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)              |
| W                                 | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)              |

(Continued Next Page)



CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2542.7

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2153909.161

DATE: 1/23/2024 - 3/21/2024

PROJECT LOCATION: Rosamod, CA

EASTING: 6515965.764

DIP/AZIMUTH: -90 /

| EL | DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities          |                        | Sampling & In Situ Testing |                |       |                            |
|----|---------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|--------------------------|------------------------|----------------------------|----------------|-------|----------------------------|
|    |               |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments |
|    |               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
|    | 2225          |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
|    | 320           |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 64    |                            |
|    |               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
|    | 2220          |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
|    | 325           |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
|    |               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
|    | 2215          |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 82    |                            |
|    | 330           |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
|    |               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
|    | 2210          |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
|    | 335           |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
|    |               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
|    | 2205          |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 81    |                            |
|    | 340           |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
|    | 341           | QTZ MONZONITE, light gray   |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
|    |               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
|    | 2200          |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
|    | 345           |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
|    |               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
|    | 2195          |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 30    |                            |

BORING TYPE: HQ3

DRILLER: Crux

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 2581

WATER OBSERVATIONS: 241 ft, 811 ft, 2336 ft.

CASING: HW to 76 ft.

REMARKS: \_\_\_\_\_

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                  |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|----------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type ___) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)       |
| L                                 | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)       |

(Continued Next Page)

**CLIENT:** Lane Power & Energy Solutions

**SURFACE ELEVATION (ft):** 2542.7

**PROJECT No:** 951-20

**PROJECT:** Hydrostor Zevsar

**NORTHING:** 2153909.161

**DATE:** 1/23/2024 - 3/21/2024

**PROJECT LOCATION:** Rosamod, CA

**EASTING:** 6515965.764

DIP/AZIMUTH: -90 /

[illegible]

**BORING TYPE:** HQ3

**DRILLER:** Crux

**LOGGED BY:** Chris Messenger

**HOLE DEPTH (ft):** 2581

**WATER OBSERVATIONS:** 241 ft, 811 ft, 2336 ft.

**CASING:** HW to 76 ft.

REMARKS:

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |
|-----------------------------------|---------------|-------|--------------------------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               |
| W                                 | Water level   | PL(D) | Point load diametral test Is(50) (psi)           |
|                                   |               | SLK   | Slake durability test (Type _____)               |
|                                   |               | TRI   | Triaxial stress test (psi)                       |
|                                   |               | UCS   | Uniaxial stress test (psi)                       |

(Continued Next Page)

**CLIENT:** Lane Power & Energy Solutions

**SURFACE ELEVATION (ft):** 2542.7

**PROJECT No:** 951-20

**PROJECT:** Hydrostor Zevsar

**NORTHING:** 2153909.161

**DATE:** 1/23/2024 - 3/21/2024

**PROJECT LOCATION:** Rosamod, CA

**EASTING:** 6515965.764

DIP/AZIMUTH: -90 /

| EL | DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities          |                       | Sampling & In Situ Testing |                |       |                            |
|----|---------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|--------------------------|-----------------------|----------------------------|----------------|-------|----------------------------|
|    |               |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear | J - Joint<br>F- Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments |
|    |               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |
|    |               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |
|    |               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |
|    |               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |
|    |               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |
|    |               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |
|    |               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |
|    |               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |
|    |               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |
|    |               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |
|    |               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |
|    |               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |
|    |               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |
|    |               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |
|    |               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |
|    |               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |
|    |               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |
|    |               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |
|    |               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |
|    |               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |
|    |               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |
|    |               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |
|    |               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |
|    |               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |
|    |               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |
|    |               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |
|    |               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |
|    |               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |
|    |               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |
|    |               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |
|    |               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |
|    |               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |
|    |               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |
|    |               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |
|    |               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |
|    |               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |
|    |               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |
|    |               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |
|    |               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |
|    |               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |
|    |               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |
|    |               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |
|    |               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |
|    |               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |
|    |               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |
|    |               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |
|    |               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |
|    |               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |
|    |               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |
|    |               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |
|    |               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |
|    |               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |
|    |               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |
|    |               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |
|    |               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |
|    |               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |
|    |               |                             |                         |    | </ |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |

**BORING TYPE:** HQ3

**DRILLER:** Crux

**LOGGED BY:** Chris Messenger

**HOLE DEPTH (ft):** 2581

**WATER OBSERVATIONS:** 241 ft, 811 ft, 2336 ft.

**CASING:** HW to 76 ft.

REMARKS:

| <b><u>SAMPLING &amp; IN SITU TESTING LEGEND</u></b>                                 |               |       |                                                  |
|-------------------------------------------------------------------------------------|---------------|-------|--------------------------------------------------|
|  | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) |
|  | Water seep    | PL(A) | Point load axial test 1s(50) (psi)               |
|  | Water level   | PL(D) | Point load diametral test 1s(50) (psi)           |
|                                                                                     |               | SLK   | Slake durability test (Type _____)               |
|                                                                                     |               | TRI   | Triaxial stress test (psi)                       |
|                                                                                     |               | UCS   | Uniaxial stress test (psi)                       |

(Continued Next Page)



CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2542.7

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2153909.161

DATE: 1/23/2024 - 3/21/2024

PROJECT LOCATION: Rosamod, CA

EASTING: 6515965.764

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities          |                       | Sampling & In Situ Testing |                |       |                            |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|--------------------------|-----------------------|----------------------------|----------------|-------|----------------------------|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear | J - Joint<br>F- Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments |
| 2120                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |
| 425                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |
| 2115                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |
| 430                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |
| 2110                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |
| 435                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |
| 2105                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |
| 440                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |
| 2100                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |
| 445                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |
| 2095                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |
| 450                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |
| 2090                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |

BORING TYPE: HQ3

DRILLER: Crux

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 2581

WATER OBSERVATIONS: 241 ft, 811 ft, 2336 ft.

CASING: HW to 76 ft.

REMARKS: \_\_\_\_\_

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                         |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|-----------------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type <u>  </u> ) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)              |
| WL                                | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)              |

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CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2542.7

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2153909.161

DATE: 1/23/2024 - 3/21/2024

PROJECT LOCATION: Rosamod, CA

EASTING: 6515965.764

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata                                                                                | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities          |                        | Sampling & In Situ Testing |                |       |                            |
|---------------------|------------------------------------------------------------------------------------------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|--------------------------|------------------------|----------------------------|----------------|-------|----------------------------|
|                     |                                                                                                            | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments |
| 2085<br>460         |                                                                                                            |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 85    |                            |
| 2080<br>465         |                                                                                                            |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 466                 | QTZ MONZONITE, light gray to white, phaneritic, with K-Na feldspar and biotite, trace amounts of muscovite |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 2075<br>470         |                                                                                                            |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 78    |                            |
| 2070<br>475         |                                                                                                            |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 476                 | QTZ MONZONITE, light gray to white to pink, phaneritic                                                     |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 2065<br>480         |                                                                                                            |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 53    |                            |
| 2060<br>485         |                                                                                                            |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 2055                |                                                                                                            |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 37    |                            |
|                     |                                                                                                            |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |

BORING TYPE: HQ3

DRILLER: Crux

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 2581

WATER OBSERVATIONS: 241 ft, 811 ft, 2336 ft.

CASING: HW to 76 ft.

REMARKS: \_\_\_\_\_

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                   |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|-----------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type ____) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)        |
| L                                 | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)        |

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CLIENT: Lane Power & Energy Solutions  
PROJECT: Hydrostor Zevsar  
PROJECT LOCATION: Rosamod, CA

SURFACE ELEVATION (ft): 2542.7  
NORTHING: 2153909.161  
EASTING: 6515965.764

PROJECT No: 951-20  
DATE: 1/23/2024 - 3/21/2024  
DIP/AZIMUTH: -90 /

| EL | DEPTH<br>(ft) | Description<br>of<br>Strata                                                                                             | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log                                                                     | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft)          |                          | Discontinuities        |      | Sampling & In Situ Testing |       |                            |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
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|    |               |                                                                                                                         | Fr                      | SA | MA | HA | CA |                                                                                    | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       | 0.05<br>0.25<br>0.50<br>2.50<br>5.00 | B - Bedding<br>S - Shear | J - Joint<br>F - Fault | Type | Core<br>Rec. %             | RQD % | Test Results<br>& Comments |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|    |               |                                                                                                                         |                         |    |    |    |    |                                                                                    |               |      |          |      |           |         |       |                                      |                          |                        |      |                            |       |                            |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|    | 491           | QTZ MONZONITE, light gray to white, phaneritic, with K-Na feldspar, biotite, and hornblende, trace amounts of muscovite |                         |    |    |    |    |  |               |      |          |      |           |         |       |                                      |                          |                        |      |                            |       |                            |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |

BORING TYPE: HQ3  
HOLE DEPTH (ft): 2581  
REMARKS: \_\_\_\_\_

DRILLER: Crux  
WATER OBSERVATIONS: 241 ft, 811 ft, 2336 ft.

LOGGED BY: Chris Messenger  
CASING: HW to 76 ft.

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                   |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|-----------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type ____) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)        |
| L                                 | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)        |

(Continued Next Page)



CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2542.7

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2153909.161

DATE: 1/23/2024 - 3/21/2024

PROJECT LOCATION: Rosamod, CA

EASTING: 6515965.764

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata                                                                                            | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities          |                        | Sampling & In Situ Testing |                |       |                            |
|---------------------|------------------------------------------------------------------------------------------------------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|--------------------------|------------------------|----------------------------|----------------|-------|----------------------------|
|                     |                                                                                                                        | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments |
| 2015                |                                                                                                                        |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 530                 |                                                                                                                        |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 533                 | QTZ MONZONITE, light gray to white, phaneritic, with K-Na feldspar, biotite and hornblende                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 60    |                            |
| 535                 |                                                                                                                        |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 2005                |                                                                                                                        |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 540                 |                                                                                                                        |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 30    |                            |
| 545                 |                                                                                                                        |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1995                |                                                                                                                        |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 550                 |                                                                                                                        |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 59    |                            |
| 554                 | QTZ MONZONITE, light gray to white, phaneritic, with qtz feldspar, biotite, and hornblende, trace amounts of muscovite |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 555                 |                                                                                                                        |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1985                |                                                                                                                        |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 51    |                            |

BORING TYPE: HQ3

DRILLER: Crux

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 2581

WATER OBSERVATIONS: 241 ft, 811 ft, 2336 ft.

CASING: HW to 76 ft.

REMARKS:

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                  |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|----------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type ___) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)       |
| L                                 | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)       |

(Continued Next Page)





CLIENT: Lane Power & Energy Solutions  
PROJECT: Hydrostor Zevsar  
PROJECT LOCATION: Rosamod, CA

SURFACE ELEVATION (ft): 2542.7  
NORTHING: 2153909.161  
EASTING: 6515965.764

PROJECT No: 951-20  
DATE: 1/23/2024 - 3/21/2024  
DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata                       | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities                                    |                       | Sampling & In Situ Testing |                |       |                            |
|---------------------|---------------------------------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|----------------------------------------------------|-----------------------|----------------------------|----------------|-------|----------------------------|
|                     |                                                   | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear                           | J - Joint<br>F- Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments |
| 1980<br>565         |                                                   |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | -560.75': 41° Planar<br>smooth (vein)              |                       |                            |                |       |                            |
|                     |                                                   |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | -562.75': 19° Undulating<br>rough                  |                       |                            |                |       |                            |
| 1975<br>570         |                                                   |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | -565.8': 42° Undulating<br>rough                   |                       |                            |                |       |                            |
|                     |                                                   |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 566.5' to 567': (3)<br>21° J. Planar rough    |                       |                            |                |       |                            |
|                     |                                                   |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 568' to 567.1': 0°<br>Planar smooth           | C                     | 100                        | 77             |       |                            |
| 1970<br>575         |                                                   |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 571.2' to 586': (9)<br>0° - 20° Planar smooth |                       |                            |                |       |                            |
| 1965<br>580         |                                                   |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                    |                       | C                          | 100            | 74    |                            |
| 1960<br>585         |                                                   |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                    |                       |                            |                |       |                            |
| 586                 | QTZ MONZONITE, light gray to white,<br>phaneritic |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 586' to 601': (15)<br>0° - 27° Planar smooth  |                       |                            |                |       |                            |
| 1955<br>590         |                                                   |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                    |                       | C                          | 100            | 87    |                            |
| 1950                |                                                   |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                    |                       |                            |                |       |                            |

BORING TYPE: HQ3  
HOLE DEPTH (ft): 2581  
REMARKS: \_\_\_\_\_

DRILLER: Crux  
WATER OBSERVATIONS: 241 ft, 811 ft, 2336 ft.

LOGGED BY: Chris Messenger  
CASING: HW to 76 ft.

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                   |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|-----------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type ____) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)        |
| WL                                | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)        |

(Continued Next Page)

**CLIENT:** Lane Power & Energy Solutions

**SURFACE ELEVATION (ft):** 2542.7

**PROJECT No:** 951-20

**PROJECT:** Hydrostor Zevsar

**NORTHING:** 2153909.161

**DATE:** 1/23/2024 - 3/21/2024

**PROJECT LOCATION:** Rosamod, CA

**EASTING:** 6515965.764

DIP/AZIMUTH: -90 /

| EL    | DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) |      |      |      | Discontinuities |                          | Sampling & In Situ Testing |      |                |       |                            |
|-------|---------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|------|------|------|-----------------|--------------------------|----------------------------|------|----------------|-------|----------------------------|
|       |               |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       | 0.05                        | 0.25 | 0.50 | 2.50 | 5.00            | B - Bedding<br>S - Shear | J - Joint<br>F- Fault      | Type | Core<br>Rec. % | RQD % | Test Results<br>& Comments |
|       |               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |      |      |                 |                          |                            |      |                |       |                            |
| 1945' | 600           |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |      |      | C               | 100                      | 66                         |      |                |       |                            |
| 1940' | 605           |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |      |      |                 |                          |                            |      |                |       |                            |
| 1935' | 610           |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |      |      | C               | 100                      | 65                         |      |                |       |                            |
| 1930' | 615           |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |      |      |                 |                          |                            |      |                |       |                            |
| 1925' | 620           |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |      |      | C               | 100                      | 51                         |      |                |       |                            |
| 1920' | 625           |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |      |      |                 |                          |                            |      |                |       |                            |
| 1915' |               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |      |      | C               | 100                      | 53                         |      |                |       |                            |

**BORING TYPE:** HQ3

**DRILLER:** Crux

**LOGGED BY:** Chris Messenger

HOLE DEPTH (ft): 2581

**WATER OBSERVATIONS:** 241 ft, 811 ft, 2336 ft.

**CASING:** HW to 76 ft.

REMARKS:

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |
|-----------------------------------|---------------|-------|--------------------------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) |
| W                                 | Water seep    | PL(A) | Point load axial test 1s(50) (psi)               |
| W                                 | Water level   | PL(D) | Point load diametral test 1s(50) (psi)           |
|                                   |               | SLK   | Slake durability test (Type _____)               |
|                                   |               | TRI   | Triaxial stress test (psi)                       |
|                                   |               | UCS   | Uniaxial stress test (psi)                       |

(Continued Next Page)



CLIENT: Lane Power & Energy Solutions  
PROJECT: Hydrostor Zevsar  
PROJECT LOCATION: Rosamod, CA

SURFACE ELEVATION (ft): 2542.7  
NORTHING: 2153909.161  
EASTING: 6515965.764

PROJECT No: 951-20  
DATE: 1/23/2024 - 3/21/2024  
DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata                                                                                                               | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft)          |                          | Discontinuities       |      | Sampling & In Situ Testing |       |                            |  |
|---------------------|-------------------------------------------------------------------------------------------------------------------------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|--------------------------------------|--------------------------|-----------------------|------|----------------------------|-------|----------------------------|--|
|                     |                                                                                                                                           | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       | 0.05<br>0.25<br>0.50<br>2.50<br>5.00 | B - Bedding<br>S - Shear | J - Joint<br>F- Fault | Type | Core<br>Rec. %             | RQD % | Test Results<br>& Comments |  |
|                     |                                                                                                                                           |                         |    |    |    |    |                |               |      |          |      |           |         |       |                                      |                          |                       |      |                            |       |                            |  |
| 1910<br>635         | QTZ MONZONITE, light gray to white, phaneritic, with feldspar, biotite, and hornblende, trace amounts of chlorite, epidote, and muscovite |                         |    |    |    |    |                |               |      |          |      |           |         |       |                                      |                          |                       |      |                            |       |                            |  |
|                     |                                                                                                                                           |                         |    |    |    |    |                |               |      |          |      |           |         |       |                                      |                          |                       |      |                            |       |                            |  |
|                     |                                                                                                                                           |                         |    |    |    |    |                |               |      |          |      |           |         |       |                                      |                          |                       |      |                            |       |                            |  |
| 640                 |                                                                                                                                           |                         |    |    |    |    |                |               |      |          |      |           |         |       |                                      |                          |                       |      |                            |       |                            |  |
| 641                 |                                                                                                                                           |                         |    |    |    |    |                |               |      |          |      |           |         |       |                                      |                          |                       |      |                            |       |                            |  |
|                     |                                                                                                                                           |                         |    |    |    |    |                |               |      |          |      |           |         |       |                                      |                          |                       |      |                            |       |                            |  |
| 1900                |                                                                                                                                           |                         |    |    |    |    |                |               |      |          |      |           |         |       |                                      |                          |                       |      |                            |       |                            |  |
| 645                 |                                                                                                                                           |                         |    |    |    |    |                |               |      |          |      |           |         |       |                                      |                          |                       |      |                            |       |                            |  |
|                     |                                                                                                                                           |                         |    |    |    |    |                |               |      |          |      |           |         |       |                                      |                          |                       |      |                            |       |                            |  |
| 1895                |                                                                                                                                           |                         |    |    |    |    |                |               |      |          |      |           |         |       |                                      |                          |                       |      |                            |       |                            |  |
| 650                 |                                                                                                                                           |                         |    |    |    |    |                |               |      |          |      |           |         |       |                                      |                          |                       |      |                            |       |                            |  |
|                     |                                                                                                                                           |                         |    |    |    |    |                |               |      |          |      |           |         |       |                                      |                          |                       |      |                            |       |                            |  |
| 1890                |                                                                                                                                           |                         |    |    |    |    |                |               |      |          |      |           |         |       |                                      |                          |                       |      |                            |       |                            |  |
| 655                 |                                                                                                                                           |                         |    |    |    |    |                |               |      |          |      |           |         |       |                                      |                          |                       |      |                            |       |                            |  |
|                     |                                                                                                                                           |                         |    |    |    |    |                |               |      |          |      |           |         |       |                                      |                          |                       |      |                            |       |                            |  |
| 1885                |                                                                                                                                           |                         |    |    |    |    |                |               |      |          |      |           |         |       |                                      |                          |                       |      |                            |       |                            |  |
| 660                 |                                                                                                                                           |                         |    |    |    |    |                |               |      |          |      |           |         |       |                                      |                          |                       |      |                            |       |                            |  |
|                     |                                                                                                                                           |                         |    |    |    |    |                |               |      |          |      |           |         |       |                                      |                          |                       |      |                            |       |                            |  |
| 1880                |                                                                                                                                           |                         |    |    |    |    |                |               |      |          |      |           |         |       |                                      |                          |                       |      |                            |       |                            |  |

BORING TYPE: HQ3  
HOLE DEPTH (ft): 2581  
REMARKS: \_\_\_\_\_

DRILLER: Crux  
WATER OBSERVATIONS: 241 ft, 811 ft, 2336 ft.

LOGGED BY: Chris Messenger  
CASING: HW to 76 ft.

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                  |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|----------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type ___) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)       |
| L                                 | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)       |

**CLIENT:** Lane Power & Energy Solutions

**SURFACE ELEVATION (ft):** 2542.7

**PROJECT No:** 951-20

**PROJECT:** Hydrostor Zevsar

**NORTHING:** 2153909.161

**DATE:** 1/23/2024 - 3/21/2024

**PROJECT LOCATION:** Rosamod, CA

**EASTING:** 6515965.764

DIP/AZIMUTH: -90 /

[illegible]

**BORING TYPE:** HQ3

**DRILLER:** Crux

**LOGGED BY:** Chris Messenger

**HOLE DEPTH (ft):** 2581

**WATER OBSERVATIONS:** 241 ft, 811 ft, 2336 ft.

**CASING:** HW to 76 ft.

REMARKS:

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |
|-----------------------------------|---------------|-------|--------------------------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               |
| W                                 | Water level   | PL(D) | Point load diametral test Is(50) (psi)           |
|                                   |               | SLK   | Slake durability test (Type _____)               |
|                                   |               | TRI   | Triaxial stress test (psi)                       |
|                                   |               | UCS   | Uniaxial stress test (psi)                       |

(Continued Next Page)



CLIENT: Lane Power & Energy Solutions  
PROJECT: Hydrostor Zevsar  
PROJECT LOCATION: Rosamod, CA

SURFACE ELEVATION (ft): 2542.7  
NORTHING: 2153909.161  
EASTING: 6515965.764

PROJECT No: 951-20  
DATE: 1/23/2024 - 3/21/2024  
DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities                |                        | Sampling & In Situ Testing |                |       |                            |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|--------------------------------|------------------------|----------------------------|----------------|-------|----------------------------|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear       | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments |
| 1840                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 700': 35° Undulating rough     |                        |                            |                |       |                            |
| 705                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 703': Planar smooth            |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 703.7': 50° Stepped rough      |                        |                            |                |       |                            |
| 1835                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 706': 30° Planar smooth        |                        |                            |                |       |                            |
| 710                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 708': Planar smooth            |                        | C                          | 100            | 90    |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 709.3': 25° Planar smooth      |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 710': Undulating stepped rough |                        |                            |                |       |                            |
| 1830                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 712': 35° Planar rough         |                        |                            |                |       |                            |
| 715                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 713.7': 35° Planar smooth      |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 715': Planar smooth            |                        |                            |                |       |                            |
| 1825                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 719': Planar rough             |                        | C                          | 100            | 84    |                            |
| 720                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 719.9': 0° Undulating smooth   |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 722': 65° Planar smooth        |                        |                            |                |       |                            |
| 1820                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 722.5': Planar rough           |                        |                            |                |       |                            |
| 725                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 723': Multiple J. fractures    |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 725.5': J. fracture            |                        |                            |                |       |                            |
| 1815                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 729.6': Planar rough           |                        | C                          | 100            | 74    |                            |
| 730                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 732': 25° Planar rough         |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 732.8': 30° Planar rough       |                        |                            |                |       |                            |
| 1810                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 733': 50° Planar smooth        |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 734': 60° Planar rough         |                        |                            |                |       |                            |

BORING TYPE: HQ3  
HOLE DEPTH (ft): 2581  
REMARKS: \_\_\_\_\_

DRILLER: Crux  
WATER OBSERVATIONS: 241 ft, 811 ft, 2336 ft.

LOGGED BY: Chris Messenger  
CASING: HW to 76 ft.

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                  |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|----------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type ___) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)       |
| WL                                | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)       |



CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2542.7

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2153909.161

DATE: 1/23/2024 - 3/21/2024

PROJECT LOCATION: Rosamod, CA

EASTING: 6515965.764

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities                    |                        | Sampling & In Situ Testing |                |       |                            |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|------------------------------------|------------------------|----------------------------|----------------|-------|----------------------------|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear           | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments |
| 1805<br>740         |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 735.8': 25° Planar rough           |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 736.3': 40° Undulating rough       |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 737.2': 50° Planar smooth          |                        | C                          | 100            | 79    |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 739': 50° Planar rough             |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 740': J. fracture                  |                        |                            |                |       |                            |
| 1800<br>745         |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 742': Planar smooth                |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 742.6': 40° Stepped rough          |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 743.7': J. fracture                |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 744.5': 0° Undulating rough        |                        |                            |                |       |                            |
| 1795<br>750         |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 746.8': Planar rough               |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 747' to 747.7': S. fracture   |                        | C                          | 100            | 66    |                            |
| 1790<br>755         |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 753' to 753.4': J. fracture   |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 754': 25° Planar smooth            |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 755': 25° Stepped rough            |                        |                            |                |       |                            |
| 1785<br>760         |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 756.5': 45° Undulating rough       |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 759': 45° Planar smooth            |                        | C                          | 100            | 74    |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 760.5': 40° Planar smooth          |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 760.7': Planar smooth              |                        |                            |                |       |                            |
| 1780<br>765         |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 761.4': 60° Planar smooth          |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 761.7': 40° Planar rough           |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 762.5': 45° Planar smooth          |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 763': 45° Planar smooth            |                        |                            |                |       |                            |
| 1775                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 763.8': 45° Planar rough           |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 764': 45° Undulating stepped rough |                        | C                          | 100            | 72    |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 765': 45° Planar rough             |                        |                            |                |       |                            |

BORING TYPE: HQ3

DRILLER: Crux

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 2581

WATER OBSERVATIONS: 241 ft, 811 ft, 2336 ft.

CASING: HW to 76 ft.

REMARKS: \_\_\_\_\_

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                    |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|------------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type _____) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)         |
| W                                 | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)         |

(Continued Next Page)



CLIENT: Lane Power & Energy Solutions  
PROJECT: Hydrostor Zevsar  
PROJECT LOCATION: Rosamod, CA

SURFACE ELEVATION (ft): 2542.7  
NORTHING: 2153909.161  
EASTING: 6515965.764

PROJECT No: 951-20  
DATE: 1/23/2024 - 3/21/2024  
DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities                                 |                        | Sampling & In Situ Testing |                |       |                            |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|-------------------------------------------------|------------------------|----------------------------|----------------|-------|----------------------------|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear                        | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments |
| 1770                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 765.7': 45° Planar<br>smooth                    |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 769.1': Planar rough                            |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 770.5': 40° undulating<br>rough                 |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 772.8': 70° S. fracture                         |                        |                            |                |       |                            |
| 775                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 774.5': 45° Planar<br>smooth                    |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 775.6': Planar rough                            |                        |                            |                |       |                            |
| 1765                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                 |                        | C                          | 100            | 72    |                            |
| 780                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 779': 65° Planar smooth                         |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 780': Planar rough                              |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 782.3': 55° Planar rough                        |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 783': Planar rough                              |                        |                            |                |       |                            |
| 1760                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 784.3': 0° Planar rough                         |                        |                            |                |       |                            |
| 785                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 786': 60° Stepped rough                         |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 786.9': 45° Planar rough                        |                        |                            |                |       |                            |
| 1755                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 787.6' to 788.5':<br>Multiple J. fractures |                        | C                          | 100            | 61    |                            |
| 790                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 789.9': 50° Planar<br>smooth                    |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 790': 45° Planar smooth                         |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 790.8': 45° Undulating<br>rough                 |                        |                            |                |       |                            |
| 1750                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 793.3': 45° Stepped<br>rough                    |                        |                            |                |       |                            |
| 795                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 795': 45° Planar smooth                         |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 795.8': 50° Stepped<br>rough                    |                        |                            |                |       |                            |
| 1745                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 797': 50° Planar rough                          |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 797.1' to 798.5':<br>Multiple J. fractures |                        | C                          | 100            | 62    |                            |
| 800                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 800': 0° Planar rough                           |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 803.7': 75° S. fracture                         |                        |                            |                |       |                            |
| 1740                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                 |                        |                            |                |       |                            |

BORING TYPE: HQ3  
HOLE DEPTH (ft): 2581  
REMARKS: \_\_\_\_\_

DRILLER: Crux  
WATER OBSERVATIONS: 241 ft, 811 ft, 2336 ft.

LOGGED BY: Chris Messenger  
CASING: HW to 76 ft.

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                    |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|------------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type _____) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)         |
| W                                 | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)         |

(Continued Next Page)



CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2542.7

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2153909.161

DATE: 1/23/2024 - 3/21/2024

PROJECT LOCATION: Rosamod, CA

EASTING: 6515965.764

DIP/AZIMUTH: -90 /

| EL     | DEPTH<br>(ft) | Description<br>of<br>Strata                                                                                                              | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities                   |                        | Sampling & In Situ Testing |                |       |                            |
|--------|---------------|------------------------------------------------------------------------------------------------------------------------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|-----------------------------------|------------------------|----------------------------|----------------|-------|----------------------------|
|        |               |                                                                                                                                          | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear          | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments |
| 805    |               | PEGMATITE DIKE                                                                                                                           |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 804.9': 50° Planar smooth         |                        |                            |                |       |                            |
|        |               |                                                                                                                                          |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 805': 50° Planar smooth           |                        |                            |                |       |                            |
|        |               |                                                                                                                                          |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 805.7': Planar rough              |                        |                            |                |       |                            |
| 808.5  |               |                                                                                                                                          |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 807.3': 35° Planar smooth         | C                      | 100                        | 74             |       |                            |
|        |               |                                                                                                                                          |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 808.5': 55° Planar smooth         |                        |                            |                |       |                            |
| 810    |               |                                                                                                                                          |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 810.9': Planar rough              |                        |                            |                |       |                            |
|        |               |                                                                                                                                          |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                   |                        |                            |                |       |                            |
|        |               |                                                                                                                                          |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 814.1': 55° Undulating rough      |                        |                            |                |       |                            |
| 815    |               |                                                                                                                                          |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 814.6': 35° Planar smooth         |                        |                            |                |       |                            |
|        |               |                                                                                                                                          |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 816': 45° Stepped rough           | C                      | 100                        | 82             |       |                            |
|        |               |                                                                                                                                          |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 816.7': 50° Undulating rough      |                        |                            |                |       |                            |
|        |               |                                                                                                                                          |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 818': Planar rough                |                        |                            |                |       |                            |
| 819.75 |               | PEGMATITE DIKE                                                                                                                           |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 819': 75° Planar rough            |                        |                            |                |       |                            |
|        |               |                                                                                                                                          |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 819.5': 65° Planar rough          |                        |                            |                |       |                            |
|        |               |                                                                                                                                          |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                   |                        |                            |                |       |                            |
|        |               |                                                                                                                                          |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                   |                        |                            |                |       |                            |
| 823.3  |               |                                                                                                                                          |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 823': Planar smooth               |                        |                            |                |       |                            |
|        |               |                                                                                                                                          |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 823.6': Planar rough              |                        |                            |                |       |                            |
| 826    |               | QTZ MONZONITE, light gray to white, phaneritic, with qtz feldspar and biotite, trace amounts of pyrite, muscovite, chlorite, and epidote |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 824.3': 72° Planar smooth         |                        |                            |                |       |                            |
|        |               |                                                                                                                                          |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                   |                        |                            |                |       |                            |
|        |               |                                                                                                                                          |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                   |                        |                            |                |       |                            |
| 830    |               |                                                                                                                                          |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 832': 38° Planar smooth           |                        |                            |                |       |                            |
|        |               |                                                                                                                                          |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 833.6': 0° Planar irregular rough |                        |                            |                |       |                            |
|        |               |                                                                                                                                          |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 834.7': 0° Planar irregular rough |                        |                            |                |       |                            |
| 835    |               |                                                                                                                                          |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 836.2': 42° Planar smooth         |                        |                            |                |       |                            |
|        |               |                                                                                                                                          |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                   |                        |                            |                |       |                            |
|        |               |                                                                                                                                          |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 838.2': 7° Planar smooth          | C                      | 100                        | 81             |       |                            |

BORING TYPE: HQ3

DRILLER: Crux

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 2581

WATER OBSERVATIONS: 241 ft, 811 ft, 2336 ft.

CASING: HW to 76 ft.

REMARKS:

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                  |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|----------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type ___) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)       |
| WL                                | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)       |





CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2542.7

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2153909.161

DATE: 1/23/2024 - 3/21/2024

PROJECT LOCATION: Rosamod, CA

EASTING: 6515965.764

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities          |                        | Sampling & In Situ Testing |                |       |                            |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|--------------------------|------------------------|----------------------------|----------------|-------|----------------------------|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments |
| 1700                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 845                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1695                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 850                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1690                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 855                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1685                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 860                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1680                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 865                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1675                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 870                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1670                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |

BORING TYPE: HQ3

DRILLER: Crux

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 2581

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REMARKS: \_\_\_\_\_

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                   |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|-----------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type ____) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)        |
| WL                                | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)        |

(Continued Next Page)



CLIENT: Lane Power & Energy Solutions  
PROJECT: Hydrostor Zevsar  
PROJECT LOCATION: Rosamod, CA

SURFACE ELEVATION (ft): 2542.7  
NORTHING: 2153909.161  
EASTING: 6515965.764

PROJECT No: 951-20  
DATE: 1/23/2024 - 3/21/2024  
DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water                                | Fracture<br>Spacing<br>(ft)                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                         | Discontinuities          |                        | Sampling & In Situ Testing |                |       |                            |  |  |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|--------------------------------------|-------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|--------------------------|------------------------|----------------------------|----------------|-------|----------------------------|--|--|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |                                      |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     | B - Bedding<br>S - Shear | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments |  |  |
| 1665<br>880         |                             |                         |    |    |    |    |                |               |      |          |      |           |         | 0.05<br>0.25<br>0.50<br>2.50<br>5.00 | <div>879.8': 7° Undulating rough</div> <div>881.35': 17° Planar smooth</div> <div>From 884' to 884.6': (2)<br/>42° - 44° Planar smooth</div> <div>887.5': 42° Planar smooth</div> <div>888.4': 90° Planar smooth</div> <div>889.4': 22° Planar smooth</div> <div>890.2': 21° Planar smooth</div> <div>894.6': 44° Planar smooth</div> <div>From 897.6' to 898': (2)<br/>38° - 22° Planar smooth</div> <div>From 898.8' to 900.4':<br/>82° Planar smooth</div> <div>From 901' to 903': (3)<br/>42° - 46° Planar smooth</div> <div>904.9': 47° Undulating rough</div> <div>905': 45° Undulating smooth</div> <div>906.2': 22° Planar rough</div> <div>908.3': 37° Planar smooth</div> | C                        | 100                    | 76                         |                |       |                            |  |  |
| 1660<br>885         |                             |                         |    |    |    |    |                |               |      |          |      |           |         |                                      |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     |                          |                        |                            |                |       |                            |  |  |
| 1655<br>890         |                             |                         |    |    |    |    |                |               |      |          |      |           |         |                                      |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     |                          |                        |                            |                |       |                            |  |  |
| 1650<br>895         |                             |                         |    |    |    |    |                |               |      |          |      |           |         |                                      |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     |                          |                        |                            |                |       |                            |  |  |
| 1645<br>900         |                             |                         |    |    |    |    |                |               |      |          |      |           |         |                                      |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     |                          |                        |                            |                |       |                            |  |  |
| 1640<br>905         |                             |                         |    |    |    |    |                |               |      |          |      |           |         |                                      |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     |                          |                        |                            |                |       |                            |  |  |
| 1635                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |                                      |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     |                          |                        |                            |                |       |                            |  |  |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |                                      |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     |                          |                        |                            |                |       |                            |  |  |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |                                      |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     |                          |                        |                            |                |       |                            |  |  |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |                                      |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     |                          |                        |                            |                |       |                            |  |  |

BORING TYPE: HQ3  
HOLE DEPTH (ft): 2581  
REMARKS: \_\_\_\_\_

DRILLER: Crux  
WATER OBSERVATIONS: 241 ft, 811 ft, 2336 ft.

LOGGED BY: Chris Messenger  
CASING: HW to 76 ft.

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                  |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|----------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type ___) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)       |
| WL                                | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)       |

(Continued Next Page)



**CLIENT:** Lane Power & Energy Solutions  
**PROJECT:** Hydrostor Zevsar  
**PROJECT LOCATION:** Rosamod, CA

**SURFACE ELEVATION (ft):** 2542.7  
**NORTHING:** 2153909.161  
**EASTING:** 6515965.764

**PROJECT No:** 951-20  
**DATE:** 1/23/2024 - 3/21/2024  
**DIP/AZIMUTH:** -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata                                                                                                                  | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities                                                                      |                        | Sampling & In Situ Testing |                |       |                            |
|---------------------|----------------------------------------------------------------------------------------------------------------------------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|--------------------------------------------------------------------------------------|------------------------|----------------------------|----------------|-------|----------------------------|
|                     |                                                                                                                                              | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear                                                             | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments |
| 1630                | QTZ MONZONITE, light gray to white, phaneritic, with qtz feldspar, hornblende, and biotite, trace amounts of muscovite, chlorite, and pyrite |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 910': 17° Planar smooth                                                              |                        |                            |                |       |                            |
| 915                 |                                                                                                                                              |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 910.5' to 911':<br>Rubble                                                       |                        |                            |                |       |                            |
| 916                 |                                                                                                                                              |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 911' to 912': (3)<br>38° - 43° Planar smooth                                    |                        |                            |                |       |                            |
| 1625                |                                                                                                                                              |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 912.5': 52° Planar<br>smooth                                                         |                        |                            |                |       |                            |
| 920                 |                                                                                                                                              |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 914': 74° Planar smooth                                                              |                        |                            |                |       |                            |
| 925                 |                                                                                                                                              |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 915': (2) 45° Planar<br>smooth                                                       |                        |                            |                |       |                            |
| 1620                |                                                                                                                                              |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 917' to 919':<br>Multiple 70° - 90°<br>reverse angle fractures<br>planar smooth | C                      | 100                        | 43             |       |                            |
| 930                 |                                                                                                                                              |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 919' to 921':<br>Rubble                                                         |                        |                            |                |       |                            |
| 935                 |                                                                                                                                              |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 922.3': 38° Undulating<br>rough                                                      |                        |                            |                |       |                            |
| 1615                |                                                                                                                                              |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 923': 45° Undulating<br>rough                                                        |                        |                            |                |       |                            |
| 940                 |                                                                                                                                              |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 924': 7° Planar smooth                                                               |                        |                            |                |       |                            |
| 1610                |                                                                                                                                              |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 928' to 929':<br>Rubble                                                         | C                      | 100                        | 46             |       |                            |
| 945                 |                                                                                                                                              |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 930' to 931': (6)<br>40° Planar smooth                                          |                        |                            |                |       |                            |
| 1605                |                                                                                                                                              |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 931' to 932.75':<br>90° Undulating rough                                        |                        |                            |                |       |                            |
| 950                 |                                                                                                                                              |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 934': 42° Planar smooth                                                              |                        |                            |                |       |                            |
| 955                 |                                                                                                                                              |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 935.3': 22° Undulating<br>rough                                                      |                        |                            |                |       |                            |
| 960                 |                                                                                                                                              |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 935.6' to 937': (2)<br>43° - 45° Planar smooth                                  |                        |                            |                |       |                            |
| 965                 |                                                                                                                                              |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 939': 0° Undulating<br>smooth                                                        | C                      | 100                        | 50             |       |                            |
| 970                 |                                                                                                                                              |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 940': 45° Undulating<br>smooth                                                       |                        |                            |                |       |                            |
| 975                 |                                                                                                                                              |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 944': 27° Undulating<br>rough                                                        |                        |                            |                |       |                            |

**BORING TYPE:** HQ3  
**HOLE DEPTH (ft):** 2581  
**REMARKS:**

**DRILLER:** Crux  
**WATER OBSERVATIONS:** 241 ft, 811 ft, 2336 ft.

**LOGGED BY:** Chris Messenger  
**CASING:** HW to 76 ft.

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                                        |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|--------------------------------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type <input type="checkbox"/> ) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)                             |
| W                                 | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)                             |



CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2542.7

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2153909.161

DATE: 1/23/2024 - 3/21/2024

PROJECT LOCATION: Rosamod, CA

EASTING: 6515965.764

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata                                                                                                       | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities          |                        | Sampling & In Situ Testing |                |       |                            |
|---------------------|-----------------------------------------------------------------------------------------------------------------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|--------------------------|------------------------|----------------------------|----------------|-------|----------------------------|
|                     |                                                                                                                                   | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments |
| 1595<br>950         |                                                                                                                                   |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 69    |                            |
| 1590<br>955         |                                                                                                                                   |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1585<br>960         |                                                                                                                                   |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 69    |                            |
| 1580<br>965         |                                                                                                                                   |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1575<br>970         |                                                                                                                                   |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 66    |                            |
| 1570<br>975         |                                                                                                                                   |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1565<br>976         | QTZ MONZONITE, light gray to white, phaneritic, with qtz feldspar, hornblende, and biotite, trace amounts of muscovite and pyrite |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |

BORING TYPE: HQ3

DRILLER: Crux

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 2581

WATER OBSERVATIONS: 241 ft, 811 ft, 2336 ft.

CASING: HW to 76 ft.

REMARKS: \_\_\_\_\_

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                   |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|-----------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type ____) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)        |
| WL                                | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)        |



CLIENT: Lane Power & Energy Solutions  
PROJECT: Hydrostor Zevsar  
PROJECT LOCATION: Rosamod, CA

SURFACE ELEVATION (ft): 2542.7  
NORTHING: 2153909.161  
EASTING: 6515965.764

PROJECT No: 951-20  
DATE: 1/23/2024 - 3/21/2024  
DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities          |                        | Sampling & In Situ Testing |                |       |                            |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|--------------------------|------------------------|----------------------------|----------------|-------|----------------------------|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments |
| 1560                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 985                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1555                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 990                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 36    |                            |
| 1550                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 995                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1545                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 46    |                            |
| 1000                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1540                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1005                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1535                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 52    |                            |
| 1010                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1530                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |

BORING TYPE: HQ3  
HOLE DEPTH (ft): 2581  
REMARKS: \_\_\_\_\_

DRILLER: Crux  
WATER OBSERVATIONS: 241 ft, 811 ft, 2336 ft.

LOGGED BY: Chris Messenger  
CASING: HW to 76 ft.

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                  |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|----------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type ___) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)       |
| WL                                | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)       |

(Continued Next Page)



CLIENT: Lane Power & Energy Solutions  
PROJECT: Hydrostor Zevsar  
PROJECT LOCATION: Rosamod, CA

SURFACE ELEVATION (ft): 2542.7  
NORTHING: 2153909.161  
EASTING: 6515965.764

PROJECT No: 951-20  
DATE: 1/23/2024 - 3/21/2024  
DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities          |                        | Sampling & In Situ Testing |                |       |                            |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|--------------------------|------------------------|----------------------------|----------------|-------|----------------------------|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments |
| 1525                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1020                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1520                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1025                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1515                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1030                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1510                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1035                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1505                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1040                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1500                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1045                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1495                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |

BORING TYPE: HQ3  
HOLE DEPTH (ft): 2581  
REMARKS: \_\_\_\_\_

DRILLER: Crux  
WATER OBSERVATIONS: 241 ft, 811 ft, 2336 ft.

LOGGED BY: Chris Messenger  
CASING: HW to 76 ft.

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                    |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|------------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type _____) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)         |
| WL                                | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)         |



CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2542.7

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2153909.161

DATE: 1/23/2024 - 3/21/2024

PROJECT LOCATION: Rosamod, CA

EASTING: 6515965.764

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata                                                          | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities          |                        | Sampling & In Situ Testing |                |       |                            |
|---------------------|--------------------------------------------------------------------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|--------------------------|------------------------|----------------------------|----------------|-------|----------------------------|
|                     |                                                                                      | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments |
| 1490                |                                                                                      |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1055                |                                                                                      |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1485                |                                                                                      |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1060                |                                                                                      |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1480                |                                                                                      |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1065                |                                                                                      |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1475                |                                                                                      |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1070                |                                                                                      |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1470                |                                                                                      |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1075                |                                                                                      |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1465                |                                                                                      |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1080                |                                                                                      |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1081                | QTZ MONZONITE, light gray to green to pink, phaneritic, rich in chlorite and epidote |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1460                |                                                                                      |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |

BORING TYPE: HQ3

DRILLER: Crux

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 2581

WATER OBSERVATIONS: 241 ft, 811 ft, 2336 ft.

CASING: HW to 76 ft.

REMARKS: \_\_\_\_\_

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                  |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|----------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type ___) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)       |
| WL                                | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)       |

(Continued Next Page)



CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2542.7

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2153909.161

DATE: 1/23/2024 - 3/21/2024

PROJECT LOCATION: Rosamod, CA

EASTING: 6515965.764

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities          |                        | Sampling & In Situ Testing |                |       |                            |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|--------------------------|------------------------|----------------------------|----------------|-------|----------------------------|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments |
| 1455                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1090                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1450                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1095                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1445                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1100                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1440                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1105                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1435                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1110                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1430                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1115                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1425                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |

BORING TYPE: HQ3

DRILLER: Crux

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 2581

WATER OBSERVATIONS: 241 ft, 811 ft, 2336 ft.

CASING: HW to 76 ft.

REMARKS: \_\_\_\_\_

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                  |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|----------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type ___) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)       |
| WL                                | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)       |

(Continued Next Page)





CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2542.7

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2153909.161

DATE: 1/23/2024 - 3/21/2024

PROJECT LOCATION: Rosamod, CA

EASTING: 6515965.764

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities          |                        | Sampling & In Situ Testing |                |       |                            |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|--------------------------|------------------------|----------------------------|----------------|-------|----------------------------|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments |
| 1420                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1125                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1415                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1130                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1410                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1135                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1405                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1140                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1400                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1145                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1395                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1150                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1390                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |

BORING TYPE: HQ3

DRILLER: Crux

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 2581

WATER OBSERVATIONS: 241 ft, 811 ft, 2336 ft.

CASING: HW to 76 ft.

REMARKS: \_\_\_\_\_

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                  |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|----------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type ___) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)       |
| WL                                | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)       |

(Continued Next Page)



CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2542.7

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2153909.161

DATE: 1/23/2024 - 3/21/2024

PROJECT LOCATION: Rosamod, CA

EASTING: 6515965.764

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata                                                    | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities          |                        | Sampling & In Situ Testing |                |       |                            |
|---------------------|--------------------------------------------------------------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|--------------------------|------------------------|----------------------------|----------------|-------|----------------------------|
|                     |                                                                                | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments |
| 1385                |                                                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1160                |                                                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1380                |                                                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1165                |                                                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1375                |                                                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1170                |                                                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1370                |                                                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1175                |                                                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1365                |                                                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1180                |                                                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1360                |                                                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1185                |                                                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1180                | QTZ MONZONITE, light to dark gray,<br>phaneritic, rich in chlorite and epidote |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1355                |                                                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |

BORING TYPE: HQ3

DRILLER: Crux

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 2581

WATER OBSERVATIONS: 241 ft, 811 ft, 2336 ft.

CASING: HW to 76 ft.

REMARKS: \_\_\_\_\_

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                  |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|----------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type ___) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)       |
| L                                 | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)       |

(Continued Next Page)



CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2542.7

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2153909.161

DATE: 1/23/2024 - 3/21/2024

PROJECT LOCATION: Rosamod, CA

EASTING: 6515965.764

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities          |                        | Sampling & In Situ Testing |                |       |                            |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|--------------------------|------------------------|----------------------------|----------------|-------|----------------------------|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments |
| 1350                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1195                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1345                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1200                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1340                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1205                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1335                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1210                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1330                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1215                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1325                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1220                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1320                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |

BORING TYPE: HQ3

DRILLER: Crux

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 2581

WATER OBSERVATIONS: 241 ft, 811 ft, 2336 ft.

CASING: HW to 76 ft.

REMARKS: \_\_\_\_\_

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                  |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|----------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type ___) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)       |
| WL                                | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)       |

(Continued Next Page)



CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2542.7

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2153909.161

DATE: 1/23/2024 - 3/21/2024

PROJECT LOCATION: Rosamod, CA

EASTING: 6515965.764

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata                                                                                                        | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities          |                        | Sampling & In Situ Testing |                |       |                            |
|---------------------|------------------------------------------------------------------------------------------------------------------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|--------------------------|------------------------|----------------------------|----------------|-------|----------------------------|
|                     |                                                                                                                                    | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments |
| 1315                |                                                                                                                                    |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1230                |                                                                                                                                    |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1231                | QTZ MONZONITE, light gray to white, phaneritic, with K-Na feldspar, biotite, and hornblende, trace amounts of chlorite and epidote |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 33    |                            |
| 1310                |                                                                                                                                    |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1235                |                                                                                                                                    |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1305                |                                                                                                                                    |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1240                |                                                                                                                                    |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 43    |                            |
| 1300                |                                                                                                                                    |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1245                |                                                                                                                                    |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1248                | QTZ MONZONITE, dark gray to white                                                                                                  |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1295                |                                                                                                                                    |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 46    |                            |
| 1250                |                                                                                                                                    |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1290                |                                                                                                                                    |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1255                |                                                                                                                                    |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1285                |                                                                                                                                    |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 33    |                            |

BORING TYPE: HQ3

DRILLER: Crux

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 2581

WATER OBSERVATIONS: 241 ft, 811 ft, 2336 ft.

CASING: HW to 76 ft.

REMARKS: \_\_\_\_\_

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                    |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|------------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type _____) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)         |
| WL                                | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)         |

(Continued Next Page)



CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2542.7

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2153909.161

DATE: 1/23/2024 - 3/21/2024

PROJECT LOCATION: Rosamod, CA

EASTING: 6515965.764

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities          |                        | Sampling & In Situ Testing |                |       |                            |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|--------------------------|------------------------|----------------------------|----------------|-------|----------------------------|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments |
| 1280                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1265                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1275                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1270                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1270                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1275                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1265                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1280                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1260                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1285                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1255                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1290                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1250                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |

BORING TYPE: HQ3

DRILLER: CruX

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 2581

WATER OBSERVATIONS: 241 ft, 811 ft, 2336 ft.

CASING: HW to 76 ft.

REMARKS: \_\_\_\_\_

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                         |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|-----------------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type <u>  </u> ) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)              |
| WL                                | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)              |



CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2542.7

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2153909.161

DATE: 1/23/2024 - 3/21/2024

PROJECT LOCATION: Rosamod, CA

EASTING: 6515965.764

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata                                                          | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities          |                        | Sampling & In Situ Testing |                |       |                            |
|---------------------|--------------------------------------------------------------------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|--------------------------|------------------------|----------------------------|----------------|-------|----------------------------|
|                     |                                                                                      | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments |
| 1245                | QTZ MONZONITE, dark gray to white,<br>with K-Na feldspar, biotite, and<br>hornblende |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1300                |                                                                                      |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1240                |                                                                                      |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1305                |                                                                                      |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1306                |                                                                                      |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1235                |                                                                                      |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1310                |                                                                                      |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1230                |                                                                                      |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1315                |                                                                                      |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1225                |                                                                                      |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1320                |                                                                                      |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1220                |                                                                                      |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1325                |                                                                                      |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1215                |                                                                                      |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
|                     |                                                                                      |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |

BORING TYPE: HQ3

DRILLER: Crux

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 2581

WATER OBSERVATIONS: 241 ft, 811 ft, 2336 ft.

CASING: HW to 76 ft.

REMARKS: \_\_\_\_\_

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                    |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|------------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type _____) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)         |
| WL                                | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)         |

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**CLIENT:** Lane Power & Energy Solutions  
**PROJECT:** Hydrostor Zevsar  
**PROJECT LOCATION:** Rosamod, CA

**SURFACE ELEVATION (ft):** 2542.7  
**NORTHING:** 2153909.161  
**EASTING:** 6515965.764

**PROJECT No:** 951-20  
**DATE:** 1/23/2024 - 3/21/2024  
**DIP/AZIMUTH:** -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata                                          | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities                                                      |                        | Sampling & In Situ Testing |                |       |                            |
|---------------------|----------------------------------------------------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|----------------------------------------------------------------------|------------------------|----------------------------|----------------|-------|----------------------------|
|                     |                                                                      | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear                                             | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments |
| 1335                |                                                                      |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1332': 90° Undulating rough                                          |                        |                            |                |       |                            |
|                     |                                                                      |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1333.1': 45° Planar smooth                                           |                        |                            |                |       |                            |
|                     |                                                                      |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1334': 42° Planar smooth                                             |                        |                            |                |       |                            |
| 1340                |                                                                      |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1335' to 1335.6':<br>(2) 42° - 44° Undulating rough             |                        |                            |                |       |                            |
|                     |                                                                      |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1336' to 1337': 71°<br>Planar smooth, 12° - 36°<br>Planar rough |                        | C                          | 100            | 44    |                            |
|                     |                                                                      |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1339': 6° Undulating rough                                           |                        |                            |                |       |                            |
| 1345                |                                                                      |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1344': (2) 4° - 7°<br>Undulating rough                               |                        |                            |                |       |                            |
|                     |                                                                      |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1345.9': 4° Planar rough                                             |                        |                            |                |       |                            |
| 1350                |                                                                      |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1349.8': Planar smooth                                               |                        | C                          | 100            | 54    |                            |
|                     |                                                                      |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1350' to 1351': (2)<br>64° - 66° Planar rough                   |                        |                            |                |       |                            |
| 1355                |                                                                      |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                                      |                        |                            |                |       |                            |
|                     |                                                                      |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                                      |                        |                            |                |       |                            |
| 1360                |                                                                      |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                                      |                        |                            |                |       |                            |
| 1361                | QTZ MONZONITE, light gray to dark gray, rich in chlorite and epidote |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1361' to 1371':<br>Fractures throughout,<br>decomposed          |                        | C                          | 100            | 86    |                            |

**BORING TYPE:** HQ3  
**HOLE DEPTH (ft):** 2581  
**REMARKS:** \_\_\_\_\_

**DRILLER:** Crux  
**WATER OBSERVATIONS:** 241 ft, 811 ft, 2336 ft.

**LOGGED BY:** Chris Messenger  
**CASING:** HW to 76 ft.

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                  |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|----------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type ___) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)       |
| WL                                | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)       |

(Continued Next Page)



CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2542.7

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2153909.161

DATE: 1/23/2024 - 3/21/2024

PROJECT LOCATION: Rosamod, CA

EASTING: 6515965.764

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities          |                        | Sampling & In Situ Testing |                |       |                            |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|--------------------------|------------------------|----------------------------|----------------|-------|----------------------------|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments |
| 1175'               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1370                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 80    |                            |
| 1170'               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1375                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1165'               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 45    |                            |
| 1380                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1160'               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1385                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1155'               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 25    |                            |
| 1390                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1150'               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1395                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1145'               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 18    |                            |

BORING TYPE: HQ3

DRILLER: Crux

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 2581

WATER OBSERVATIONS: 241 ft, 811 ft, 2336 ft.

CASING: HW to 76 ft.

REMARKS: \_\_\_\_\_

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                  |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|----------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type ___) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)       |
| WL                                | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)       |

(Continued Next Page)





CLIENT: Lane Power & Energy Solutions  
PROJECT: Hydrostor Zevsar  
PROJECT LOCATION: Rosamod, CA

SURFACE ELEVATION (ft): 2542.7  
NORTHING: 2153909.161  
EASTING: 6515965.764

PROJECT No: 951-20  
DATE: 1/23/2024 - 3/21/2024  
DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities          |                       | Sampling & In Situ Testing |                |       |                            |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|--------------------------|-----------------------|----------------------------|----------------|-------|----------------------------|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear | J - Joint<br>F- Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments |
| 1140'               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |
| 1405                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |
| 1135'               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       | C                          | 100            | 15    |                            |
| 1410                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |
| 1130'               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |
| 1415                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |
| 1125'               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       | C                          | 100            | 36    |                            |
| 1420                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |
| 1120'               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |
| 1425                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |
| 1115'               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       | C                          | 100            | 53    |                            |
| 1430                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |
| 1110'               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |

BORING TYPE: HQ3  
HOLE DEPTH (ft): 2581  
REMARKS: \_\_\_\_\_

DRILLER: CruX  
WATER OBSERVATIONS: 241 ft, 811 ft, 2336 ft.

LOGGED BY: Chris Messenger  
CASING: HW to 76 ft.

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                  |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|----------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type ___) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)       |
| WL                                | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)       |

(Continued Next Page)



CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2542.7

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2153909.161

DATE: 1/23/2024 - 3/21/2024

PROJECT LOCATION: Rosamod, CA

EASTING: 6515965.764

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities          |                        | Sampling & In Situ Testing |                |       |                            |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|--------------------------|------------------------|----------------------------|----------------|-------|----------------------------|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments |
| 1105                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1440                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 17    |                            |
| 1445                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1095                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 33    |                            |
| 1450                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1090                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1455                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1085                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 47    |                            |
| 1460                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1080                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1465                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1075                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 29    |                            |

BORING TYPE: HQ3

DRILLER: Crux

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 2581

WATER OBSERVATIONS: 241 ft, 811 ft, 2336 ft.

CASING: HW to 76 ft.

REMARKS: \_\_\_\_\_

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                         |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|-----------------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type <u>  </u> ) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)              |
| WL                                | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)              |

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**CLIENT:** Lane Power & Energy Solutions

**SURFACE ELEVATION (ft):** 2542.7

**PROJECT No:** 951-20

**PROJECT:** Hydrostor Zevsar

**NORTHING:** 2153909.161

**DATE:** 1/23/2024 - 3/21/2024

**PROJECT LOCATION:** Rosamod, CA

**EASTING:** 6515965.764

DIP/AZIMUTH: -90 /

[illegible]

**BORING TYPE:** HQ3

**DRILLER:** Crux

**LOGGED BY:** Chris Messenger

**HOLE DEPTH (ft):** 2581

**WATER OBSERVATIONS:** 241 ft, 811 ft, 2336 ft.

**CASING:** HW to 76 ft.

REMARKS:

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |
|-----------------------------------|---------------|-------|--------------------------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               |
| W                                 | Water level   | PL(D) | Point load diametral test Is(50) (psi)           |
|                                   |               | SLK   | Slake durability test (Type _____)               |
|                                   |               | TRI   | Triaxial stress test (psi)                       |
|                                   |               | UCS   | Uniaxial stress test (psi)                       |

(Continued Next Page)



CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2542.7

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2153909.161

DATE: 1/23/2024 - 3/21/2024

PROJECT LOCATION: Rosamod, CA

EASTING: 6515965.764

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities          |                        | Sampling & In Situ Testing |                |       |                                  |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|--------------------------|------------------------|----------------------------|----------------|-------|----------------------------------|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments       |
| 1035                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                  |
| 1510                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 47    | PL(A) = 443.38                   |
| 1030                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       | UCS = 3,658.91                   |
| 1515                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                  |
| 1025                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                  |
| 1520                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 43    | PL(A) = 293.37<br>ITS = 1,049.89 |
| 1020                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                  |
| 1525                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       | UCS = 13,670.18                  |
| 1015                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                  |
| 1530                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 91    | PL(A) = 211.82                   |
| 1010                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                  |
| 1535                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                  |
| 1005                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 78    | PL(D) = 55.19                    |

BORING TYPE: HQ3

DRILLER: Crux

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 2581

WATER OBSERVATIONS: 241 ft, 811 ft, 2336 ft.

CASING: HW to 76 ft.

REMARKS: \_\_\_\_\_

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                   |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|-----------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type ____) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)        |
| L                                 | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)        |

(Continued Next Page)



CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2542.7

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2153909.161

DATE: 1/23/2024 - 3/21/2024

PROJECT LOCATION: Rosamod, CA

EASTING: 6515965.764

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata                                    | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities                                             |                        | Sampling & In Situ Testing |                |       |                                 |
|---------------------|----------------------------------------------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|-------------------------------------------------------------|------------------------|----------------------------|----------------|-------|---------------------------------|
|                     |                                                                | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear                                    | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments      |
| 1543                | QTZ MONZONITE, light to dark gray<br>to green, black, and pink |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1540' 49" Undulating<br>stepped                             |                        |                            |                |       |                                 |
| 1545                |                                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1542.2' 0° - 7°<br>Undulating smooth                        |                        |                            |                |       |                                 |
| 1550                |                                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1543' 74° Planar<br>smooth                                  |                        |                            |                |       |                                 |
| 1555                |                                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1546' to 1556':<br>Fractures throughout,<br>decomposed |                        | C                          | 100            | 20    |                                 |
| 1560                |                                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1556' to 1566':<br>Fractures throughout,<br>decomposed |                        | C                          | 100            | 19    | PL(D) = 160.94<br>PL(A) = 74.51 |
| 1565                |                                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1566' to 1576':<br>Fractures throughout,<br>decomposed |                        | C                          | 100            | 12    |                                 |
| 1570                |                                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                             |                        |                            |                |       |                                 |

BORING TYPE: HQ3

DRILLER: Crux

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 2581

WATER OBSERVATIONS: 241 ft, 811 ft, 2336 ft.

CASING: HW to 76 ft.

REMARKS: \_\_\_\_\_

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                         |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|-----------------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type <u>  </u> ) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)              |
| WL                                | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)              |

(Continued Next Page)



CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2542.7

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2153909.161

DATE: 1/23/2024 - 3/21/2024

PROJECT LOCATION: Rosamod, CA

EASTING: 6515965.764

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) |      | Discontinuities<br><br>B - Bedding<br>S - Shear      J - Joint<br>F- Fault | Sampling & In Situ Testing                                  |      |      |      |                                                                  |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|------|----------------------------------------------------------------------------|-------------------------------------------------------------|------|------|------|------------------------------------------------------------------|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       | 0.05                        | 0.25 |                                                                            | 0.50                                                        | 1.00 | 2.50 | 5.00 | Type                                                             |
| 965<br>1580         |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |                                                                            | From 1576' to 1586':<br>Fractures throughout,<br>decomposed | C    | 100  | 27   | PL(D) = 30.35<br>PL(A) = 16.05<br>PL(D) = 88.92<br>PL(A) = 45.22 |
| 960<br>1585         |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |                                                                            |                                                             |      |      |      |                                                                  |
| 955<br>1590         |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |                                                                            |                                                             | C    | 100  | 20   | PL(D) = 23.44                                                    |
| 950<br>1595         |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |                                                                            |                                                             |      |      |      |                                                                  |
| 945<br>1600         |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |                                                                            | From 1596' to 1606':<br>Fractures throughout,<br>decomposed | C    | 100  | 3    |                                                                  |
| 940<br>1605         |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |                                                                            |                                                             |      |      |      |                                                                  |
| 935                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |                                                                            | From 1606' to 1616':<br>Fractures throughout,<br>decomposed | C    | 100  | 0    | PL(A) = 94.10                                                    |

BORING TYPE: HQ3

DRILLER: Crux

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 2581

WATER OBSERVATIONS: 241 ft, 811 ft, 2336 ft.

CASING: HW to 76 ft.

REMARKS: \_\_\_\_\_

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                  |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|----------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type ___) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)       |
| L                                 | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)       |

(Continued Next Page)



CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2542.7

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2153909.161

DATE: 1/23/2024 - 3/21/2024

PROJECT LOCATION: Rosamod, CA

EASTING: 6515965.764

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities          |                        | Sampling & In Situ Testing |                |       |                                 |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|--------------------------|------------------------|----------------------------|----------------|-------|---------------------------------|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments      |
| 930                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                 |
| 1615                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                 |
| 925                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       | ITS = 346.89<br>PL(D) = 624.83  |
| 1620                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 32    |                                 |
| 920                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                 |
| 1625                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                 |
| 915                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       | UCS = 5,667.33                  |
| 1630                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 33    |                                 |
| 910                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       | PL(A) = 24.07<br>PL(D) = 145.63 |
| 1635                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                 |
| 905                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                 |
| 1640                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 34    |                                 |
| 900                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                 |

BORING TYPE: HQ3

DRILLER: Crux

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 2581

WATER OBSERVATIONS: 241 ft, 811 ft, 2336 ft.

CASING: HW to 76 ft.

REMARKS: \_\_\_\_\_

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                         |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|-----------------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type <u>  </u> ) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)              |
| WL                                | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)              |

(Continued Next Page)



CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2542.7

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2153909.161

DATE: 1/23/2024 - 3/21/2024

PROJECT LOCATION: Rosamod, CA

EASTING: 6515965.764

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities          |                        | Sampling & In Situ Testing |                |       |                                 |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|--------------------------|------------------------|----------------------------|----------------|-------|---------------------------------|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments      |
| 895                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       | PL(D) = 50.99                   |
| 1650                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 65    | PL(D) = 63.26<br>PL(A) = 131.83 |
| 890                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                 |
| 1655                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                 |
| 885                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 68    | PL(D) = 42.71<br>PL(A) = 202.28 |
| 1660                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                 |
| 880                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                 |
| 1665                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                 |
| 875                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 33    |                                 |
| 1670                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                 |
| 870                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                 |
| 1675                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       | PL(D) = 268.78<br>PL(A) = 97.08 |
| 865                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 22    |                                 |

BORING TYPE: HQ3

DRILLER: Crux

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 2581

WATER OBSERVATIONS: 241 ft, 811 ft, 2336 ft.

CASING: HW to 76 ft.

REMARKS: \_\_\_\_\_

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                  |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|----------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type ___) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)       |
| L                                 | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)       |

(Continued Next Page)





CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2542.7

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2153909.161

DATE: 1/23/2024 - 3/21/2024

PROJECT LOCATION: Rosamod, CA

EASTING: 6515965.764

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities          |                        | Sampling & In Situ Testing |                |       |                            |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|--------------------------|------------------------|----------------------------|----------------|-------|----------------------------|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments |
| 860                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       | PL(D) = 93.94              |
| 1685                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 855                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 52    | PL(A) = 39.54              |
| 1690                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 850                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1695                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 35    | PL(A) = 68.50              |
| 845                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1700                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 840                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1705                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 835                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 38    | ITS = 47.07                |
| 1710                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 830                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |

BORING TYPE: HQ3

DRILLER: Crux

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 2581

WATER OBSERVATIONS: 241 ft, 811 ft, 2336 ft.

CASING: HW to 76 ft.

REMARKS: \_\_\_\_\_

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                         |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|-----------------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type <u>  </u> ) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)              |
| WL                                | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)              |

(Continued Next Page)



CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2542.7

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2153909.161

DATE: 1/23/2024 - 3/21/2024

PROJECT LOCATION: Rosamod, CA

EASTING: 6515965.764

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities          |                        | Sampling & In Situ Testing |                |       |                                |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|--------------------------|------------------------|----------------------------|----------------|-------|--------------------------------|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments     |
| 825<br>1720         |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 50    | PL(D) = 48.41<br>PL(A) = 12.30 |
| 820<br>1725         |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                |
| 815<br>1730         |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 33    | PL(D) = 23.79<br>PL(A) = 26.12 |
| 810<br>1735         |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                |
| 805<br>1740         |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 37    |                                |
| 800<br>1745         |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                |
| 795                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 48    |                                |

BORING TYPE: HQ3

DRILLER: Crux

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 2581

WATER OBSERVATIONS: 241 ft, 811 ft, 2336 ft.

CASING: HW to 76 ft.

REMARKS: \_\_\_\_\_

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                  |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|----------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type ___) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)       |
| L                                 | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)       |

(Continued Next Page)

**CLIENT:** Lane Power & Energy Solutions

**SURFACE ELEVATION (ft):** 2542.7

**PROJECT No:** 951-20

**PROJECT:** Hydrostor Zevsar

**NORTHING:** 2153909.161

**DATE:** 1/23/2024 - 3/21/2024

**PROJECT LOCATION:** Rosamod, CA

**EASTING:** 6515965.764

DIP/AZIMUTH: -90 /

[illegible]

**BORING TYPE:** HQ3

**DRILLER:** Crux

**LOGGED BY:** Chris Messenger

**HOLE DEPTH (ft):** 2581

**WATER OBSERVATIONS:** 241 ft, 811 ft, 2336 ft.

**CASING:** HW to 76 ft.

REMARKS:

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |
|-----------------------------------|---------------|-------|--------------------------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               |
| W                                 | Water level   | PL(D) | Point load diametral test Is(50) (psi)           |
|                                   |               | SLK   | Slake durability test (Type _____)               |
|                                   |               | TRI   | Triaxial stress test (psi)                       |
|                                   |               | UCS   | Uniaxial stress test (psi)                       |

(Continued Next Page)

**CLIENT:** Lane Power & Energy Solutions

**SURFACE ELEVATION (ft):** 2542.7

**PROJECT No:** 951-20

**PROJECT:** Hydrostor Zevsar

**NORTHING:** 2153909.161

**DATE:** 1/23/2024 - 3/21/2024

**PROJECT LOCATION:** Rosamod, CA

EASTING: 6515965.764

DIP/AZIMUTH: -90 /

| EL      | DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) |      |      |      | Discontinuities |                          | Sampling & In Situ Testing |      |                                  |       |
|---------|---------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|------|------|------|-----------------|--------------------------|----------------------------|------|----------------------------------|-------|
|         |               |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       | 0.05                        | 0.25 | 0.50 | 2.50 | 5.00            | B - Bedding<br>S - Shear | J - Joint<br>F- Fault      | Type | Core<br>Rec. %                   | RQD % |
| 755'    |               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |      |      |                 |                          |                            |      | PL(D) = 288.55                   |       |
| 1790    |               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |      |      | C               | 100                      | 57                         |      | PL(D) = 178.65<br>PL(A) = 442.75 |       |
| 750'    |               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |      |      |                 |                          |                            |      |                                  |       |
| 1795    |               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |      |      |                 |                          |                            |      |                                  |       |
| 745'    |               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |      |      | C               | 100                      | 50                         |      |                                  |       |
| 1799.5' |               | PEGMATITE DIKE              |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |      |      |                 |                          |                            |      |                                  |       |
| 1800    |               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |      |      |                 |                          |                            |      |                                  |       |
| 1801    |               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |      |      |                 |                          |                            |      |                                  |       |
| 740'    |               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |      |      |                 |                          |                            |      |                                  |       |
| 1805    |               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |      |      |                 |                          |                            |      |                                  |       |
| 1806    |               | PEGMATITE DIKE              |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |      |      |                 |                          |                            |      |                                  |       |
| 1808    |               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |      |      | C               | 100                      | 62                         |      |                                  |       |
| 1810    |               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |      |      |                 |                          |                            |      |                                  |       |
| 730'    |               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |      |      |                 |                          |                            |      |                                  |       |
| 1815    |               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |      |      |                 |                          |                            |      |                                  |       |
| 725'    |               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |      |      | C               | 100                      | 35                         |      |                                  |       |

**BORING TYPE:** HQ3

**DRILLER:** Crux

**LOGGED BY:** Chris Messenger

**HOLE DEPTH (ft):** 2581

**WATER OBSERVATIONS:** 241 ft, 811 ft, 2336 ft.

**CASING:** HW to 76 ft.

REMARKS:

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |
|-----------------------------------|---------------|-------|--------------------------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               |
| W                                 | Water level   | PL(D) | Point load diametral test Is(50) (psi)           |
|                                   |               | SLK   | Slake durability test (Type _____)               |
|                                   |               | TRI   | Triaxial stress test (psi)                       |
|                                   |               | UCS   | Uniaxial stress test (psi)                       |

(Continued Next Page)



CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2542.7

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2153909.161

DATE: 1/23/2024 - 3/21/2024

PROJECT LOCATION: Rosamod, CA

EASTING: 6515965.764

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata                                                                                                                                      | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities                                                                              |                        | Sampling & In Situ Testing |                |       |                                                        |
|---------------------|------------------------------------------------------------------------------------------------------------------------------------------------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|----------------------------------------------------------------------------------------------|------------------------|----------------------------|----------------|-------|--------------------------------------------------------|
|                     |                                                                                                                                                                  | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear                                                                     | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments                             |
| 1823                | PEGMATITE DIKE                                                                                                                                                   |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1819.9' to 1820':<br>42° Rough                                                          |                        |                            |                |       | PL(A) = 455.75<br>PL(D) = 956.72<br>UCS =<br>13,816.64 |
| 1825                |                                                                                                                                                                  |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | ~1821.4': 57° Undulating<br>rough                                                            |                        |                            |                |       |                                                        |
| 1826                |                                                                                                                                                                  |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1824' to 1827':<br>Rubble                                                               |                        |                            |                |       |                                                        |
| 1830                |                                                                                                                                                                  |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1828.2' to 1829':<br>79° Undulating rough                                               |                        | C                          | 100            | 51    |                                                        |
| 1831                | QTZ MONZONITE, light gray to white,<br>phaneritic to aphanitic, with qtz<br>feldspar, biotite, and hornblende, trace<br>amounts of chlorite, epidote, and pyrite |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1829' to 1831': (3)<br>20° - 30° Planar rough                                           |                        |                            |                |       |                                                        |
| 1835                |                                                                                                                                                                  |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | ~1831.67': 7° Undulating<br>smooth                                                           |                        |                            |                |       |                                                        |
| 1840                |                                                                                                                                                                  |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1834' to 1837': 90°<br>Undulating with adjacent<br>sub fracture rough                   |                        |                            |                |       |                                                        |
| 1845                |                                                                                                                                                                  |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1839' to 1840': (3)<br>38° - 44° Planar smooth                                          |                        | C                          | 100            | 46    | ITS = 92.22                                            |
| 1850                |                                                                                                                                                                  |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1842' to 1843':<br>Rubble                                                               |                        |                            |                |       |                                                        |
| 1855                |                                                                                                                                                                  |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | ~1842.4': 31° Planar<br>smooth                                                               |                        |                            |                |       |                                                        |
| 1860                |                                                                                                                                                                  |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1843' to 1844': 69°<br>Planar smooth reverse<br>49° planar smooth, 37°<br>planar smooth |                        |                            |                |       | PL(D) = 159.28                                         |
| 1865                |                                                                                                                                                                  |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | ~1844.3': 35° Planar<br>smooth                                                               |                        |                            |                |       |                                                        |
| 1870                |                                                                                                                                                                  |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1845' to 1848': (6)<br>0° - 6° Planar smooth                                            |                        | C                          | 100            | 31    |                                                        |
| 1875                |                                                                                                                                                                  |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | ~1849': 67° - 90° S.<br>undulating rough                                                     |                        |                            |                |       |                                                        |
| 1880                |                                                                                                                                                                  |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | ~1850.6': 4° Planar<br>smooth                                                                |                        |                            |                |       |                                                        |
| 1885                |                                                                                                                                                                  |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | ~1851.78': 62° Planar<br>smooth                                                              |                        |                            |                |       |                                                        |
| 1890                |                                                                                                                                                                  |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1853' to 1855': 90°<br>- 60° - 55° Undulating<br>smooth                                 |                        |                            |                |       |                                                        |

BORING TYPE: HQ3

DRILLER: Crux

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 2581

WATER OBSERVATIONS: 241 ft, 811 ft, 2336 ft.

CASING: HW to 76 ft.

REMARKS: \_\_\_\_\_

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                    |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|------------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type _____) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)         |
| L                                 | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)         |

(Continued Next Page)



CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2542.7

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2153909.161

DATE: 1/23/2024 - 3/21/2024

PROJECT LOCATION: Rosamod, CA

EASTING: 6515965.764

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities                                 |                        | Sampling & In Situ Testing |                |       |                            |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|-------------------------------------------------|------------------------|----------------------------|----------------|-------|----------------------------|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear                        | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments |
| 685                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1853.75' to 1860':<br>90° S. Planar smooth |                        |                            |                |       |                            |
| 1860                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1856.2': 42° Planar<br>smooth                   |                        | C                          | 100            | 51    |                            |
| 680                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1861' to 1869':<br>Rubble                  |                        |                            |                |       |                            |
| 1865                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                 |                        | C                          | 100            | 10    |                            |
| 675                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1869.67': Undulating /<br>Planar rough          |                        |                            |                |       |                            |
| 1870                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1871.67' to 1881':<br>Rubble               |                        |                            |                |       | PL(A) = 35.62              |
| 670                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                 |                        |                            |                |       |                            |
| 1875                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                 |                        | C                          | 100            | 1     |                            |
| 665                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1883' to 1884.6': J.<br>fracture           |                        |                            |                |       |                            |
| 1880                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1885' to 1886':<br>Rubble                  |                        |                            |                |       | PL(D) = 65.16              |
| 660                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1887.3': Planar smooth                          |                        |                            |                |       |                            |
| 1885                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1889' to 1891': 0° -<br>17° Planar smooth  |                        | C                          | 100            | 34    |                            |
| 655                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                 |                        |                            |                |       |                            |

BORING TYPE: HQ3

DRILLER: Crux

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 2581

WATER OBSERVATIONS: 241 ft, 811 ft, 2336 ft.

CASING: HW to 76 ft.

REMARKS: \_\_\_\_\_

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                  |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|----------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type ___) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)       |
| WL                                | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)       |

(Continued Next Page)

**CLIENT:** Lane Power & Energy Solutions

**SURFACE ELEVATION (ft):** 2542.7

**PROJECT No:** 951-20

**PROJECT:** Hydrostor Zevsar

**NORTHING:** 2153909.161

**DATE:** 1/23/2024 - 3/21/2024

**PROJECT LOCATION:** Rosamod, CA

**EASTING:** 6515965.764

DIP/AZIMUTH: -90 /[illegible]BORING TYPE: HQ3

**DRILLER:** Crux

**LOGGED BY:** Chris Messenger

HOLE DEPTH (ft): 2581

**WATER OBSERVATIONS:** 241 ft, 811 ft, 2336 ft.

**CASING:** HW to 76 ft.

REMARKS:

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |
|-----------------------------------|---------------|-------|--------------------------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) |
| W                                 | Water seep    | PL(A) | Point load axial test ts(50) (psi)               |
| W                                 | Water level   | PL(D) | Point load diametral test ts(50) (psi)           |
|                                   |               | SLK   | Slake durability test (Type _____)               |
|                                   |               | TRI   | Triaxial stress test (psi)                       |
|                                   |               | UCS   | Uniaxial stress test (psi)                       |

(Continued Next Page)



CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2542.7

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2153909.161

DATE: 1/23/2024 - 3/21/2024

PROJECT LOCATION: Rosamod, CA

EASTING: 6515965.764

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata                                                                                                                                      | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities                                                                      |                        | Sampling & In Situ Testing |                |       |                                  |
|---------------------|------------------------------------------------------------------------------------------------------------------------------------------------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|--------------------------------------------------------------------------------------|------------------------|----------------------------|----------------|-------|----------------------------------|
|                     |                                                                                                                                                                  | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear                                                             | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments       |
| 615<br>1930         | QTZ MONZONITE, light gray to dark gray to white and pink, phaneritic, with plagioclase, potassium, biotite, and hornblende, trace amounts of biotite and epidote |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1927' to 1931': (4)<br>0° - 4° Planar smooth,<br>(1) 47° Planar smooth          |                        | C                          | 100            | 9     | PL(D) = 71.90                    |
| 610<br>1935         |                                                                                                                                                                  |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1931' to 1932':<br>Rubble                                                       |                        |                            |                |       |                                  |
| 605<br>1936         |                                                                                                                                                                  |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1932.7': 87° S. Planar<br>smooth                                                     |                        |                            |                |       |                                  |
| 600<br>1940         |                                                                                                                                                                  |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1933.2' to 1934':<br>(8) 0° - 7° Planar smooth                                  |                        |                            |                |       |                                  |
| 595<br>1945         |                                                                                                                                                                  |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1935' to 1936': (2)<br>0° Planar, 90° undulating<br>rough                       |                        |                            |                |       |                                  |
| 590<br>1950         |                                                                                                                                                                  |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1936.25': 45° Stepped<br>smooth                                                      |                        | C                          | 100            | 27    | TRI = 35,439.20                  |
| 585<br>1955         |                                                                                                                                                                  |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1936.4' to<br>1937.45': Stepped /<br>rough and smooth                           |                        |                            |                |       |                                  |
|                     |                                                                                                                                                                  |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1937' to 1951': 90°<br>- 70° Vertical healed<br>fractures                       |                        |                            |                |       |                                  |
|                     |                                                                                                                                                                  |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1938': 61° Planar<br>smooth                                                          |                        |                            |                |       | SLK = Type I                     |
|                     |                                                                                                                                                                  |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1939.3' to 1940':<br>Rubble                                                     |                        |                            |                |       |                                  |
|                     |                                                                                                                                                                  |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1941' to 1942': (3)<br>0° - 17° X-fractures<br>along 84° - 79° planar<br>smooth |                        |                            |                |       | PL(D) = 340.07<br>PL(A) = 99.57  |
|                     |                                                                                                                                                                  |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1942.8': 28° Planar<br>smooth                                                        |                        |                            |                |       |                                  |
|                     |                                                                                                                                                                  |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1943.8': 23° Planar<br>smooth                                                        |                        | C                          | 100            | 43    |                                  |
|                     |                                                                                                                                                                  |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1944': 72° Stepped<br>rough                                                          |                        |                            |                |       |                                  |
|                     |                                                                                                                                                                  |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1945': Rubble                                                                        |                        |                            |                |       |                                  |
|                     |                                                                                                                                                                  |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1946.8': 21° Planar<br>smooth                                                        |                        |                            |                |       | SLK = Type I                     |
|                     |                                                                                                                                                                  |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1947.1': 14° Undulating<br>smooth                                                    |                        |                            |                |       |                                  |
|                     |                                                                                                                                                                  |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1947.5' to 1948':<br>79° Stepped smooth                                         |                        |                            |                |       |                                  |
|                     |                                                                                                                                                                  |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1948' to 1949': (5)<br>0° - 13° Planar smooth                                   |                        |                            |                |       |                                  |
|                     |                                                                                                                                                                  |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1949' to 1950.31':<br>90° Opened healed<br>fracture undulating<br>rough         |                        |                            |                |       | TRI = 4,082.60<br>PL(A) = 533.81 |
|                     |                                                                                                                                                                  |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1950.25' to 1951':<br>Rubble                                                    |                        | C                          | 100            | 42    |                                  |

BORING TYPE: HQ3

DRILLER: Cruz

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 2581

WATER OBSERVATIONS: 241 ft, 811 ft, 2336 ft.

CASING: HW to 76 ft.

REMARKS: \_\_\_\_\_

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                    |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|------------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type _____) |
| W                                 | Water seep    | PL(A) | Point load axial test (50) (psi)                 | TRI | Triaxial stress test (psi)         |
| L                                 | Water level   | PL(D) | Point load diametral test (50) (psi)             | UCS | Uniaxial stress test (psi)         |





**CLIENT:** Lane Power & Energy Solutions  
**PROJECT:** Hydrostor Zevsar  
**PROJECT LOCATION:** Rosamod, CA

**SURFACE ELEVATION (ft):** 2542.7  
**NORTHING:** 2153909.161  
**EASTING:** 6515965.764

**PROJECT No:** 951-20  
**DATE:** 1/23/2024 - 3/21/2024  
**DIP/AZIMUTH:** -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities                                                                              |                        | Sampling & In Situ Testing |                |       |                            |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|----------------------------------------------------------------------------------------------|------------------------|----------------------------|----------------|-------|----------------------------|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear                                                                     | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments |
| 580                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1951' to 1951.8':<br>79° Undulating rough,<br>(2) 79° - 81° Stepped                     |                        |                            |                |       |                            |
| 1965                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1953.28': 75° Undulating<br>smooth                                                           |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1955': 69° Stepped<br>rough                                                                  |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1956': 74° Planar<br>smooth                                                                  |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1957': 14° Planar rough                                                                      |                        |                            |                |       |                            |
| 575                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1958.1': 19° Planar<br>rough                                                                 |                        |                            |                |       |                            |
| 1970                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1959': 62° Undulating<br>rough                                                               | C                      | 100                        | 19             |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1959.1' to 1959.6':<br>28° - 44° - 32° Smooth                                           |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1959.85': 29° Planar<br>rough                                                                |                        |                            |                |       |                            |
| 570                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1960.8' to 1962':<br>Rubble                                                             |                        |                            |                |       |                            |
| 1975                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1962.75': 81° Planar<br>smooth                                                               |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1963.1': 80° - 90°<br>Undulating rough                                                       |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1965.1': 57° Undulating<br>smooth                                                            |                        |                            |                |       | PL(D) = 768.50             |
| 565                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1966' to 1966.5':<br>90° Undulating rough                                               |                        |                            |                |       | PL(D) =<br>2,203.80        |
| 1980                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1966.5' to 1971':<br>Rubble, multiple vertical<br>fractures                             | C                      | 100                        | 21             |       | PL(A) = 821.93             |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1971' to 1972.7':<br>(1) 27° Planar smooth,<br>(1) 67° Undulating rough                 |                        |                            |                |       | ITS = 238.86               |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1973' to 1974': 58°<br>Undulating smooth along<br>healed vein                           |                        |                            |                |       |                            |
| 560                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1974': Multiple 39° - 44°<br>healed veins                                                    |                        |                            |                |       | PL(D) = 934.14             |
| 1985                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1975': 66° Planar<br>smooth                                                                  |                        |                            |                |       | PL(A) =<br>1,008.63        |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1977.6': 45° Planar<br>rough                                                                 |                        |                            |                |       |                            |
| 555                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1978': (3) 30° - 34°<br>Undulating rough                                                     | C                      | 100                        | 36             |       |                            |
| 1990                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1979': 84° S. fracture                                                                       |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1979.75' to 1981':<br>Rubble                                                            |                        |                            |                |       |                            |
| 550                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1982.2' to 1984':<br>(2) 30° - 40° Planar<br>smooth, (1) 85° - 90°<br>Undulating smooth |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1986' to 1996':<br>Spider web multi<br>directional fracturing,<br>rubble                |                        |                            |                |       |                            |

**BORING TYPE:** HQ3  
**HOLE DEPTH (ft):** 2581  
**REMARKS:** \_\_\_\_\_

**DRILLER:** Crux  
**WATER OBSERVATIONS:** 241 ft, 811 ft, 2336 ft.

**LOGGED BY:** Chris Messenger  
**CASING:** HW to 76 ft.

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                   |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|-----------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type ____) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)        |
| WL                                | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)        |

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**CLIENT:** Lane Power & Energy Solutions

**SURFACE ELEVATION (ft):** 2542.7

**PROJECT No:** 951-20

**PROJECT:** Hydrostor Zevsar

**NORTHING:** 2153909.161

**DATE:** 1/23/2024 - 3/21/2024

**PROJECT LOCATION:** Rosamod, CA

EASTING: 6515965.764

DIP/AZIMUTH: -90 /

| EL   | DEPTH<br>(ft) | Description<br>of Strata                                                                                                                                    | Degree of Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture Spacing<br>(ft) |      |      |      | Discontinuities |                          | Sampling & In Situ Testing |      |                |       |                            |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
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|      |               |                                                                                                                                                             | Fr                   | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       | 0.05                     | 0.25 | 0.50 | 2.50 | 5.00            | B - Bedding<br>S - Shear | J - Joint<br>F - Fault     | Type | Core<br>Rec. % | RQD % | Test Results<br>& Comments |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|      |               |                                                                                                                                                             |                      |    |    |    |    |                |               |      |          |      |           |         |       |                          |      |      |      |                 |                          |                            |      |                |       |                            |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 545' |               | QTZ MONZONITE, light gray to dark gray to white, phaneritic, with Ca-Na-K feldspar, biotite, and hornblende, trace amounts of epidote, chlorite, and pyrite |                      |    |    |    |    |                |               |      |          |      |           |         |       |                          |      |      |      |                 |                          |                            |      |                |       |                            |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |

**BORING TYPE:** HQ3

**DRILLER:** Crux

**LOGGED BY:** Chris Messenger

**HOLE DEPTH (ft):** 2581

**WATER OBSERVATIONS:** 241 ft, 811 ft, 2336 ft.

**CASING:** HW to 76 ft.

REMARKS:

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |
|-----------------------------------|---------------|-------|--------------------------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               |
| W                                 | Water level   | PL(D) | Point load diametral test Is(50) (psi)           |
|                                   |               | SLK   | Slake durability test (Type _____)               |
|                                   |               | TRI   | Triaxial stress test (psi)                       |
|                                   |               | UCS   | Uniaxial stress test (psi)                       |

(Continued Next Page)

**CLIENT:** Lane Power & Energy Solutions

**SURFACE ELEVATION (ft):** 2542.7

**PROJECT No:** 951-20

**PROJECT:** Hydrostor Zevsar

**NORTHING:** 2153909.161

**DATE:** 1/23/2024 - 3/21/2024

**PROJECT LOCATION:** Rosamod, CA

EASTING: 6515965.764

DIP/AZIMUTH: -90 /

| EL   | DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) |      |      | Discontinuities |      | Sampling & In Situ Testing |                       |      |                |                                         |                            |
|------|---------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|------|------|-----------------|------|----------------------------|-----------------------|------|----------------|-----------------------------------------|----------------------------|
|      |               |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       | 0.05                        | 0.25 | 0.50 | 2.50            | 5.00 | B - Bedding<br>S - Shear   | J - Joint<br>F- Fault | Type | Core<br>Rec. % | RQD %                                   | Test Results<br>& Comments |
|      |               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |      |                 |      |                            |                       |      |                |                                         |                            |
| 510' | 2035          |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |      |                 |      |                            |                       |      | ITS = 387.59   |                                         |                            |
| 505' |               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |      |                 |      |                            |                       |      |                |                                         |                            |
| 500' | 2040          |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |      |                 |      |                            |                       |      |                | UCS =<br>12,668.30<br><br>PL(A) = 38.95 |                            |
| 500' |               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |      |                 |      |                            |                       |      |                |                                         |                            |
| 500' |               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |      |                 |      |                            |                       |      |                |                                         |                            |
| 500' | 2045          |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |      |                 |      |                            |                       |      |                |                                         |                            |
| 500' |               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |      |                 |      |                            |                       |      |                |                                         |                            |
| 500' |               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |      |                 |      |                            |                       |      |                |                                         |                            |
| 500' | 2045          |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |      |                 |      |                            |                       |      |                |                                         |                            |
| 500' |               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |      |                 |      |                            |                       |      |                |                                         |                            |
| 500' |               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |      |                 |      |                            |                       |      |                |                                         |                            |
| 500' | 2045          |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |      |                 |      |                            |                       |      |                |                                         |                            |
| 500' |               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |      |                 |      |                            |                       |      |                |                                         |                            |
| 500' |               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |      |                 |      |                            |                       |      |                |                                         |                            |
| 500' | 2045          |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |      |                 |      |                            |                       |      |                |                                         |                            |
| 500' |               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |      |                 |      |                            |                       |      |                |                                         |                            |
| 500' |               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |      |                 |      |                            |                       |      |                |                                         |                            |
| 500' | 2045          |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |      |                 |      |                            |                       |      |                |                                         |                            |
| 500' |               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |      |                 |      |                            |                       |      |                |                                         |                            |
| 500' |               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |      |                 |      |                            |                       |      |                |                                         |                            |
| 500' | 2045          |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |      |                 |      |                            |                       |      |                |                                         |                            |
| 500' |               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |      |                 |      |                            |                       |      |                |                                         |                            |
| 500' |               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |      |                 |      |                            |                       |      |                |                                         |                            |
| 500' | 2045          |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |      |                 |      |                            |                       |      |                |                                         |                            |
| 500' |               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |      |                 |      |                            |                       |      |                |                                         |                            |
| 500' |               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |      |                 |      |                            |                       |      |                |                                         |                            |
| 500' | 2045          |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |      |                 |      |                            |                       |      |                |                                         |                            |
| 500' |               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |      |                 |      |                            |                       |      |                |                                         |                            |
| 500' |               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |      |                 |      |                            |                       |      |                |                                         |                            |
| 500' | 2045          |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |      |                 |      |                            |                       |      |                |                                         |                            |
| 500' |               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |      |                 |      |                            |                       |      |                |                                         |                            |
| 500' |               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |      |                 |      |                            |                       |      |                |                                         |                            |
| 500' | 2045          |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |      |                 |      |                            |                       |      |                |                                         |                            |
| 500' |               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |      |                 |      |                            |                       |      |                |                                         |                            |
| 500' |               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |      |                 |      |                            |                       |      |                |                                         |                            |
| 500' | 2045          |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |      |                 |      |                            |                       |      |                |                                         |                            |
| 500' |               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |      |                 |      |                            |                       |      |                |                                         |                            |
| 500' |               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |      |                 |      |                            |                       |      |                |                                         |                            |
| 500' | 2045          |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |      |                 |      |                            |                       |      |                |                                         |                            |
| 500' |               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |      |                 |      |                            |                       |      |                |                                         |                            |
| 500' |               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |      |                 |      |                            |                       |      |                |                                         |                            |
| 500' | 2045          |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |      |                 |      |                            |                       |      |                |                                         |                            |
| 500' |               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |      |                 |      |                            |                       |      |                |                                         |                            |
| 500' |               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |      |                 |      |                            |                       |      |                |                                         |                            |
| 500' | 2045          |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |      |                 |      |                            |                       |      |                |                                         |                            |
| 500' |               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |      |                 |      |                            |                       |      |                |                                         |                            |

**BORING TYPE:** HQ3

**DRILLER:** CruX

**LOGGED BY:** Chris Messenger

**HOLE DEPTH (ft):** 2581

**WATER OBSERVATIONS:** 241 ft, 811 ft, 2336 ft.

**CASING:** HW to 76 ft.

REMARKS:

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |
|-----------------------------------|---------------|-------|--------------------------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               |
| W                                 | Water level   | PL(D) | Point load diametral test Is(50) (psi)           |
|                                   |               | SLK   | Slake durability test (Type _____)               |
|                                   |               | TRI   | Triaxial stress test (psi)                       |
|                                   |               | UCS   | Uniaxial stress test (psi)                       |

(Continued Next Page)



CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2542.7

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2153909.161

DATE: 1/23/2024 - 3/21/2024

PROJECT LOCATION: Rosamod, CA

EASTING: 6515965.764

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities                                                                                      |                        | Sampling & In Situ Testing |                |       |                                         |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|------------------------------------------------------------------------------------------------------|------------------------|----------------------------|----------------|-------|-----------------------------------------|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear                                                                             | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments              |
| 475                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | (2) 74° - 82° Planar<br>smooth                                                                       |                        |                            |                |       | PL(D) = 176.77                          |
| 2070                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2067°: 47° Undulating<br>smooth                                                                      |                        |                            |                |       |                                         |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2068°: 0° Planar smooth                                                                              |                        |                            |                |       |                                         |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2068.9' to 2069.9':<br>(2) 38° - 42° Planar<br>smooth                                           |                        |                            |                |       |                                         |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2070.2°: 6° Planar<br>smooth                                                                         |                        |                            |                |       |                                         |
| 470                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2071' to 2072':<br>Rubble                                                                       |                        |                            |                |       | PL(D) =<br>1,080.21<br><br>SLK = Type I |
| 2075                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2074.2' to 2076.3':<br>(5) 32° - 62° Undulating<br>smooth                                       |                        |                            |                |       |                                         |
| 465                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2077' to 2078': 88°<br>S. undulating rough                                                      |                        |                            |                |       |                                         |
| 2080                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2078°: 28° - 32° - 90°<br>Wedge undulating<br>smooth                                                 |                        |                            |                |       |                                         |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2080' to 2081': 90°<br>and 30° cut radiating<br>fracture                                        |                        |                            |                |       |                                         |
| 460                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2081.2°: 2° Stepped<br>smooth                                                                        |                        |                            |                |       | PL(A) = 218.64                          |
| 2083                | PEGMATITE DIKE              |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2082.6' to 2084':<br>90° Undulating smooth,<br>multiple                                         |                        |                            |                |       |                                         |
| 2084                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2084.9°: 67° Planar<br>smooth                                                                        |                        |                            |                |       |                                         |
| 2085                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2085.2°: 67° Planar<br>smooth                                                                        |                        |                            |                |       |                                         |
| 2086                | CORE LOSS                   |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2085.78°: 67° Planar<br>smooth                                                                       |                        |                            |                |       |                                         |
| 455                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2086.6' to 2089':<br>Multiple 60° - 90°<br>fractures along veins                                |                        |                            |                |       |                                         |
| 2090                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2090°: 22° Planar<br>smooth                                                                          |                        |                            |                |       |                                         |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2090.5°: 28° Planar<br>rough                                                                         |                        |                            |                |       |                                         |
| 450                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2091.2°: 0° Planar<br>smooth                                                                         |                        |                            |                |       |                                         |
| 2095                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2092.75' to<br>2095.1': (3) 40° - 88° -<br>74° - 69° Wedges, 74°<br>stress undulating<br>smooth |                        |                            |                |       | UCS =<br>12,776.93<br><br>ITS = 531.03  |
| 445                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2099°: (2) 69° Undulating<br>smooth                                                                  |                        |                            |                |       |                                         |

BORING TYPE: HQ3

DRILLER: Crux

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 2581

WATER OBSERVATIONS: 241 ft, 811 ft, 2336 ft.

CASING: HW to 76 ft.

REMARKS: \_\_\_\_\_

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                    |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|------------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type _____) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)         |
| L                                 | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)         |

(Continued Next Page)



CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2542.7

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2153909.161

DATE: 1/23/2024 - 3/21/2024

PROJECT LOCATION: Rosamod, CA

EASTING: 6515965.764

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities                                                                               |                        | Sampling & In Situ Testing |                |       |                            |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|-----------------------------------------------------------------------------------------------|------------------------|----------------------------|----------------|-------|----------------------------|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear                                                                      | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments |
| 440                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                                                               |                        |                            |                |       |                            |
| 2105                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2100' to 2101':<br>Rubble, 90° fracture                                                  |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2101.7': 84° Planar<br>smooth                                                                 |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2102' to 2108': (8)<br>90° healed open<br>fracture, 70° - 84° stress<br>J, planar smooth |                        |                            |                |       |                            |
| 435                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                                                               |                        |                            |                |       |                            |
| 2110                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2109' to 2110.6':<br>90° S. undulating<br>smooth                                         |                        | C                          | 100            | 62    |                            |
| 430                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                                                               |                        |                            |                |       |                            |
| 2115                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2114' to 2114.9':<br>87° Planar smooth                                                   |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2115' to 2116': 74°<br>Planar smooth                                                     |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2116' to 2123':<br>(19) 60° - 90° Undulating<br>smooth healed open<br>fractures          |                        | C                          | 100            | 51    |                            |
| 425                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                                                               |                        |                            |                |       |                            |
| 2120                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                                                               |                        |                            |                |       |                            |
| 420                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                                                               |                        |                            |                |       |                            |
| 2125                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2125' to 2126':<br>Rubble                                                                |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2127': 64° Undulating<br>smooth                                                               |                        |                            |                |       |                            |
| 415                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2128.7': (2) 70° - 90°<br>Healed fractures                                                    |                        | C                          | 100            | 35    |                            |
| 2130                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                                                               |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2130.8': 32° Planar<br>rough                                                                  |                        |                            |                |       |                            |
| 2131                | PEGMATITE DIKE              |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2131.6': 82° Undulating<br>smooth                                                             |                        |                            |                |       |                            |
| 410                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2132.3': 45° Planar<br>smooth                                                                 |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2133': 45° Planar                                                                             |                        |                            |                |       |                            |

PL(D) = 910.09  
UCS =  
22,893.39  
ITS = 562.52

SLK = Type I

BORING TYPE: HQ3

DRILLER: Crux

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 2581

WATER OBSERVATIONS: 241 ft, 811 ft, 2336 ft.

CASING: HW to 76 ft.

REMARKS:

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                         |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|-----------------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type <u>  </u> ) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)              |
| W                                 | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)              |

(Continued Next Page)



**CLIENT:** Lane Power & Energy Solutions  
**PROJECT:** Hydrostor Zevsar  
**PROJECT LOCATION:** Rosamod, CA

**SURFACE ELEVATION (ft):** 2542.7  
**NORTHING:** 2153909.161  
**EASTING:** 6515965.764

**PROJECT No:** 951-20  
**DATE:** 1/23/2024 - 3/21/2024  
**DIP/AZIMUTH:** -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities                                                                              |                        | Sampling & In Situ Testing |                |       |                                         |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|----------------------------------------------------------------------------------------------|------------------------|----------------------------|----------------|-------|-----------------------------------------|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear                                                                     | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments              |
| 405                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | smooth                                                                                       |                        |                            |                |       | PL(D) = 461.30                          |
| 2140                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2133.4': 80° Undulating<br>smooth                                                            |                        |                            |                |       |                                         |
| 2142                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2134' to 2135': (6)<br>Healed fractures                                                 |                        |                            |                |       |                                         |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2137' to 2142.3':<br>(26) 0° - 40° Undulating<br>smooth, rubble                         |                        | C                          | 100            | 47    |                                         |
| 2145                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2143.3': 45° Undulating<br>rough                                                             |                        |                            |                |       | ITS = 654.32<br><br>SLK = Type I        |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2143.9': 38° Planar<br>smooth                                                                |                        |                            |                |       |                                         |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2144.7': 84° Undulating<br>smooth                                                            |                        |                            |                |       |                                         |
| 2150                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2146.9': 38° Planar<br>smooth                                                                |                        | C                          | 100            | 47    |                                         |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2147.2': 32° Planar<br>smooth                                                                |                        |                            |                |       | PL(A) = 497.05<br>UCS =<br>19,136.48    |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2148.4': (2) 74° Planar<br>rough                                                             |                        |                            |                |       |                                         |
| 2155                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2154.2': 61° Planar<br>rough                                                                 |                        |                            |                |       |                                         |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2156' to 2157': 90°<br>S. planar rough, healed                                          |                        |                            |                |       | SLK = Type I<br><br>PL(D) =<br>1,169.34 |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2157.2': 0° Planar<br>smooth                                                                 |                        | C                          | 100            | 54    |                                         |
| 2160                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2158.2': 86° and 62°<br>Undulating smooth                                                    |                        |                            |                |       |                                         |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2160': 52° Planar rough                                                                      |                        |                            |                |       | SLK = Type I<br><br>PL(D) =<br>1,169.34 |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2160.1' to 2161':<br>(2) 60° - 70° (1) 90°<br>Healed open fracture<br>undulating smooth |                        |                            |                |       |                                         |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2162.8': 0° Undulating<br>rough                                                              |                        |                            |                |       |                                         |
| 2165                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2164': (3) 60° - 74°<br>Undulating smooth                                                    |                        |                            |                |       | SLK = Type I<br><br>PL(D) =<br>1,169.34 |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2165': 29° Planar rough                                                                      |                        |                            |                |       |                                         |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2166' to 2167': (2)<br>10° - 12° Planar rough                                           |                        |                            |                |       |                                         |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2167.1' to 2167.7':<br>Rubble                                                           |                        | C                          | 100            | 32    |                                         |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2168': 0° - 17° Stepped<br>rough                                                             |                        |                            |                |       |                                         |

**BORING TYPE:** HQ3  
**HOLE DEPTH (ft):** 2581  
**REMARKS:**

**DRILLER:** Crux  
**WATER OBSERVATIONS:** 241 ft, 811 ft, 2336 ft.

**LOGGED BY:** Chris Messenger  
**CASING:** HW to 76 ft.

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                               |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|-------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type ) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)    |
| W                                 | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)    |



CLIENT: Lane Power & Energy Solutions  
PROJECT: Hydrostor Zevsar  
PROJECT LOCATION: Rosamod, CA

SURFACE ELEVATION (ft): 2542.7  
NORTHING: 2153909.161  
EASTING: 6515965.764

PROJECT No: 951-20  
DATE: 1/23/2024 - 3/21/2024  
DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata                                                                                    | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities          |                        | Sampling & In Situ Testing |                |       |                            |
|---------------------|----------------------------------------------------------------------------------------------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|--------------------------|------------------------|----------------------------|----------------|-------|----------------------------|
|                     |                                                                                                                | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments |
| 370                 |                                                                                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 2175                |                                                                                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       | PL(A) = 326.27             |
|                     |                                                                                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       | TRI = 14,171.32            |
|                     |                                                                                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       | ITS = 546.64               |
| 365                 |                                                                                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 2180                |                                                                                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
|                     |                                                                                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 360                 |                                                                                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 2185                |                                                                                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       | PL(D) = 105.57             |
|                     |                                                                                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       | UCS =<br>20,616.27         |
|                     |                                                                                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 355                 |                                                                                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 2190                |                                                                                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
|                     |                                                                                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 219                 | QTZ MONZONITE, light gray to white to pink, phaneritic, with K-Na feldspar, biotite, muscovite, and hornblende |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
|                     |                                                                                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 350                 |                                                                                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 2195                |                                                                                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
|                     |                                                                                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 345                 |                                                                                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 2200                |                                                                                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
|                     |                                                                                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 340                 |                                                                                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |

BORING TYPE: HQ3  
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| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                    |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|------------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type _____) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)         |
| L                                 | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)         |





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PROJECT No: 951-20  
DATE: 1/23/2024 - 3/21/2024  
DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft)                                                                                                                                  | Description<br>of<br>Strata                                                  | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft)          |                          | Discontinuities        |      | Sampling & In Situ Testing |       |                            |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
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|                                                                                                                                                      |                                                                              | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       | 0.05<br>0.25<br>0.50<br>2.50<br>5.00 | B - Bedding<br>S - Shear | J - Joint<br>F - Fault | Type | Core<br>Rec. %             | RQD % | Test Results<br>& Comments |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|                                                                                                                                                      |                                                                              |                         |    |    |    |    |                |               |      |          |      |           |         |       |                                      |                          |                        |      |                            |       |                            |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 335<br><br>2210<br><br>221<br>330<br><br>2215<br><br>325<br><br>2220<br><br>320<br><br>2225<br><br>315<br><br>2230<br><br>310<br><br>2235<br><br>305 | QTZ MONZONITE, light to dark gray to green to pink, phaneritic and aphanitic |                         |    |    |    |    |                |               |      |          |      |           |         |       |                                      |                          |                        |      |                            |       |                            |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |

BORING TYPE: HQ3  
HOLE DEPTH (ft): 2581  
REMARKS: \_\_\_\_\_

DRILLER: Crux  
WATER OBSERVATIONS: 241 ft, 811 ft, 2336 ft.

LOGGED BY: Chris Messenger  
CASING: HW to 76 ft.

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                  |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|----------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type ___) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)       |
| WL                                | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)       |

(Continued Next Page)



**CLIENT:** Lane Power & Energy Solutions

**SURFACE ELEVATION (ft):** 2542.7

**PROJECT No:** 951-20

**PROJECT:** Hydrostor Zevsar

**NORTHING:** 2153909.161

**DATE:** 1/23/2024 - 3/21/2024

**PROJECT LOCATION:** Rosamod, CA

EASTING: 6515965.764

DIP/AZIMUTH: -90 /

[illegible]

**BORING TYPE:** HQ3

**DRILLER:** Cruix

**LOGGED BY:** Chris Messenger

**HOLE DEPTH (ft):** 2581

**WATER OBSERVATIONS:** 241 ft, 811 ft, 2336 ft.

**CASING:** HW to 76 ft.

REMARKS:

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                    |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|------------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type _____) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)         |
| W                                 | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)         |

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**CLIENT:** Lane Power & Energy Solutions

**SURFACE ELEVATION (ft):** 2542.7

**PROJECT No:** 951-20

**PROJECT:** Hydrostor Zevsar

**NORTHING:** 2153909.161

**DATE:** 1/23/2024 - 3/21/2024

**PROJECT LOCATION:** Rosamod, CA

**EASTING:** 6515965.764

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata                                                                                                                               | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) |      |      | Discontinuities          |                       | Sampling & In Situ Testing |                                    |              |                            |
|---------------------|-----------------------------------------------------------------------------------------------------------------------------------------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|------|------|--------------------------|-----------------------|----------------------------|------------------------------------|--------------|----------------------------|
|                     |                                                                                                                                                           |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |      | B - Bedding<br>S - Shear | J - Joint<br>F- Fault | Type                       | Core<br>Rec. %                     | RQD %        | Test Results<br>& Comments |
|                     |                                                                                                                                                           | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       | 0.05                        | 0.25 | 0.50 | 2.50                     | 5.00                  |                            |                                    |              |                            |
| 2265                | QTZ MONZONITE, dark gray to light gray, phaneritic, with qtz feldspar, biotite, and hornblende, trace amounts of muscovite, pyrite, chlorite, and epidote |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |      | C                        | 100                   | 25                         | SLK = Type I<br><br>PL(D) = 517.41 |              |                            |
| 2280                |                                                                                                                                                           |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |      |                          |                       |                            |                                    |              |                            |
| 260                 |                                                                                                                                                           |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |      |                          |                       |                            |                                    |              |                            |
| 2285                |                                                                                                                                                           |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |      |                          |                       |                            |                                    |              |                            |
| 2286                |                                                                                                                                                           |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |      |                          |                       |                            |                                    |              |                            |
| 255                 |                                                                                                                                                           |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |      |                          | C                     | 100                        |                                    | 18           |                            |
| 2290                |                                                                                                                                                           |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |      |                          |                       |                            |                                    |              |                            |
| 250                 |                                                                                                                                                           |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |      |                          |                       |                            |                                    |              |                            |
| 2295                |                                                                                                                                                           |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |      |                          |                       |                            |                                    |              |                            |
| 245                 |                                                                                                                                                           |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |      |                          |                       |                            |                                    |              |                            |
| 2300                |                                                                                                                                                           |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |      | C                        | 100                   | 25                         |                                    |              |                            |
| 240                 |                                                                                                                                                           |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |      |                          |                       |                            |                                    |              |                            |
| 2305                |                                                                                                                                                           |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |      |                          |                       |                            |                                    |              |                            |
| 235                 |                                                                                                                                                           |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |      |                          | C                     | 100                        | 10                                 | ITS = 284.59 |                            |

**BORING TYPE:** HQ3

**DRILLER:** Crux

**LOGGED BY:** Chris Messenger

**HOLE DEPTH (ft):** 2581

**WATER OBSERVATIONS:** 241 ft, 811 ft, 2336 ft.

**CASING:** HW to 76 ft.

REMARKS:

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |
|-----------------------------------|---------------|-------|--------------------------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               |
| W                                 | Water level   | PL(D) | Point load diametral test Is(50) (psi)           |
|                                   |               | SLK   | Slake durability test (Type _____)               |
|                                   |               | TRI   | Triaxial stress test (psi)                       |
|                                   |               | UCS   | Uniaxial stress test (psi)                       |

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**CLIENT:** Lane Power & Energy Solutions

**SURFACE ELEVATION (ft):** 2542.7

**PROJECT No:** 951-20

**PROJECT:** Hydrostor Zevsar

**NORTHING:** 2153909.161

**DATE:** 1/23/2024 - 3/21/2024

**PROJECT LOCATION:** Rosamod, CA

**EASTING:** 6515965.764

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata                                                                                                                         | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |          |          |           |           |         | Water | Fracture<br>Spacing<br>(ft) |      |      | Discontinuities                                            |                                                                                                                                                                                                                               | Sampling & In Situ Testing |                       |                                    |                            |
|---------------------|-----------------------------------------------------------------------------------------------------------------------------------------------------|-------------------------|----|----|----|----|----------------|---------------|----------|----------|-----------|-----------|---------|-------|-----------------------------|------|------|------------------------------------------------------------|-------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|----------------------------|-----------------------|------------------------------------|----------------------------|
|                     |                                                                                                                                                     |                         |    |    |    |    |                | Very Soft     | Soft     | Med-Hard | Hard      | Very Hard | Ex Hard |       | 0.05                        | 0.25 | 0.50 | 2.50                                                       | 5.00                                                                                                                                                                                                                          | B - Bedding<br>S - Shear   | J - Joint<br>F- Fault | Type                               | Core<br>Rec. %             |
|                     |                                                                                                                                                     | Fr                      | SA | MA | HA | CA | Very Soft      | Soft          | Med-Hard | Hard     | Very Hard | Ex Hard   | 0.05    | 0.25  | 0.50                        | 2.50 | 5.00 | B - Bedding<br>S - Shear                                   | J - Joint<br>F- Fault                                                                                                                                                                                                         | Type                       | Core<br>Rec. %        | RQD %                              | Test Results<br>& Comments |
| 2300                | QTZ MONZONITE, light gray to white,<br>phaneritic, with qtz feldspar, biotite,<br>and hornblende, trace amounts of<br>pyrite, chlorite, and epidote |                         |    |    |    |    |                |               |          |          |           |           |         |       |                             |      |      | 2309.9': 45° Undulating rough                              |                                                                                                                                                                                                                               |                            |                       | PL(D) = 9.45<br><br>ITS = 230.43   |                            |
| 2315                |                                                                                                                                                     |                         |    |    |    |    |                |               |          |          |           |           |         |       |                             |      |      | -2311.9': 45° Stepped rough                                |                                                                                                                                                                                                                               |                            |                       |                                    |                            |
| 2330                |                                                                                                                                                     |                         |    |    |    |    |                |               |          |          |           |           |         |       |                             |      |      | -2313': 27° Planar smooth<br>From 2313.7' to 2324': Rubble |                                                                                                                                                                                                                               |                            |                       | SLK = Type I<br><br>PL(D) = 946.82 |                            |
| 2320                |                                                                                                                                                     |                         |    |    |    |    |                |               |          |          |           |           |         |       |                             |      |      |                                                            |                                                                                                                                                                                                                               | C                          | 100                   |                                    | 47                         |
| 2325                |                                                                                                                                                     |                         |    |    |    |    |                |               |          |          |           |           |         |       |                             |      |      |                                                            | From 2326' to 2327': (2)<br>25° - 35° Planar smooth                                                                                                                                                                           |                            |                       |                                    | TRI = 5,224.81             |
| 2335                |                                                                                                                                                     |                         |    |    |    |    |                |               |          |          |           |           |         |       |                             |      |      |                                                            | From 2327' to 2328': 79° Undulating rough<br>From 2328' to 2328.3': 45° Planar smooth<br>From 2328.5' to 2332': Rubble                                                                                                        |                            |                       |                                    |                            |
| 2340                |                                                                                                                                                     |                         |    |    |    |    |                |               |          |          |           |           |         |       |                             |      |      |                                                            | -2333': 47° Planar smooth<br>-2334.5': 47° Planar rough<br>From 2335.3' to 2337': Rubble<br>From 2337' to 2340': (4) 60° Undulating rough<br>From 2340' to 2341': Rubble<br>From 2342' to 2347.5': (6) 30° - 42° Planar rough |                            |                       |                                    |                            |
| 2342                |                                                                                                                                                     |                         |    |    |    |    |                |               |          |          |           |           |         |       |                             |      |      |                                                            | C                                                                                                                                                                                                                             | 100                        | 21                    |                                    |                            |

**BORING TYPE:** HQ3

**DRILLER:** CruX

**LOGGED BY:** Chris Messenger

**HOLE DEPTH (ft):** 2581

**WATER OBSERVATIONS:** 241 ft, 811 ft, 2336 ft.

**CASING:** HW to 76 ft.

REMARKS:

| <b><u>SAMPLING &amp; IN SITU TESTING LEGEND</u></b>                                 |               |       |                                                  |
|-------------------------------------------------------------------------------------|---------------|-------|--------------------------------------------------|
|  | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) |
|  | Water seep    | PL(A) | Point load axial test Is(50) (psi)               |
|  | Water level   | PL(D) | Point load diametral test Is(50) (psi)           |
|                                                                                     |               | SLK   | Slake durability test (Type _____)               |
|                                                                                     |               | TRI   | Triaxial stress test (psi)                       |
|                                                                                     |               | UCS   | Uniaxial stress test (psi)                       |

(Continued Next Page)



CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2542.7

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2153909.161

DATE: 1/23/2024 - 3/21/2024

PROJECT LOCATION: Rosamod, CA

EASTING: 6515965.764

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities                                            |                        | Sampling & In Situ Testing |                |       |                            |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|------------------------------------------------------------|------------------------|----------------------------|----------------|-------|----------------------------|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear                                   | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments |
| 195                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                            |                        |                            |                |       | ITS = 844.95               |
| 2350                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                            |                        | C                          | 100            | 26    | ITS = 775.87               |
| 190                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | -2350.3': 69° Planar<br>rough                              |                        |                            |                |       |                            |
| 2355                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2351' to 2352.5':<br>Rubble                           |                        |                            |                |       | PL(D) =<br>1,122.41        |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2352' to 2352.3':<br>0° - 17° Planar rough            |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2353.6': 58° Planar<br>rough                               |                        |                            |                |       | SLK = Type I               |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2354.9' to 2355.7':<br>72° Planar smooth              |                        |                            |                |       | PL(A) = 619.80             |
| 185                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                            |                        |                            |                |       |                            |
| 2360                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | -2358': 55° and 80°<br>Undulating smooth                   |                        | C                          | 100            | 29    |                            |
| 2361                | QTZ MONZONITE               |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2358.65' to 2363':<br>Rubble                          |                        |                            |                |       |                            |
| 180                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                            |                        |                            |                |       |                            |
| 2365                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | -2364.2': 47° Planar<br>smooth                             |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2364.9': 0° Planar<br>smooth                               |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2365.6': 48° Planar                                        |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2367' to 2369':<br>Rubble                             |                        | C                          | 100            | 8     |                            |
| 175                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                            |                        |                            |                |       |                            |
| 2370                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2370' to 2371': (6)<br>40° Planar smooth              |                        |                            |                |       |                            |
| 2371                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                            |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | -2371.9': 61° Planar<br>rough                              |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2372.75': Undulating<br>smooth                             |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2372.9' to 2375.2':<br>(7) 30° - 45° Planar<br>smooth |                        |                            |                |       | PL(D) =<br>1,350.83        |
| 2375                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2376': 48° Undulating<br>smooth                            |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2377': 42° Planar<br>smooth                                |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2377.5' to 2378':<br>42° Planar smooth                |                        | C                          | 100            | 39    |                            |
| 165                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                            |                        |                            |                |       |                            |

BORING TYPE: HQ3

DRILLER: Crux

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 2581

WATER OBSERVATIONS: 241 ft, 811 ft, 2336 ft.

CASING: HW to 76 ft.

REMARKS: \_\_\_\_\_

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                   |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|-----------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type ____) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)        |
| L                                 | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)        |

(Continued Next Page)



**CLIENT:** Lane Power & Energy Solutions  
**PROJECT:** Hydrostor Zevsar  
**PROJECT LOCATION:** Rosamod, CA

**SURFACE ELEVATION (ft):** 2542.7  
**NORTHING:** 2153909.161  
**EASTING:** 6515965.764

**PROJECT No:** 951-20  
**DATE:** 1/23/2024 - 3/21/2024  
**DIP/AZIMUTH:** -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities                                                    |                        | Sampling & In Situ Testing |                |       |                                        |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|--------------------------------------------------------------------|------------------------|----------------------------|----------------|-------|----------------------------------------|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear                                           | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments             |
| 160                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2379.2': 38° Planar rough, 84° Undulating rough                    |                        |                            |                |       | UCS = 30,757.48                        |
| 2385                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2380' to 2381': Rubble                                        |                        |                            |                |       |                                        |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2381.7' to 2382.7': (2) 45° Planar smooth                     |                        |                            |                |       |                                        |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2383.6': 47° Undulating smooth                                     |                        |                            |                |       | PL(A) = 778.03<br><br>PL(D) = 1,035.21 |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2385' to 2386': Rubble                                        |                        |                            |                |       |                                        |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2387': 67° Planar smooth                                           |                        |                            |                |       |                                        |
| 2390                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2387.9': 51° Planar rough                                          | C                      | 100                        | 47             |       | SLK = Type I<br><br>ITS = 886.66       |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2389': 90° Undulating smooth                                       |                        |                            |                |       |                                        |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                                    |                        |                            |                |       |                                        |
| 2395                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2395.3': 42° Planar smooth                                         |                        |                            |                |       | SLK = Type I                           |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2396' to 2397': (5) 30° - 42° Planar rough                    |                        |                            |                |       |                                        |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2398' to 2399': (4) 50° - 67° Planar smooth                   | C                      | 100                        | 40             |       |                                        |
| 2400                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2399': (4) 80° Planar rough                                        |                        |                            |                |       | SLK = Type I                           |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2400' to 2401': 0° - 17° Planar smooth                        |                        |                            |                |       |                                        |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2401.75': 51° Planar smooth                                        |                        |                            |                |       |                                        |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2402.8': 50° Planar smooth                                         |                        |                            |                |       | UCS = 7,538.34                         |
| 2405                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2403' to 2404': Rubble                                        |                        |                            |                |       |                                        |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2405': 70° - 90° Stepped rough                                     |                        |                            |                |       |                                        |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2406' to 2408.8': (10) 10° - 20° Planar smooth                | C                      | 100                        | 18             |       | PL(D) = 1,355.73                       |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2410' to 2411.1': 78° Undulating smooth, 45° Undulating rough |                        |                            |                |       |                                        |
| 2410                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2411.6': 7° Planar smooth                                          |                        |                            |                |       |                                        |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2412.3': 83° Undulating rough                                      |                        |                            |                |       |                                        |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2413.1': 22° Stepped rough                                         |                        |                            |                |       |                                        |

**BORING TYPE:** HQ3  
**HOLE DEPTH (ft):** 2581  
**REMARKS:** \_\_\_\_\_

**DRILLER:** Crux  
**WATER OBSERVATIONS:** 241 ft, 811 ft, 2336 ft.

**LOGGED BY:** Chris Messenger  
**CASING:** HW to 76 ft.

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                    |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|------------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type _____) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)         |
| L                                 | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)         |

(Continued Next Page)



CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2542.7

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2153909.161

DATE: 1/23/2024 - 3/21/2024

PROJECT LOCATION: Rosamod, CA

EASTING: 6515965.764

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities          |                        | Sampling & In Situ Testing |                |       |                            |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|--------------------------|------------------------|----------------------------|----------------|-------|----------------------------|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments |
| 125                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 2420                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 120                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 2425                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 115                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 2430                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 110                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 2435                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 105                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 2440                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 100                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 2445                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 95                  |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |

BORING TYPE: HQ3

DRILLER: Crux

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 2581

WATER OBSERVATIONS: 241 ft, 811 ft, 2336 ft.

CASING: HW to 76 ft.

REMARKS: \_\_\_\_\_

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                    |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|------------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type _____) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)         |
| W                                 | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)         |

(Continued Next Page)



CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2542.7

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2153909.161

DATE: 1/23/2024 - 3/21/2024

PROJECT LOCATION: Rosamod, CA

EASTING: 6515965.764

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities                                                                                    |                        | Sampling & In Situ Testing |                |       |                                                                    |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|----------------------------------------------------------------------------------------------------|------------------------|----------------------------|----------------|-------|--------------------------------------------------------------------|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear                                                                           | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments                                         |
| 90                  |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 84° Planar smooth                                                                                  |                        |                            |                |       |                                                                    |
| 2455                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | -2451.3': 38° Planar smooth                                                                        |                        |                            |                |       |                                                                    |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2453.9' to 2454':<br>Undulating smooth                                                        |                        |                            |                |       |                                                                    |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2454.9': 32° Planar smooth                                                                         |                        |                            |                |       |                                                                    |
| 2460                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2456' to 2461':<br>(17) 10° - 35° Planar smooth                                               |                        | C                          | 100            | 42    |                                                                    |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2462.75' to 2467':<br>(3) 50° - 60° Undulating rough, (1) 80° - 90°<br>Undulating healed open |                        |                            |                |       |                                                                    |
| 2465                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                                                                    |                        |                            |                |       |                                                                    |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                                                                    |                        | C                          | 100            | 38    | UCS =<br>16,272.19<br><br>UCS =<br>13,177.98<br><br>PL(D) = 970.52 |
| 2470                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | -2470.1': 39° Planar smooth                                                                        |                        |                            |                |       |                                                                    |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2472' to 2475.9':<br>42° Planar smooth<br>healed vein                                         |                        |                            |                |       |                                                                    |
| 2475                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                                                                    |                        |                            |                |       |                                                                    |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | -2476.45': 61° Stepped smooth                                                                      |                        |                            |                |       |                                                                    |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                                                                    |                        | C                          | 100            | 58    |                                                                    |
| 2480                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | -2479.2': 47° Undulating smooth                                                                    |                        |                            |                |       |                                                                    |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2481' to 2489': 81° - 84° Planar smooth                                                       |                        |                            |                |       |                                                                    |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2482' to 2483': (2)<br>40° Planar rough                                                       |                        |                            |                |       | PL(D) =<br>1,345.27                                                |

BORING TYPE: HQ3

DRILLER: Crux

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 2581

WATER OBSERVATIONS: 241 ft, 811 ft, 2336 ft.

CASING: HW to 76 ft.

REMARKS: \_\_\_\_\_

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                    |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|------------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type _____) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)         |
| L                                 | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)         |

(Continued Next Page)





CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2542.7

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2153909.161

DATE: 1/23/2024 - 3/21/2024

PROJECT LOCATION: Rosamod, CA

EASTING: 6515965.764

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities                                        |                        | Sampling & In Situ Testing |                |       |                            |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|--------------------------------------------------------|------------------------|----------------------------|----------------|-------|----------------------------|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear                               | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments |
| 55<br>2490          |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2487': 45° Undulating rough                            |                        |                            |                |       | ITS = 1,233.78             |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2488.9': 39° Planar smooth                             |                        | C                          | 100            | 45    | SLK = Type I               |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2489.7': 70° - 90° Stepped and planar rough            |                        |                            |                |       | PL(A) = 1,336.05           |
| 50<br>2495          |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2491.2': 71° Planar rough                              |                        |                            |                |       | ITS = 1,391.22             |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                        |                        |                            |                |       | UCS = 16,976.75            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                        |                        |                            |                |       | TRI = 39,389.37            |
| 45<br>2500          |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2496.8' to 2497.6': 52° - 47° Wedge planar smooth |                        |                            |                |       | SLK = Type I               |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2498.9': 70° Stepped smooth                            |                        | C                          | 100            | 64    | PL(A) = 754.43             |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2499.9': 45° Planar smooth                             |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2500.5': 49° Planar smooth                             |                        |                            |                |       |                            |
| 40<br>2505          |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2502': 17° Planar smooth                               |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2504.1': 70° Planar smooth                             |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2505': 7° Undulating rough                             |                        |                            |                |       |                            |
| 35<br>2510          |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2506' to 2507.3': (3) 50° - 57° Planar smooth     |                        |                            |                |       | PL(D) = 442.58             |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2507.7' to 2511': Rubble                          |                        | C                          | 100            | 47    |                            |
| 2511                | CORE LOSS                   |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                        |                        |                            |                |       |                            |
| 30<br>2515          |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                        |                        |                            |                |       |                            |
| 25<br>2518          |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2518': (4) 45° - 50° Planar smooth                     |                        | C                          | 100            | 7     |                            |

BORING TYPE: HQ3

DRILLER: Crux

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 2581

WATER OBSERVATIONS: 241 ft, 811 ft, 2336 ft.

CASING: HW to 76 ft.

REMARKS: \_\_\_\_\_

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                   |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|-----------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type ____) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)        |
| WL                                | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)        |

(Continued Next Page)





**CLIENT:** Lane Power & Energy Solutions  
**PROJECT:** Hydrostor Zevsar  
**PROJECT LOCATION:** Rosamod, CA

**SURFACE ELEVATION (ft):** 2542.7  
**NORTHING:** 2153909.161  
**EASTING:** 6515965.764

**PROJECT No:** 951-20  
**DATE:** 1/23/2024 - 3/21/2024  
**DIP/AZIMUTH:** -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities                                           |                        | Sampling & In Situ Testing |                |       |                            |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|-----------------------------------------------------------|------------------------|----------------------------|----------------|-------|----------------------------|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear                                  | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments |
| 20                  |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2520': 90° Planar<br>smooth                               |                        |                            |                |       | PL(A) = 664.80             |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2521.2': 47° Planar<br>smooth                             |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2522.6' to 2525':<br>90° Planar smooth               |                        |                            |                |       | PL(D) =<br>1,194.35        |
| -2525               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2524.42': 11° Undulating<br>rough                         |                        |                            |                |       | PL(A) =<br>1,126.08        |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2525.6': 27° Planar<br>smooth                             |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2526' to 2528.5':<br>(5) 35° - 42° Planar<br>smooth  |                        | C                          | 100            | 27    | ITS = 788.68               |
| -2530               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2531' to 2535': (2)<br>60° - 70° Undulating<br>rough |                        |                            |                |       | UCS =<br>19,964.81         |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                           |                        |                            |                |       |                            |
| -2535               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                           |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2536' to 2537': (3)<br>30° - 42° Planar smooth       |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2537.5' to 2539':<br>45° Planar smooth               |                        | C                          | 100            | 59    |                            |
| -2540               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2539.5': 0° Planar<br>smooth                              |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2540.4': 62° Planar<br>rough                              |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2541.5' to 2542.5':<br>84° Stepped rough             |                        |                            |                |       | SLK = Type I               |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2543': 22° Undulating<br>rough                            |                        |                            |                |       | TRI = 40,371.88            |
| -2545               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2545.7': 42° Undulating<br>smooth                         |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2546' to 2547': 67°<br>- 44° Planar smooth           |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2548' to 2551': 40°<br>- 90° Healed open             |                        | C                          | 100            | 39    |                            |
| -2550               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                           |                        |                            |                |       | UCS =<br>14,013.33         |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2552.3': 87° Undulating<br>smooth                         |                        |                            |                |       | SLK = Type I               |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2553': 61° Planar<br>smooth                               |                        |                            |                |       |                            |

**BORING TYPE:** HQ3  
**HOLE DEPTH (ft):** 2581  
**REMARKS:** \_\_\_\_\_

**DRILLER:** Crux  
**WATER OBSERVATIONS:** 241 ft, 811 ft, 2336 ft.

**LOGGED BY:** Chris Messenger  
**CASING:** HW to 76 ft.

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                   |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|-----------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type ____) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)        |
| L                                 | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)        |

(Continued Next Page)



CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2542.7

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2153909.161

DATE: 1/23/2024 - 3/21/2024

PROJECT LOCATION: Rosamod, CA

EASTING: 6515965.764

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata                      | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities          |                        | Sampling & In Situ Testing |                |       |                                       |
|---------------------|--------------------------------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|--------------------------|------------------------|----------------------------|----------------|-------|---------------------------------------|
|                     |                                                  | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments            |
| -15                 |                                                  |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       | PL(D) = 450.49<br>PL(A) = 966.84      |
| -2560               |                                                  |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 36    | TRI = 22,770.84<br>ITS = 1,567.92     |
| -2565               |                                                  |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                       |
| 2568                | QTZ MONZONITE, light gray to pink,<br>phaneritic |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 38    | PL(D) =<br>1,088.56<br>PL(A) = 494.83 |
| -2570               |                                                  |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                       |
| -2575               |                                                  |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                       |
| -2580               |                                                  |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                       |
| -40                 | Bottom of borehole at 2581.0 feet.               |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                       |
| -45                 |                                                  |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                       |

BORING TYPE: HQ3

DRILLER: CruX

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 2581

WATER OBSERVATIONS: 241 ft, 811 ft, 2336 ft.

CASING: HW to 76 ft.

REMARKS: \_\_\_\_\_

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                         |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|-----------------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type <u>  </u> ) |
| W                                 | Water seep    | PL(A) | Point load axial test $I_s(50)$ (psi)            | TRI | Triaxial stress test (psi)              |
| WL                                | Water level   | PL(D) | Point load diametral test $I_s(50)$ (psi)        | UCS | Uniaxial stress test (psi)              |



CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2541.1

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2153505.177

DATE: 4/26/2024 - 5/17/2024

PROJECT LOCATION: Rosamod, CA

EASTING: 6515177.339

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities          |                        | Sampling & In Situ Testing |                |       |                            |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|--------------------------|------------------------|----------------------------|----------------|-------|----------------------------|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments |
| 0<br>2540           | Well Casing                 |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 5<br>2535           |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 10<br>2530          |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 15<br>2525          |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 20<br>2520          |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 25<br>2515          |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 30<br>2510          |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |

BORING TYPE: HQ3

DRILLER: CruX

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 2285

WATER OBSERVATIONS: 730 ft, 828 ft.

CASING: HW to 75 ft.

REMARKS: \_\_\_\_\_

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                    |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|------------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type _____) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)         |
| WL                                | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)         |

(Continued Next Page)



CLIENT: Lane Power & Energy Solutions  
PROJECT: Hydrostor Zevsar  
PROJECT LOCATION: Rosamod, CA

SURFACE ELEVATION (ft): 2541.1  
NORTHING: 2153505.177  
EASTING: 6515177.339

PROJECT No: 951-20  
DATE: 4/26/2024 - 5/17/2024  
DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities          |                        | Sampling & In Situ Testing |                |       |                            |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|--------------------------|------------------------|----------------------------|----------------|-------|----------------------------|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments |
| 2505                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 40                  |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 2500                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 45                  |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 2495                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 50                  |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 2490                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 55                  |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 2485                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 60                  |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 2480                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 65                  |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 2475                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |

BORING TYPE: HQ3  
HOLE DEPTH (ft): 2285  
REMARKS: \_\_\_\_\_

DRILLER: CruX  
WATER OBSERVATIONS: 730 ft, 828 ft.

LOGGED BY: Chris Messenger  
CASING: HW to 75 ft.

| <b>SAMPLING &amp; IN SITU TESTING LEGEND</b> |               |       |                                                  |     |                                    |
|----------------------------------------------|---------------|-------|--------------------------------------------------|-----|------------------------------------|
| C                                            | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type _____) |
| W                                            | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)         |
| WL                                           | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)         |

**CLIENT:** Lane Power & Energy Solutions

**SURFACE ELEVATION (ft):** 2541.1

**PROJECT No:** 951-20

**PROJECT:** Hydrostor Zevsar

**NORTHING:** 2153505.177

**DATE:** 4/26/2024 - 5/17/2024

**PROJECT LOCATION:** Rosamod, CA

**EASTING:** 6515177.339

DIP/AZIMUTH: -90 /

[illegible]

**BORING TYPE:** HQ3

**DRILLER:** Crux

**LOGGED BY:** Chris Messenger

HOLE DEPTH (ft): 2285

**WATER OBSERVATIONS:** 730 ft, 828 ft.

**CASING:** HW to 75 ft.

REMARKS:

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |
|-----------------------------------|---------------|-------|--------------------------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               |
| W                                 | Water level   | PL(D) | Point load diametral test Is(50) (psi)           |
|                                   |               | SLK   | Slake durability test (Type _____)               |
|                                   |               | TRI   | Triaxial stress test (psi)                       |
|                                   |               | UCS   | Uniaxial stress test (psi)                       |

(Continued Next Page)

**CLIENT:** Lane Power & Energy Solutions

**SURFACE ELEVATION (ft):** 2541.1

**PROJECT No:** 951-20

**PROJECT:** Hydrostor Zevsar

**NORTHING:** 2153505.177

**DATE:** 4/26/2024 - 5/17/2024

**PROJECT LOCATION:** Rosamod, CA

**EASTING:** 6515177.339

DIP/AZIMUTH: -90 /

| EL    | DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft)                       | Discontinuities          |                       | Sampling & In Situ Testing |                |       |                            |                                                 |     |
|-------|---------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|---------------------------------------------------|--------------------------|-----------------------|----------------------------|----------------|-------|----------------------------|-------------------------------------------------|-----|
|       |               |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex-Hard |       |                                                   | B - Bedding<br>S - Shear | J - Joint<br>F- Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments |                                                 |     |
| 2435' | -110          |                             | .                       | .  | .  | .  | .  |                | .             | .    | .        | .    | .         | .       |       | From 108' to 120': (19)<br>0° - 17° Planar smooth | C                        | 100                   | 33                         | PL(A) = 73.02  |       |                            |                                                 |     |
| 2430' | .             |                             | .                       | .  | .  | .  | .  |                | .             | .    | .        | .    | .         | .       |       |                                                   |                          |                       |                            |                | .     | .                          | .                                               | .   |
| -115  | 2425'         |                             | .                       | .  | .  | .  | .  |                | .             | .    | .        | .    | .         | .       |       |                                                   | .                        | .                     | .                          |                | .     | .                          | TRI = 12,163.24                                 |     |
| -120  | 2420'         |                             | .                       | .  | .  | .  | .  |                | .             | .    | .        | .    | .         | .       |       |                                                   | .                        | .                     | .                          |                | .     | .                          |                                                 |     |
| -125  | 2415'         |                             | .                       | .  | .  | .  | .  |                | .             | .    | .        | .    | .         | .       |       |                                                   | .                        | .                     | .                          | .              | .     | PL(D) = 49.16              |                                                 |     |
| -130  | 2410'         |                             | .                       | .  | .  | .  | .  |                | .             | .    | .        | .    | .         | .       |       |                                                   | .                        | .                     | .                          | .              | .     |                            | UCS = 6,385.94<br>ITS = 182.34<br>PL(A) = 77.72 |     |
| -135  | 2405'         |                             | .                       | .  | .  | .  | .  |                | .             | .    | .        | .    | .         | .       |       |                                                   | .                        | .                     | .                          | .              | .     | C                          |                                                 | 100 |
|       |               |                             | .                       | .  | .  | .  | .  |                | .             | .    | .        | .    | .         | .       |       |                                                   | .                        | .                     | .                          | .              | .     |                            | C                                               |     |

**BORING TYPE:** HQ3

**DRILLER:** Crux

**LOGGED BY:** Chris Messenger

HOLE DEPTH (ft): 2285

**WATER OBSERVATIONS:** 730 ft, 828 ft.

**CASING:** HW to 75 ft.

REMARKS:

| SAMPLING & IN SITU TESTING LEGEND                                                   |               |       |                                                  |
|-------------------------------------------------------------------------------------|---------------|-------|--------------------------------------------------|
| C                                                                                   | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) |
|  | Water seep    | SLK   | Slake durability test (Type _____)               |
|  | Water level   | PL(A) | Point load axial test (s/50) (psi)               |
|                                                                                     |               | PL(D) | Point load diametral test (s/50) (psi)           |
|                                                                                     |               | TRI   | Triaxial stress test (psi)                       |
|                                                                                     |               | UCS   | Uniaxial stress test (psi)                       |

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**CLIENT:** Lane Power & Energy Solutions  
**PROJECT:** Hydrostor Zevsar  
**PROJECT LOCATION:** Rosamod, CA

**SURFACE ELEVATION (ft):** 2541.1  
**NORTHING:** 2153505.177  
**EASTING:** 6515177.339

**PROJECT No:** 951-20  
**DATE:** 4/26/2024 - 5/17/2024  
**DIP/AZIMUTH:** -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities          |                        | Sampling & In Situ Testing |                |       |                                   |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|--------------------------|------------------------|----------------------------|----------------|-------|-----------------------------------|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments        |
| 2400'               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       | SLK = Type II                     |
| 145                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       | PL(D) = 43.38<br>ITS = 149.02     |
| 2395'               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                   |
| 150                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 61    |                                   |
| 2390'               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       | TRI = 13,862.32<br>UCS = 6,245.10 |
| 155                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                   |
| 2385'               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 62    | PL(D) = 76.18                     |
| 160                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                   |
| 2380'               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                   |
| 165                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                   |
| 2375'               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       | PL(A) = 85.69                     |
| 170                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 75    | TRI = 17,483.60<br>PL(D) = 68.50  |
| 2370'               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                   |

**BORING TYPE:** HQ3  
**HOLE DEPTH (ft):** 2285  
**REMARKS:** \_\_\_\_\_

**DRILLER:** CruX  
**WATER OBSERVATIONS:** 730 ft, 828 ft.

**LOGGED BY:** Chris Messenger  
**CASING:** HW to 75 ft.

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                   |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|-----------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type ____) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)        |
| WL                                | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)        |

(Continued Next Page)



CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2541.1

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2153505.177

DATE: 4/26/2024 - 5/17/2024

PROJECT LOCATION: Rosamod, CA

EASTING: 6515177.339

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities                                   |                        | Sampling & In Situ Testing |                |       |                                   |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|---------------------------------------------------|------------------------|----------------------------|----------------|-------|-----------------------------------|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear                          | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments        |
| 2365                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | Planar rough                                      |                        |                            |                |       |                                   |
| 180                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 177' to 182': 12° -<br>33° Planar smooth     |                        | C                          | 100            | 62    | PL(D) = 89.86<br>PL(A) = 42.77    |
| 2360                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                   |                        |                            |                |       |                                   |
| 185                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 185.9': 45° Planar<br>smooth                      |                        |                            |                |       | ITS = 85.55                       |
| 2355                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 187' to 192': 0° -<br>21° Planar smooth      |                        | C                          | 100            | 74    |                                   |
| 190                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                   |                        |                            |                |       |                                   |
| 2350                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                   |                        |                            |                |       | UCS = 8,802.21<br>TRI = 22,497.75 |
| 195                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 195.8': Undulating<br>smooth                      |                        |                            |                |       |                                   |
| 2345                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 196.4' to 198':<br>Rubble                    |                        | C                          | 100            | 46    | PL(D) = 203.43                    |
| 200                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 198' to 200': (3)<br>30° - 42° Planar smooth |                        |                            |                |       |                                   |
| 2340                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 202': 0° - 27° Planar<br>smooth                   |                        |                            |                |       |                                   |
| 205                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                   |                        |                            |                |       | ITS = 282.53<br>PL(A) = 71.26     |
| 2335                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 206.9': 2° Planar rough                           |                        | C                          | 100            | 53    |                                   |

BORING TYPE: HQ3

DRILLER: Crux

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 2285

WATER OBSERVATIONS: 730 ft, 828 ft.

CASING: HW to 75 ft.

REMARKS: \_\_\_\_\_

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                         |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|-----------------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type <u>  </u> ) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)              |
| L                                 | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)              |

(Continued Next Page)





CLIENT: Lane Power & Energy Solutions  
PROJECT: Hydrostor Zevsar  
PROJECT LOCATION: Rosamod, CA

SURFACE ELEVATION (ft): 2541.1  
NORTHING: 2153505.177  
EASTING: 6515177.339

PROJECT No: 951-20  
DATE: 4/26/2024 - 5/17/2024  
DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities          |                        | Sampling & In Situ Testing |                |       |                            |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|--------------------------|------------------------|----------------------------|----------------|-------|----------------------------|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments |
| 2330                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 211.2': 7° Planar rough  |                        |                            |                |       | SLK = Type II              |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 212.75': 11° Undulating  |                        |                            |                |       | PL(D) = 25.41              |
| 215                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 2325                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 46    |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 220                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 2320                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       | PL(A) = 88.68              |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       | UCS = 346.71               |
| 225                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 2315                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       | PL(A) = 72.78              |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 230                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 39    |                            |
| 2310                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 235                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 2305                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       | ITS = 187.90               |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 240                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 46    |                            |
| 2300                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       | PL(D) = 45.96              |

BORING TYPE: HQ3  
HOLE DEPTH (ft): 2285  
REMARKS: \_\_\_\_\_

DRILLER: Crux  
WATER OBSERVATIONS: 730 ft, 828 ft.

LOGGED BY: Chris Messenger  
CASING: HW to 75 ft.

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                  |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|----------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type ___) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)       |
| WL                                | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)       |

(Continued Next Page)



CLIENT: Lane Power & Energy Solutions  
PROJECT: Hydrostor Zevsar  
PROJECT LOCATION: Rosamod, CA

SURFACE ELEVATION (ft): 2541.1  
NORTHING: 2153505.177  
EASTING: 6515177.339

PROJECT No: 951-20  
DATE: 4/26/2024 - 5/17/2024  
DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities          |                        | Sampling & In Situ Testing |                |       |                            |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|--------------------------|------------------------|----------------------------|----------------|-------|----------------------------|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments |
| 2295                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       | UCS = 5,081.44             |
| 250                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 52    | PL(D) = 34.64              |
| 2290                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       | PL(A) = 70.54              |
| 255                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       | PL(D) = 64.55              |
| 2285                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 54    | ITS = 387.53               |
| 260                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       | UCS = 6,203.76             |
| 2280                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       | PL(A) = 67.27              |
| 265                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 2275                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 42    |                            |
| 270                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       | SLK = Type I               |
| 2270                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 275                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 2265                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       | PL(A) = 64.75              |

BORING TYPE: HQ3  
HOLE DEPTH (ft): 2285  
REMARKS:

DRILLER: Crux  
WATER OBSERVATIONS: 730 ft, 828 ft.

LOGGED BY: Chris Messenger  
CASING: HW to 75 ft.

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                  |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|----------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type ___) |
| W                                 | Water seep    | PL(A) | Point load axial test $I_s(50)$ (psi)            | TRI | Triaxial stress test (psi)       |
| L                                 | Water level   | PL(D) | Point load diametral test $I_s(50)$ (psi)        | UCS | Uniaxial stress test (psi)       |

(Continued Next Page)

**CLIENT:** Lane Power & Energy Solutions

**SURFACE ELEVATION (ft):** 2541.1

**PROJECT No:** 951-20

**PROJECT:** Hydrostor Zevsar

**NORTHING:** 2153505.177

**DATE:** 4/26/2024 - 5/17/2024

**PROJECT LOCATION:** Rosamod, CA

**EASTING:** 6515177.339

DIP/AZIMUTH: -90 /

[illegible]

**BORING TYPE:** HQ3

**DRILLER:** Crux

**LOGGED BY:** Chris Messenger

HOLE DEPTH (ft): 2285

**WATER OBSERVATIONS:** 730 ft, 828 ft.

**CASING:** HW to 75 ft.

REMARKS:

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |
|-----------------------------------|---------------|-------|--------------------------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               |
| W                                 | Water level   | PL(D) | Point load diametral test Is(50) (psi)           |
|                                   |               | SLK   | Slake durability test (Type _____)               |
|                                   |               | TRI   | Triaxial stress test (psi)                       |
|                                   |               | UCS   | Uniaxial stress test (psi)                       |

(Continued Next Page)



CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2541.1

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2153505.177

DATE: 4/26/2024 - 5/17/2024

PROJECT LOCATION: Rosamod, CA

EASTING: 6515177.339

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata                                                                                                                         | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities          |                        | Sampling & In Situ Testing |                |       |                                 |
|---------------------|-----------------------------------------------------------------------------------------------------------------------------------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|--------------------------|------------------------|----------------------------|----------------|-------|---------------------------------|
|                     |                                                                                                                                                     | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments      |
| 315                 | QTZ MONZONITE, light gray,<br>aphanitic/phaneritic                                                                                                  |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       | ITS = 339.85                    |
| 2225                |                                                                                                                                                     |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 25    |                                 |
| 320                 |                                                                                                                                                     |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       | PL(A) = 37.47<br>UCS = 2,558.32 |
| 2220                |                                                                                                                                                     |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                 |
| 325                 |                                                                                                                                                     |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                 |
| 2215                |                                                                                                                                                     |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 13    | PL(D) = 95.69                   |
| 330                 |                                                                                                                                                     |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                 |
| 2210                |                                                                                                                                                     |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                 |
| 335                 |                                                                                                                                                     |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                 |
| 2205                |                                                                                                                                                     |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 16    | PL(A) = 39.24<br>PL(D) = 27.47  |
| 340                 |                                                                                                                                                     |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                 |
| 2200                |                                                                                                                                                     |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                 |
| 345                 |                                                                                                                                                     |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                 |
| 2195                | QTZ MONZONITE, light gray to white,<br>phaneritic, with K-Na-Ca feldspar,<br>biotite, hornblende, and trace amounts<br>of pyrite, chlorite, epidote |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 32    | PL(D) = 92.19<br>ITS = 215.08   |
| 350                 |                                                                                                                                                     |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                 |
| 353                 |                                                                                                                                                     |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                 |

BORING TYPE: HQ3

DRILLER: Crux

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 2285

WATER OBSERVATIONS: 730 ft, 828 ft.

CASING: HW to 75 ft.

REMARKS: \_\_\_\_\_

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                  |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|----------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type ___) |
| W                                 | Water seep    | PL(A) | Point load axial test $I_s(50)$ (psi)            | TRI | Triaxial stress test (psi)       |
| WL                                | Water level   | PL(D) | Point load diametral test $I_s(50)$ (psi)        | UCS | Uniaxial stress test (psi)       |

**CLIENT:** Lane Power & Energy Solutions

**SURFACE ELEVATION (ft):** 2541.1

**PROJECT No:** 951-20

**PROJECT:** Hydrostor Zevsar

**NORTHING:** 2153505.177

**DATE:** 4/26/2024 - 5/17/2024

**PROJECT LOCATION:** Rosamod, CA

**EASTING:** 6515177.339

DIP/AZIMUTH: -90 /

[illegible]

**BORING TYPE:** HQ3

**DRILLER:** Crux

**LOGGED BY:** Chris Messenger

HOLE DEPTH (ft): 2285

**WATER OBSERVATIONS:** 730 ft, 828 ft.

**CASING:** HW to 75 ft.

REMARKS:

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |
|-----------------------------------|---------------|-------|--------------------------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               |
| W                                 | Water level   | PL(D) | Point load diametral test Is(50) (psi)           |
|                                   |               | SLK   | Slake durability test (Type _____)               |
|                                   |               | TRI   | Triaxial stress test (psi)                       |
|                                   |               | UCS   | Uniaxial stress test (psi)                       |

(Continued Next Page)



CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2541.1

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2153505.177

DATE: 4/26/2024 - 5/17/2024

PROJECT LOCATION: Rosamod, CA

EASTING: 6515177.339

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities          |                        | Sampling & In Situ Testing |                |       |                                |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|--------------------------|------------------------|----------------------------|----------------|-------|--------------------------------|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments     |
| 2155                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       | PL(A) = 41.06                  |
| 390                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 33    |                                |
| 2150                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       | PL(A) = 47.96<br>PL(D) = 31.49 |
| 395                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                |
| 2145                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 6     |                                |
| 400                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       | PL(A) = 39.60                  |
| 2140                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                |
| 405                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                |
| 2135                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 0     |                                |
| 410                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                |
| 2130                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                |
| 415                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                |
| 2125                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 18    |                                |

BORING TYPE: HQ3

DRILLER: Crux

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 2285

WATER OBSERVATIONS: 730 ft, 828 ft.

CASING: HW to 75 ft.

REMARKS: \_\_\_\_\_

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                  |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|----------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type ___) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)       |
| WL                                | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)       |

(Continued Next Page)



CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2541.1

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2153505.177

DATE: 4/26/2024 - 5/17/2024

PROJECT LOCATION: Rosamod, CA

EASTING: 6515177.339

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities          |                        | Sampling & In Situ Testing |                |       |                                |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|--------------------------|------------------------|----------------------------|----------------|-------|--------------------------------|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments     |
| 2120                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       | PL(D) = 42.96                  |
| 425                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                |
| 2115                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 11    | ITS = 17.13                    |
| 430                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                |
| 2110                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       | PL(A) = 133.68                 |
| 435                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                |
| 2105                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 44    | ITS = 439.14                   |
| 440                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                |
| 2100                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                |
| 445                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                |
| 2095                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 18    | PL(D) = 41.81<br>PL(A) = 57.71 |
| 450                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                |
| 2090                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                |

BORING TYPE: HQ3

DRILLER: Crux

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 2285

WATER OBSERVATIONS: 730 ft, 828 ft.

CASING: HW to 75 ft.

REMARKS: \_\_\_\_\_

| <b><u>SAMPLING &amp; IN SITU TESTING LEGEND</u></b> |               |       |                                                  |     |                                    |
|-----------------------------------------------------|---------------|-------|--------------------------------------------------|-----|------------------------------------|
| C                                                   | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type _____) |
| W                                                   | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)         |
| WL                                                  | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)         |

(Continued Next Page)



CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2541.1

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2153505.177

DATE: 4/26/2024 - 5/17/2024

PROJECT LOCATION: Rosamod, CA

EASTING: 6515177.339

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities          |                        | Sampling & In Situ Testing |                |       |                                 |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|--------------------------|------------------------|----------------------------|----------------|-------|---------------------------------|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments      |
| 2085                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       | SLK = Type I                    |
| 460                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 25    | PL(A) = 406.25                  |
| 2080                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       | PL(D) = 42.77<br>UCS = 3,515.77 |
| 465                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                 |
| 2075                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                 |
| 470                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 36    | ITS = 171.01                    |
| 2070                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                 |
| 475                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       | PL(D) = 131.52                  |
| 2065                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                 |
| 480                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 47    | PL(D) = 31.31<br>UCS = 2,915.03 |
| 2060                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                 |
| 485                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                 |
| 2055                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       | SLK = Type II                   |

BORING TYPE: HQ3

DRILLER: Crux

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 2285

WATER OBSERVATIONS: 730 ft, 828 ft.

CASING: HW to 75 ft.

REMARKS: \_\_\_\_\_

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                   |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|-----------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type ____) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)        |
| L                                 | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)        |

(Continued Next Page)





CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2541.1

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2153505.177

DATE: 4/26/2024 - 5/17/2024

PROJECT LOCATION: Rosamod, CA

EASTING: 6515177.339

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities          |                       | Sampling & In Situ Testing |                |       |                               |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|--------------------------|-----------------------|----------------------------|----------------|-------|-------------------------------|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear | J - Joint<br>F- Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments    |
| 2050                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                               |
| 495                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                               |
| 2045                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       | C                          | 100            | 19    |                               |
| 500                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                               |
| 2040                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       | PL(D) = 116.94                |
| 505                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                               |
| 2035                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       | C                          | 100            | 23    |                               |
| 510                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       | PL(A) = 79.13<br>ITS = 424.29 |
| 2030                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                               |
| 515                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       | PL(A) = 160.89                |
| 2025                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       | C                          | 100            | 21    |                               |
| 520                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       | PL(D) = 98.09                 |
| 2020                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                               |

BORING TYPE: HQ3

DRILLER: CruX

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 2285

WATER OBSERVATIONS: 730 ft, 828 ft.

CASING: HW to 75 ft.

REMARKS: \_\_\_\_\_

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                   |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|-----------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type ____) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)        |
| L                                 | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)        |

(Continued Next Page)



CLIENT: Lane Power & Energy Solutions  
PROJECT: Hydrostor Zevsar  
PROJECT LOCATION: Rosamod, CA

SURFACE ELEVATION (ft): 2541.1  
NORTHING: 2153505.177  
EASTING: 6515177.339

PROJECT No: 951-20  
DATE: 4/26/2024 - 5/17/2024  
DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities                                                  |                        | Sampling & In Situ Testing |                |       |                                                 |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|------------------------------------------------------------------|------------------------|----------------------------|----------------|-------|-------------------------------------------------|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear                                         | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments                      |
| 2015                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | Planar rough                                                     |                        |                            |                |       |                                                 |
| 530                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 525' to 527': (4)<br>25° - 71° Undulating<br>smooth         |                        | C                          | 100            | 17    | PL(D) = 103.78<br><br>SLK = Type I              |
| 2010                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 528': 38° Planar smooth                                          |                        |                            |                |       |                                                 |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 528.9': 17° Planar<br>smooth                                     |                        |                            |                |       |                                                 |
| 535                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 530' to 531':<br>Rubble, (3) 20° - 32°                      |                        |                            |                |       | UCS = 2,627.13<br>ITS = 109.52<br>PL(A) = 26.90 |
| 2005                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 532.9': 32° Planar<br>smooth                                     |                        |                            |                |       |                                                 |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 535' to 539': (14)<br>0° - 29° Planar breaks<br>(Rubble)    |                        | C                          | 100            | 21    |                                                 |
| 540                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 540' to 546':<br>Multiple 30° - 45° Planar<br>Smooth        |                        |                            |                |       | UCS = 6,077.09                                  |
| 2000                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                                  |                        |                            |                |       |                                                 |
| 545                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                                  |                        |                            |                |       | PL(D) = 770.18                                  |
| 1995                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 546' to 551':<br>Rubble                                     |                        | C                          | 100            | 7     |                                                 |
| 550                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                                  |                        |                            |                |       |                                                 |
| 1990                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 552' to 554': (4)<br>60-70° Undulating<br>smooth, rubble    |                        |                            |                |       | PL(A) = 73.87                                   |
| 555                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                                  |                        |                            |                |       | PL(D) = 100.06                                  |
| 1985                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 555.6': 67° Planar<br>smooth                                     |                        |                            |                |       |                                                 |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 556.3' to 558.6':<br>(4) 40° - 50° Planar<br>rough / smooth |                        | C                          | 100            | 17    | UCS = 3,304.84                                  |

BORING TYPE: HQ3  
HOLE DEPTH (ft): 2285  
REMARKS: \_\_\_\_\_

DRILLER: Crux  
WATER OBSERVATIONS: 730 ft, 828 ft.

LOGGED BY: Chris Messenger  
CASING: HW to 75 ft.

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                    |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|------------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type _____) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)         |
| WL                                | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)         |

(Continued Next Page)



CLIENT: Lane Power & Energy Solutions  
PROJECT: Hydrostor Zevsar  
PROJECT LOCATION: Rosamod, CA

SURFACE ELEVATION (ft): 2541.1  
NORTHING: 2153505.177  
EASTING: 6515177.339

PROJECT No: 951-20  
DATE: 4/26/2024 - 5/17/2024  
DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) |                        | Discontinuities |                                                   | Sampling & In Situ Testing |     |     |                                  |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|------------------------|-----------------|---------------------------------------------------|----------------------------|-----|-----|----------------------------------|
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                        |                 |                                                   | Test Results<br>& Comments |     |     |                                  |
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       | B - Bedding<br>S - Shear    | J - Joint<br>F - Fault | Type            | Core<br>Rec. %                                    | RQD %                      |     |     |                                  |
| 1980                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                        |                 | From 560' to 560.4': 90°<br>Undulating smooth     |                            |     |     | ITS = 377.96                     |
| 565                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                        |                 | From 561' to 567': (7)<br>10° - 35° Planar rough  |                            |     |     | PL(D) = 308.76                   |
| 1975                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                        |                 |                                                   |                            |     |     | PL(A) = 76.86                    |
| 570                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                        |                 | 570': 67° Undulating<br>smooth                    |                            |     |     |                                  |
| 1970                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                        |                 | From 571' to 573': (5)<br>60° - 70° Planar smooth |                            |     |     |                                  |
| 575                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                        |                 | 574.2': 62° Undulating<br>smooth                  |                            |     |     |                                  |
| 1965                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                        |                 | 576': 69° Undulating<br>rough                     |                            |     |     |                                  |
| 580                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                        |                 | From 576.5' to 580':<br>Rubble                    |                            | C   | 100 | 22                               |
| 1960                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                        |                 | From 582' to 585': (9)<br>10° - 42° Planar smooth |                            |     |     | ITS = 368.89                     |
| 585                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                        |                 | From 585' to 590':<br>Multiple planar smooth      |                            |     |     | PL(D) = 125.01                   |
| 1955                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                        |                 |                                                   | C                          | 100 | 34  | UCS = 4,436.99<br>PL(D) = 915.86 |
| 590                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                        |                 |                                                   |                            |     |     | PL(A) = 192.08                   |
| 1950                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                        |                 |                                                   |                            |     |     |                                  |

BORING TYPE: HQ3  
HOLE DEPTH (ft): 2285  
REMARKS: \_\_\_\_\_

DRILLER: Crux  
WATER OBSERVATIONS: 730 ft, 828 ft.

LOGGED BY: Chris Messenger  
CASING: HW to 75 ft.

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                   |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|-----------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type ____) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)        |
| WL                                | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)        |

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**CLIENT:** Lane Power & Energy Solutions

**SURFACE ELEVATION (ft):** 2541.1

**PROJECT No:** 951-20

**PROJECT:** Hydrostor Zevsar

**NORTHING:** 2153505.177

**DATE:** 4/26/2024 - 5/17/2024

**PROJECT LOCATION:** Rosamod, CA

**EASTING:** 6515177.339

DIP/AZIMUTH: -90 /

[illegible]

**BORING TYPE:** HQ3

**DRILLER:** Crux

**LOGGED BY:** Chris Messenger

HOLE DEPTH (ft): 2285

**WATER OBSERVATIONS:** 730 ft, 828 ft.

**CASING:** HW to 75 ft.

REMARKS:

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |
|-----------------------------------|---------------|-------|--------------------------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               |
| W                                 | Water level   | PL(D) | Point load diametral test Is(50) (psi)           |
|                                   |               | SLK   | Slake durability test (Type _____)               |
|                                   |               | TRI   | Triaxial stress test (psi)                       |
|                                   |               | UCS   | Uniaxial stress test (psi)                       |

(Continued Next Page)



CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2541.1

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2153505.177

DATE: 4/26/2024 - 5/17/2024

PROJECT LOCATION: Rosamod, CA

EASTING: 6515177.339

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata                                                                                                  | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities | Sampling & In Situ Testing                          |                                                     |                                                             |                |               |                            |                               |
|---------------------|------------------------------------------------------------------------------------------------------------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|-----------------|-----------------------------------------------------|-----------------------------------------------------|-------------------------------------------------------------|----------------|---------------|----------------------------|-------------------------------|
|                     |                                                                                                                              | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             |                 | B - Bedding<br>S - Shear                            | J - Joint<br>F- Fault                               | Type                                                        | Core<br>Rec. % | RQD %         | Test Results<br>& Comments |                               |
| 1910                | QTZ MONZONITE, light gray to white, phaneritic, with qtz feldspar, biotite, trace amounts of mica, pyrite, chlorite, epidote |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                 | From 629.7' to 630': 90° vert, undulating smooth    |                                                     |                                                             |                | PL(D) = 52.97 |                            |                               |
| 635                 |                                                                                                                              |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                 |                                                     | From 632.5' to 632.75': (3) 11° - 17° Planar smooth |                                                             |                |               |                            |                               |
| 1905                |                                                                                                                              |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                 |                                                     | 634.75': 51° Planar rough                           |                                                             |                |               |                            |                               |
| 640                 |                                                                                                                              |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | C               | 100                                                 | 34                                                  | From 638' to 641': 99° Undulating rough, rubble             |                |               | ITS = 366.89               |                               |
| 1900                |                                                                                                                              |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                 |                                                     |                                                     |                                                             |                |               |                            |                               |
| 645                 |                                                                                                                              |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                 |                                                     |                                                     | From 644' to 645': 78° Planar smooth, rubble                |                |               |                            |                               |
| 1895                |                                                                                                                              |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                 |                                                     |                                                     | From 645' to 650': (5) 70° - 90° Undulating smooth          | C              | 100           | 10                         | PL(D) = 52.97<br>ITS = 784.22 |
| 650                 |                                                                                                                              |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                 |                                                     |                                                     | From 650' to 658': Rubble                                   |                |               |                            |                               |
| 1890                |                                                                                                                              |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                 |                                                     |                                                     |                                                             |                |               |                            | PL(A) = 38.12                 |
| 655                 |                                                                                                                              |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                 |                                                     |                                                     | From 658' to 659': (5) 70° - 80° Stress free, planar smooth | C              | 100           | 0                          |                               |
| 1885                |                                                                                                                              |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                 | From 660' to 675': (46) 20° - 90° Fractures, rubble |                                                     |                                                             |                |               |                            |                               |
| 660                 |                                                                                                                              |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                 |                                                     |                                                     |                                                             |                |               |                            |                               |
| 1880                |                                                                                                                              |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                 |                                                     |                                                     |                                                             |                |               |                            |                               |

BORING TYPE: HQ3

DRILLER: Crux

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 2285

WATER OBSERVATIONS: 730 ft, 828 ft.

CASING: HW to 75 ft.

REMARKS: \_\_\_\_\_

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                  |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|----------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type ___) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)       |
| L                                 | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)       |

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**CLIENT:** Lane Power & Energy Solutions

**SURFACE ELEVATION (ft):** 2541.1

**PROJECT No:** 951-20

**PROJECT:** Hydrostor Zevsar

**NORTHING:** 2153505.177

**DATE:** 4/26/2024 - 5/17/2024

**PROJECT LOCATION:** Rosamod, CA

**EASTING:** 6515177.339

DIP/AZIMUTH: -90 /

[illegible]

**BORING TYPE:** HQ3

**DRILLER:** Crux

**LOGGED BY:** Chris Messenger

HOLE DEPTH (ft): 2285

WATER OBSERVATIONS: 730 ft, 828 ft.

**CASING:** HW to 75 ft.

REMARKS:

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |
|-----------------------------------|---------------|-------|--------------------------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) |
| W                                 | Water seep    | PL(A) | Point load axial test 1s(50) (psi)               |
| W                                 | Water level   | PL(D) | Point load diametral test 1s(50) (psi)           |
|                                   |               | SLK   | Slake durability test (Type _____)               |
|                                   |               | TRI   | Triaxial stress test (psi)                       |
|                                   |               | UCS   | Uniaxial stress test (psi)                       |

(Continued Next Page)



CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2541.1

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2153505.177

DATE: 4/26/2024 - 5/17/2024

PROJECT LOCATION: Rosamod, CA

EASTING: 6515177.339

DIP/AZIMUTH: -90 /

| EL   | DEPTH<br>(ft) | Description<br>of<br>Strata                          | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft)                   | Discontinuities | Sampling & In Situ Testing |                        |                 |                |
|------|---------------|------------------------------------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------------------------|-----------------|----------------------------|------------------------|-----------------|----------------|
|      |               |                                                      | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                                               |                 | B - Bedding<br>S - Shear   | J - Joint<br>F - Fault | Type            | Core<br>Rec. % |
| 1840 |               |                                                      |                         |    |    |    |    |                |               |      |          |      |           |         |       | 699': 0° Planar rough                         |                 |                            |                        |                 |                |
|      | 705           |                                                      |                         |    |    |    |    |                |               |      |          |      |           |         |       | 704.6': 68° Planar rough                      |                 |                            |                        |                 |                |
| 1835 |               |                                                      |                         |    |    |    |    |                |               |      |          |      |           |         |       | 706.25': 0° - 61° Planar,<br>undulating rough | C               | 100                        | 69                     | PL(D) = 777.75  |                |
|      | 710           |                                                      |                         |    |    |    |    |                |               |      |          |      |           |         |       |                                               |                 |                            |                        | TRI = 20,031.34 |                |
| 1830 |               |                                                      |                         |    |    |    |    |                |               |      |          |      |           |         |       |                                               |                 |                            |                        | SLK = Type I    |                |
|      | 715           |                                                      |                         |    |    |    |    |                |               |      |          |      |           |         |       | 713.2': 2° Planar rough                       |                 |                            |                        |                 |                |
|      | 716           | QTZ MONZONITE, light gray to dark<br>gray, aphanitic |                         |    |    |    |    |                |               |      |          |      |           |         |       | 714': 8° Planar smooth                        |                 |                            |                        | ITS = 435.38    |                |
| 1825 |               |                                                      |                         |    |    |    |    |                |               |      |          |      |           |         |       |                                               | C               | 100                        | 57                     | UCS = 7,455.70  |                |
|      | 720           |                                                      |                         |    |    |    |    |                |               |      |          |      |           |         |       |                                               |                 |                            |                        | PL(A) = 518.98  |                |
| 1820 |               |                                                      |                         |    |    |    |    |                |               |      |          |      |           |         |       |                                               |                 |                            |                        | PL(D) = 29.30   |                |
|      | 725           |                                                      |                         |    |    |    |    |                |               |      |          |      |           |         |       |                                               |                 |                            |                        |                 |                |
| 1815 |               |                                                      |                         |    |    |    |    |                |               |      |          |      |           |         |       |                                               | C               | 100                        | 31                     | UCS = 1,840.32  |                |
|      | 730           |                                                      |                         |    |    |    |    |                |               |      |          |      |           |         |       |                                               |                 |                            |                        | PL(A) = 26.08   |                |
| 1810 |               |                                                      |                         |    |    |    |    |                |               |      |          |      |           |         |       |                                               |                 |                            |                        |                 |                |
|      | 733           | QTZ MONZONITE, light gray to white,<br>phaneritic    |                         |    |    |    |    |                |               |      |          |      |           |         |       |                                               |                 |                            |                        |                 |                |

BORING TYPE: HQ3

DRILLER: Crux

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 2285

WATER OBSERVATIONS: 730 ft, 828 ft.

CASING: HW to 75 ft.

REMARKS: \_\_\_\_\_

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                         |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|-----------------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type <u>  </u> ) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)              |
| W                                 | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)              |

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CLIENT: Lane Power & Energy Solutions  
PROJECT: Hydrostor Zevsar  
PROJECT LOCATION: Rosamod, CA

SURFACE ELEVATION (ft): 2541.1  
NORTHING: 2153505.177  
EASTING: 6515177.339

PROJECT No: 951-20  
DATE: 4/26/2024 - 5/17/2024  
DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities                                |                        | Sampling & In Situ Testing |                |       |                                  |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|------------------------------------------------|------------------------|----------------------------|----------------|-------|----------------------------------|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear                       | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments       |
| 1805                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 735' to 736': 17° - 29° Planar smooth     |                        |                            |                |       |                                  |
| 740                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 737.7' to 742': 90° fractures, rubble     | C                      | 100                        | 14             |       |                                  |
| 1800                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                |                        |                            |                |       | PL(D) = 110.32<br>PL(A) = 19.81  |
| 745                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 743.9': 69° Undulating smooth                  |                        |                            |                |       |                                  |
| 1795                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 744' to 745': (2) 40° - 50° Planar smooth |                        |                            |                |       |                                  |
| 750                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 745.8': Undulating smooth                      | C                      | 100                        | 34             |       |                                  |
| 1790                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 746.3': Undulating smooth                      |                        |                            |                |       |                                  |
| 755                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 748': Planar smooth                            |                        |                            |                |       |                                  |
| 1785                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 749.75' to 750': Rubble                   |                        |                            |                |       |                                  |
| 760                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 750' to 753': (3) 0° - 11° Planar smooth  |                        |                            |                |       |                                  |
| 1780                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 753' to 755': 90° Stepped smooth          |                        |                            |                |       |                                  |
| 765                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 755' to 756': Rubble                      |                        |                            |                |       |                                  |
| 1775                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 756.7': 84° Undulating rough                   | C                      | 100                        | 35             |       |                                  |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 758' to 759': (2) 76° - 81° Planar smooth |                        |                            |                |       |                                  |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 760' to 763': (4) 42° - 61° Planar smooth |                        |                            |                |       |                                  |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                |                        |                            |                |       | UCS = 6,465.23<br>PL(D) = 402.87 |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                |                        |                            |                |       |                                  |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 765': 40° Planar smooth                        |                        |                            |                |       |                                  |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 766' to 767': 51° - 72° Wedge             | C                      | 100                        | 68             |       |                                  |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                |                        |                            |                |       | UCS = 8,992.07                   |

BORING TYPE: HQ3  
HOLE DEPTH (ft): 2285  
REMARKS: \_\_\_\_\_

DRILLER: Crux  
WATER OBSERVATIONS: 730 ft, 828 ft.

LOGGED BY: Chris Messenger  
CASING: HW to 75 ft.

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                    |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|------------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type _____) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)         |
| WL                                | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)         |

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CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2541.1

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2153505.177

DATE: 4/26/2024 - 5/17/2024

PROJECT LOCATION: Rosamod, CA

EASTING: 6515177.339

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata                                                                                            | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities          |                        | Sampling & In Situ Testing |                |       |                            |
|---------------------|------------------------------------------------------------------------------------------------------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|--------------------------|------------------------|----------------------------|----------------|-------|----------------------------|
|                     |                                                                                                                        | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments |
| 1770                |                                                                                                                        |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 775                 |                                                                                                                        |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1765                |                                                                                                                        |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 780                 |                                                                                                                        |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1760                |                                                                                                                        |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 785                 |                                                                                                                        |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1755                |                                                                                                                        |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 790                 |                                                                                                                        |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1750                |                                                                                                                        |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 795                 |                                                                                                                        |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1745                |                                                                                                                        |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 800                 |                                                                                                                        |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1740                |                                                                                                                        |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
|                     | QTZ MONZONITE, light gray to white, phaneritic, with feldspar, biotite, hornblende, trace amounts of muscovite, pyrite |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |

BORING TYPE: HQ3

DRILLER: Crux

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 2285

WATER OBSERVATIONS: 730 ft, 828 ft.

CASING: HW to 75 ft.

REMARKS: \_\_\_\_\_

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                   |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|-----------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type ____) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)        |
| WL                                | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)        |

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**CLIENT:** Lane Power & Energy Solutions  
**PROJECT:** Hydrostor Zevsar  
**PROJECT LOCATION:** Rosamod, CA

**SURFACE ELEVATION (ft):** 2541.1  
**NORTHING:** 2153505.177  
**EASTING:** 6515177.339

**PROJECT No:** 951-20  
**DATE:** 4/26/2024 - 5/17/2024  
**DIP/AZIMUTH:** -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata                                                                       | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft)                  |                          | Discontinuities       |      | Sampling & In Situ Testing |       |                            |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
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|                     |                                                                                                   | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       | 0.05<br>0.25<br>0.50<br>1.00<br>2.50<br>5.00 | B - Bedding<br>S - Shear | J - Joint<br>F- Fault | Type | Core<br>Rec. %             | RQD % | Test Results<br>& Comments |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|                     |                                                                                                   |                         |    |    |    |    |                |               |      |          |      |           |         |       |                                              |                          |                       |      |                            |       |                            |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1735                | QTZ MONZONITE, light gray to white, phaneritic, with feldspar, trace amounts of muscovite, pyrite |                         |    |    |    |    |                |               |      |          |      |           |         |       |                                              |                          |                       |      |                            |       |                            |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |

**BORING TYPE:** HQ3  
**HOLE DEPTH (ft):** 2285  
**REMARKS:**

**DRILLER:** Crux  
**WATER OBSERVATIONS:** 730 ft, 828 ft.

**LOGGED BY:** Chris Messenger  
**CASING:** HW to 75 ft.

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                  |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|----------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type ___) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)       |
| W                                 | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)       |

(Continued Next Page)



CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2541.1

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2153505.177

DATE: 4/26/2024 - 5/17/2024

PROJECT LOCATION: Rosamod, CA

EASTING: 6515177.339

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata                                                                                                               | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities                                           |                        | Sampling & In Situ Testing |                |       |                                                    |
|---------------------|-------------------------------------------------------------------------------------------------------------------------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|-----------------------------------------------------------|------------------------|----------------------------|----------------|-------|----------------------------------------------------|
|                     |                                                                                                                                           | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear                                  | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments                         |
| 1700                |                                                                                                                                           |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 839.6': 8° Planar smooth                                  |                        |                            |                |       | PL(D) = 421.72<br><br>UCS = 6,371.04               |
| 845                 |                                                                                                                                           |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 841' to 844': (8) 0°<br>- 9° Planar smooth,<br>rough |                        |                            |                |       |                                                    |
| 1695                |                                                                                                                                           |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 845' to 846': (3) 0°<br>- 17° Planar rough           |                        |                            |                |       |                                                    |
| 850                 |                                                                                                                                           |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                           |                        | C                          | 100            | 35    |                                                    |
| 1690                |                                                                                                                                           |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 851.9' to 854':<br>Rubble                            |                        |                            |                |       | PL(A) = 77.81                                      |
| 855                 |                                                                                                                                           |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 854' to 855': (3) 0°<br>- 7° Planar smooth           |                        |                            |                |       |                                                    |
| 1685                |                                                                                                                                           |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 856': 39° Planar smooth                                   |                        |                            |                |       |                                                    |
| 860                 |                                                                                                                                           |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 857': 42° Planar smooth                                   |                        |                            |                |       | PL(D) = 592.94<br><br>PL(A) = 360.53               |
| 1680                |                                                                                                                                           |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 858': 84° Undulating<br>rough                             |                        |                            |                |       |                                                    |
| 865                 |                                                                                                                                           |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 859.6': 80° Undulating<br>smooth                          |                        |                            |                |       |                                                    |
| 1675                |                                                                                                                                           |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 862': 90° Rough                                           |                        |                            |                |       | ITS = 408.19<br><br>SLK = Type I<br>PL(D) = 618.82 |
| 870                 |                                                                                                                                           |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 863' to 865':<br>Rubble                              |                        |                            |                |       |                                                    |
| 1670                |                                                                                                                                           |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 865.5': 67° Planar rough                                  |                        |                            |                |       |                                                    |
| 872                 | QTZ MONZONITE, light gray to white,<br>phaneritic, with feldspar, biotite,<br>hornblende, trace amounts of<br>muscovite, pyrite, chlorite |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 866.2': 17° Planar<br>smooth                              |                        |                            |                |       | ITS = 408.19<br><br>SLK = Type I<br>PL(D) = 618.82 |
|                     |                                                                                                                                           |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 867': 61° Planar rough                                    |                        |                            |                |       |                                                    |
|                     |                                                                                                                                           |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 868.9': 74° - 35°<br>Stepped rough                        |                        |                            |                |       |                                                    |
|                     |                                                                                                                                           |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 871.9': 7° Planar rough                                   |                        |                            |                |       |                                                    |
|                     |                                                                                                                                           |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 872.6' to 873': 79°<br>Rough                         |                        |                            |                |       |                                                    |
|                     |                                                                                                                                           |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 873' to 874.6': 82°<br>Planar rough                  |                        |                            |                |       |                                                    |

BORING TYPE: HQ3

DRILLER: Crux

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 2285

WATER OBSERVATIONS: 730 ft, 828 ft.

CASING: HW to 75 ft.

REMARKS: \_\_\_\_\_

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                   |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|-----------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type ____) |
| W                                 | Water seep    | PL(A) | Point load axial test $I_s(50)$ (psi)            | TRI | Triaxial stress test (psi)        |
| WL                                | Water level   | PL(D) | Point load diametral test $I_s(50)$ (psi)        | UCS | Uniaxial stress test (psi)        |

(Continued Next Page)



CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2541.1

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2153505.177

DATE: 4/26/2024 - 5/17/2024

PROJECT LOCATION: Rosamod, CA

EASTING: 6515177.339

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities          |                        | Sampling & In Situ Testing |                |       |                            |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|--------------------------|------------------------|----------------------------|----------------|-------|----------------------------|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments |
| 1665                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 880                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1660                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 885                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1655                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 890                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1650                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 895                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1645                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 900                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1640                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 905                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1635                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |

BORING TYPE: HQ3

DRILLER: Crux

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 2285

WATER OBSERVATIONS: 730 ft, 828 ft.

CASING: HW to 75 ft.

REMARKS: \_\_\_\_\_

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                         |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|-----------------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type <u>  </u> ) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)              |
| WL                                | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)              |

(Continued Next Page)



CLIENT: Lane Power & Energy Solutions  
PROJECT: Hydrostor Zevsar  
PROJECT LOCATION: Rosamod, CA

SURFACE ELEVATION (ft): 2541.1  
NORTHING: 2153505.177  
EASTING: 6515177.339

PROJECT No: 951-20  
DATE: 4/26/2024 - 5/17/2024  
DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) |      | Discontinuities |                                                                | Sampling & In Situ Testing                                  |      |                          |                        |                |                                   |                |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|------|-----------------|----------------------------------------------------------------|-------------------------------------------------------------|------|--------------------------|------------------------|----------------|-----------------------------------|----------------|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       | 0.05                        | 0.25 | 0.50            | 1.00                                                           | 2.50                                                        | 5.00 | B - Bedding<br>S - Shear | J - Joint<br>F - Fault | Type           | Core<br>Rec. %                    | RQD %          |
| 1630                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |                 | 909.7': (2) 67° Planar smooth                                  |                                                             |      |                          |                        | PL(D) = 309.47 |                                   |                |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |                 |                                                                | From 911' to 915': (5) 40° - 60° Planar smooth              |      |                          |                        |                | PL(D) = 908.69<br>UCS = 10,324.29 |                |
| 915                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |                 |                                                                |                                                             |      |                          |                        |                |                                   |                |
| 1625                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |                 |                                                                | From 916' to 916.7': 80° Planar rough                       |      |                          |                        |                |                                   |                |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |                 |                                                                |                                                             |      | C                        | 100                    | 35             | ITS = 534.93                      |                |
| 920                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |                 |                                                                |                                                             |      |                          |                        |                |                                   | PL(D) = 164.73 |
| 1620                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |                 |                                                                | 921': 0° Planar smooth                                      |      |                          |                        |                |                                   |                |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |                 |                                                                | From 921.3' to 922.5': Rubble                               |      |                          |                        |                |                                   |                |
| 925                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |                 |                                                                | From 923' to 925': (3), 0° Planar and 90° vertical / smooth |      |                          |                        |                |                                   |                |
| 1615                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |                 |                                                                | 925': 71° Planar                                            |      |                          |                        |                |                                   |                |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |                 |                                                                | 925.5': 70° Planar smooth                                   |      |                          |                        |                |                                   |                |
| 930                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |                 |                                                                | 927.2': 81° Undulating smooth                               |      |                          | C                      | 100            | 28                                |                |
| 1610                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |                 |                                                                | 929': 84° Planar smooth                                     |      |                          |                        |                |                                   |                |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |                 |                                                                | From 929.5' to 930': Rubble                                 |      |                          |                        |                |                                   |                |
| 935                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |                 |                                                                | 930': 71° Planar                                            |      |                          |                        |                |                                   |                |
| 1605                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |                 |                                                                | 931.3': 27° Undulating rough                                |      |                          |                        |                |                                   |                |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |                 |                                                                | 932': 38° Planar rough                                      |      |                          |                        |                |                                   |                |
| 940                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |                 |                                                                | 932.8': 57° Undulating smooth                               |      |                          |                        |                |                                   |                |
| 1600                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |                 |                                                                | From 933' to 934': 79° Undulating smooth                    |      |                          |                        |                |                                   | PL(D) = 305.61 |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |                 | From 935' to 940': (7) 22° - 45° Planar smooth                 |                                                             |      | C                        | 100                    | 45             | PL(A) = 54.45<br>UCS = 2,923.14   |                |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |                 |                                                                |                                                             |      |                          |                        |                |                                   |                |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |                 | From 940' to 942': (1) 90° Planar rough, 90° Undulating smooth |                                                             |      |                          |                        |                |                                   |                |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |                 |                                                                |                                                             |      |                          |                        |                | SLK = Type I                      |                |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |                 | From 944' to 945': 90° Planar smooth                           |                                                             |      |                          |                        |                |                                   |                |

BORING TYPE: HQ3  
HOLE DEPTH (ft): 2285  
REMARKS: \_\_\_\_\_

DRILLER: Crux  
WATER OBSERVATIONS: 730 ft, 828 ft.

LOGGED BY: Chris Messenger  
CASING: HW to 75 ft.

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                   |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|-----------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type ____) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)        |
| W                                 | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)        |

(Continued Next Page)



CLIENT: Lane Power & Energy Solutions  
PROJECT: Hydrostor Zevsar  
PROJECT LOCATION: Rosamod, CA

SURFACE ELEVATION (ft): 2541.1  
NORTHING: 2153505.177  
EASTING: 6515177.339

PROJECT No: 951-20  
DATE: 4/26/2024 - 5/17/2024  
DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities                                  |                        | Sampling & In Situ Testing |                |       |                                                              |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|--------------------------------------------------|------------------------|----------------------------|----------------|-------|--------------------------------------------------------------|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear                         | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments                                   |
| 1595                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 945': 67° Planar rough                           |                        |                            |                |       | PL(D) = 904.30<br>PL(A) = 446.95<br>PL(A) = 106.70           |
| 950                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 947' to 950': (4)<br>20° - 30° Planar rough | C                      | 100                        | 61             |       |                                                              |
| 1590                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                  |                        |                            |                |       |                                                              |
| 955                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 952.3': 90° Planar                               |                        |                            |                |       | PL(D) = 734.45<br><br>UCS =<br>11,227.11<br><br>ITS = 915.98 |
| 1585                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 954': 50° - 60° Planar<br>smooth                 |                        |                            |                |       |                                                              |
| 960                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 955' to 956': (3)<br>30° Planar smooth      | C                      | 100                        | 58             |       |                                                              |
| 1580                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 957.7' to 960':<br>Rubble                   |                        |                            |                |       | UCS = 7,009.49<br><br>PL(D) =<br>1,388.35                    |
| 965                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 960' to 961': 90°<br>Undulating rough       |                        |                            |                |       |                                                              |
| 1575                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 961.3': 25° Planar                               |                        |                            |                |       |                                                              |
| 970                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 964.3': 47° Undulating<br>rough                  |                        |                            |                |       |                                                              |
| 1570                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 965.3': 72° Undulating<br>smooth                 | C                      | 100                        | 61             |       |                                                              |
| 975                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 971': 69° Planar smooth                          |                        |                            |                |       |                                                              |
| 1565                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 972': 79° Planar rough                           |                        |                            |                |       |                                                              |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 974': 87° Planar rough                           |                        |                            |                |       |                                                              |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 975.5': 61° Planar<br>smooth                     |                        |                            |                |       |                                                              |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 976.6': 0° Planar smooth                         |                        |                            |                |       |                                                              |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 978.3': 12° Planar rough                         | C                      | 100                        | 50             |       |                                                              |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 978.5' to 979.6':<br>(2) 62°-71° Undulating |                        |                            |                |       |                                                              |

BORING TYPE: HQ3  
HOLE DEPTH (ft): 2285  
REMARKS: \_\_\_\_\_

DRILLER: Crux  
WATER OBSERVATIONS: 730 ft, 828 ft.

LOGGED BY: Chris Messenger  
CASING: HW to 75 ft.

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                  |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|----------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type ___) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)       |
| WL                                | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)       |

(Continued Next Page)



CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2541.1

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2153505.177

DATE: 4/26/2024 - 5/17/2024

PROJECT LOCATION: Rosamod, CA

EASTING: 6515177.339

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities                                    |                        | Sampling & In Situ Testing |                |       |                                  |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|----------------------------------------------------|------------------------|----------------------------|----------------|-------|----------------------------------|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear                           | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments       |
| 1560                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | rough                                              |                        |                            |                |       |                                  |
| 985                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 981.6' to 982': 80°<br>Undulating rough       |                        |                            |                |       |                                  |
| 1555                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 983': 3° Planar smooth                             |                        |                            |                |       |                                  |
| 990                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 986' to 987.7': (4)<br>30 - 40° Planar smooth |                        | C                          | 100            | 43    | SLK = Type I                     |
| 1550                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 991': 4° Planar smooth                             |                        |                            |                |       |                                  |
| 995                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 991.7' to 991.8': 4°<br>Planar smooth         |                        |                            |                |       |                                  |
| 1545                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 993.4': 90° Undulating<br>rough                    |                        |                            |                |       |                                  |
| 1000                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 995': 47° Planar rough                             |                        |                            |                |       |                                  |
| 1540                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 997' to 1000': (4)<br>20° - 45° Planar smooth |                        | C                          | 100            | 54    | PL(A) = 932.47<br>PL(D) = 565.73 |
| 1005                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1001': 38° Planar<br>smooth                        |                        |                            |                |       |                                  |
| 1535                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1004.1': Irregular 71°<br>rough                    |                        |                            |                |       |                                  |
| 1010                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1005.5' to 1006':<br>(2) 20° Planar smooth    |                        |                            |                |       |                                  |
| 1530                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1008': 0° Planar smooth                            |                        | C                          | 100            | 71    | ITS = 268.69<br>PL(D) = 145.43   |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1009.1': 42° Planar<br>smooth                      |                        |                            |                |       |                                  |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1014': 61° Planar rough                            |                        |                            |                |       | UCS =<br>13,555.81               |

BORING TYPE: HQ3

DRILLER: Crux

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 2285

WATER OBSERVATIONS: 730 ft, 828 ft.

CASING: HW to 75 ft.

REMARKS: \_\_\_\_\_

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                         |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|-----------------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type <u>  </u> ) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)              |
| W                                 | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)              |

(Continued Next Page)





CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2541.1

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2153505.177

DATE: 4/26/2024 - 5/17/2024

PROJECT LOCATION: Rosamod, CA

EASTING: 6515177.339

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities          |                        | Sampling & In Situ Testing |                |       |                            |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|--------------------------|------------------------|----------------------------|----------------|-------|----------------------------|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments |
| 1525                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1020                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       | ITS = 322.42               |
| 1020                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       | PL(D) = 736.55             |
| 1025                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1025                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1030                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1030                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1035                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1035                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1040                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1040                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1045                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1045                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1495                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |

BORING TYPE: HQ3

DRILLER: Crux

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 2285

WATER OBSERVATIONS: 730 ft, 828 ft.

CASING: HW to 75 ft.

REMARKS: \_\_\_\_\_

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                   |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|-----------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type ____) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)        |
| W                                 | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)        |

(Continued Next Page)





CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2541.1

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2153505.177

DATE: 4/26/2024 - 5/17/2024

PROJECT LOCATION: Rosamod, CA

EASTING: 6515177.339

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata                       | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities          |                        | Sampling & In Situ Testing |                |       |                                  |
|---------------------|---------------------------------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|--------------------------|------------------------|----------------------------|----------------|-------|----------------------------------|
|                     |                                                   | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments       |
| 1490                |                                                   |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       | PL(D) = 506.52                   |
| 1055                |                                                   |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       | PL(A) = 99.14                    |
| 1485                |                                                   |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       | ITS = 922.67                     |
| 1060                |                                                   |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 59    |                                  |
| 1480                |                                                   |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                  |
| 1065                |                                                   |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                  |
| 1475                |                                                   |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       | UCS = 5,476.04                   |
| 1070                |                                                   |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 80    | PL(D) = 832.97<br>PL(A) = 566.91 |
| 1470                |                                                   |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       | PL(D) = 631.07<br>PL(A) = 339.47 |
| 1075                |                                                   |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                  |
| 1465                |                                                   |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                  |
| 1080                | QTZ MONZONITE, light gray to white,<br>phaneritic |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 58    | PL(D) = 579.90                   |
| 1460                |                                                   |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       | ITS = 875.88<br>UCS = 14,462.72  |

BORING TYPE: HQ3

DRILLER: Crux

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 2285

WATER OBSERVATIONS: 730 ft, 828 ft.

CASING: HW to 75 ft.

REMARKS: \_\_\_\_\_

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                    |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|------------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type _____) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)         |
| L                                 | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)         |

(Continued Next Page)



CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2541.1

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2153505.177

DATE: 4/26/2024 - 5/17/2024

PROJECT LOCATION: Rosamod, CA

EASTING: 6515177.339

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities                                                   |                        | Sampling & In Situ Testing |                |       |                            |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|-------------------------------------------------------------------|------------------------|----------------------------|----------------|-------|----------------------------|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear                                          | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments |
| 1455                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 22° - 47° Undulating rough                                        |                        | C                          | 100            | 42    | PL(A) = 694.19             |
| 1090                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1090' to 1095':<br>(16) 90° - 45° Multiple fractures, rubble |                        |                            |                |       |                            |
| 1450                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                                   |                        |                            |                |       |                            |
| 1095                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1095' to 1099':<br>Rubble                                    |                        | C                          | 100            | 47    | ITS = 855.86               |
| 1445                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                                   |                        |                            |                |       |                            |
| 1100                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1100' to 1101': 40°<br>- 45° Planar rough                    |                        |                            |                |       | UCS = 7,763.07             |
| 1440                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1102.2': 45° Undulating smooth                                    |                        |                            |                |       | TRI = 7,802.98             |
| 1105                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1103.9' to 1104.7':<br>70° - 90° Planar smooth               |                        |                            |                |       |                            |
| 1435                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1105' to 1109.3':<br>(9) 35° - 45° Planar smooth             |                        | C                          | 100            | 16    | PL(D) = 688.01             |
| 1110                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                                   |                        |                            |                |       | PL(A) = 4.90               |
| 1430                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1111.3' to 1113':<br>Rubble                                  |                        |                            |                |       | PL(D) = 704.28             |
| 1115                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1113.5' to 1114':<br>(2) 45° Planar rough                    |                        |                            |                |       | SLK = Type I               |
| 1425                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1115' to 1125':<br>Heavily fractured throughout              |                        | C                          | 100            | 9     |                            |

BORING TYPE: HQ3

DRILLER: Crux

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 2285

WATER OBSERVATIONS: 730 ft, 828 ft.

CASING: HW to 75 ft.

REMARKS: \_\_\_\_\_

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                   |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|-----------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type ____) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)        |
| L                                 | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)        |

(Continued Next Page)



**CLIENT:** Lane Power & Energy Solutions  
**PROJECT:** Hydrostor Zevsar  
**PROJECT LOCATION:** Rosamod, CA

**SURFACE ELEVATION (ft):** 2541.1  
**NORTHING:** 2153505.177  
**EASTING:** 6515177.339

**PROJECT No:** 951-20  
**DATE:** 4/26/2024 - 5/17/2024  
**DIP/AZIMUTH:** -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities          |                        | Sampling & In Situ Testing |                |       |                                                     |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|--------------------------|------------------------|----------------------------|----------------|-------|-----------------------------------------------------|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments                          |
| 1420                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       | PL(A) = 363.95                                      |
| 1125                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                                     |
| 1415                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       | PL(D) = 284.53<br>PL(A) = 716.47<br>TRI = 17,978.32 |
| 1130                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       | UCS = 9,638.25                                      |
| 1410                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                                     |
| 1135                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                                     |
| 1405                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                                     |
| 1140                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                                     |
| 1400                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                                     |
| 1145                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                                     |
| 1395                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                                     |
| 1150                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       | ITS = 772.00<br>PL(D) = 568.62                      |
| 1390                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       | PL(A) = 40.22                                       |

**BORING TYPE:** HQ3  
**HOLE DEPTH (ft):** 2285  
**REMARKS:**

**DRILLER:** Crux  
**WATER OBSERVATIONS:** 730 ft, 828 ft.

**LOGGED BY:** Chris Messenger  
**CASING:** HW to 75 ft.

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                         |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|-----------------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type <u>  </u> ) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)              |
| WL                                | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)              |

(Continued Next Page)



**CLIENT:** Lane Power & Energy Solutions  
**PROJECT:** Hydrostor Zevsar  
**PROJECT LOCATION:** Rosamod, CA

**SURFACE ELEVATION (ft):** 2541.1  
**NORTHING:** 2153505.177  
**EASTING:** 6515177.339

**PROJECT No:** 951-20  
**DATE:** 4/26/2024 - 5/17/2024  
**DIP/AZIMUTH:** -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata                                                                                                                  | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft)          | Discontinuities                                                     |                        | Sampling & In Situ Testing |                |       |                                                                     |
|---------------------|----------------------------------------------------------------------------------------------------------------------------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|--------------------------------------|---------------------------------------------------------------------|------------------------|----------------------------|----------------|-------|---------------------------------------------------------------------|
|                     |                                                                                                                                              | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                                      | B - Bedding<br>S - Shear                                            | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments                                          |
| 1155<br>1385        | QTZ MONZONITE, light gray to white, phaneritic, with Ca - Na - K feldspar, biotite, hornblende, trace amounts of muscovite, pyrite, chlorite |                         |    |    |    |    |                |               |      |          |      |           |         |       | 0.05<br>0.25<br>0.50<br>2.50<br>5.00 |                                                                     |                        |                            |                |       | PL(A) = 993.11<br>SLK = Type I<br>UCS = 8,139.46<br>TRI = 42,771.22 |
| 1160<br>1380        |                                                                                                                                              |                         |    |    |    |    |                |               |      |          |      |           |         |       |                                      | From 1158' to 1160': (3)<br>50° - 60° Undulating<br>smooth          |                        | C                          | 100            | 69    |                                                                     |
| 1165<br>1375        |                                                                                                                                              |                         |    |    |    |    |                |               |      |          |      |           |         |       |                                      | From 1161' to 1163':<br>1161, 1161.9, 1163 0° -<br>11° Planar rough |                        |                            |                |       | PL(D) = 614.89<br>UCS =<br>11,040.83                                |
| 1170<br>1370        |                                                                                                                                              |                         |    |    |    |    |                |               |      |          |      |           |         |       |                                      | -1163.7': 67° Stepped<br>rough                                      |                        |                            |                |       |                                                                     |
| 1175<br>1365        |                                                                                                                                              |                         |    |    |    |    |                |               |      |          |      |           |         |       |                                      | From 1165' to 1166': (2)<br>19° - 38° Planar rough                  |                        | C                          | 100            | 77    |                                                                     |
| 1180<br>1360        |                                                                                                                                              |                         |    |    |    |    |                |               |      |          |      |           |         |       |                                      | From 1170' to 1172.2':<br>74° Undulating smooth                     |                        |                            |                |       | PL(D) = 320.72                                                      |
| 1185<br>1355        |                                                                                                                                              |                         |    |    |    |    |                |               |      |          |      |           |         |       |                                      | -1178.9': 49° Stepped<br>rough                                      |                        | C                          | 100            | 42    |                                                                     |
|                     |                                                                                                                                              |                         |    |    |    |    |                |               |      |          |      |           |         |       |                                      | 1179.4': 12° Planar<br>smooth                                       |                        |                            |                |       | PL(A) = 391.48                                                      |
|                     |                                                                                                                                              |                         |    |    |    |    |                |               |      |          |      |           |         |       |                                      | From 1180' to 1182':<br>Planar smooth                               |                        |                            |                |       |                                                                     |
|                     |                                                                                                                                              |                         |    |    |    |    |                |               |      |          |      |           |         |       |                                      | From 1180.5' to 1185':<br>(9) 45° - 67° Planar<br>rough             |                        |                            |                |       |                                                                     |
|                     |                                                                                                                                              |                         |    |    |    |    |                |               |      |          |      |           |         |       |                                      | From 1185' to 1190': (6)<br>67° - 84° Planar smooth                 |                        | C                          | 100            | 27    | ITS = 829.26                                                        |

**BORING TYPE:** HQ3  
**HOLE DEPTH (ft):** 2285  
**REMARKS:** \_\_\_\_\_

**DRILLER:** Crux  
**WATER OBSERVATIONS:** 730 ft, 828 ft.

**LOGGED BY:** Chris Messenger  
**CASING:** HW to 75 ft.

| SAMPLING & IN SITU TESTING LEGEND |                                                      |                                       |  |  |
|-----------------------------------|------------------------------------------------------|---------------------------------------|--|--|
| C Core drilling                   | ITS Indirect tensile strength (Brazilian) test (psi) | SLK Slake durability test (Type ____) |  |  |
| W Water seep                      | PL(A) Point load axial test Is(50) (psi)             | TRI Triaxial stress test (psi)        |  |  |
| W Water level                     | PL(D) Point load diametral test Is(50) (psi)         | UCS Uniaxial stress test (psi)        |  |  |

(Continued Next Page)



CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2541.1

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2153505.177

DATE: 4/26/2024 - 5/17/2024

PROJECT LOCATION: Rosamod, CA

EASTING: 6515177.339

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata                       | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities                                            |                        | Sampling & In Situ Testing |                |       |                                  |
|---------------------|---------------------------------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|------------------------------------------------------------|------------------------|----------------------------|----------------|-------|----------------------------------|
|                     |                                                   | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear                                   | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments       |
| 1350                |                                                   |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | -1190.9': 12° Planar<br>smooth                             |                        |                            |                |       | SLK = 1 type I                   |
| 1195                |                                                   |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1192' to 1193': (3)<br>70° - 80° Undulating<br>smooth |                        |                            |                |       | PL(A) = 376.86                   |
| 1345                |                                                   |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | -1193.6': 17° Planar<br>rough                              |                        |                            |                |       |                                  |
| 1200                |                                                   |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | -1194.4': 45° Planar<br>rough                              |                        |                            |                |       | PL(D) = 115.72                   |
| 1340                | QTZ MONZONITE, light gray to white,<br>phaneritic |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1195' to 1200': (7)<br>30° - 42° Planar smooth        |                        | C                          | 100            | 26    |                                  |
| 1205                |                                                   |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1200' to 1206':<br>Rubble                             |                        |                            |                |       |                                  |
| 1335                |                                                   |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1206' to 1209': 0° -<br>17° smooth                    |                        | C                          | 100            | 31    | PL(D) = 344.44                   |
| 1210                |                                                   |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1209' to 1213': 90°<br>Undulating smooth              |                        |                            |                |       |                                  |
| 1330                |                                                   |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                            |                        |                            |                |       | PL(D) =<br>1,112.47              |
| 1215                |                                                   |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1216': 30° Planar rough                                    |                        |                            |                |       | PL(A) = 722.01                   |
| 1325                |                                                   |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1217' to 1228':<br>Rubble                             |                        | C                          | 100            | 19    | UCS = 7,809.38<br>UCS = 3,766.60 |
| 1220                |                                                   |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                            |                        |                            |                |       |                                  |
| 1320                |                                                   |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                            |                        |                            |                |       | PL(A) = 30.98                    |

BORING TYPE: HQ3

DRILLER: CruX

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 2285

WATER OBSERVATIONS: 730 ft, 828 ft.

CASING: HW to 75 ft.

REMARKS: \_\_\_\_\_

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                         |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|-----------------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type <u>  </u> ) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)              |
| WL                                | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)              |

(Continued Next Page)



CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2541.1

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2153505.177

DATE: 4/26/2024 - 5/17/2024

PROJECT LOCATION: Rosamod, CA

EASTING: 6515177.339

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities          |                        | Sampling & In Situ Testing |                |       |                            |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|--------------------------|------------------------|----------------------------|----------------|-------|----------------------------|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments |
| 1315                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1230                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1310                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1235                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1305                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1240                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1300                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1245                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1295                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1250                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1290                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1255                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1285                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |

BORING TYPE: HQ3

DRILLER: CruX

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 2285

WATER OBSERVATIONS: 730 ft, 828 ft.

CASING: HW to 75 ft.

REMARKS: \_\_\_\_\_

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                   |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|-----------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type ____) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)        |
| WL                                | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)        |

(Continued Next Page)



CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2541.1

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2153505.177

DATE: 4/26/2024 - 5/17/2024

PROJECT LOCATION: Rosamod, CA

EASTING: 6515177.339

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities                                 |                        | Sampling & In Situ Testing |                |       |                             |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|-------------------------------------------------|------------------------|----------------------------|----------------|-------|-----------------------------|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear                        | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments  |
| 1280                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1260' to 1275':<br>Rubble                  |                        |                            |                |       |                             |
| 1265                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                 |                        | C                          | 100            | 17    |                             |
| 1270                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                 |                        |                            |                |       |                             |
| 1275                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1275' to 1280': (3)<br>40° - 45° fractures |                        | C                          | 100            | 48    |                             |
| 1265                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                 |                        |                            |                |       |                             |
| 1280                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1280' to 1282':<br>Rubble                  |                        |                            |                |       |                             |
| 1260                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1282' to 1284': (8)<br>30° Planar smooth   |                        |                            |                |       | SLK = Type I<br>ITS = 53.93 |
| 1285                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1285' to 1286':<br>Rubble                  |                        |                            |                |       | PL(A) = 18.50               |
| 1255                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1287' to 1590': 22°<br>- 32° Planar smooth |                        | C                          | 100            | 31    | PL(D) = 49.07               |
| 1290                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1290' to 1305':<br>Rubble                  |                        |                            |                |       |                             |
| 1250                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                 |                        |                            |                |       |                             |

BORING TYPE: HQ3

DRILLER: Crux

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 2285

WATER OBSERVATIONS: 730 ft, 828 ft.

CASING: HW to 75 ft.

REMARKS: \_\_\_\_\_

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                  |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|----------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type ___) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)       |
| WL                                | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)       |

(Continued Next Page)



CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2541.1

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2153505.177

DATE: 4/26/2024 - 5/17/2024

PROJECT LOCATION: Rosamod, CA

EASTING: 6515177.339

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities          |                        | Sampling & In Situ Testing |                |       |                            |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|--------------------------|------------------------|----------------------------|----------------|-------|----------------------------|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments |
| 1245                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1300                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 13    |                            |
| 1240                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1305                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1235                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 30    |                            |
| 1310                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1230                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1315                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1225                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 36    |                            |
| 1320                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1220                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1325                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1215                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 16    | ITS = 592.82               |

BORING TYPE: HQ3

DRILLER: Crux

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 2285

WATER OBSERVATIONS: 730 ft, 828 ft.

CASING: HW to 75 ft.

REMARKS: \_\_\_\_\_

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                  |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|----------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type ___) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)       |
| L                                 | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)       |

(Continued Next Page)



**CLIENT:** Lane Power & Energy Solutions

**SURFACE ELEVATION (ft):** 2541.1

**PROJECT No:** 951-20

**PROJECT:** Hydrostor Zevsar

**NORTHING:** 2153505.177

**DATE:** 4/26/2024 - 5/17/2024

**PROJECT LOCATION:** Rosamod, CA

**EASTING:** 6515177.339

DIP/AZIMUTH: -90 /

[illegible]

**BORING TYPE:** HQ3

**DRILLER:** Crux

**LOGGED BY:** Chris Messenger

HOLE DEPTH (ft): 2285

WATER OBSERVATIONS: 730 ft, 828 ft.

**CASING:** HW to 75 ft.

REMARKS:

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                    |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|------------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type _____) |
| W                                 | Water seep    | PL(A) | Point load axial test 1s(50) (psi)               | TRI | Triaxial stress test (psi)         |
| W                                 | Water level   | PL(D) | Point load diametral test 1s(50) (psi)           | UCS | Uniaxial stress test (psi)         |

(Continued Next Page)



CLIENT: Lane Power & Energy Solutions  
PROJECT: Hydrostor Zevsar  
PROJECT LOCATION: Rosamod, CA

SURFACE ELEVATION (ft): 2541.1  
NORTHING: 2153505.177  
EASTING: 6515177.339

PROJECT No: 951-20  
DATE: 4/26/2024 - 5/17/2024  
DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities          |                        | Sampling & In Situ Testing |                |       |                                |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|--------------------------|------------------------|----------------------------|----------------|-------|--------------------------------|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments     |
| 1175                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 16    |                                |
| 1370                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                |
| 1170                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                |
| 1375                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                |
| 1165                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 18    |                                |
| 1380                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                |
| 1160                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                |
| 1385                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                |
| 1155                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 20    |                                |
| 1390                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                |
| 1150                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                |
| 1395                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                |
| 1145                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 71    | PL(A) = 13.01<br>PL(D) = 30.70 |

BORING TYPE: HQ3  
HOLE DEPTH (ft): 2285  
REMARKS: \_\_\_\_\_

DRILLER: Crux  
WATER OBSERVATIONS: 730 ft, 828 ft.

LOGGED BY: Chris Messenger  
CASING: HW to 75 ft.

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                   |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|-----------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type ____) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)        |
| WL                                | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)        |

(Continued Next Page)

**CLIENT:** Lane Power & Energy Solutions

**SURFACE ELEVATION (ft):** 2541.1

**PROJECT No:** 951-20

**PROJECT:** Hydrostor Zevsar

**NORTHING:** 2153505.177

**DATE:** 4/26/2024 - 5/17/2024

**PROJECT LOCATION:** Rosamod, CA

**EASTING:** 6515177.339

DIP/AZIMUTH: -90 /

[illegible]

**BORING TYPE:** HQ3

**DRILLER:** Crux

**LOGGED BY:** Chris Messenger

HOLE DEPTH (ft): 2285

**WATER OBSERVATIONS:** 730 ft, 828 ft.

**CASING:** HW to 75 ft.

REMARKS:

| <b><u>SAMPLING &amp; IN SITU TESTING LEGEND</u></b>                                 |               |       |                                                  |
|-------------------------------------------------------------------------------------|---------------|-------|--------------------------------------------------|
|  | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) |
|  | Water seep    | PL(A) | Point load axial test 1s(50) (psi)               |
|  | Water level   | PL(D) | Point load diametral test 1s(50) (psi)           |
|                                                                                     |               | SLK   | Slake durability test (Type _____)               |
|                                                                                     |               | TRI   | Triaxial stress test (psi)                       |
|                                                                                     |               | UCS   | Uniaxial stress test (psi)                       |

(Continued Next Page)



CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2541.1

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2153505.177

DATE: 4/26/2024 - 5/17/2024

PROJECT LOCATION: Rosamod, CA

EASTING: 6515177.339

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities          |                        | Sampling & In Situ Testing |                |       |                                                       |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|--------------------------|------------------------|----------------------------|----------------|-------|-------------------------------------------------------|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments                            |
| 1105                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                                       |
| 1440                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 42    |                                                       |
| 1445                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                                       |
| 1095                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 61    | PL(A) = 15.70<br><br>PL(D) = 5.07<br><br>ITS = 363.66 |
| 1450                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                                       |
| 1090                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                                       |
| 1455                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 63    | UCS = 1,868.52<br><br>PL(A) = 85.42<br>PL(D) = 41.63  |
| 1085                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                                       |
| 1460                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                                       |
| 1080                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                                       |
| 1465                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 47    | SLK = Type I                                          |
| 1075                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                                       |

BORING TYPE: HQ3

DRILLER: Crux

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 2285

WATER OBSERVATIONS: 730 ft, 828 ft.

CASING: HW to 75 ft.

REMARKS: \_\_\_\_\_

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                   |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|-----------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type ____) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)        |
| WL                                | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)        |

(Continued Next Page)

**CLIENT:** Lane Power & Energy Solutions

**SURFACE ELEVATION (ft):** 2541.1

**PROJECT No:** 951-20

**PROJECT:** Hydrostor Zevsar

**NORTHING:** 2153505.177

**DATE:** 4/26/2024 - 5/17/2024

**PROJECT LOCATION:** Rosamod, CA

**EASTING:** 6515177.339

DIP/AZIMUTH: -90 /

[illegible]

**BORING TYPE:** HQ3

**DRILLER:** Crux

**LOGGED BY:** Chris Messenger

HOLE DEPTH (ft): 2285

WATER OBSERVATIONS: 730 ft, 828 ft.

**CASING:** HW to 75 ft.

REMARKS:

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |
|-----------------------------------|---------------|-------|--------------------------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               |
| W                                 | Water level   | PL(D) | Point load diametral test Is(50) (psi)           |
|                                   |               | SLK   | Slake durability test (Type _____)               |
|                                   |               | TRI   | Triaxial stress test (psi)                       |
|                                   |               | UCS   | Uniaxial stress test (psi)                       |

(Continued Next Page)



**CLIENT:** Lane Power & Energy Solutions  
**PROJECT:** Hydrostor Zevsar  
**PROJECT LOCATION:** Rosamod, CA

**SURFACE ELEVATION (ft):** 2541.1  
**NORTHING:** 2153505.177  
**EASTING:** 6515177.339

**PROJECT No:** 951-20  
**DATE:** 4/26/2024 - 5/17/2024  
**DIP/AZIMUTH:** -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata                              | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft)  | Discontinuities | Sampling & In Situ Testing                        |      |                               |       |                            |  |  |               |              |              |
|---------------------|----------------------------------------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|------------------------------|-----------------|---------------------------------------------------|------|-------------------------------|-------|----------------------------|--|--|---------------|--------------|--------------|
|                     |                                                          | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                              |                 | B - Bedding<br>S - Shear<br>J - Joint<br>F- Fault | Type | Core<br>Rec. %                | RQD % | Test Results<br>& Comments |  |  |               |              |              |
|                     |                                                          |                         |    |    |    |    |                |               |      |          |      |           |         |       |                              |                 |                                                   |      |                               |       |                            |  |  |               |              |              |
| 1035                | QTZ MONZONITE, light gray to white/pink/green, aphanitic |                         |    |    |    |    |                |               |      |          |      |           |         |       | Heavily fractured throughout | C               | 100                                               | 83   | SLK = Type I                  |       |                            |  |  |               |              |              |
| 1510                |                                                          |                         |    |    |    |    |                |               |      |          |      |           |         |       |                              |                 |                                                   |      |                               |       |                            |  |  | PL(D) = 40.15 |              |              |
| 1030                |                                                          |                         |    |    |    |    |                |               |      |          |      |           |         |       |                              |                 |                                                   |      |                               |       |                            |  |  |               |              |              |
| 1515                |                                                          |                         |    |    |    |    |                |               |      |          |      |           |         |       |                              |                 |                                                   |      |                               |       |                            |  |  |               | PL(D) = 4.37 |              |
| 1025                |                                                          |                         |    |    |    |    |                |               |      |          |      |           |         |       |                              |                 |                                                   |      |                               |       |                            |  |  |               |              | PL(A) = 4.72 |
| 1520                |                                                          |                         |    |    |    |    |                |               |      |          |      |           |         |       |                              |                 |                                                   |      |                               |       |                            |  |  |               |              |              |
| 1020                |                                                          |                         |    |    |    |    |                |               |      |          |      |           |         |       |                              |                 |                                                   |      |                               |       |                            |  |  |               |              |              |
| 1525                |                                                          |                         |    |    |    |    |                |               |      |          |      |           |         |       |                              |                 |                                                   |      |                               |       |                            |  |  |               |              |              |
| 1015                |                                                          |                         |    |    |    |    |                |               |      |          |      |           |         |       |                              |                 |                                                   |      |                               |       |                            |  |  |               |              |              |
| 1530                |                                                          |                         |    |    |    |    |                |               |      |          |      |           |         |       |                              |                 |                                                   |      |                               |       |                            |  |  |               |              |              |
| 1010                |                                                          |                         |    |    |    |    |                |               |      |          |      |           |         |       |                              |                 |                                                   |      |                               |       |                            |  |  |               |              |              |
| 1535                |                                                          |                         |    |    |    |    |                |               |      |          |      |           |         |       |                              |                 |                                                   |      |                               |       |                            |  |  |               |              |              |
| 1005                |                                                          |                         |    |    |    |    |                |               |      |          |      |           |         |       |                              |                 |                                                   |      | ITS = 288.18<br>PL(A) = 86.82 |       |                            |  |  |               |              |              |

**BORING TYPE:** HQ3  
**HOLE DEPTH (ft):** 2285  
**REMARKS:**

**DRILLER:** Crux  
**WATER OBSERVATIONS:** 730 ft, 828 ft.

**LOGGED BY:** Chris Messenger  
**CASING:** HW to 75 ft.

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                  |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|----------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type ___) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)       |
| WL                                | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)       |

(Continued Next Page)



CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2541.1

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2153505.177

DATE: 4/26/2024 - 5/17/2024

PROJECT LOCATION: Rosamod, CA

EASTING: 6515177.339

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities          |                        | Sampling & In Situ Testing |                |       |                              |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|--------------------------|------------------------|----------------------------|----------------|-------|------------------------------|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments   |
| 1000'               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                              |
| 1545                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       | PL(D) = 29.30                |
| 995'                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                              |
| 1550                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                              |
| 990'                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                              |
| 1555                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       | PL(D) = 19.24<br>ITS = 79.69 |
| 985'                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                              |
| 1560                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                              |
| 980'                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                              |
| 1565                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                              |
| 975'                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                              |
| 1570                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                              |
| 970'                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                              |
| 1573                | PEGMATITE DIKE              |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                              |

BORING TYPE: HQ3

DRILLER: CruX

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 2285

WATER OBSERVATIONS: 730 ft, 828 ft.

CASING: HW to 75 ft.

REMARKS: \_\_\_\_\_

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                         |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|-----------------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type <u>  </u> ) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)              |
| WL                                | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)              |

(Continued Next Page)



CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2541.1

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2153505.177

DATE: 4/26/2024 - 5/17/2024

PROJECT LOCATION: Rosamod, CA

EASTING: 6515177.339

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities          |                        | Sampling & In Situ Testing |                |       |                            |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|--------------------------|------------------------|----------------------------|----------------|-------|----------------------------|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments |
| 1575                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1575': Rubble            |                        |                            |                |       |                            |
| 965                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 39    |                            |
| 1580                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 960                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1585                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 955                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1590                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 950                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1595                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 945                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1600                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 940                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1605                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 935                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |

BORING TYPE: HQ3

DRILLER: Crux

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 2285

WATER OBSERVATIONS: 730 ft, 828 ft.

CASING: HW to 75 ft.

REMARKS: \_\_\_\_\_

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                         |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|-----------------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type <u>  </u> ) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)              |
| WL                                | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)              |

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CLIENT: Lane Power & Energy Solutions  
PROJECT: Hydrostor Zevsar  
PROJECT LOCATION: Rosamod, CA

SURFACE ELEVATION (ft): 2541.1  
NORTHING: 2153505.177  
EASTING: 6515177.339

PROJECT No: 951-20  
DATE: 4/26/2024 - 5/17/2024  
DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities                                                      |                        | Sampling & In Situ Testing |                |       |                              |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|----------------------------------------------------------------------|------------------------|----------------------------|----------------|-------|------------------------------|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear                                             | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments   |
| 930'                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1610' to 1613': (6)<br>40° - 47° Planar smooth                  |                        |                            |                |       | SLK = Type II                |
| 1615                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1612' to 1613.5':<br>(4) 60°                                    |                        |                            |                |       |                              |
| 925'                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1615': (3) Planar smooth                                             |                        |                            |                |       |                              |
| 1620                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1618': 0° Planar smooth                                              |                        | C                          | 100            | 54    | PL(A) = 4.72                 |
| 920'                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1619': (2) 40° Planar<br>smooth                                      |                        |                            |                |       |                              |
| 1625                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1622.9' to 1623.7':<br>47° Planar smooth                        |                        |                            |                |       |                              |
| 915'                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1625' to 1630': (4)<br>47° - 52° Planar smooth                  |                        | C                          | 100            | 67    | ITS = 17.63<br>PL(D) = 47.58 |
| 1630                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1630' to 1631.5':<br>(3) 17° - 22° Planar<br>smooth             |                        |                            |                |       |                              |
| 910'                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1632': 37° Planar<br>smooth                                          |                        |                            |                |       |                              |
| 1635                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1636' to 1642.5':<br>(12) 30° - 52° Undulating<br>planar smooth |                        | C                          | 100            | 70    | PL(A) = 118.73               |
| 905'                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                                      |                        |                            |                |       |                              |
| 1640                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                                      |                        |                            |                |       |                              |
| 900'                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                                      |                        |                            |                |       |                              |

BORING TYPE: HQ3  
HOLE DEPTH (ft): 2285  
REMARKS: \_\_\_\_\_

DRILLER: Crux  
WATER OBSERVATIONS: 730 ft, 828 ft.

LOGGED BY: Chris Messenger  
CASING: HW to 75 ft.

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                   |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|-----------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type ____) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)        |
| WL                                | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)        |

(Continued Next Page)



CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2541.1

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2153505.177

DATE: 4/26/2024 - 5/17/2024

PROJECT LOCATION: Rosamod, CA

EASTING: 6515177.339

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities          |                       | Sampling & In Situ Testing |                |                |                            |                                    |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|--------------------------|-----------------------|----------------------------|----------------|----------------|----------------------------|------------------------------------|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear | J - Joint<br>F- Fault | Type                       | Core<br>Rec. % | RQD %          | Test Results<br>& Comments |                                    |
| 895                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |                |                            |                                    |
| 1650                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |                |                            | SLK = Type II<br><br>PL(D) = 64.71 |
| 890                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |                |                            |                                    |
| 1655                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |                |                            | PL(D) = 86.77                      |
| 885                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |                |                            | ITS = 737.72<br>PL(A) = 79.93      |
| 1660                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |                |                            |                                    |
| 880                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |                |                            |                                    |
| 1665                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |                |                            | PL(A) = 16.39                      |
| 875                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |                |                            |                                    |
| 1670                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |                |                            |                                    |
| 870                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |                |                            |                                    |
| 1675                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                | TRI = 3,875.71 |                            |                                    |
| 865                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                | PL(D) = 21.69  |                            |                                    |

BORING TYPE: HQ3

DRILLER: Crux

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 2285

WATER OBSERVATIONS: 730 ft, 828 ft.

CASING: HW to 75 ft.

REMARKS: \_\_\_\_\_

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                   |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|-----------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type ____) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)        |
| WL                                | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)        |

(Continued Next Page)



CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2541.1

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2153505.177

DATE: 4/26/2024 - 5/17/2024

PROJECT LOCATION: Rosamod, CA

EASTING: 6515177.339

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities          |                        | Sampling & In Situ Testing |                |       |                                |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|--------------------------|------------------------|----------------------------|----------------|-------|--------------------------------|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments     |
| 860                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                |
| 1685                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       | PL(A) = 9.34                   |
| 855                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 56    | ITS = 111.14<br>PL(D) = 587.95 |
| 1690                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                |
| 850                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                |
| 1695                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       | PL(D) = 142.48                 |
| 845                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 60    | PL(A) = 70.16                  |
| 1700                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       | SLK = Type II                  |
| 840                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                |
| 1705                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                |
| 835                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 64    |                                |
| 1710                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       | PL(D) = 21.64                  |
| 830                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                |

BORING TYPE: HQ3

DRILLER: Crux

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 2285

WATER OBSERVATIONS: 730 ft, 828 ft.

CASING: HW to 75 ft.

REMARKS: \_\_\_\_\_

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                         |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|-----------------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type <u>  </u> ) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)              |
| WL                                | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)              |

(Continued Next Page)

**CLIENT:** Lane Power & Energy Solutions

**SURFACE ELEVATION (ft):** 2541.1

**PROJECT No:** 951-20

**PROJECT:** Hydrostor Zevsar

**NORTHING:** 2153505.177

**DATE:** 4/26/2024 - 5/17/2024

**PROJECT LOCATION:** Rosamod, CA

**EASTING:** 6515177.339

DIP/AZIMUTH: -90 /

[illegible]

**BORING TYPE:** HQ3

**DRILLER:** Crux

**LOGGED BY:** Chris Messenger

HOLE DEPTH (ft): 2285

**WATER OBSERVATIONS:** 730 ft, 828 ft.

**CASING:** HW to 75 ft.

REMARKS:

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                    |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|------------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type _____) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)         |
| W                                 | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)         |

(Continued Next Page)



CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2541.1

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2153505.177

DATE: 4/26/2024 - 5/17/2024

PROJECT LOCATION: Rosamod, CA

EASTING: 6515177.339

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities          |                       | Sampling & In Situ Testing |                |       |                            |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|--------------------------|-----------------------|----------------------------|----------------|-------|----------------------------|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear | J - Joint<br>F- Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments |
| 790                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |
| 1755                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |
| 785                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |
| 1760                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |
| 780                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |
| 1763                | PEGMATITE DIKE              |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |
| 1764                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |
| 1765                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |
| 775                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |
| 1770                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |
| 770                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |
| 1775                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |
| 765                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |
| 1780                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |
| 760                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |

BORING TYPE: HQ3

DRILLER: Crux

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 2285

WATER OBSERVATIONS: 730 ft, 828 ft.

CASING: HW to 75 ft.

REMARKS: \_\_\_\_\_

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                         |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|-----------------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type <u>  </u> ) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)              |
| WL                                | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)              |

(Continued Next Page)



CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2541.1

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2153505.177

DATE: 4/26/2024 - 5/17/2024

PROJECT LOCATION: Rosamod, CA

EASTING: 6515177.339

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata                                                                                    | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities          |                        | Sampling & In Situ Testing |                |       |                            |
|---------------------|----------------------------------------------------------------------------------------------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|--------------------------|------------------------|----------------------------|----------------|-------|----------------------------|
|                     |                                                                                                                | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments |
| 755                 |                                                                                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1790                |                                                                                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 750                 |                                                                                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1795                |                                                                                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 745                 |                                                                                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1800                | QTZ MONZONITE                                                                                                  |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 740                 |                                                                                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1804                |                                                                                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1805                | QTZ MONZONITE, light gray to white, phaneritic, with feldspar, biotite, hornblende, trace amounts of muscovite |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 735                 |                                                                                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1810                |                                                                                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 730                 | 1811 PEGMATITE DIKE                                                                                            |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1812                |                                                                                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1813                | PEGMATITE DIKE                                                                                                 |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1814                |                                                                                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1815                |                                                                                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 725                 |                                                                                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |

BORING TYPE: HQ3

DRILLER: Crux

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 2285

WATER OBSERVATIONS: 730 ft, 828 ft.

CASING: HW to 75 ft.

REMARKS: \_\_\_\_\_

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                         |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|-----------------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type <u>  </u> ) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)              |
| WL                                | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)              |



CLIENT: Lane Power & Energy Solutions  
PROJECT: Hydrostor Zevsar  
PROJECT LOCATION: Rosamod, CA

SURFACE ELEVATION (ft): 2541.1  
NORTHING: 2153505.177  
EASTING: 6515177.339

PROJECT No: 951-20  
DATE: 4/26/2024 - 5/17/2024  
DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities          |                        | Sampling & In Situ Testing |                |       |                                             |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|--------------------------|------------------------|----------------------------|----------------|-------|---------------------------------------------|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments                  |
| 720                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       | TRI = 16,404.88                             |
| 1825                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                             |
| 715                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 57    |                                             |
| 1830                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                             |
| 1831                | PEGMATITE DIKE              |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       | PL(D) = 307.88                              |
| 1833.4              |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                             |
| 1835                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       | ITS = 348.86                                |
| 705                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       | PL(D) = 60.53                               |
| 1840                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 65    | UCS =<br>16816.09348<br>PL(A) =<br>1,261.42 |
| 700                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                             |
| 1845                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                             |
| 1848                | PEGMATITE DIKE              |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 73    | PL(A) = 73.87                               |
| 1849                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       | SLK = Type I                                |
| 1850                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       | UCS =<br>10532.88792                        |
| 690                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                             |

BORING TYPE: HQ3  
HOLE DEPTH (ft): 2285  
REMARKS: \_\_\_\_\_

DRILLER: Crux  
WATER OBSERVATIONS: 730 ft, 828 ft.

LOGGED BY: Chris Messenger  
CASING: HW to 75 ft.

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                   |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|-----------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type ____) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)        |
| WL                                | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)        |

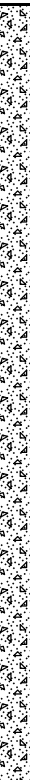
(Continued Next Page)



CLIENT: Lane Power & Energy Solutions  
PROJECT: Hydrostor Zevsar  
PROJECT LOCATION: Rosamod, CA

SURFACE ELEVATION (ft): 2541.1  
NORTHING: 2153505.177  
EASTING: 6515177.339

PROJECT No: 951-20  
DATE: 4/26/2024 - 5/17/2024  
DIP/AZIMUTH: -90 /

| EL   | DEPTH<br>(ft) | Description<br>of<br>Strata                                                                                                    | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log                                                                     | Rock Strength |      |          |      |           | Water | Fracture<br>Spacing<br>(ft) |      | Discontinuities |                                      | Sampling & In Situ Testing                        |      |                          |                       |                   |                                    |
|------|---------------|--------------------------------------------------------------------------------------------------------------------------------|-------------------------|----|----|----|----|------------------------------------------------------------------------------------|---------------|------|----------|------|-----------|-------|-----------------------------|------|-----------------|--------------------------------------|---------------------------------------------------|------|--------------------------|-----------------------|-------------------|------------------------------------|
|      |               |                                                                                                                                | Fr                      | SA | MA | HA | CA |                                                                                    | Very Soft     | Soft | Med-Hard | Hard | Very Hard |       | Ex Hard                     | 0.05 | 0.25            | 0.50                                 | 2.50                                              | 5.00 | B - Bedding<br>S - Shear | J - Joint<br>F- Fault | Type              | Core<br>Rec. %                     |
| 685  | 1856          | QTZ MONZONITE, light gray to white, phaneritic, with feldspar biotite, hornblende, trace amounts of muscovite, epidote, pyrite |                         |    |    |    |    |  |               |      |          |      |           |       |                             |      |                 | 61° Planar rough                     |                                                   |      |                          |                       | UCS = 13590.69599 |                                    |
|      | 1857          |                                                                                                                                |                         |    |    |    |    |                                                                                    |               |      |          |      |           |       |                             |      |                 |                                      | 1856.2': Planar smooth                            |      | C                        | 100                   | 75                | PL(D) = 27.55<br>UCS = 13486.4     |
|      |               |                                                                                                                                |                         |    |    |    |    |                                                                                    |               |      |          |      |           |       |                             |      |                 |                                      | From 1860' to 1861': 79° Stepped rough            |      |                          |                       |                   |                                    |
| 1860 |               |                                                                                                                                |                         |    |    |    |    |                                                                                    |               |      |          |      |           |       |                             |      |                 |                                      | 1862': 51° Planar smooth                          |      |                          |                       |                   |                                    |
|      |               |                                                                                                                                |                         |    |    |    |    |                                                                                    |               |      |          |      |           |       |                             |      |                 |                                      | 1863': 39° Planar rough                           |      |                          |                       |                   |                                    |
|      |               |                                                                                                                                |                         |    |    |    |    |                                                                                    |               |      |          |      |           |       |                             |      |                 |                                      | 1864': 39° Planar rough                           |      |                          |                       |                   | ITS = 586.74                       |
| 1865 |               |                                                                                                                                |                         |    |    |    |    |                                                                                    |               |      |          |      |           |       |                             |      |                 |                                      |                                                   |      | C                        | 100                   | 64                | TRI = 11,003.99<br>UCS = 12,242.44 |
| 675  |               |                                                                                                                                |                         |    |    |    |    |                                                                                    |               |      |          |      |           |       |                             |      |                 |                                      | 1869': 62° Planar rough                           |      |                          |                       |                   |                                    |
|      |               |                                                                                                                                |                         |    |    |    |    |                                                                                    |               |      |          |      |           |       |                             |      |                 |                                      | From 1871' to 1873.5': (6) 30° - 42° Planar rough |      |                          |                       |                   | UCS = 16389.73151                  |
| 1870 |               |                                                                                                                                |                         |    |    |    |    |                                                                                    |               |      |          |      |           |       |                             |      |                 |                                      |                                                   |      |                          |                       |                   | PL(D) = 1,183.33                   |
| 670  |               |                                                                                                                                |                         |    |    |    |    |                                                                                    |               |      |          |      |           |       |                             |      |                 |                                      |                                                   |      |                          |                       |                   |                                    |
|      | 1875          |                                                                                                                                |                         |    |    |    |    |                                                                                    |               |      |          |      |           |       |                             |      |                 | 1875': (1) 45° Planar smooth, rubble |                                                   |      |                          |                       | PL(A) = 743.39    |                                    |
| 665  |               |                                                                                                                                |                         |    |    |    |    |                                                                                    |               |      |          |      |           |       |                             |      |                 | 1877.3': 41° Planar smooth           |                                                   | C    | 100                      | 37                    |                   |                                    |
|      |               |                                                                                                                                |                         |    |    |    |    |                                                                                    |               |      |          |      |           |       |                             |      |                 | 1877.7': 48° Stepped                 |                                                   |      |                          |                       |                   |                                    |
|      |               |                                                                                                                                |                         |    |    |    |    |                                                                                    |               |      |          |      |           |       |                             |      |                 | 1878.2': 84° Undulating smooth       |                                                   |      |                          |                       |                   |                                    |
| 1880 |               |                                                                                                                                |                         |    |    |    |    |                                                                                    |               |      |          |      |           |       |                             |      |                 | From 1878.3' to 1888': Rubble        |                                                   |      |                          |                       |                   |                                    |
| 660  |               |                                                                                                                                |                         |    |    |    |    |                                                                                    |               |      |          |      |           |       |                             |      |                 |                                      |                                                   |      |                          |                       |                   |                                    |
|      |               |                                                                                                                                |                         |    |    |    |    |                                                                                    |               |      |          |      |           |       |                             |      |                 |                                      |                                                   |      |                          |                       |                   |                                    |
|      | 1885          |                                                                                                                                |                         |    |    |    |    |                                                                                    |               |      |          |      |           |       |                             |      |                 |                                      |                                                   | C    | 100                      | 10                    |                   |                                    |
| 655  |               |                                                                                                                                |                         |    |    |    |    |                                                                                    |               |      |          |      |           |       |                             |      |                 | 1888.9': 42° Planar smooth           |                                                   |      |                          |                       |                   |                                    |

BORING TYPE: HQ3  
HOLE DEPTH (ft): 2285  
REMARKS: \_\_\_\_\_

DRILLER: Crux  
WATER OBSERVATIONS: 730 ft, 828 ft.

LOGGED BY: Chris Messenger  
CASING: HW to 75 ft.

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                  |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|----------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type ___) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)       |
| WL                                | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)       |

(Continued Next Page)





CLIENT: Lane Power & Energy Solutions  
PROJECT: Hydrostor Zevsar  
PROJECT LOCATION: Rosamod, CA

SURFACE ELEVATION (ft): 2541.1  
NORTHING: 2153505.177  
EASTING: 6515177.339

PROJECT No: 951-20  
DATE: 4/26/2024 - 5/17/2024  
DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities                                                |                        | Sampling & In Situ Testing |                |       |                            |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|----------------------------------------------------------------|------------------------|----------------------------|----------------|-------|----------------------------|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear                                       | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments |
| 650                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1889' to 1891.9':<br>Rubble                               |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1892' to 1893': (1)<br>Undulating rough                   |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1893' to 1896.7':<br>Rubble                               |                        |                            |                |       |                            |
| 1895                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1894' to 1595':<br>Rubble                                 |                        |                            |                |       |                            |
| 645                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1897': 45° Undulating<br>rough                                 |                        | C                          | 100            | 39    |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1899' to 1900': 71°<br>- 77° Planar rough                 |                        |                            |                |       |                            |
| 1900                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1900.2': 57° Planar<br>smooth                                  |                        |                            |                |       |                            |
| 640                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1901': 30° Planar<br>smooth                                    |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1901.8': 41° Planar<br>rough                                   |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1902.5' to 1903.6':<br>90° Undulating smooth              |                        |                            |                |       | SLK = Type I               |
| 1905                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1905' to 1906': (4)<br>7° - 21° Planar smooth             |                        |                            |                |       | PL(D) = 407.77             |
| 635                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1906.7': 47° - 90°<br>Stepped rough                            |                        | C                          | 100            | 37    |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1907': 90° Undulating                                          |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1908.8': 46° Planar<br>rough                                   |                        |                            |                |       | PL(A) = 376.41             |
| 1910                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1909.9': 16° Planar<br>smooth                                  |                        |                            |                |       |                            |
| 630                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1910' to 1915':<br>(13) 20° - 40° Planar<br>smooth        |                        |                            |                |       |                            |
| 1912                | QTZ MONZONITE               |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1913': 67° Planar<br>smooth                                    |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1915' to 1920':<br>(12) 15° - 60° Planar<br>smooth        |                        | C                          | 100            | 39    |                            |
| 1915                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1919' to 1920':<br>Radiating fractures                    |                        |                            |                |       |                            |
| 625                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1920' to 1930':<br>(20) 10° - 35° Planar<br>rough (4) 45° |                        |                            |                |       |                            |
| 1920                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                                |                        |                            |                |       |                            |
| 620                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                                |                        |                            |                |       |                            |
| 1921                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                                |                        |                            |                |       |                            |

BORING TYPE: HQ3  
HOLE DEPTH (ft): 2285  
REMARKS: \_\_\_\_\_

DRILLER: Crux  
WATER OBSERVATIONS: 730 ft, 828 ft.

LOGGED BY: Chris Messenger  
CASING: HW to 75 ft.

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                   |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|-----------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type ____) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)        |
| WL                                | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)        |

(Continued Next Page)



CLIENT: Lane Power & Energy Solutions  
PROJECT: Hydrostor Zevsar  
PROJECT LOCATION: Rosamod, CA

SURFACE ELEVATION (ft): 2541.1  
NORTHING: 2153505.177  
EASTING: 6515177.339

PROJECT No: 951-20  
DATE: 4/26/2024 - 5/17/2024  
DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft)                                                                                   | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities                                                                                                                                                                                      |                        | Sampling & In Situ Testing |                |       |                                                                     |
|-------------------------------------------------------------------------------------------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|------------------------|----------------------------|----------------|-------|---------------------------------------------------------------------|
|                                                                                                       |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear                                                                                                                                                                             | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments                                          |
| 615<br>1930<br>610<br>1935<br>605<br>1940<br>600<br>1945<br>595<br>1950<br>590<br>1954<br>1955<br>585 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                                                                                                                                                                      |                        | C                          | 100            | 35    | ITS = 919.21                                                        |
|                                                                                                       |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1931.5' to 1933':<br>Rubble, multiple<br>fractures                                                                                                                                              |                        |                            |                |       |                                                                     |
|                                                                                                       |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1935.6': 7° Planar rough<br>From 1936' to 1937': 90°<br>Planar smooth                                                                                                                                |                        | C                          | 100            | 45    | PL(A) = 23.74<br>PL(D) = 555.25<br>TRI = 15,413.87<br>PL(A) = 12.23 |
|                                                                                                       |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1937.6': 69° Planar<br>smooth<br>1938.2': 21° Undulating<br>smooth<br>1940.5': 17° Planar<br>smooth<br>From 1941' to 1942': 90°<br>Undulating smooth<br>From 1943' to 1946': (4)<br>30° Planar rough |                        |                            |                |       | PL(D) = 15.83                                                       |
|                                                                                                       |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1946.5' to 1958.3':<br>Rubble                                                                                                                                                                   |                        | C                          | 100            | 18    | SLK = Type II                                                       |
|                                                                                                       |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                                                                                                                                                                      |                        |                            |                |       |                                                                     |
|                                                                                                       |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                                                                                                                                                                      |                        | C                          | 100            | 21    |                                                                     |
|                                                                                                       |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1959.2': 2° Planar rough                                                                                                                                                                             |                        |                            |                |       |                                                                     |

BORING TYPE: HQ3  
HOLE DEPTH (ft): 2285  
REMARKS:

DRILLER: Crux  
WATER OBSERVATIONS: 730 ft, 828 ft.

LOGGED BY: Chris Messenger  
CASING: HW to 75 ft.

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                         |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|-----------------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type <u>  </u> ) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)              |
| WL                                | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)              |



CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2541.1

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2153505.177

DATE: 4/26/2024 - 5/17/2024

PROJECT LOCATION: Rosamod, CA

EASTING: 6515177.339

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata                                                                                                             | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities          |                        | Sampling & In Situ Testing |                |       |                            |
|---------------------|-----------------------------------------------------------------------------------------------------------------------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|--------------------------|------------------------|----------------------------|----------------|-------|----------------------------|
|                     |                                                                                                                                         | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments |
| 580                 | QTZ MONZONITE, light gray to white,<br>phanaritic, with Na - Ca feldspar,<br>biotite, hornblende, trace amounts of<br>muscovite, pyrite |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       | ITS = 135.43               |
| 1965                |                                                                                                                                         |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 575                 |                                                                                                                                         |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 48    |                            |
| 1970                |                                                                                                                                         |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 570                 |                                                                                                                                         |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1972                |                                                                                                                                         |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1975                |                                                                                                                                         |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 565                 |                                                                                                                                         |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1980                |                                                                                                                                         |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       | PL(A) = 226.31             |
| 560                 |                                                                                                                                         |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1985                |                                                                                                                                         |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       | PL(D) = 58.86              |
| 555                 |                                                                                                                                         |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1990                |                                                                                                                                         |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 550                 |                                                                                                                                         |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       | ITS = 1,324.48             |

BORING TYPE: HQ3

DRILLER: Crux

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 2285

WATER OBSERVATIONS: 730 ft, 828 ft.

CASING: HW to 75 ft.

REMARKS: \_\_\_\_\_

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                   |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|-----------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type ____) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)        |
| WL                                | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)        |

(Continued Next Page)



CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2541.1

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2153505.177

DATE: 4/26/2024 - 5/17/2024

PROJECT LOCATION: Rosamod, CA

EASTING: 6515177.339

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities                                          |                        | Sampling & In Situ Testing |                |       |                                |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|----------------------------------------------------------|------------------------|----------------------------|----------------|-------|--------------------------------|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear                                 | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments     |
| 545                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1995.5': 40-49° Planar rough                             |                        |                            |                |       | ITS = 1,385.81                 |
| 2000                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1997.2' to 1998': 55° Planar rough                  |                        | C                          | 100            | 68    | UCS = 14466.51496              |
| 540                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                          |                        |                            |                |       | PL(D) = 6.56<br>PL(A) = 108.51 |
| 2005                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2004.2' to 2005': 62° Planar rough                  |                        |                            |                |       |                                |
| 535                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2007' to 2010': Rubble                              |                        | C                          | 100            | 47    | SLK = Type I                   |
| 2010                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2009' to 2010': 62° Planar rough                    |                        |                            |                |       | PL(D) = 68.22<br>PL(A) = 46.94 |
| 530                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2010' to 2011': (4) 110° - 50° Planar rough         |                        |                            |                |       | UCS = 12252.27                 |
| 2015                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2013.9': 61° Planar rough                                |                        |                            |                |       |                                |
| 525                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2014.5': 71° Planar smooth                               |                        |                            |                |       |                                |
| 2020                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2015' to 2017': 80° - 90° Open fracture, undulating |                        | C                          | 100            | 50    |                                |
| 520                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2017' to 2018': Rubble                              |                        |                            |                |       |                                |
| 2021                | PEGMATITE DIKE              |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2019': 49° Planar smooth                                 |                        |                            |                |       |                                |
| 520                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2021': 0° Planar smooth                                  |                        |                            |                |       |                                |
| 2023                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2021.9' to 2023': Rubble                            |                        |                            |                |       |                                |
| 515                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2024' to 2025': (6) 60° - 50° Undulating / rough    |                        |                            |                |       | PL(D) = 776.70                 |
| 2025                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2026' to 2027': (2) 55° - 62° Planar rough          |                        |                            |                |       |                                |
| 515                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2028' to 2031': (11) 0° - 4° Planar rough           |                        | C                          | 100            | 61    | UCS = 10,687.81                |

BORING TYPE: HQ3

DRILLER: Crux

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 2285

WATER OBSERVATIONS: 730 ft, 828 ft.

CASING: HW to 75 ft.

REMARKS: \_\_\_\_\_

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                   |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|-----------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type ____) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)        |
| WL                                | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)        |

(Continued Next Page)



CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2541.1

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2153505.177

DATE: 4/26/2024 - 5/17/2024

PROJECT LOCATION: Rosamod, CA

EASTING: 6515177.339

DIP/AZIMUTH: -90 /

| EL  | DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities          |                        | Sampling & In Situ Testing |                |       |                                  |
|-----|---------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|--------------------------|------------------------|----------------------------|----------------|-------|----------------------------------|
|     |               |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments       |
| 510 | 2031          |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       | PL(A) = 561.58<br>ITS = 1,110.77 |
| 505 | 2032.5        |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                  |
| 500 | 2035          |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                  |
| 495 | 2040          |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                  |
| 490 | 2045          |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       | PL(A) = 546.31<br>PL(D) = 879.30 |
| 485 | 2047          |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                  |
| 480 | 2050          |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                  |
| 475 | 2053.0        |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                  |
| 470 | 2055          |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       | UCS =<br>17,710.56               |
| 465 | 2057          |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                  |
| 460 | 2060          |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       | UCS =<br>14,627.72               |
| 455 | 2061          |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                  |

BORING TYPE: HQ3

DRILLER: Crux

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 2285

WATER OBSERVATIONS: 730 ft, 828 ft.

CASING: HW to 75 ft.

REMARKS: \_\_\_\_\_

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                   |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|-----------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type ____) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)        |
| WL                                | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)        |

(Continued Next Page)



CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2541.1

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2153505.177

DATE: 4/26/2024 - 5/17/2024

PROJECT LOCATION: Rosamod, CA

EASTING: 6515177.339

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities                                                                    |                        | Sampling & In Situ Testing |                |       |                            |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|------------------------------------------------------------------------------------|------------------------|----------------------------|----------------|-------|----------------------------|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear                                                           | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments |
| 475                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                                                    |                        | C                          | 100            | 66    | UCS =<br>18,597.42         |
| 2070                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | -2068.96': 32° Planar<br>smooth                                                    |                        |                            |                |       |                            |
| 470                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | -2072.6': 59° Planar<br>rough                                                      |                        |                            |                |       | ITS = 344.18               |
| 2075                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | -2073.7': 68° Undulating<br>smooth                                                 |                        |                            |                |       | SLK = Type I               |
| 465                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | -2075.9': 74° Stepped<br>rough                                                     |                        |                            |                |       |                            |
| 2080                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | -2077.1': 32° Planar<br>rough                                                      |                        | C                          | 100            | 70    |                            |
| 460                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | -2078.7': 7° Planar rough                                                          |                        |                            |                |       |                            |
| 2085                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2080' to 2082': (5)<br>20° - (1) 57° Planar<br>smooth                         |                        |                            |                |       |                            |
| 455                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | -2084': 3° Undulating -<br>27° Smooth                                              |                        |                            |                |       |                            |
| 2090                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | -2085.1': 27° Planar<br>rough                                                      |                        |                            |                |       |                            |
| 450                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | -2085.75': 27° Planar<br>rough                                                     |                        | C                          | 100            | 45    |                            |
| 2095                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2087.25' to 2089':<br>(3) 47° - 67° Planar<br>rough                           |                        |                            |                |       |                            |
| 445                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | -2089.7': 7° Planar rough                                                          |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2090' to 2096': 90°<br>Undulating open<br>fractures, rough                    |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | -2090.2': 66° - 71° Planar<br>smooth                                               |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2095' to 2098': 79°<br>- 90° Undulating open<br>fractures, stepped /<br>rough |                        | C                          | 100            | 60    |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | -2099': Rubble                                                                     |                        |                            |                |       | PL(D) = 269.44             |

BORING TYPE: HQ3

DRILLER: Crux

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 2285

WATER OBSERVATIONS: 730 ft, 828 ft.

CASING: HW to 75 ft.

REMARKS: \_\_\_\_\_

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                   |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|-----------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type ____) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)        |
| WL                                | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)        |

(Continued Next Page)



CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2541.1

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2153505.177

DATE: 4/26/2024 - 5/17/2024

PROJECT LOCATION: Rosamod, CA

EASTING: 6515177.339

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities          |                        | Sampling & In Situ Testing |                |       |                            |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|--------------------------|------------------------|----------------------------|----------------|-------|----------------------------|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments |
| 440                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 2102.6              | PEGMATITE DIKE              |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 2104                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 2105                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 435                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 2110                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 430                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 2115                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 425                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 2120                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 420                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 2125                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 415                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 2130                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 410                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |

BORING TYPE: HQ3

DRILLER: Crux

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 2285

WATER OBSERVATIONS: 730 ft, 828 ft.

CASING: HW to 75 ft.

REMARKS: \_\_\_\_\_

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                   |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|-----------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type ____) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)        |
| WL                                | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)        |

(Continued Next Page)





CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2541.1

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2153505.177

DATE: 4/26/2024 - 5/17/2024

PROJECT LOCATION: Rosamod, CA

EASTING: 6515177.339

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) |                        |  |                                                                | Discontinuities |     | Sampling & In Situ Testing |                                      |                |  |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|------------------------|--|----------------------------------------------------------------|-----------------|-----|----------------------------|--------------------------------------|----------------|--|
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                        |  |                                                                |                 |     | Type                       |                                      |                |  |
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       | B - Bedding<br>S - Shear    | J - Joint<br>F - Fault |  |                                                                |                 |     |                            |                                      |                |  |
| 2135                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                        |  | From 2134.4' to 2136':<br>Rubble                               |                 |     |                            |                                      |                |  |
| 2136                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                        |  | From 2136.9' to 2139.3':<br>(4) 0° Planar rough                | C               | 100 | 34                         | SLK = Type I                         |                |  |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                        |  | 2139.6': 32° Planar<br>smooth                                  |                 |     |                            |                                      |                |  |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                        |  | From 2140' to 2142': (3)<br>60° - 74° Planar rough             |                 |     |                            |                                      |                |  |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                        |  | From 2142' to 2143': 90°<br>Healed                             |                 |     |                            |                                      |                |  |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                        |  | From 2144.5' to 2145':<br>(2) 7° - 10° Planar rough            |                 |     |                            |                                      |                |  |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                        |  | From 2145' to 2148': (9)<br>17° - 40° Planar rough             | C               | 100 | 66                         | PL(A) = 913.70<br>UCS =<br>15,270.44 |                |  |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                        |  | From 2149' to 2150.75':<br>67° - 47° - 49°<br>Undulating rough |                 |     |                            |                                      |                |  |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                        |  | 2151.4': 4° Planar<br>smooth                                   |                 |     |                            |                                      |                |  |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                        |  | 2152.4': 4° - 7° Planar<br>smooth                              |                 |     |                            |                                      |                |  |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                        |  | From 2154' to 2156': (3)<br>10° - 22° Planar smooth            |                 |     |                            |                                      |                |  |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                        |  | From 2156' to 2156.3':<br>71° Planar smooth                    | C               | 100 | 69                         | PL(D) = 104.08                       |                |  |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                        |  | From 2161' to 2163': (4)<br>50° - 60° Planar rough             |                 |     |                            |                                      |                |  |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                        |  | 2164': 19° Planar<br>smooth                                    |                 |     |                            |                                      | PL(D) = 599.32 |  |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                        |  | From 2167' to 2171.4':<br>(9) 20° - 52° Planar<br>smooth       | C               | 100 | 40                         | PL(A) = 669.63<br>ITS = 657.36       |                |  |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                        |  | From 2169' to 2170':<br>Rubble                                 |                 |     |                            |                                      |                |  |

BORING TYPE: HQ3

DRILLER: Crux

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 2285

WATER OBSERVATIONS: 730 ft, 828 ft.

CASING: HW to 75 ft.

REMARKS: \_\_\_\_\_

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                    |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|------------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type _____) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)         |
| W                                 | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)         |

(Continued Next Page)





CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2541.1

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2153505.177

DATE: 4/26/2024 - 5/17/2024

PROJECT LOCATION: Rosamod, CA

EASTING: 6515177.339

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities                               |                        | Sampling & In Situ Testing |                |       |                                                                                               |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|-----------------------------------------------|------------------------|----------------------------|----------------|-------|-----------------------------------------------------------------------------------------------|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear                      | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments                                                                    |
| 370                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                               |                        |                            |                |       |                                                                                               |
| 2175                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2173' to 2175': 84°<br>Undulating smooth |                        |                            |                |       |                                                                                               |
| 365                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                               |                        | C                          | 100            | 66    | PL(D) = 794.81                                                                                |
| 2180                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                               |                        |                            |                |       |                                                                                               |
| 360                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                               |                        |                            |                |       |                                                                                               |
| 2185                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                               |                        |                            |                |       |                                                                                               |
| 355                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                               |                        |                            |                |       |                                                                                               |
| 2190                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                               |                        | C                          | 100            | 43    | UCS =<br>14,115.66<br><br>PL(A) =<br>1,157.05<br><br>UCS =<br>13,315.63<br><br>PL(D) = 908.51 |
| 350                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                               |                        |                            |                |       |                                                                                               |
| 2195                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                               |                        |                            |                |       |                                                                                               |
| 345                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                               |                        |                            |                |       |                                                                                               |
| 2200                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                               |                        | C                          | 100            | 52    | SLK = Type I<br>ITS = 1,572.39                                                                |
| 340                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                               |                        |                            |                |       |                                                                                               |

BORING TYPE: HQ3

DRILLER: CruX

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 2285

WATER OBSERVATIONS: 730 ft, 828 ft.

CASING: HW to 75 ft.

REMARKS: \_\_\_\_\_

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                    |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|------------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type _____) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)         |
| L                                 | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)         |

(Continued Next Page)



PAGE 64 OF 66

**PROJECT No:** 951-20

DIP/AZIMUTH: -90 /

| EL  | DEPTH (ft) | Description of Strata | Degree of Alteration<br>Fr<br>SA<br>MA<br>HA<br>CA | Graphic Log | Rock Strength<br>Very Soft<br>Soft<br>Med-Hard<br>Hard<br>Very Hard<br>Ex Hard | Water | Fracture Spacing (ft)<br>0.05<br>0.25<br>0.50<br>2.50<br>5.00 | Discontinuities<br>B - Bedding<br>S - Shear<br>J - Joint<br>F - Fault                                                                                                                  | Sampling & In Situ Testing |             |       | Test Results & Comments<br>PL(A) = 56.95                                |
|-----|------------|-----------------------|----------------------------------------------------|-------------|--------------------------------------------------------------------------------|-------|---------------------------------------------------------------|----------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|----------------------------|-------------|-------|-------------------------------------------------------------------------|
|     |            |                       |                                                    |             |                                                                                |       |                                                               |                                                                                                                                                                                        | Type                       | Core Rec. % | RQD % |                                                                         |
| 335 |            |                       |                                                    |             |                                                                                |       |                                                               |                                                                                                                                                                                        |                            |             |       | PL(A) = 790.04                                                          |
| 335 |            |                       |                                                    |             |                                                                                |       |                                                               | 2206.25': 59° Planar smooth<br>From 2206.8' to 2207.17° - 21° Planar smooth<br>2209': 7° Undulating rough<br>From 2209.5' to 2210': Rubble<br>2211': 27° Planar rough                  | C                          | 100         | 73    | PL(A) = 279.29<br>PL(D) = 825.16<br>ITS = 1,361.97                      |
| 330 |            |                       |                                                    |             |                                                                                |       |                                                               | 2212.9': 7° Planar smooth<br>2213.4': 71° Planar smooth<br>2216': 74° Planar rough<br>From 2216.3' to 2218': 50° Undulating smooth<br>From 2218' to 2220': (7) 17° - 20° Planar smooth |                            |             |       | UCS = 8,715.76                                                          |
| 325 |            |                       |                                                    |             |                                                                                |       |                                                               | From 2220.9' to 2221.7': 90° Planar smooth, joint fractures<br>2222.7': 45° Planar, Undulating rough<br>From 2222.9' to 2224': Rubble                                                  |                            |             |       |                                                                         |
| 320 |            |                       |                                                    |             |                                                                                |       |                                                               |                                                                                                                                                                                        |                            |             |       |                                                                         |
| 315 |            |                       |                                                    |             |                                                                                |       |                                                               |                                                                                                                                                                                        |                            |             |       |                                                                         |
| 310 |            |                       |                                                    |             |                                                                                |       |                                                               | From 2228' to 2229': Rubble<br>From 2229' to 2230': 90° Undulating rough<br>From 2230' to 2231': (3) 40° - 60° Planar / rough                                                          | C                          | 72          | 27    | ITS = 1,405.09                                                          |
| 305 |            |                       |                                                    |             |                                                                                |       |                                                               | 2236.4': (4) 40° - 49° Planar smooth, (2) Healed 40° fractures<br>2237.2': 74° S. undulating rough<br>2238': 51° Planar smooth                                                         | C                          | 100         | 65    | PL(A) = 829.13<br>PL(D) = 61.66<br>PL(A) = 1,092.52<br>PL(D) = 1,152.98 |

**LOGGED BY:** Chris Messenger

**CASING:** HW to 75 ft.

REMARKS:

### SAMPLING & IN SITU TESTING LEGEND

C Core drilling  
W Water seep  
T Water level

| ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Stake durability test (Type |
|-------|--------------------------------------------------|-----|-----------------------------|
| PL(A) | Point load axial test (550) (psi)                | TRI | Triaxial stress test (psi)  |
| PL(D) | Point load diametral test (550) (psi)            | UCS | Uniaxial stress test (psi)  |

(Continued Next Page)



CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2541.1

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2153505.177

DATE: 4/26/2024 - 5/17/2024

PROJECT LOCATION: Rosamod, CA

EASTING: 6515177.339

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities                                  |                        | Sampling & In Situ Testing |                |       |                                                     |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|--------------------------------------------------|------------------------|----------------------------|----------------|-------|-----------------------------------------------------|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear                         | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments                          |
| 300'                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2238.62': 67° Undulating smooth                  |                        |                            |                |       |                                                     |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2240': 82° Undulating rough                      |                        |                            |                |       |                                                     |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2242': 47° Planar smooth                         |                        |                            |                |       |                                                     |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2243': 88° - 90° Stepped rough                   |                        |                            |                |       |                                                     |
| -2245               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2245' to 2246': Rubble                      |                        |                            |                |       |                                                     |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2246.3' to 2250': (3) 0° - 7° Planar smooth |                        | C                          | 100            | 78    |                                                     |
| -2250               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                  |                        |                            |                |       |                                                     |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2251': 32° Planar rough                          |                        |                            |                |       |                                                     |
| -2255               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                  |                        |                            |                |       |                                                     |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2256.3': 45° Planar rough                        |                        | C                          | 100            | 79    |                                                     |
| -2260               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                  |                        |                            |                |       |                                                     |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2263' to 2265': 90° S. undulating rough     |                        |                            |                |       |                                                     |
| -2265               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2265' to 2266': (3) 40° Planar smooth       |                        |                            |                |       |                                                     |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                  |                        | C                          | 100            | 45    | PL(A) = 452.27<br>UCS = 13,788.80<br>ITS = 1,240.18 |
| -2270               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2270' to 2271': 90° Planar smooth           |                        |                            |                |       |                                                     |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2273.3': 42° Planar smooth                       |                        |                            |                |       | SLK = Type I                                        |

BORING TYPE: HQ3

DRILLER: Crux

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 2285

WATER OBSERVATIONS: 730 ft, 828 ft.

CASING: HW to 75 ft.

REMARKS: \_\_\_\_\_

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                    |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|------------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type _____) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)         |
| WL                                | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)         |

(Continued Next Page)



CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2541.1

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2153505.177

DATE: 4/26/2024 - 5/17/2024

PROJECT LOCATION: Rosamod, CA

EASTING: 6515177.339

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft)                     | Description<br>of<br>Strata        | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities                           |                       | Sampling & In Situ Testing |                |       |                            |
|-----------------------------------------|------------------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|-------------------------------------------|-----------------------|----------------------------|----------------|-------|----------------------------|
|                                         |                                    | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear                  | J - Joint<br>F- Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments |
| 265<br>2280<br>260<br>2285              |                                    |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2275' to 2280': (5)<br>Planar smooth |                       | C                          | 100            | 46    | PL(D) = 973.50             |
| 2285<br>255<br>250<br>245<br>240<br>235 | Bottom of borehole at 2285.0 feet. |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                           |                       |                            |                |       |                            |

BORING TYPE: HQ3

DRILLER: CruX

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 2285

WATER OBSERVATIONS: 730 ft, 828 ft.

CASING: HW to 75 ft.

REMARKS: \_\_\_\_\_

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                  |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|----------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type ___) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)       |
| WL                                | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)       |



CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2548.8

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2153392.317

DATE: 8/10/2024 - 10/13/2024

PROJECT LOCATION: Rosamod, CA

EASTING: 6514888.703

DIP/AZIMUTH: -90 /

| EL   | DEPTH<br>(ft) | Description<br>of<br>Strata        | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities          |                        | Sampling & In Situ Testing |                |       |                              |
|------|---------------|------------------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|--------------------------|------------------------|----------------------------|----------------|-------|------------------------------|
|      |               |                                    | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments   |
| 0    |               | Well Casing                        |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                              |
| 2545 | 5             |                                    |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                              |
| 2540 | 10            |                                    |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                              |
| 2535 | 15            |                                    |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                              |
| 2530 | 20            | QTZ MONZONITE, light gray to white |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 26    |                              |
| 2525 | 25            |                                    |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                              |
| 2520 | 30            |                                    |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 73    | PL(A) = 8.55<br>PL(D) = 5.48 |
| 2515 |               |                                    |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       | UCS = 257.65                 |

BORING TYPE: HQ3

DRILLER: CruX

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 2280

WATER OBSERVATIONS: 1006 ft.

CASING: HW to 20 ft.

REMARKS: \_\_\_\_\_

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                         |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|-----------------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type <u>  </u> ) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)              |
| W                                 | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)              |

(Continued Next Page)



CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2548.8

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2153392.317

DATE: 8/10/2024 - 10/13/2024

PROJECT LOCATION: Rosamod, CA

EASTING: 6514888.703

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities          |                        | Sampling & In Situ Testing |                |       |                             |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|--------------------------|------------------------|----------------------------|----------------|-------|-----------------------------|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments  |
| 2510<br>40          |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       | SLK = Type III              |
| 2505<br>45          |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 41    |                             |
| 2500<br>50          |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 31    | ITS = 31.85<br>UCS = 309.42 |
| 2495<br>55          |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       | PL(D) = 63.41               |
| 2490<br>60          |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 49    | ITS = 72.33                 |
| 2485<br>65          |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                             |
| 2480                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                             |

BORING TYPE: HQ3

DRILLER: Crux

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 2280

WATER OBSERVATIONS: 1006 ft.

CASING: HW to 20 ft.

REMARKS: \_\_\_\_\_

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                         |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|-----------------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type <u>  </u> ) |
| W                                 | Water seep    | PL(A) | Point load axial test $I_s(50)$ (psi)            | TRI | Triaxial stress test (psi)              |
| WL                                | Water level   | PL(D) | Point load diametral test $I_s(50)$ (psi)        | UCS | Uniaxial stress test (psi)              |

(Continued Next Page)



CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2548.8

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2153392.317

DATE: 8/10/2024 - 10/13/2024

PROJECT LOCATION: Rosamod, CA

EASTING: 6514888.703

DIP/AZIMUTH: -90 /

| EL   | DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft)                  |                          | Discontinuities        |      | Sampling & In Situ Testing |       |                            |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
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|      |               |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       | 0.05<br>0.25<br>0.50<br>1.00<br>2.50<br>5.00 | B - Bedding<br>S - Shear | J - Joint<br>F - Fault | Type | Core<br>Rec. %             | RQD % | Test Results<br>& Comments |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|      |               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                                              |                          |                        |      |                            |       |                            |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 2475 | 75            |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                                              |                          |                        |      |                            |       |                            |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |

BORING TYPE: HQ3

DRILLER: CruX

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 2280

WATER OBSERVATIONS: 1006 ft.

CASING: HW to 20 ft.

REMARKS: \_\_\_\_\_

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                  |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|----------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type ___) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)       |
| W                                 | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)       |

(Continued Next Page)



CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2548.8

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2153392.317

DATE: 8/10/2024 - 10/13/2024

PROJECT LOCATION: Rosamod, CA

EASTING: 6514888.703

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities                                      |                        | Sampling & In Situ Testing |                |       |                                                   |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|------------------------------------------------------|------------------------|----------------------------|----------------|-------|---------------------------------------------------|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear                             | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments                        |
| 110                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                      |                        |                            |                |       | UCS = 843.28                                      |
| 115                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                      |                        | C                          | 100            | 72    | ITS = 307.49                                      |
| 120                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                      |                        |                            |                |       | PL(A) = 87.28                                     |
| 125                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                      |                        | C                          | 100            | 67    | PL(D) = 262.22<br>PL(A) = 52.66<br>UCS = 2,645.72 |
| 130                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 127' to 128': 45° -<br>48° Planar               |                        |                            |                |       |                                                   |
| 135                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 131' to 133': (7) 0°<br>- 22° Undulating smooth |                        | C                          | 100            | 70    | PL(D) = 315.40                                    |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 134.7': 51° Undulating<br>rough                      |                        |                            |                |       | PL(A) = 122.52                                    |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 135.7': 47° Undulating<br>rough                      |                        |                            |                |       |                                                   |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 137.25': 12° Undulating<br>smooth                    |                        |                            |                |       | ITS = 140.49                                      |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 137.3' to 163': 0° -<br>12° - 39° Planar smooth |                        |                            |                |       |                                                   |

BORING TYPE: HQ3

DRILLER: Crux

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 2280

WATER OBSERVATIONS: 1006 ft.

CASING: HW to 20 ft.

REMARKS: \_\_\_\_\_

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                    |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|------------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type _____) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)         |
| L                                 | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)         |

(Continued Next Page)





CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2548.8

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2153392.317

DATE: 8/10/2024 - 10/13/2024

PROJECT LOCATION: Rosamod, CA

EASTING: 6514888.703

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities                  |                        | Sampling & In Situ Testing |                |       |                                                         |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|----------------------------------|------------------------|----------------------------|----------------|-------|---------------------------------------------------------|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear         | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments                              |
| 2405<br>145         |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                  |                        | C                          | 100            | 73    | SLK = Type II                                           |
| 2400<br>150         |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                  |                        | C                          | 100            | 77    | PL(D) = 297.56<br><br>PL(A) = 34.27<br>UCS = 3,704.52   |
| 2395<br>155         |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                  |                        | C                          | 100            | 68    | PL(D) = 105.57<br><br>PL(A) = 94.80<br><br>ITS = 189.87 |
| 2390<br>160         |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                  |                        | C                          | 100            | 48    | UCS = 4,084.21                                          |
| 2385<br>165         |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | -172.7° 49° Undulating<br>smooth |                        | C                          | 100            | 48    |                                                         |
| 2380<br>170         |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                  |                        |                            |                |       |                                                         |
| 2375                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                  |                        |                            |                |       |                                                         |

BORING TYPE: HQ3

DRILLER: Crux

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 2280

WATER OBSERVATIONS: 1006 ft.

CASING: HW to 20 ft.

REMARKS: \_\_\_\_\_

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                         |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|-----------------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type <u>  </u> ) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)              |
| WL                                | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)              |

(Continued Next Page)



CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2548.8

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2153392.317

DATE: 8/10/2024 - 10/13/2024

PROJECT LOCATION: Rosamod, CA

EASTING: 6514888.703

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities          |                        | Sampling & In Situ Testing |                |       |                                  |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|--------------------------|------------------------|----------------------------|----------------|-------|----------------------------------|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments       |
| 2370                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                  |
| 180                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       | PL(D) = 131.46<br>PL(A) = 171.15 |
| 2365                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 43    | SLK = Type I                     |
| 185                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                  |
| 2360                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                  |
| 190                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                  |
| 2355                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                  |
| 195                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                  |
| 2350                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                  |
| 200                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                  |
| 2345                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                  |
| 205                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                  |
| 2340                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                  |

BORING TYPE: HQ3

DRILLER: Crux

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 2280

WATER OBSERVATIONS: 1006 ft.

CASING: HW to 20 ft.

REMARKS: \_\_\_\_\_

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                         |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|-----------------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type <u>  </u> ) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)              |
| L                                 | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)              |

(Continued Next Page)



CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2548.8

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2153392.317

DATE: 8/10/2024 - 10/13/2024

PROJECT LOCATION: Rosamod, CA

EASTING: 6514888.703

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities                                                                                                                                 |                       | Sampling & In Situ Testing |                |       |                                                |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|-------------------------------------------------------------------------------------------------------------------------------------------------|-----------------------|----------------------------|----------------|-------|------------------------------------------------|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear                                                                                                                        | J - Joint<br>F- Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments                     |
| 2335                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                                                                                                                 |                       | C                          | 100            | 50    | PL(A) = 217.61<br>PL(D) = 48.98<br>ITS = 80.36 |
| 220                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | -217': 40° - 71° Stepped smooth<br>-From 219.3' to 221': Rubble                                                                                 |                       |                            |                |       | PL(D) = 82.04                                  |
| 225                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | -222': 13° - 29° Undulating smooth<br>-223': 7° Planar smooth<br>-224': 90° Shear, (6) 7° - 29° Planar smooth<br>-From 224.1' to 226.5': Rubble |                       | C                          | 100            | 25    | PL(A) = 43.97                                  |
| 230                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | -227.25': 17° - 29° Undulating rough<br>-228.2': 17° Undulating rough                                                                           |                       |                            |                |       |                                                |
| 235                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                                                                                                                 |                       | C                          | 100            | 21    | SLK = Type I<br>PL(A) = 174.02                 |
| 240                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                                                                                                                 |                       |                            |                |       |                                                |
| 2305                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                                                                                                                 |                       | C                          | 100            | 60    | PL(D) = 81.17<br>PL(D) = 154.22                |

BORING TYPE: HQ3

DRILLER: Crux

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 2280

WATER OBSERVATIONS: 1006 ft.

CASING: HW to 20 ft.

REMARKS: \_\_\_\_\_

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                   |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|-----------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type ____) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)        |
| WL                                | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)        |

(Continued Next Page)



CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2548.8

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2153392.317

DATE: 8/10/2024 - 10/13/2024

PROJECT LOCATION: Rosamod, CA

EASTING: 6514888.703

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities          |                        | Sampling & In Situ Testing |                |       |                            |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|--------------------------|------------------------|----------------------------|----------------|-------|----------------------------|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments |
| 2300                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       | UCS = 3,881.28             |
| 250                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 2295                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 255                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 2290                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 260                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 2285                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 265                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 2280                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 270                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 2275                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 275                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 2270                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |

BORING TYPE: HQ3

DRILLER: Crux

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 2280

WATER OBSERVATIONS: 1006 ft.

CASING: HW to 20 ft.

REMARKS: \_\_\_\_\_

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                    |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|------------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type _____) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)         |
| L                                 | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)         |



CLIENT: Lane Power & Energy Solutions  
PROJECT: Hydrostor Zevsar  
PROJECT LOCATION: Rosamod, CA

SURFACE ELEVATION (ft): 2548.8  
NORTHING: 2153392.317  
EASTING: 6514888.703

PROJECT No: 951-20  
DATE: 8/10/2024 - 10/13/2024  
DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration<br><br>Fr<br>SA<br>MA<br>HA<br>CA | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft)  | Discontinuities<br><br>B - Bedding<br>S - Shear<br>J - Joint<br>F - Fault | Sampling & In Situ Testing |                |       | Test Results<br>& Comments                                           |  |
|---------------------|-----------------------------|-----------------------------------------------------------|----------------|---------------|------|----------|------|-----------|---------|-------|------------------------------|---------------------------------------------------------------------------|----------------------------|----------------|-------|----------------------------------------------------------------------|--|
|                     |                             |                                                           |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                              |                                                                           | Type                       | Core<br>Rec. % | RQD % |                                                                      |  |
| 285                 | CORE LOSS                   |                                                           |                |               |      |          |      |           |         |       | From 285' to 290':<br>Rubble | 282.85': 17° Planar<br>rough                                              | C                          | 100            | 45    | TRI = 27,306.88<br><br>PL(D) = 435.93                                |  |
|                     |                             |                                                           |                |               |      |          |      |           |         |       |                              |                                                                           |                            |                |       |                                                                      |  |
|                     |                             |                                                           |                |               |      |          |      |           |         |       |                              |                                                                           |                            |                |       |                                                                      |  |
|                     |                             |                                                           |                |               |      |          |      |           |         |       |                              |                                                                           |                            |                |       |                                                                      |  |
|                     |                             |                                                           |                |               |      |          |      |           |         |       |                              |                                                                           |                            |                |       |                                                                      |  |
|                     |                             |                                                           |                |               |      |          |      |           |         |       |                              |                                                                           |                            |                |       |                                                                      |  |
|                     |                             |                                                           |                |               |      |          |      |           |         |       |                              |                                                                           |                            |                |       |                                                                      |  |
|                     |                             |                                                           |                |               |      |          |      |           |         |       |                              |                                                                           |                            |                |       |                                                                      |  |
|                     |                             |                                                           |                |               |      |          |      |           |         |       |                              |                                                                           |                            |                |       |                                                                      |  |
|                     |                             |                                                           |                |               |      |          |      |           |         |       |                              |                                                                           |                            |                |       |                                                                      |  |
| 290                 |                             |                                                           |                |               |      |          |      |           |         |       |                              |                                                                           |                            |                |       |                                                                      |  |
| 295                 |                             |                                                           |                |               |      |          |      |           |         |       |                              |                                                                           | C                          | 100            | 47    | PL(D) = 205.37<br>ITS = 739.12                                       |  |
|                     |                             |                                                           |                |               |      |          |      |           |         |       |                              |                                                                           |                            |                |       |                                                                      |  |
|                     |                             |                                                           |                |               |      |          |      |           |         |       |                              |                                                                           |                            |                |       |                                                                      |  |
|                     |                             |                                                           |                |               |      |          |      |           |         |       |                              |                                                                           |                            |                |       |                                                                      |  |
|                     |                             |                                                           |                |               |      |          |      |           |         |       |                              |                                                                           |                            |                |       |                                                                      |  |
|                     |                             |                                                           |                |               |      |          |      |           |         |       |                              |                                                                           |                            |                |       |                                                                      |  |
|                     |                             |                                                           |                |               |      |          |      |           |         |       |                              |                                                                           |                            |                |       |                                                                      |  |
|                     |                             |                                                           |                |               |      |          |      |           |         |       |                              |                                                                           |                            |                |       |                                                                      |  |
|                     |                             |                                                           |                |               |      |          |      |           |         |       |                              |                                                                           |                            |                |       |                                                                      |  |
|                     |                             |                                                           |                |               |      |          |      |           |         |       |                              |                                                                           |                            |                |       |                                                                      |  |
| 300                 |                             |                                                           |                |               |      |          |      |           |         |       |                              |                                                                           |                            |                |       | PL(D) = 205.37<br>ITS = 739.12                                       |  |
|                     |                             |                                                           |                |               |      |          |      |           |         |       |                              |                                                                           |                            |                |       |                                                                      |  |
|                     |                             |                                                           |                |               |      |          |      |           |         |       |                              |                                                                           |                            |                |       |                                                                      |  |
|                     |                             |                                                           |                |               |      |          |      |           |         |       |                              |                                                                           |                            |                |       |                                                                      |  |
|                     |                             |                                                           |                |               |      |          |      |           |         |       |                              |                                                                           |                            |                |       |                                                                      |  |
|                     |                             |                                                           |                |               |      |          |      |           |         |       |                              |                                                                           |                            |                |       |                                                                      |  |
|                     |                             |                                                           |                |               |      |          |      |           |         |       |                              |                                                                           |                            |                |       |                                                                      |  |
|                     |                             |                                                           |                |               |      |          |      |           |         |       |                              |                                                                           |                            |                |       |                                                                      |  |
|                     |                             |                                                           |                |               |      |          |      |           |         |       |                              |                                                                           |                            |                |       |                                                                      |  |
|                     |                             |                                                           |                |               |      |          |      |           |         |       |                              |                                                                           |                            |                |       |                                                                      |  |
| 305                 |                             |                                                           |                |               |      |          |      |           |         |       |                              |                                                                           |                            |                |       | PL(A) = 151.68<br>PL(D) = 129.71<br>TRI = 20,800.38<br>SLK = Type II |  |
|                     |                             |                                                           |                |               |      |          |      |           |         |       |                              |                                                                           |                            |                |       |                                                                      |  |
|                     |                             |                                                           |                |               |      |          |      |           |         |       |                              |                                                                           |                            |                |       |                                                                      |  |
|                     |                             |                                                           |                |               |      |          |      |           |         |       |                              |                                                                           |                            |                |       |                                                                      |  |
|                     |                             |                                                           |                |               |      |          |      |           |         |       |                              |                                                                           |                            |                |       |                                                                      |  |
|                     |                             |                                                           |                |               |      |          |      |           |         |       |                              |                                                                           |                            |                |       |                                                                      |  |
|                     |                             |                                                           |                |               |      |          |      |           |         |       |                              |                                                                           |                            |                |       |                                                                      |  |
|                     |                             |                                                           |                |               |      |          |      |           |         |       |                              |                                                                           |                            |                |       |                                                                      |  |
|                     |                             |                                                           |                |               |      |          |      |           |         |       |                              |                                                                           |                            |                |       |                                                                      |  |
|                     |                             |                                                           |                |               |      |          |      |           |         |       |                              |                                                                           |                            |                |       |                                                                      |  |
| 310                 |                             |                                                           |                |               |      |          |      |           |         |       |                              |                                                                           |                            |                |       |                                                                      |  |

BORING TYPE: HQ3  
HOLE DEPTH (ft): 2280

DRILLER: Cruix  
WATER OBSERVATIONS: 1006 ft.

LOGGED BY: Chris Messenger  
CASING: HW to 20 ft.

REMARKS:

| SAMPLING & IN SITU TESTING LEGEND |                                                  |     |                                  |  |
|-----------------------------------|--------------------------------------------------|-----|----------------------------------|--|
| ITS                               | Indirect tensile strength (Brazilian) test (psi) | SLK | Stress durability test (Type II) |  |
| PL(A)                             | Point load axial test (psi)                      | TRI | Triaxial stress test (psi)       |  |
| PL(D)                             | Point load diametral test (psi)                  | LCS | Uniaxial stress test (psi)       |  |
| C                                 | Core drilling                                    |     |                                  |  |
| W                                 | Water seep                                       |     |                                  |  |
| W                                 | Water level                                      |     |                                  |  |



CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2548.8

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2153392.317

DATE: 8/10/2024 - 10/13/2024

PROJECT LOCATION: Rosamod, CA

EASTING: 6514888.703

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities          |                        | Sampling & In Situ Testing |                |       |                                                                       |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|--------------------------|------------------------|----------------------------|----------------|-------|-----------------------------------------------------------------------|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments                                            |
| 2230                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                                                       |
| 320                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 82    | UCS = 3,576.62                                                        |
| 2225                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                                                       |
| 325                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                                                       |
| 2220                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                                                       |
| 330                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 88    | PL(A) = 212.14<br>PL(D) = 286.28<br>UCS = 2,822.42<br>TRI = 14,530.54 |
| 2215                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                                                       |
| 335                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                                                       |
| 2210                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                                                       |
| 340                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       | PL(D) = 142.48                                                        |
| 2205                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 78    |                                                                       |
| 345                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                                                       |
| 2200                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       | ITS = 142.44                                                          |

BORING TYPE: HQ3

DRILLER: Crux

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 2280

WATER OBSERVATIONS: 1006 ft.

CASING: HW to 20 ft.

REMARKS: \_\_\_\_\_

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                         |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|-----------------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type <u>  </u> ) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)              |
| L                                 | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)              |

(Continued Next Page)



CLIENT: Lane Power & Energy Solutions  
PROJECT: Hydrostor Zevsar  
PROJECT LOCATION: Rosamod, CA

SURFACE ELEVATION (ft): 2548.8  
NORTHING: 2153392.317  
EASTING: 6514888.703

PROJECT No: 951-20  
DATE: 8/10/2024 - 10/13/2024  
DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata                                                                                                    | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft)          | Discontinuities                                                               |                        | Sampling & In Situ Testing |                |       |                            |
|---------------------|--------------------------------------------------------------------------------------------------------------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|--------------------------------------|-------------------------------------------------------------------------------|------------------------|----------------------------|----------------|-------|----------------------------|
|                     |                                                                                                                                | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                                      | B - Bedding<br>S - Shear                                                      | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments |
| 350                 | QTZ MONZONITE, light gray to white, phaneritic, with K-Na feldspar and hornblende, trace amounts of mica, pyrite, and chlorite |                         |    |    |    |    |                |               |      |          |      |           |         |       | 0.05<br>0.25<br>0.50<br>2.50<br>5.00 |                                                                               |                        |                            |                |       | PL(A) = 277.52             |
|                     |                                                                                                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       |                                      | From 351.45' to 352':<br>71° Undulating smooth                                |                        |                            |                |       |                            |
|                     |                                                                                                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       |                                      | 353': 38° Planar rough                                                        |                        | C                          | 100            | 48    | UCS = 4,803.76             |
|                     |                                                                                                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       |                                      | 354.2': 90° Fracture with<br>crosscuts, rubble                                |                        |                            |                |       |                            |
| 355                 |                                                                                                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       |                                      | 355': (2) 28° - 38° Planar<br>rough                                           |                        |                            |                |       |                            |
|                     |                                                                                                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       |                                      | 358': 62° Undulating<br>rough                                                 |                        |                            |                |       |                            |
|                     |                                                                                                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       |                                      | From 359' to 362': (8)<br>30° - 49° Planar rough                              |                        |                            |                |       |                            |
| 360                 |                                                                                                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       |                                      |                                                                               |                        | C                          | 100            | 41    | PL(D) = 106.97             |
|                     |                                                                                                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       |                                      | From 366' to 367': 59° -<br>67° Planar smooth                                 |                        |                            |                |       |                            |
|                     |                                                                                                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       |                                      | From 369' to 370': 90° -<br>80° Stepped rough                                 |                        |                            |                |       |                            |
|                     |                                                                                                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       |                                      | From 371' to 375': (6)<br>30° - 40° Planar rough,<br>(1) 45° - 90° Undulating |                        | C                          | 100            | 43    |                            |
| 365                 |                                                                                                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       |                                      |                                                                               |                        |                            |                |       | SLK = Type I               |
|                     |                                                                                                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       |                                      |                                                                               |                        |                            |                |       | PL(D) = 77.15              |
|                     |                                                                                                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       |                                      | 377.6': 51° Planar<br>smooth                                                  |                        |                            |                |       | PL(A) = 219.43             |
|                     |                                                                                                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       |                                      | From 378.25' to 378.75':<br>60° Planar rough                                  |                        |                            |                |       |                            |
| 370                 |                                                                                                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       |                                      | 379.8': 22° Planar rough                                                      |                        |                            |                |       |                            |
|                     |                                                                                                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       |                                      | 380.7': 22° Undulating<br>rough                                               |                        |                            |                |       |                            |
|                     |                                                                                                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       |                                      | From 381' to 386': (10)<br>22° - 61° Planar smooth                            |                        | C                          | 100            | 38    | PL(A) = 320.08             |
| 375                 |                                                                                                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       |                                      |                                                                               |                        |                            |                |       | PL(D) = 406.81             |
|                     |                                                                                                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       |                                      |                                                                               |                        |                            |                |       |                            |
| 380                 |                                                                                                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       |                                      |                                                                               |                        |                            |                |       |                            |
|                     |                                                                                                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       |                                      |                                                                               |                        |                            |                |       |                            |
| 2165'               |                                                                                                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       |                                      |                                                                               |                        |                            |                |       |                            |

BORING TYPE: HQ3  
HOLE DEPTH (ft): 2280  
REMARKS: \_\_\_\_\_

DRILLER: Crux  
WATER OBSERVATIONS: 1006 ft.

LOGGED BY: Chris Messenger  
CASING: HW to 20 ft.

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                    |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|------------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type _____) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)         |
| L                                 | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)         |

(Continued Next Page)



CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2548.8

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2153392.317

DATE: 8/10/2024 - 10/13/2024

PROJECT LOCATION: Rosamod, CA

EASTING: 6514888.703

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities          |                        | Sampling & In Situ Testing |                |       |                            |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|--------------------------|------------------------|----------------------------|----------------|-------|----------------------------|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments |
| 2160                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       | ITS = 376.55               |
| 390                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 2155                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 395                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 2150                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 400                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 2145                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 405                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 2140                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 410                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 2135                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 415                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 2130                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |

BORING TYPE: HQ3

DRILLER: CruX

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 2280

WATER OBSERVATIONS: 1006 ft.

CASING: HW to 20 ft.

REMARKS: \_\_\_\_\_

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                   |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|-----------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type ____) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)        |
| WL                                | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)        |

(Continued Next Page)





CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2548.8

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2153392.317

DATE: 8/10/2024 - 10/13/2024

PROJECT LOCATION: Rosamod, CA

EASTING: 6514888.703

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities          |                        | Sampling & In Situ Testing |                |       |                                                    |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|--------------------------|------------------------|----------------------------|----------------|-------|----------------------------------------------------|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments                         |
| 2125<br>425         |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 43    | PL(A) = 143.50                                     |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                                    |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                                    |
| 2120<br>430         |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                                    |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                                    |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                                    |
| 2115<br>435         |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 56    | UCS = 5,621.33<br>PL(A) = 198.51<br>PL(D) = 452.64 |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                                    |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                                    |
| 2110<br>440         |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                                    |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                                    |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                                    |
| 2105<br>445         |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 72    | PL(A) = 430.82<br>ITS = 612.88                     |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                                    |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                                    |
| 2100<br>450         |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                                    |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                                    |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                                    |
| 2095                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 65    | PL(D) = 449.75                                     |

BORING TYPE: HQ3

DRILLER: Crux

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 2280

WATER OBSERVATIONS: 1006 ft.

CASING: HW to 20 ft.

REMARKS: \_\_\_\_\_

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                   |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|-----------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type ____) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)        |
| WL                                | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)        |

**CLIENT:** Lane Power & Energy Solutions

**SURFACE ELEVATION (ft):** 2548.8

**PROJECT No:** 951-20

**PROJECT:** Hydrostor Zevsar

**NORTHING:** 2153392.317

**DATE:** 8/10/2024 - 10/13/2024

**PROJECT LOCATION:** Rosamod, CA

**EASTING:** 6514888.703

DIP/AZIMUTH: -90 /

| EL    | DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) |      | Discontinuities |                           | Sampling & In Situ Testing                                                                                                                         |                          |                        |                                                          |                                     |       |                            |
|-------|---------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|------|-----------------|---------------------------|----------------------------------------------------------------------------------------------------------------------------------------------------|--------------------------|------------------------|----------------------------------------------------------|-------------------------------------|-------|----------------------------|
|       |               |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex-Hard |       | 0.05                        | 0.25 | 0.50            | 2.50                      | 5.00                                                                                                                                               | B - Bedding<br>S - Shear | J - Joint<br>F - Fault | Type                                                     | Core<br>Rec. %                      | RQD % | Test Results<br>& Comments |
|       |               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |                 |                           |                                                                                                                                                    |                          |                        |                                                          |                                     |       |                            |
| 2090' | 460           |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |                 | 455.4': 42° Planar smooth |                                                                                                                                                    |                          |                        | PL(A) = 257.76<br><br>SLK = Type I<br><br>PL(A) = 179.25 |                                     |       |                            |
| 2085' | 465           |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |                 |                           | From 461' to 462': (2)<br>38° Planar smooth wedge                                                                                                  | C                        | 100                    | 57                                                       | PL(D) = 52.22<br><br>UCS = 5,842.99 |       |                            |
| 2080' | 470           |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |                 |                           | 464': 17° Planar smooth<br>From 465' to 466': 90° Planar smooth<br>From 466' to 467.5': Rubble<br>From 468' to 470': (5)<br>20° - 30° Planar rough |                          |                        |                                                          |                                     |       |                            |
| 2075' | 475           |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |                 |                           | From 476.5' to 477': Rubble                                                                                                                        | C                        | 100                    | 78                                                       | UCS = 5,379.33                      |       |                            |
| 2070' | 480           |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |                 |                           | 479': 40° Planar smooth                                                                                                                            |                          |                        |                                                          |                                     |       |                            |
| 2065' | 485           |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |                 |                           | 480.3': 44° Planar smooth                                                                                                                          | C                        | 100                    | 81                                                       | PL(A) = 407.22<br>PL(D) = 275.96    |       |                            |
| 2060' |               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |                 |                           | From 483.9' to 484.2': (2) 61° Undulating smooth                                                                                                   |                          |                        |                                                          |                                     |       |                            |
|       |               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |                 |                           | 485.2': 45° Planar smooth                                                                                                                          |                          |                        |                                                          |                                     |       |                            |
|       |               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |                 |                           | 487': 0° Planar rough                                                                                                                              |                          |                        |                                                          |                                     |       |                            |
|       |               |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |                 |                           | 488': 7° Undulating rough                                                                                                                          |                          |                        |                                                          |                                     |       |                            |

**BORING TYPE:** HQ3

**DRILLER:** Crux

**LOGGED BY:** Chris Messenger

HOLE DEPTH (ft): 2280

WATER OBSERVATIONS: 1006 ft.

**CASING:** HW to 20 ft.

REMARKS:

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |
|-----------------------------------|---------------|-------|--------------------------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               |
| W                                 | Water level   | PL(D) | Point load diametral test Is(50) (psi)           |
|                                   |               | SLK   | Slake durability test (Type _____)               |
|                                   |               | TRI   | Triaxial stress test (psi)                       |
|                                   |               | UCS   | Uniaxial stress test (psi)                       |

(Continued Next Page)



CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2548.8

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2153392.317

DATE: 8/10/2024 - 10/13/2024

PROJECT LOCATION: Rosamod, CA

EASTING: 6514888.703

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata                                                                                                         | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities                                                                                                |                        | Sampling & In Situ Testing |                |       |                                                  |
|---------------------|-------------------------------------------------------------------------------------------------------------------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|----------------------------------------------------------------------------------------------------------------|------------------------|----------------------------|----------------|-------|--------------------------------------------------|
|                     |                                                                                                                                     | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear                                                                                       | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments                       |
| 495                 |                                                                                                                                     |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 490': 61° Planar smooth                                                                                        |                        | C                          | 100            | 86    | PL(A) = 395.84<br>ITS = 274.39<br>PL(D) = 127.18 |
| 500                 |                                                                                                                                     |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 494': 70° Undulating rough<br>494.7': 71° Fracture<br>495': 17° Planar smooth<br>497.8': 71° Undulating smooth |                        | C                          | 100            | 59    | ITS = 284.11<br>UCS = 7,782.02<br>SLK = Type I   |
| 505                 |                                                                                                                                     |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 504' to 511':<br>Rubble                                                                                   |                        | C                          | 100            | 62    | PL(D) = 448.88<br>PL(A) = 124.35                 |
| 510                 |                                                                                                                                     |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 512.6' to 513': 38°<br>- 49° Planar smooth                                                                |                        | C                          | 100            | 62    | PL(A) = 302.39<br>PL(D) = 79.59                  |
| 515                 |                                                                                                                                     |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 514.5' to 515.4':<br>79° Planar smooth                                                                    |                        | C                          | 100            | 31    |                                                  |
| 516                 | QTZ MONZONITE, light gray to white, phaneritic, with hornblende and Na-K feldspar, trace amounts of pyrite and chlorite at contacts |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 516' to 538':<br>Multiple fractures throughout, rubble                                                    |                        | C                          | 100            | 31    |                                                  |
| 520                 |                                                                                                                                     |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                                                                                |                        | C                          | 100            | 31    |                                                  |

BORING TYPE: HQ3

DRILLER: CruX

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 2280

WATER OBSERVATIONS: 1006 ft.

CASING: HW to 20 ft.

REMARKS:

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                         |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|-----------------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type <u>  </u> ) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)              |
| WL                                | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)              |

(Continued Next Page)



CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2548.8

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2153392.317

DATE: 8/10/2024 - 10/13/2024

PROJECT LOCATION: Rosamod, CA

EASTING: 6514888.703

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities                                   |                        | Sampling & In Situ Testing |                |       |                                  |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|---------------------------------------------------|------------------------|----------------------------|----------------|-------|----------------------------------|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear                          | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments       |
| 2020<br>530         |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                   |                        |                            |                |       | UCS = 4,830.22                   |
| 2015<br>535         |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                   |                        | C                          | 100            | 32    |                                  |
| 2010<br>540         |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 540' to 544': (4)<br>80° Planar smooth       |                        | C                          | 100            | 36    | PL(D) = 354.94<br>PL(A) = 181.25 |
| 2005<br>545         |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 546' to 547': 90°<br>Stepped smooth          |                        |                            |                |       | PL(A) = 367.35<br>ITS = 608.41   |
| 2000<br>550         |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 549' to 551': (7)<br>17° - 34° Planar smooth |                        |                            |                |       |                                  |
| 1995<br>555         |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 554' to 557': (4)<br>19° - 44° Planar smooth |                        | C                          | 100            | 44    | SLK = Type I<br>PL(D) = 340.86   |
| 1990                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                   |                        |                            |                |       |                                  |

BORING TYPE: HQ3

DRILLER: Crux

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 2280

WATER OBSERVATIONS: 1006 ft.

CASING: HW to 20 ft.

REMARKS: \_\_\_\_\_

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                         |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|-----------------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type <u>  </u> ) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)              |
| L                                 | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)              |

(Continued Next Page)



CLIENT: Lane Power & Energy Solutions  
PROJECT: Hydrostor Zevsar  
PROJECT LOCATION: Rosamod, CA

SURFACE ELEVATION (ft): 2548.8  
NORTHING: 2153392.317  
EASTING: 6514888.703

PROJECT No: 951-20  
DATE: 8/10/2024 - 10/13/2024  
DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata                                                                                                                  | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities                                     |                        | Sampling & In Situ Testing |                |       |                                                           |
|---------------------|----------------------------------------------------------------------------------------------------------------------------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|-----------------------------------------------------|------------------------|----------------------------|----------------|-------|-----------------------------------------------------------|
|                     |                                                                                                                                              | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear                            | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments                                |
| 565                 |                                                                                                                                              |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 562' to 565': (5)<br>40° - 47° Planar rough    |                        | C                          | 100            | 51    | PL(D) = 20.99                                             |
| 570                 |                                                                                                                                              |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 566.5': 47° Planar<br>smooth                        |                        |                            |                |       |                                                           |
| 575                 |                                                                                                                                              |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 567.7' to 572': (8)<br>17° - 42° Planar smooth |                        | C                          | 100            | 43    | PL(A) = 33.62<br><br>UCS = 1,547.80                       |
| 580                 |                                                                                                                                              |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 576' to 577':<br>Rubble                        |                        |                            |                |       | ITS = 393.55<br><br>PL(D) = 521.97<br><br>TRI = 19,972.41 |
| 581                 | QTZ MONZONITE, light gray to white,<br>phaneritic, with feldspar, hornblende,<br>and biotite, trace amounts of mica,<br>pyrite, and chlorite |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 579' to 581': (2)<br>45° Planar smooth         |                        |                            |                |       |                                                           |
| 585                 |                                                                                                                                              |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 581': 40° Planar smooth                             |                        | C                          | 100            | 64    |                                                           |
|                     |                                                                                                                                              |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 581.3': 40° Planar<br>smooth                        |                        |                            |                |       |                                                           |
|                     |                                                                                                                                              |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 581.6': 70° - 80°<br>Stepped smooth                 |                        |                            |                |       |                                                           |
|                     |                                                                                                                                              |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 582.9': 27° Planar<br>smooth                        |                        |                            |                |       |                                                           |
|                     |                                                                                                                                              |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 584.4': 17° Planar<br>smooth                        |                        |                            |                |       | C                                                         |
|                     |                                                                                                                                              |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 585' to 586': (3)<br>20° - 30° Planar smooth   |                        |                            |                |       |                                                           |
|                     |                                                                                                                                              |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 589.3': 45° Planar<br>smooth                        |                        |                            |                |       |                                                           |
|                     |                                                                                                                                              |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 589.4' to 590.4':<br>90° Undulating smooth     |                        |                            |                |       | C                                                         |
|                     |                                                                                                                                              |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 593.1': 7° Planar rough                             |                        |                            |                |       |                                                           |
|                     |                                                                                                                                              |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 594.4': 20° - 30°<br>Undulating smooth              |                        |                            |                |       |                                                           |

BORING TYPE: HQ3  
HOLE DEPTH (ft): 2280  
REMARKS: \_\_\_\_\_

DRILLER: Crux  
WATER OBSERVATIONS: 1006 ft.

LOGGED BY: Chris Messenger  
CASING: HW to 20 ft.

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                    |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|------------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type _____) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)         |
| L                                 | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)         |



CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2548.8

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2153392.317

DATE: 8/10/2024 - 10/13/2024

PROJECT LOCATION: Rosamod, CA

EASTING: 6514888.703

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata                                        | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities                                                |                        | Sampling & In Situ Testing |                |       |                                                   |
|---------------------|--------------------------------------------------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|----------------------------------------------------------------|------------------------|----------------------------|----------------|-------|---------------------------------------------------|
|                     |                                                                    | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear                                       | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments                        |
| 1950<br>600         | QTZ MONZONITE, light gray to white<br>to pink to green, phaneritic |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 597' to 598': (2)<br>45° Planar smooth                    |                        |                            |                |       | TRI = 19,561.18<br>TRI = 16,068.92                |
| 1945<br>605         |                                                                    |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 599': 17° Undulating<br>rough                                  |                        |                            |                |       |                                                   |
| 1940<br>610         |                                                                    |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 600': 22° Planar smooth                                        |                        |                            |                |       |                                                   |
| 1935<br>615         |                                                                    |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 602' to 602.3': 61°<br>Planar smooth                      |                        | C                          | 100            | 47    | PL(A) = 112.38<br>UCS = 7,210.07<br>SLK = Type II |
| 1930<br>620         | QTZ MONZONITE, light gray to white,<br>phaneritic                  |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 605': 12° Planar smooth                                        |                        |                            |                |       |                                                   |
| 1925<br>625         |                                                                    |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 606' to 621':<br>Multiple fractures<br>throughout, rubble |                        |                            |                |       |                                                   |
| 1920                |                                                                    |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 624' to 626':<br>Multiple 0° - 4° Planar                  |                        | C                          | 100            | 47    | ITS = 121.59                                      |
|                     |                                                                    |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 626.8': 42° Planar<br>smooth                                   |                        |                            |                |       |                                                   |
|                     |                                                                    |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 628': (2) 7° Planar<br>smooth                                  |                        | C                          | 100            | 58    | SLK = Type II                                     |

BORING TYPE: HQ3

DRILLER: Crux

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 2280

WATER OBSERVATIONS: 1006 ft.

CASING: HW to 20 ft.

REMARKS: \_\_\_\_\_

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                  |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|----------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type ___) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)       |
| L                                 | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)       |



CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2548.8

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2153392.317

DATE: 8/10/2024 - 10/13/2024

PROJECT LOCATION: Rosamod, CA

EASTING: 6514888.703

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata                                | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities | Sampling & In Situ Testing |                        |      |                |       |                            |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
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|                     |                                                            | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             |                 | B - Bedding<br>S - Shear   | J - Joint<br>F - Fault | Type | Core<br>Rec. % | ROD % | Test Results<br>& Comments |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|                     |                                                            |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                 |                            |                        |      |                |       |                            |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1915<br>635         | QTZ MONZONITE, light gray to dark<br>gray to pink to green |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                 |                            |                        |      |                |       |                            |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |

BORING TYPE: HQ3

DRILLER: CruX

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 2280

WATER OBSERVATIONS: 1006 ft.

CASING: HW to 20 ft.

REMARKS: \_\_\_\_\_

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                   |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|-----------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type ____) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)        |
| WL                                | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)        |

(Continued Next Page)



**CLIENT:** Lane Power & Energy Solutions  
**PROJECT:** Hydrostor Zevsar  
**PROJECT LOCATION:** Rosamod, CA

**SURFACE ELEVATION (ft):** 2548.8  
**NORTHING:** 2153392.317  
**EASTING:** 6514888.703

**PROJECT No:** 951-20  
**DATE:** 8/10/2024 - 10/13/2024  
**DIP/AZIMUTH:** -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata                                                                                                                       | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities                          |                        | Sampling & In Situ Testing |                |       |                                                                     |
|---------------------|---------------------------------------------------------------------------------------------------------------------------------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|------------------------------------------|------------------------|----------------------------|----------------|-------|---------------------------------------------------------------------|
|                     |                                                                                                                                                   | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear                 | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments                                          |
| 1880<br>670         |                                                                                                                                                   |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | Multiple fractures<br>throughout, rubble |                        |                            |                |       |                                                                     |
| 1875<br>674<br>675  | QTZ MONZONITE, light gray to white,<br>phaneritic, with Na-K feldspar,<br>hornblende, and biotite, trace amounts<br>of mica, chlorite, and pyrite |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                          |                        | C                          | 100            | 57    | SLK = Type I<br>PL(D) = 36.17<br><br>PL(A) = 120.44<br>ITS = 416.31 |
| 1870<br>680         |                                                                                                                                                   |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                          |                        |                            |                |       |                                                                     |
| 1865<br>685         |                                                                                                                                                   |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                          |                        | C                          | 100            | 67    | UCS = 3,687.37<br>PL(D) = 73.65                                     |
| 1860<br>686         | QTZ MONZONITE, light gray to pink<br>to green, phaneritic to aphanitic                                                                            |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                          |                        |                            |                |       |                                                                     |
| 1855<br>690         |                                                                                                                                                   |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                          |                        |                            |                |       |                                                                     |
| 1850<br>695         |                                                                                                                                                   |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                          |                        | C                          | 100            | 63    |                                                                     |
| 699                 | QTZ MONZONITE, light gray to white<br>to pink                                                                                                     |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                          |                        |                            |                |       |                                                                     |

**BORING TYPE:** HQ3  
**HOLE DEPTH (ft):** 2280  
**REMARKS:**

**DRILLER:** Crux  
**WATER OBSERVATIONS:** 1006 ft.

**LOGGED BY:** Chris Messenger  
**CASING:** HW to 20 ft.

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                  |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|----------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type ___) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)       |
| WL                                | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)       |

(Continued Next Page)





CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2548.8

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2153392.317

DATE: 8/10/2024 - 10/13/2024

PROJECT LOCATION: Rosamod, CA

EASTING: 6514888.703

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata                            | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities                                                |                        | Sampling & In Situ Testing |                |       |                                |
|---------------------|--------------------------------------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|----------------------------------------------------------------|------------------------|----------------------------|----------------|-------|--------------------------------|
|                     |                                                        | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear                                       | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments     |
| 705                 |                                                        |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 700': 42° Planar smooth                                        |                        | C                          | 100            | 53    | ITS = 149.07                   |
| 710                 |                                                        |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 701' to 703':<br>Rubble                                   |                        |                            |                |       | PL(A) = 29.28                  |
| 715                 |                                                        |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | -706.9': 47° Undulating<br>smooth                              |                        |                            |                |       |                                |
| 719                 |                                                        |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 709' to 711': (3)<br>17° - 29° Undulating<br>smooth       |                        |                            |                |       |                                |
| 720                 | QTZ MONZONITE, light gray to white<br>to pink to green |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | -711.3': 47° Planar<br>smooth                                  |                        | C                          | 100            | 56    | SLK = Type I<br>PL(A) = 104.44 |
| 725                 |                                                        |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | -712.4': 74° Planar<br>smooth                                  |                        |                            |                |       |                                |
| 730                 |                                                        |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 715' to 716': (3)<br>30° - 33° Planar rough               |                        |                            |                |       | ITS = 474.00<br>UCS = 5,842.77 |
|                     |                                                        |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 716.5': 0° Planar smooth                                       |                        |                            |                |       |                                |
|                     |                                                        |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 719' to 729':<br>Multiple fractures<br>throughout, rubble |                        | C                          | 100            | 50    | PL(D) = 41.37                  |
|                     |                                                        |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 729' to 739':<br>Multiple fractures<br>throughout, rubble |                        |                            |                |       | PL(A) = 37.41                  |
|                     |                                                        |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                                |                        | C                          | 100            | 44    |                                |

BORING TYPE: HQ3

DRILLER: Crux

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 2280

WATER OBSERVATIONS: 1006 ft.

CASING: HW to 20 ft.

REMARKS: \_\_\_\_\_

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                  |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|----------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type ___) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)       |
| WL                                | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)       |

(Continued Next Page)



CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2548.8

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2153392.317

DATE: 8/10/2024 - 10/13/2024

PROJECT LOCATION: Rosamod, CA

EASTING: 6514888.703

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata                       | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities                                                |                        | Sampling & In Situ Testing |                |       |                                                               |
|---------------------|---------------------------------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|----------------------------------------------------------------|------------------------|----------------------------|----------------|-------|---------------------------------------------------------------|
|                     |                                                   | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear                                       | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments                                    |
| 1810<br>740         | QTZ MONZONITE, light gray to white,<br>phaneritic |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 739' to 746':<br>Multiple fractures<br>throughout, rubble |                        |                            |                |       | PL(A) = 192.63                                                |
| 1805<br>745         |                                                   |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                                |                        | C                          | 100            | 22    |                                                               |
| 1800<br>746         |                                                   |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 746' to 756':<br>Rubble                                   |                        |                            |                |       | PL(D) = 109.33<br>PL(A) = 21.44                               |
| 1795<br>750         |                                                   |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                                |                        | C                          | 100            | 15    |                                                               |
| 1790<br>755         |                                                   |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 756' to 762':<br>Rubble                                   |                        |                            |                |       |                                                               |
| 1785<br>760         |                                                   |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                                |                        |                            |                |       | UCS = 994.86                                                  |
| 1780<br>765         |                                                   |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 764' to 771': (17)<br>10° - 40° Planar smooth             |                        | C                          | 100            | 33    |                                                               |
|                     |                                                   |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                                |                        |                            |                |       | PL(A) = 54.54<br>SLK = Type II<br>UCS = 519.42<br>ITS = 93.85 |

BORING TYPE: HQ3

DRILLER: Crux

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 2280

WATER OBSERVATIONS: 1006 ft.

CASING: HW to 20 ft.

REMARKS: \_\_\_\_\_

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                  |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|----------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type ___) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)       |
| L                                 | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)       |

(Continued Next Page)



CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2548.8

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2153392.317

DATE: 8/10/2024 - 10/13/2024

PROJECT LOCATION: Rosamod, CA

EASTING: 6514888.703

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities          |                        | Sampling & In Situ Testing |                |       |                                |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|--------------------------|------------------------|----------------------------|----------------|-------|--------------------------------|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments     |
| 1775                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 49    | PL(D) = 114.06                 |
| 775                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       | PL(A) = 80.34                  |
| 1770                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                |
| 780                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                |
| 1765                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 49    | PL(D) = 71.28                  |
| 785                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                |
| 1760                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                |
| 790                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 79    | PL(D) = 74.00<br>PL(A) = 19.70 |
| 1755                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                |
| 795                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                |
| 1750                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                |
| 800                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       | ITS = 68.69                    |
| 1745                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 71    | PL(D) = 39.80                  |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                |

BORING TYPE: HQ3

DRILLER: Crux

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 2280

WATER OBSERVATIONS: 1006 ft.

CASING: HW to 20 ft.

REMARKS: \_\_\_\_\_

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                         |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|-----------------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type <u>  </u> ) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)              |
| L                                 | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)              |

(Continued Next Page)



CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2548.8

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2153392.317

DATE: 8/10/2024 - 10/13/2024

PROJECT LOCATION: Rosamod, CA

EASTING: 6514888.703

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities          |                        | Sampling & In Situ Testing |                |       |                                    |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|--------------------------|------------------------|----------------------------|----------------|-------|------------------------------------|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments         |
| 1740<br>810         |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       | PL(A) = 392.19                     |
| 1735<br>815         |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 56    |                                    |
| 1730<br>820         |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       | UCS =<br>12,941.04<br>SLK = Type I |
| 1725<br>825         |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 66    |                                    |
| 1720<br>830         |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       | PL(D) = 186.65<br>ITS = 240.11     |
| 1715<br>835         |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 51    | PL(A) = 14.77<br>UCS = 4,063.04    |

BORING TYPE: HQ3

DRILLER: CruX

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 2280

WATER OBSERVATIONS: 1006 ft.

CASING: HW to 20 ft.

REMARKS: \_\_\_\_\_

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                   |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|-----------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type ____) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)        |
| WL                                | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)        |

(Continued Next Page)



CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2548.8

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2153392.317

DATE: 8/10/2024 - 10/13/2024

PROJECT LOCATION: Rosamod, CA

EASTING: 6514888.703

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata                                                                                   | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Fracture<br>Spacing<br>(ft) | Discontinuities                          |                        | Sampling & In Situ Testing |                |       |                                    |
|---------------------|---------------------------------------------------------------------------------------------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-----------------------------|------------------------------------------|------------------------|----------------------------|----------------|-------|------------------------------------|
|                     |                                                                                                               | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |                             | B - Bedding<br>S - Shear                 | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments         |
| 1705                |                                                                                                               |                         |    |    |    |    |                |               |      |          |      |           |         |                             |                                          |                        | C                          | 100            | 37    | PL(D) = 191.99                     |
| 846                 | QTZ MONZONITE, light gray to dark gray to pink to green                                                       |                         |    |    |    |    |                |               |      |          |      |           |         |                             | From 846' to 854':<br>Decomposed, rubble |                        | C                          | 100            | 62    | ITS = 341.45                       |
| 854                 | QTZ MONZONITE, light gray to white, phaneritic, with hornblende, Na-K feldspar, biotite, chlorite, and pyrite |                         |    |    |    |    |                |               |      |          |      |           |         |                             | From 857.7' to 858.4':<br>Rubble         |                        | C                          | 100            | 46    | PL(D) = 157.70<br>PL(A) = 18.74    |
| 860                 |                                                                                                               |                         |    |    |    |    |                |               |      |          |      |           |         |                             | -860.45': 42° Planar<br>smooth           |                        | C                          | 100            | 54    | UCS = 2,424.25<br><br>SLK = Type I |
| 870                 |                                                                                                               |                         |    |    |    |    |                |               |      |          |      |           |         |                             |                                          |                        | C                          | 100            | 54    | PL(A) = 177.29<br>PL(D) = 180.88   |

BORING TYPE: HQ3

DRILLER: Crux

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 2280

WATER OBSERVATIONS: 1006 ft.

CASING: HW to 20 ft.

REMARKS: \_\_\_\_\_

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                         |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|-----------------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type <u>  </u> ) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)              |
| WL                                | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)              |

(Continued Next Page)

**CLIENT:** Lane Power & Energy Solutions

**SURFACE ELEVATION (ft):** 2548.8

**PROJECT No:** 951-20

**PROJECT:** Hydrostor Zevsar

**NORTHING:** 2153392.317

**DATE:** 8/10/2024 - 10/13/2024

**PROJECT LOCATION:** Rosamod, CA

**EASTING:** 6514888.703

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata                       | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft)                | Discontinuities                                                                         |                        | Sampling & In Situ Testing |                |                                                                         |                            |
|---------------------|---------------------------------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|--------------------------------------------|-----------------------------------------------------------------------------------------|------------------------|----------------------------|----------------|-------------------------------------------------------------------------|----------------------------|
|                     |                                                   | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                                            | B - Bedding<br>S - Shear                                                                | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD %                                                                   | Test Results<br>& Comments |
|                     |                                                   |                         |    |    |    |    |                |               |      |          |      |           |         |       |                                            |                                                                                         |                        |                            |                |                                                                         |                            |
| 1670'<br>880        | QTZ MONZONITE, light gray to white,<br>phaneritic |                         |    |    |    |    |                |               |      |          |      |           |         |       |                                            | From 877' to 877.7':<br>Rubble                                                          |                        |                            |                | PL(D) = 255.75<br><br>ITS = 596.40<br><br><br>PL(A) = 133.77            |                            |
|                     |                                                   |                         |    |    |    |    |                |               |      |          |      |           |         |       |                                            | From 882.9' to 883.5':<br>(1) 47° Undulating<br>smooth, (1) 69° Planar<br>smooth, wedge | C                      | 100                        | 68             |                                                                         |                            |
| 1665'<br>885        |                                                   |                         |    |    |    |    |                |               |      |          |      |           |         |       |                                            | 884': 39° Planar smooth                                                                 |                        |                            |                |                                                                         |                            |
| 887                 |                                                   |                         |    |    |    |    |                |               |      |          |      |           |         |       |                                            | 886': 27° Planar smooth<br>886.5': 90° S. fracture                                      |                        |                            |                |                                                                         |                            |
| 1660'<br>890        |                                                   |                         |    |    |    |    |                |               |      |          |      |           |         |       |                                            | From 887' to 897':<br>Multiple fractures<br>throughout, rubble                          |                        |                            |                |                                                                         |                            |
|                     |                                                   |                         |    |    |    |    |                |               |      |          |      |           |         |       | From 888.2' to 888.7': 7°<br>Planar smooth |                                                                                         |                        |                            |                | PL(D) = 394.47<br>PL(A) = 39.48<br><br>PL(D) = 107.42<br>UCS = 1,258.76 |                            |
| 1655'<br>895        |                                                   |                         |    |    |    |    |                |               |      |          |      |           |         |       |                                            |                                                                                         | C                      | 100                        | 76             |                                                                         |                            |
|                     |                                                   |                         |    |    |    |    |                |               |      |          |      |           |         |       |                                            |                                                                                         |                        |                            |                |                                                                         |                            |
| 1650'<br>900        |                                                   |                         |    |    |    |    |                |               |      |          |      |           |         |       |                                            |                                                                                         |                        |                            |                |                                                                         |                            |
|                     |                                                   |                         |    |    |    |    |                |               |      |          |      |           |         |       |                                            |                                                                                         |                        |                            |                |                                                                         |                            |
| 1645'<br>905        |                                                   |                         |    |    |    |    |                |               |      |          |      |           |         |       |                                            |                                                                                         |                        |                            |                |                                                                         |                            |
|                     |                                                   |                         |    |    |    |    |                |               |      |          |      |           |         |       |                                            |                                                                                         |                        |                            |                |                                                                         |                            |
| 1640'               |                                                   |                         |    |    |    |    |                |               |      |          |      |           |         |       |                                            | From 907' to 912':<br>Multiple fractures<br>throughout, rubble                          |                        |                            |                |                                                                         |                            |

**BORING TYPE:** HQ3

**DRILLER:** Crux

**LOGGED BY:** Chris Messenger

HOLE DEPTH (ft): 2280

WATER OBSERVATIONS: 1006 ft.

**CASING:** HW to 20 ft.

REMARKS:

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |
|-----------------------------------|---------------|-------|--------------------------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               |
| W                                 | Water level   | PL(D) | Point load diametral test Is(50) (psi)           |
|                                   |               | SLK   | Slake durability test (Type _____)               |
|                                   |               | TRI   | Triaxial stress test (psi)                       |
|                                   |               | UCS   | Uniaxial stress test (psi)                       |

(Continued Next Page)



CLIENT: Lane Power & Energy Solutions  
PROJECT: Hydrostor Zevsar  
PROJECT LOCATION: Rosamod, CA

SURFACE ELEVATION (ft): 2548.8  
NORTHING: 2153392.317  
EASTING: 6514888.703

PROJECT No: 951-20  
DATE: 8/10/2024 - 10/13/2024  
DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata                                                                                                         | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities          |                       | Sampling & In Situ Testing |                |                                                                  |                            |
|---------------------|-------------------------------------------------------------------------------------------------------------------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|--------------------------|-----------------------|----------------------------|----------------|------------------------------------------------------------------|----------------------------|
|                     |                                                                                                                                     | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear | J - Joint<br>F- Fault | Type                       | Core<br>Rec. % | RQD %                                                            | Test Results<br>& Comments |
|                     |                                                                                                                                     |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |                                                                  |                            |
| 912                 | QTZ MONZONITE, light gray to white, phaneritic, with feldspar, biotite, and hornblende, trace amounts of mica, pyrite, and chlorite |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            | PL(A) = 220.27 |                                                                  |                            |
| 915                 |                                                                                                                                     |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            | ITS = 190.14   |                                                                  |                            |
|                     |                                                                                                                                     |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |                                                                  |                            |
| 920                 |                                                                                                                                     |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |                                                                  |                            |
|                     |                                                                                                                                     |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                | UCS = 6,127.31<br>PL(D) = 18.89<br>SLK = Type I<br>PL(A) = 57.86 |                            |
| 925                 |                                                                                                                                     |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |                                                                  |                            |
|                     |                                                                                                                                     |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |                                                                  |                            |
| 930                 |                                                                                                                                     |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |                                                                  |                            |
|                     |                                                                                                                                     |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |                                                                  |                            |
| 935                 |                                                                                                                                     |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |                                                                  |                            |
| 938                 | QTZ MONZONITE, light gray to white, phaneritic, with Na-K feldspar and hornblende                                                   |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            | ITS = 603.22   |                                                                  |                            |
| 940                 |                                                                                                                                     |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            | PL(D) = 130.85 |                                                                  |                            |
|                     |                                                                                                                                     |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |                                                                  |                            |
| 942.9'              |                                                                                                                                     |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |                                                                  |                            |
| 943.1'              |                                                                                                                                     |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |                                                                  |                            |

BORING TYPE: HQ3  
HOLE DEPTH (ft): 2280  
REMARKS: \_\_\_\_\_

DRILLER: Crux  
WATER OBSERVATIONS: 1006 ft.

LOGGED BY: Chris Messenger  
CASING: HW to 20 ft.

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                  |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|----------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type ___) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)       |
| W                                 | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)       |

(Continued Next Page)



CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2548.8

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2153392.317

DATE: 8/10/2024 - 10/13/2024

PROJECT LOCATION: Rosamod, CA

EASTING: 6514888.703

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata                                    | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities                                                            |                        | Sampling & In Situ Testing |                |       |                                                      |
|---------------------|----------------------------------------------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|----------------------------------------------------------------------------|------------------------|----------------------------|----------------|-------|------------------------------------------------------|
|                     |                                                                | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear                                                   | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments                           |
| 1600                |                                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 943.8' to 944.3':<br>81° Undulating rough                             |                        |                            |                |       | PL(A) = 152.93                                       |
| 950                 |                                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 944.9' to 947': 90°<br>- 62° S. Undulating<br>rough                   |                        |                            |                |       |                                                      |
|                     |                                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 950.3': 41° Planar<br>smooth                                               |                        |                            |                |       |                                                      |
| 1595                |                                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 952': 17° Planar rough                                                     | C                      | 100                        | 52             |       | PL(A) = 205.94<br>UCS =<br>11,379.32<br>ITS = 822.64 |
| 955                 |                                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 957' to 957.6': (1)<br>79° Undulating rough,<br>(1) 11° Planar smooth |                        |                            |                |       |                                                      |
|                     |                                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 958': 90° Healed fracture                                                  |                        |                            |                |       |                                                      |
| 1590                |                                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 960' to 961':<br>Rubble                                               |                        |                            |                |       | SLK = Type II<br>PL(D) = 34.64                       |
| 960                 |                                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 962' to 963': 90° S.<br>Rough                                         | C                      | 100                        | 50             |       |                                                      |
| 1585                |                                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 966' to 976':<br>Decomposed, rubble                                   |                        |                            |                |       |                                                      |
| 965                 |                                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                                            |                        |                            |                |       | C                                                    |
| 966                 | QTZ MONZONITE, light gray to green,<br>phaneritic to aphanitic |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                                            |                        |                            |                |       |                                                      |
| 1580                |                                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                                            |                        |                            |                |       |                                                      |
| 970                 |                                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                                            |                        |                            |                |       | C                                                    |
| 1575                |                                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                                            |                        |                            |                |       |                                                      |
| 975                 |                                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                                            |                        |                            |                |       |                                                      |
| 976                 | QTZ MONZONITE, light gray to dark<br>gray, phaneritic          |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 976' to 980': (6)<br>40° - 42° Planar smooth                          |                        |                            |                |       | C                                                    |
| 1570                |                                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                                            |                        |                            |                |       |                                                      |

BORING TYPE: HQ3

DRILLER: Crux

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 2280

WATER OBSERVATIONS: 1006 ft.

CASING: HW to 20 ft.

REMARKS: \_\_\_\_\_

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                    |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|------------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type _____) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)         |
| WL                                | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)         |

(Continued Next Page)





CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2548.8

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2153392.317

DATE: 8/10/2024 - 10/13/2024

PROJECT LOCATION: Rosamod, CA

EASTING: 6514888.703

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities          |                        | Sampling & In Situ Testing |                |       |                                                        |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|--------------------------|------------------------|----------------------------|----------------|-------|--------------------------------------------------------|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments                             |
| 1565<br>985         |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 37    | UCS = 4,232.72<br><br>PL(A) = 72.19                    |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                                        |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                                        |
| 1560<br>990         |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       | ITS = 1,361.85<br><br>PL(D) = 213.85<br>SLK = Type III |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                                        |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                                        |
| 1555<br>995         |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 31    |                                                        |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                                        |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                                        |
| 1550<br>1000        |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                                        |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                                        |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                                        |
| 1545<br>1005        |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 39    |                                                        |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                                        |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                                        |
| 1540<br>1010        |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                                        |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                                        |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                                        |
| 1535                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 44    |                                                        |

BORING TYPE: HQ3

DRILLER: Crux

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 2280

WATER OBSERVATIONS: 1006 ft.

CASING: HW to 20 ft.

REMARKS: \_\_\_\_\_

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                    |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|------------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type _____) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)         |
| W                                 | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)         |

(Continued Next Page)



CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2548.8

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2153392.317

DATE: 8/10/2024 - 10/13/2024

PROJECT LOCATION: Rosamod, CA

EASTING: 6514888.703

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata                                                                                                                   | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities                               |                        | Sampling & In Situ Testing |                |       |                                                                    |
|---------------------|-----------------------------------------------------------------------------------------------------------------------------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|-----------------------------------------------|------------------------|----------------------------|----------------|-------|--------------------------------------------------------------------|
|                     |                                                                                                                                               | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear                      | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments                                         |
| 1530<br>1020        | QTZ MONZONITE, light gray to white, phaneritic, with Na-K feldspar, biotite, and hornblende, trace amounts of chlorite, pyrite, and muscovite |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | -1016': 90° S. Planar rough                   |                        |                            |                |       | PL(D) = 20.55                                                      |
|                     |                                                                                                                                               |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | -1018': 80° - 90° Undulating smooth           |                        |                            |                |       | ITS = 106.76                                                       |
| 1525<br>1025        |                                                                                                                                               |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | -1022': 61° Undulating rough                  |                        | C                          | 100            | 41    | UCS = 10,190.76                                                    |
| 1026                |                                                                                                                                               |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | -From 1025' to 1026': 90° S. Planar rough     |                        |                            |                |       | PL(D) = 78.24                                                      |
|                     |                                                                                                                                               |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | -From 1026' to 1028': Rubble                  |                        |                            |                |       |                                                                    |
| 1520<br>1030        |                                                                                                                                               |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | -1028.48': 77° Undulating rough               |                        |                            |                |       | PL(A) = 489.54                                                     |
|                     |                                                                                                                                               |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | -1029': 74° Planar smooth                     |                        |                            |                |       |                                                                    |
|                     |                                                                                                                                               |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | -1029.85': 80° - 90° Undulating rough, healed |                        | C                          | 100            | 47    |                                                                    |
| 1515<br>1035        |                                                                                                                                               |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | -From 1031' to 1033.75': 80° Planar smooth    |                        |                            |                |       |                                                                    |
|                     |                                                                                                                                               |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | -1035.1': 51° Planar smooth                   |                        |                            |                |       | UCS = 6,095.43<br>ITS = 875.39<br>PL(A) = 416.46<br>PL(A) = 487.81 |
| 1510<br>1040        |                                                                                                                                               |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | -1038.75': 81° Undulating smooth              |                        |                            |                |       |                                                                    |
|                     |                                                                                                                                               |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | -1040': 61° Planar smooth                     |                        |                            |                |       |                                                                    |
|                     |                                                                                                                                               |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | -1041.9': 61° Undulating rough                |                        | C                          | 100            | 82    |                                                                    |
| 1505<br>1045        |                                                                                                                                               |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | -1043': 7° Planar                             |                        |                            |                |       |                                                                    |
|                     |                                                                                                                                               |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | -1045.7': 12° Planar smooth                   |                        |                            |                |       |                                                                    |
|                     |                                                                                                                                               |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | -From 1046' to 1047': 80° Undulating smooth   |                        |                            |                |       |                                                                    |
| 1500                |                                                                                                                                               |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | -1047.15': (2) 62° J. Planar smooth           |                        |                            |                |       |                                                                    |

BORING TYPE: HQ3

DRILLER: Crux

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 2280

WATER OBSERVATIONS: 1006 ft.

CASING: HW to 20 ft.

REMARKS:

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                         |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|-----------------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type <u>  </u> ) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)              |
| L                                 | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)              |

(Continued Next Page)



CLIENT: Lane Power & Energy Solutions  
PROJECT: Hydrostor Zevsar  
PROJECT LOCATION: Rosamod, CA

SURFACE ELEVATION (ft): 2548.8  
NORTHING: 2153392.317  
EASTING: 6514888.703

PROJECT No: 951-20  
DATE: 8/10/2024 - 10/13/2024  
DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities                                                |                        | Sampling & In Situ Testing |                |       |                                 |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|----------------------------------------------------------------|------------------------|----------------------------|----------------|-------|---------------------------------|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear                                       | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments      |
| 1495                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1050': 47° - 90° Stepped rough                                 |                        |                            |                |       | PL(D) = 204.85                  |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1050.1': 79° Stepped rough                                     |                        |                            |                |       |                                 |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1052': 42° Planar smooth                                       |                        | C                          | 100            | 80    |                                 |
| 1055                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1053.6' to 1056': 90° Healed fracture                     |                        |                            |                |       |                                 |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1054' to 1055': 45° - 48° Undulating rough                |                        |                            |                |       |                                 |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1056' to 1057': (2) 7° - 10° Planar smooth                |                        |                            |                |       | PL(D) = 200.47                  |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1057' to 1058': Healed fracture                           |                        |                            |                |       |                                 |
| 1060                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                                |                        |                            |                |       |                                 |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1061.3': 59° Undulating smooth                                 |                        | C                          | 100            | 65    |                                 |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1063': 52° Planar rough                                        |                        |                            |                |       |                                 |
| 1065                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1064.65': 32° Planar smooth                                    |                        |                            |                |       | PL(A) = 86.33<br>SLK = Type I   |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1066' to 1069': (8) 40° - 50° J. Planar smooth            |                        |                            |                |       |                                 |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                                |                        |                            |                |       |                                 |
| 1070                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                                |                        |                            |                |       |                                 |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                                |                        |                            |                |       |                                 |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1073.8' to 1074': 29° Planar smooth and 42° Planar smooth |                        | C                          | 100            | 53    | UCS = 8,715.97<br>PL(A) = 37.70 |
| 1075                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1075.75': 53° Planar smooth/slickenside                        |                        |                            |                |       |                                 |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1078.5': 71° Undulating smooth                                 |                        |                            |                |       |                                 |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                                |                        |                            |                |       |                                 |
| 1080                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1082.45': 29° Planar rough and 60° Planar smooth               |                        | C                          | 100            | 47    |                                 |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1083.6': 40° Planar smooth                                     |                        |                            |                |       | PL(D) = 545.79                  |

BORING TYPE: HQ3  
HOLE DEPTH (ft): 2280  
REMARKS: \_\_\_\_\_

DRILLER: Crux  
WATER OBSERVATIONS: 1006 ft.

LOGGED BY: Chris Messenger  
CASING: HW to 20 ft.

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                   |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|-----------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type ____) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)        |
| W                                 | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)        |

(Continued Next Page)



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EASTING: 6514888.703

PROJECT No: 951-20  
DATE: 8/10/2024 - 10/13/2024  
DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities          |                        | Sampling & In Situ Testing |                |       |                                |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|--------------------------|------------------------|----------------------------|----------------|-------|--------------------------------|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments     |
| 1460                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       | ITS = 921.15                   |
| 1090                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       | PL(D) = 378.20                 |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 60    |                                |
| 1455                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       | PL(A) = 60.04                  |
| 1095                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                |
| 1450                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                |
| 1100                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 48    |                                |
| 1445                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       | PL(A) = 959.79                 |
| 1105                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       | PL(D) = 785.10<br>SLK = Type I |
| 1440                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                |
| 1110                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       | UCS =<br>11,591.41             |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                |
| 1435                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 66    |                                |
| 1115                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       | ITS = 976.85                   |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                |
| 1430                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                                |

BORING TYPE: HQ3  
HOLE DEPTH (ft): 2280  
REMARKS: \_\_\_\_\_

DRILLER: Crux  
WATER OBSERVATIONS: 1006 ft.

LOGGED BY: Chris Messenger  
CASING: HW to 20 ft.

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                    |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|------------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type _____) |
| W                                 | Water seep    | PL(A) | Point load axial test $I_s(50)$ (psi)            | TRI | Triaxial stress test (psi)         |
| L                                 | Water level   | PL(D) | Point load diametral test $I_s(50)$ (psi)        | UCS | Uniaxial stress test (psi)         |

(Continued Next Page)



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DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities                                               |                        | Sampling & In Situ Testing |                |       |                                                                                                                                           |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|---------------------------------------------------------------|------------------------|----------------------------|----------------|-------|-------------------------------------------------------------------------------------------------------------------------------------------|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear                                      | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments                                                                                                                |
| 1125                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1119.7': 67° Planar<br>smooth                                 |                        |                            |                |       | PL(A) = 966.47                                                                                                                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1122': 38° Planar rough                                       | C                      | 100                        | 76             |       |                                                                                                                                           |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1124.2': 17° Planar<br>rough                                  |                        |                            |                |       |                                                                                                                                           |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1127': 47° Healed<br>smooth                                   |                        |                            |                |       |                                                                                                                                           |
| 1130                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1129': 31° - 47° Planar<br>smooth                             |                        |                            |                |       |                                                                                                                                           |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1132.78': 38° Planar<br>rough                                 | C                      | 100                        | 56             |       | PL(A) = 391.06<br>SLK = Type I<br><br>UCS = 2,336.26<br>PL(D) =<br>1,136.19<br><br>PL(A) = 730.97<br>ITS = 1,074.04<br><br>PL(D) = 481.50 |
| 1135                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1133.8' to 1136':<br>(4) 30° - 42° Planar<br>smooth      |                        |                            |                |       |                                                                                                                                           |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1136' to 1146':<br>Radial healed fractures<br>throughout |                        |                            |                |       |                                                                                                                                           |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1136.5' to 1137':<br>90° Planar smooth                   |                        |                            |                |       |                                                                                                                                           |
| 1140                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1137' to 1138': 90°<br>Stepped smooth                    |                        |                            |                |       |                                                                                                                                           |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1138' to 1139.2':<br>84° Planar smooth                   |                        |                            |                |       | PL(A) = 391.06<br>SLK = Type I<br><br>UCS = 2,336.26<br>PL(D) =<br>1,136.19<br><br>PL(A) = 730.97<br>ITS = 1,074.04<br><br>PL(D) = 481.50 |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1142': 62° Planar<br>smooth                                   | C                      | 100                        | 72             |       |                                                                                                                                           |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1143.1': 38° Planar<br>rough                                  |                        |                            |                |       |                                                                                                                                           |
| 1145                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1144.78': 33° Planar<br>smooth                                |                        |                            |                |       |                                                                                                                                           |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1147.3': 32° Undulating<br>smooth                             |                        |                            |                |       |                                                                                                                                           |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1149.65' to 1151':<br>(3) 20° - 45° Planar<br>smooth     |                        |                            |                |       | PL(D) = 481.50                                                                                                                            |
| 1150                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1151' to 1154': 80°<br>- 90° Healed fracture             |                        |                            |                |       |                                                                                                                                           |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1153': 42° Planar<br>smooth                                   | C                      | 100                        | 36             |       |                                                                                                                                           |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1154.1': 29° Planar<br>rough                                  |                        |                            |                |       |                                                                                                                                           |

BORING TYPE: HQ3  
HOLE DEPTH (ft): 2280  
REMARKS: \_\_\_\_\_

DRILLER: Crux  
WATER OBSERVATIONS: 1006 ft.

LOGGED BY: Chris Messenger  
CASING: HW to 20 ft.

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                    |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|------------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type _____) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)         |
| WL                                | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)         |

**CLIENT:** Lane Power & Energy Solutions

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**PROJECT No:** 951-20

**PROJECT:** Hydrostor Zevsar

**NORTHING:** 2153392.317

**DATE:** 8/10/2024 - 10/13/2024

**PROJECT LOCATION:** Rosamod, CA

**EASTING:** 6514888.703

DIP/AZIMUTH: -90 /

[illegible]

**BORING TYPE:** HQ3

**DRILLER:** Crux

**LOGGED BY:** Chris Messenger

HOLE DEPTH (ft): 2280

**WATER OBSERVATIONS:** 1006 ft.

**CASING:** HW to 20 ft.

REMARKS:

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |
|-----------------------------------|---------------|-------|--------------------------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               |
| W                                 | Water level   | PL(D) | Point load diametral test Is(50) (psi)           |
|                                   |               | SLK   | Slake durability test (Type _____)               |
|                                   |               | TRI   | Triaxial stress test (psi)                       |
|                                   |               | UCS   | Uniaxial stress test (psi)                       |

(Continued Next Page)



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| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata                                                                                                                      | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) |      | Discontinuities                             |                                                             | Sampling & In Situ Testing |                          |                        |                |                |       |                            |
|---------------------|--------------------------------------------------------------------------------------------------------------------------------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|------|---------------------------------------------|-------------------------------------------------------------|----------------------------|--------------------------|------------------------|----------------|----------------|-------|----------------------------|
|                     |                                                                                                                                                  | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       | 0.05                        | 0.25 | 0.50                                        | 2.50                                                        | 5.00                       | B - Bedding<br>S - Shear | J - Joint<br>F - Fault | Type           | Core<br>Rec. % | RQD % | Test Results<br>& Comments |
|                     | QTZ MONZONITE, light gray to white, phaneritic, with Na-Ca-K feldspar, biotite, and hornblende, trace amounts of pyrite, chlorite, and muscovite |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |                                             | From 1190' to 1191': (3) 30° - 35° Planar smooth            | C                          | 100                      | 19                     | PL(D) = 715.82 |                |       |                            |
|                     |                                                                                                                                                  |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |                                             | From 1191' to 1195.3': 80° - 90° Undulating rough           |                            |                          |                        |                |                |       | PL(D) = 188.75             |
| 1195                |                                                                                                                                                  |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |                                             | From 1196.5' to 1199': 90° Healed fracture                  |                            |                          |                        |                |                |       | PL(D) = 422.16             |
|                     |                                                                                                                                                  |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |                                             | From 1197.8' to 1198': (2) 41° J. Rough                     | C                          | 100                      | 24                     |                |                |       |                            |
|                     |                                                                                                                                                  |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |                                             | From 1199.3' to 1201': Rubble                               |                            |                          |                        |                |                |       |                            |
| 1200                |                                                                                                                                                  |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |                                             | From 1201.55' to 1202.4': 79° - 84° Planar rough            |                            |                          |                        |                |                |       |                            |
|                     |                                                                                                                                                  |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |                                             | From 1203' to 1204.4': (4) 90° Stepped and Undulating rough | C                          | 100                      | 62                     | PL(D) = 43.73  |                |       |                            |
|                     |                                                                                                                                                  |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |                                             | From 1206' to 1208': 80° - 90° Undulating rough             |                            |                          |                        |                |                |       |                            |
| 1205                |                                                                                                                                                  |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |                                             | From 1209.3' to 1211.8': Rubble                             |                            |                          |                        |                |                |       |                            |
|                     |                                                                                                                                                  |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |                                             | 1213': 27° - 90° Stepped smooth                             | C                          | 100                      | 64                     | PL(A) = 93.88  |                |       |                            |
|                     |                                                                                                                                                  |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      | 1214.5': 67° Undulating rough               |                                                             |                            |                          |                        |                |                |       |                            |
| 1210                |                                                                                                                                                  |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      | 1215': 48° Undulating smooth                |                                                             |                            |                          |                        |                |                |       |                            |
|                     |                                                                                                                                                  |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      | From 1216.7' to 1217.2': 71° Planar rough   | C                                                           | 100                        | 64                       |                        |                |                |       |                            |
|                     |                                                                                                                                                  |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      | 1219': 41° Planar smooth                    |                                                             |                            |                          |                        |                |                |       |                            |
| 1215                |                                                                                                                                                  |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      | From 1219.6' to 1220.1': Undulating smooth  |                                                             |                            |                          |                        |                |                |       |                            |
|                     |                                                                                                                                                  |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      | 1220.2': 38° Planar smooth                  | C                                                           | 100                        | 64                       |                        |                |                |       |                            |
|                     |                                                                                                                                                  |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      | 1220.5': 45° Undulating smooth              |                                                             |                            |                          |                        |                |                |       |                            |
| 1220                |                                                                                                                                                  |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      | From 1221.45' to 1222.3': (3) 45° J. Planar |                                                             |                            |                          |                        |                |                |       |                            |
|                     |                                                                                                                                                  |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |                                             |                                                             |                            |                          |                        |                |                |       |                            |
| 1225                |                                                                                                                                                  |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |      |                                             |                                                             |                            |                          |                        |                |                |       |                            |

BORING TYPE: HQ3  
HOLE DEPTH (ft): 2280  
REMARKS: \_\_\_\_\_

DRILLER: Crux  
WATER OBSERVATIONS: 1006 ft.

LOGGED BY: Chris Messenger  
CASING: HW to 20 ft.

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                   |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|-----------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type ____) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)        |
| L                                 | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)        |





CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2548.8

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2153392.317

DATE: 8/10/2024 - 10/13/2024

PROJECT LOCATION: Rosamod, CA

EASTING: 6514888.703

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata        | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities                            |                        | Sampling & In Situ Testing |                |       |                            |
|---------------------|------------------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|--------------------------------------------|------------------------|----------------------------|----------------|-------|----------------------------|
|                     |                                    | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear                   | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments |
| 1230                |                                    |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | smooth                                     |                        |                            |                |       | UCS =<br>14,964.07         |
| 1235                |                                    |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1221.9°: 80° - 90° S.<br>Undulating rough  |                        |                            |                |       |                            |
| 1236                | QTZ MONZONITE, light gray to green |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1227°: 47° Undulating<br>smooth            |                        |                            |                |       | SLK = Type I               |
| 1240                |                                    |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1236' to 1246':<br>Decomposed, rubble |                        | C                          | 100            | 66    | PL(A) = 143.39             |
| 1245                |                                    |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1246' to 1256':<br>Decomposed, rubble |                        | C                          | 100            | 53    | ITS = 678.83               |
| 1250                |                                    |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1256' to 1266':<br>Decomposed, rubble |                        | C                          | 100            | 46    | UCS = 2,719.81             |
| 1255                |                                    |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                            |                        |                            |                |       |                            |
| 1290                |                                    |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                            |                        |                            |                |       |                            |

BORING TYPE: HQ3

DRILLER: Crux

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 2280

WATER OBSERVATIONS: 1006 ft.

CASING: HW to 20 ft.

REMARKS: \_\_\_\_\_

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                  |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|----------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type ___) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)       |
| WL                                | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)       |

(Continued Next Page)





CLIENT: Lane Power & Energy Solutions  
PROJECT: Hydrostor Zevsar  
PROJECT LOCATION: Rosamod, CA

SURFACE ELEVATION (ft): 2548.8  
NORTHING: 2153392.317  
EASTING: 6514888.703

PROJECT No: 951-20  
DATE: 8/10/2024 - 10/13/2024  
DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata              | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities                                          |                        | Sampling & In Situ Testing |                |       |                                  |
|---------------------|------------------------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|----------------------------------------------------------|------------------------|----------------------------|----------------|-------|----------------------------------|
|                     |                                          | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear                                 | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments       |
| 1265                | QTZ MONZONITE, light gray,<br>phaneritic |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                          |                        | C                          | 100            | 34    | ITS = 247.14                     |
| 1270                |                                          |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1266' to 1276':<br>Decomposed, rubble               |                        |                            |                |       | PL(A) = 264.48                   |
| 1275                |                                          |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                          |                        | C                          | 100            | 43    | PL(D) = 26.06                    |
| 1280                |                                          |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1276' to 1286':<br>Multiple fractures<br>throughout |                        |                            |                |       |                                  |
| 1285                |                                          |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1286' to 1296':<br>Multiple fractures<br>throughout |                        | C                          | 100            | 45    | UCS = 3,062.45<br>PL(D) = 354.41 |
| 1290                |                                          |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                          |                        | C                          | 100            | 58    | PL(A) = 75.28<br>SLK = Type II   |

BORING TYPE: HQ3  
HOLE DEPTH (ft): 2280  
REMARKS: \_\_\_\_\_

DRILLER: Crux  
WATER OBSERVATIONS: 1006 ft.

LOGGED BY: Chris Messenger  
CASING: HW to 20 ft.

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                         |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|-----------------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type <u>  </u> ) |
| W                                 | Water seep    | PL(A) | Point load axial test $I_s(50)$ (psi)            | TRI | Triaxial stress test (psi)              |
| WL                                | Water level   | PL(D) | Point load diametral test $I_s(50)$ (psi)        | UCS | Uniaxial stress test (psi)              |



CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2548.8

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2153392.317

DATE: 8/10/2024 - 10/13/2024

PROJECT LOCATION: Rosamod, CA

EASTING: 6514888.703

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata                                                                                                   | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities          |                        | Sampling & In Situ Testing |                |       |                            |
|---------------------|-------------------------------------------------------------------------------------------------------------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|--------------------------|------------------------|----------------------------|----------------|-------|----------------------------|
|                     |                                                                                                                               | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments |
| 1250'               |                                                                                                                               |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1300                |                                                                                                                               |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1245'               |                                                                                                                               |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1305                |                                                                                                                               |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1240'               |                                                                                                                               |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1310                |                                                                                                                               |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1311                | QTZ MONZONITE, light gray to white, phaneritic, with feldspar, hornblende, and biotite, trace amounts of muscovite and pyrite |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1235'               |                                                                                                                               |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1315                |                                                                                                                               |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1230'               |                                                                                                                               |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1320                |                                                                                                                               |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1225'               |                                                                                                                               |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1325                |                                                                                                                               |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 1220'               |                                                                                                                               |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |

BORING TYPE: HQ3

DRILLER: Crux

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 2280

WATER OBSERVATIONS: 1006 ft.

CASING: HW to 20 ft.

REMARKS: \_\_\_\_\_

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                  |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|----------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type ___) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)       |
| L                                 | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)       |

**CLIENT:** Lane Power & Energy Solutions

**SURFACE ELEVATION (ft):** 2548.8

**PROJECT No:** 951-20

**PROJECT:** Hydrostor Zevsar

**NORTHING:** 2153392.317

**DATE:** 8/10/2024 - 10/13/2024

**PROJECT LOCATION:** Rosamod, CA

**EASTING:** 6514888.703

DIP/AZIMUTH: -90 /

[illegible]

**BORING TYPE:** HQ3

**DRILLER:** Crux

**LOGGED BY:** Chris Messenger

**HOLE DEPTH (ft):** 2280

**WATER OBSERVATIONS:** 1006 ft.

**CASING:** HW to 20 ft.

REMARKS:

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |
|-----------------------------------|---------------|-------|--------------------------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               |
| W                                 | Water level   | PL(D) | Point load diametral test Is(50) (psi)           |
|                                   |               | SLK   | Slake durability test (Type _____)               |
|                                   |               | TRI   | Triaxial stress test (psi)                       |
|                                   |               | UCS   | Uniaxial stress test (psi)                       |

(Continued Next Page)



CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2548.8

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2153392.317

DATE: 8/10/2024 - 10/13/2024

PROJECT LOCATION: Rosamod, CA

EASTING: 6514888.703

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities                                         |                       | Sampling & In Situ Testing |                |       |                            |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|---------------------------------------------------------|-----------------------|----------------------------|----------------|-------|----------------------------|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear                                | J - Joint<br>F- Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments |
| 1180                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 40° Planar smooth                                       |                       |                            |                |       | PL(D) =<br>1,044.52        |
| 1370                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1366' to 1368': (5)<br>38° - 45° Planar rough      |                       |                            |                |       | PL(A) =<br>1,033.12        |
| 1375                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1368' to 1369': 90°<br>Undulating rough,<br>healed |                       |                            |                |       |                            |
| 1380                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                         |                       | C                          | 100            | 14    |                            |
| 1385                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                         |                       |                            |                |       | UCS =<br>11,881.09         |
| 1389                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                         |                       |                            |                |       | PL(A) = 762.02             |
| 1390                | PEGMATITE                   |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                         |                       | C                          | 100            | 18    |                            |
| 1394                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1386.9' to 1394':<br>Rubble                        |                       |                            |                |       | ITS = 512.34               |
| 1395                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                         |                       |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                         |                       | C                          | 100            | 58    |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1394': 70° Undulating<br>smooth                         |                       |                            |                |       | PL(A) = 262.67             |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1394.8': 68° Planar<br>rough, 47° Planar<br>smooth      |                       |                            |                |       | PL(D) = 397.01             |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1397': 90° Planar rough                                 |                       |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1399': 45° Planar<br>smooth                             |                       |                            |                |       |                            |

BORING TYPE: HQ3

DRILLER: Crux

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 2280

WATER OBSERVATIONS: 1006 ft.

CASING: HW to 20 ft.

REMARKS: \_\_\_\_\_

| <b><u>SAMPLING &amp; IN SITU TESTING LEGEND</u></b> |               |       |                                                  |     |                                    |
|-----------------------------------------------------|---------------|-------|--------------------------------------------------|-----|------------------------------------|
| C                                                   | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type _____) |
| W                                                   | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)         |
| L                                                   | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)         |

(Continued Next Page)



CLIENT: Lane Power & Energy Solutions  
PROJECT: Hydrostor Zevsar  
PROJECT LOCATION: Rosamod, CA

SURFACE ELEVATION (ft): 2548.8  
NORTHING: 2153392.317  
EASTING: 6514888.703

PROJECT No: 951-20  
DATE: 8/10/2024 - 10/13/2024  
DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata                                                                                                  | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities<br><br>B - Bedding<br>S - Shear      J - Joint<br>F - Fault                                                                                                                                                | Sampling & In Situ Testing |                |       |                                                                   |
|---------------------|------------------------------------------------------------------------------------------------------------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|----------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|----------------------------|----------------|-------|-------------------------------------------------------------------|
|                     |                                                                                                                              | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             |                                                                                                                                                                                                                            | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments                                        |
| 1405                |                                                                                                                              |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1400.15': 47° Planar smooth<br>1401.3': 45° Fracture<br>From 1402' to 1402.8':<br>45° Planar rough<br>1403.5': 16° Undulating smooth<br><br>From 1407.7' to 1409':<br>90° Planar smooth                                    | C                          | 100            | 48    | ITS = 896.35<br><br>UCS =<br>18,143.59<br><br>PL(A) =<br>1,034.32 |
| 1410                |                                                                                                                              |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1410.2': 38° Planar smooth<br>1411.8': 7° Planar smooth<br>1411.9': 81° Planar smooth<br>1413': 11° Planar smooth<br>1414': 38° Planar smooth<br>1416.1': 61° Fracture<br><br>From 1419' to 1421': 90°<br>Undulating rough | C                          | 100            | 62    | PL(D) = 178.61                                                    |
| 1415                |                                                                                                                              |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                                                                                                                                                                                            |                            |                |       | PL(A) = 440.36<br>SLK = Type I                                    |
| 1420                |                                                                                                                              |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                                                                                                                                                                                            | C                          | 100            | 72    |                                                                   |
| 1425                |                                                                                                                              |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                                                                                                                                                                                            |                            |                |       | PL(D) = 29.74                                                     |
| 1430                |                                                                                                                              |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                                                                                                                                                                                            |                            |                |       |                                                                   |
| 1431                | QTZ MONZONITE, light gray to white, phaneritic, with feldspar, biotite, and hornblende, trace amounts of chlorite and pyrite |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1429.5': (2) 45° Planar smooth<br>1430': 47° Planar smooth<br>1432': 45° Planar rough<br>1432.6': (2) 80° - 90° J. Undulating rough                                                                                        | C                          | 100            | 68    |                                                                   |

BORING TYPE: HQ3  
HOLE DEPTH (ft): 2280  
REMARKS: \_\_\_\_\_

DRILLER: Crux  
WATER OBSERVATIONS: 1006 ft.

LOGGED BY: Chris Messenger  
CASING: HW to 20 ft.

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                   |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|-----------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type ____) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)        |
| WL                                | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)        |



CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2548.8

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2153392.317

DATE: 8/10/2024 - 10/13/2024

PROJECT LOCATION: Rosamod, CA

EASTING: 6514888.703

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities                                     |                        | Sampling & In Situ Testing |                |       |                                                      |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|-----------------------------------------------------|------------------------|----------------------------|----------------|-------|------------------------------------------------------|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear                            | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments                           |
| 1110                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1435': 16° Planar rough                             |                        |                            |                |       | PL(A) = 834.92<br>PL(D) = 761.83                     |
| 1440                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1436.8': 45° Planar rough                           |                        |                            |                |       |                                                      |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1439' to 1443': (4)<br>45° Planar smooth       |                        | C                          | 100            | 83    | TRI = 36,190.92<br>ITS = 1,126.10<br>UCS = 19,041.35 |
| 1445                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                     |                        |                            |                |       |                                                      |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1447.7' to 1450':<br>(6) Fractures             |                        |                            |                |       |                                                      |
| 1450                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1449': 90° Planar smooth                            |                        |                            |                |       | PL(A) = 437.23<br>PL(D) = 150.53                     |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                     |                        |                            |                |       |                                                      |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1452' to 1459': (6)<br>47° - 63° Planar smooth |                        | C                          | 100            | 81    |                                                      |
| 1455                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                     |                        |                            |                |       |                                                      |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                     |                        |                            |                |       |                                                      |
| 1460                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                     |                        |                            |                |       |                                                      |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1461' to 1464': (4)<br>50° Planar smooth       |                        | C                          | 100            | 76    |                                                      |
| 1465                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                     |                        |                            |                |       |                                                      |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1467': (2) 45° - 47°<br>Reverse angle smooth        |                        |                            |                |       | SLK = Type I                                         |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1469': 72° Undulating<br>smooth                     |                        |                            |                |       |                                                      |

BORING TYPE: HQ3

DRILLER: Crux

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 2280

WATER OBSERVATIONS: 1006 ft.

CASING: HW to 20 ft.

REMARKS: \_\_\_\_\_

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                         |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|-----------------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type <u>  </u> ) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)              |
| WL                                | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)              |

(Continued Next Page)



CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2548.8

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2153392.317

DATE: 8/10/2024 - 10/13/2024

PROJECT LOCATION: Rosamod, CA

EASTING: 6514888.703

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata                            | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities                                     |                       | Sampling & In Situ Testing |                |       |                                                   |
|---------------------|--------------------------------------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|-----------------------------------------------------|-----------------------|----------------------------|----------------|-------|---------------------------------------------------|
|                     |                                                        | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear                            | J - Joint<br>F- Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments                        |
| 1475                |                                                        |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1471.6' to 1472.8':<br>82° Undulating smooth   |                       | C                          | 100            | 85    | PL(A) = 61.59<br>PL(D) = 378.99<br>UCS = 6,117.67 |
| 1480                |                                                        |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1473' to 1474': (2)<br>45° Planar smooth       |                       |                            |                |       |                                                   |
|                     |                                                        |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1474.3': 45° Undulating<br>rough                    |                       |                            |                |       |                                                   |
| 1485                |                                                        |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1479.8': 38° Planar<br>smooth                       |                       |                            |                |       | TRI = 35,047.28<br>TRI = 38,983.97                |
|                     |                                                        |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1482.3': 62° Undulating<br>smooth                   |                       | C                          | 100            | 77    |                                                   |
|                     |                                                        |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1483': 90° Fracture                                 |                       |                            |                |       |                                                   |
|                     |                                                        |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1484.5': 17° Planar<br>smooth                       |                       |                            |                |       |                                                   |
|                     |                                                        |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1486' to 1487.2':<br>(4) 45° Planar smooth     |                       |                            |                |       | ITS = 659.70<br>PL(D) = 762.85<br>PL(D) = 551.04  |
| 1490                |                                                        |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1488.6': 12° Planar<br>smooth                       |                       |                            |                |       |                                                   |
|                     |                                                        |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1488.8': 0° Planar<br>smooth                        |                       |                            |                |       |                                                   |
|                     |                                                        |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1489.4': 24° Undulating<br>rough                    |                       |                            |                |       | UCS = 5,097.03<br>ITS = 484.97<br>PL(D) = 876.94  |
|                     |                                                        |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1491.9': 39° Planar<br>smooth                       |                       | C                          | 100            | 69    |                                                   |
| 1495                |                                                        |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1492': (2) 47° Planar<br>smooth                     |                       |                            |                |       |                                                   |
|                     |                                                        |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1492.1': 39° Planar<br>smooth                       |                       |                            |                |       | SLK = Type II                                     |
|                     |                                                        |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1492.8': 79° Planar<br>smooth                       |                       |                            |                |       |                                                   |
| 1497                | QTZ MONZONITE, light gray to white<br>to pink to green |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1492.9' to 1493.3':<br>Undulating smooth       |                       |                            |                |       | PL(A) = 37.72                                     |
|                     |                                                        |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1493' to 1497': (5)<br>30° - 48° Planar smooth |                       |                            |                |       |                                                   |
| 1500                |                                                        |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1493.3': Stepped slightly<br>rough                  |                       |                            |                |       |                                                   |
|                     |                                                        |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1494.8': Planar rough                               |                       |                            |                |       |                                                   |
|                     |                                                        |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1495.1': Planar rough                               |                       | C                          | 100            | 68    |                                                   |
|                     |                                                        |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1496' to 1496.5':<br>Undulating rough          |                       |                            |                |       |                                                   |
|                     |                                                        |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1499.7' to 1500.2':                            |                       |                            |                |       |                                                   |

BORING TYPE: HQ3

DRILLER: Crux

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 2280

WATER OBSERVATIONS: 1006 ft.

CASING: HW to 20 ft.

REMARKS: \_\_\_\_\_

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                    |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|------------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type _____) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)         |
| L                                 | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)         |

(Continued Next Page)





CLIENT: Lane Power & Energy Solutions  
PROJECT: Hydrostor Zevsar  
PROJECT LOCATION: Rosamod, CA

SURFACE ELEVATION (ft): 2548.8  
NORTHING: 2153392.317  
EASTING: 6514888.703

PROJECT No: 951-20  
DATE: 8/10/2024 - 10/13/2024  
DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities                                |                        | Sampling & In Situ Testing |                |       |                                                          |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|------------------------------------------------|------------------------|----------------------------|----------------|-------|----------------------------------------------------------|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear                       | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments                               |
| 1510                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 60° Planar smooth                              |                        |                            |                |       | PL(D) = 38.31<br><br>PL(A) = 361.47<br>UCS = 8,638.61    |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1505.2' to 1505.6':<br>60° Planar smooth  |                        |                            |                |       |                                                          |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1506.55': 54° Planar<br>smooth                 |                        |                            |                |       |                                                          |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1509.3': 36° Undulating<br>rough               |                        |                            |                |       |                                                          |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1510.3' to 1511':<br>75° Planar rough     |                        |                            |                |       |                                                          |
| 1515                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1512.3': 37° Planar<br>smooth                  | C                      | 100                        | 59             |       | PL(D) = 48.89<br><br>PL(A) = 63.69<br><br>UCS = 4,298.12 |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1513.2': 62° Planar<br>smooth                  |                        |                            |                |       |                                                          |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1514.5': 45° Planar<br>smooth                  |                        |                            |                |       |                                                          |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1514.9': 30° Planar<br>rough                   |                        |                            |                |       |                                                          |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1516.8' to 1517':<br>85° Undulating rough |                        |                            |                |       |                                                          |
| 1520                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1518.8': 42° Planar<br>smooth                  |                        |                            |                |       | PL(D) = 48.89<br><br>PL(A) = 63.69<br><br>UCS = 4,298.12 |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1519.9': 66° Stepped<br>rough                  |                        |                            |                |       |                                                          |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1520' to 1521':<br>Rubble                 |                        |                            |                |       |                                                          |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1521.5': 45° Planar<br>rough                   | C                      | 100                        | 53             |       |                                                          |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1522' to 1523': 90°<br>Planar rough       |                        |                            |                |       |                                                          |
| 1525                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1524.5': 67° Undulating<br>smooth              |                        |                            |                |       | PL(D) = 48.89<br><br>PL(A) = 63.69<br><br>UCS = 4,298.12 |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1527': 15° Undulating<br>smooth                |                        |                            |                |       |                                                          |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1528': 90° Undulating<br>smooth                |                        |                            |                |       |                                                          |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1529': 75° Undulating<br>smooth                |                        |                            |                |       |                                                          |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1530.1' to 1531.6':<br>Rubble             |                        |                            |                |       |                                                          |
| 1530                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1533.2': 53° Undulating<br>smooth              | C                      | 100                        | 61             |       | PL(D) = 48.89<br><br>PL(A) = 63.69<br><br>UCS = 4,298.12 |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1533.6': 57° Undulating<br>smooth              |                        |                            |                |       |                                                          |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1533.9': 45° Planar<br>rough                   |                        |                            |                |       |                                                          |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1534.5': 65° Undulating<br>smooth              |                        |                            |                |       |                                                          |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1536.5': 55° Planar<br>rough                   |                        |                            |                |       |                                                          |
| 1535                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1538.3': 63° Undulating                        |                        |                            |                |       | PL(D) = 48.89<br><br>PL(A) = 63.69<br><br>UCS = 4,298.12 |
| 1539                | DIABASE                     |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                |                        |                            |                |       |                                                          |

BORING TYPE: HQ3  
HOLE DEPTH (ft): 2280  
REMARKS: \_\_\_\_\_

DRILLER: Crux  
WATER OBSERVATIONS: 1006 ft.

LOGGED BY: Chris Messenger  
CASING: HW to 20 ft.

| <b><u>SAMPLING &amp; IN SITU TESTING LEGEND</u></b> |               |       |                                                  |     |                                    |
|-----------------------------------------------------|---------------|-------|--------------------------------------------------|-----|------------------------------------|
| C                                                   | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type _____) |
| W                                                   | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)         |
| L                                                   | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)         |

(Continued Next Page)





CLIENT: Lane Power & Energy Solutions  
PROJECT: Hydrostor Zevsar  
PROJECT LOCATION: Rosamod, CA

SURFACE ELEVATION (ft): 2548.8  
NORTHING: 2153392.317  
EASTING: 6514888.703

PROJECT No: 951-20  
DATE: 8/10/2024 - 10/13/2024  
DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities                                 |                        | Sampling & In Situ Testing |                |       |                            |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|-------------------------------------------------|------------------------|----------------------------|----------------|-------|----------------------------|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear                        | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments |
| 1540                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | smooth                                          |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1539.1': 70° Planar<br>smooth                   |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1540.2': 73° Undulating<br>smooth               | C                      | 100                        | 46             |       | PL(D) = 120.18             |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1541.5': 83° Undulating<br>smooth               |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1542.9': 83° Undulating<br>smooth               |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1545.1': 73° Planar<br>rough                    |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1545.6' to 1546.7':<br>Rubble              |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1548.1': 80° Undulating<br>rough                |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1549.2': 47° Planar<br>rough                    |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1550.2' to 1550.5':<br>Rubble              |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1551.25': 60° Undulating<br>rough               | C                      | 100                        | 35             |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1552.7': 65° Undulating<br>smooth               |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1553.4': 67° Undulating<br>smooth               |                        |                            |                |       | SLK = Type II              |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1554': 60° Undulating<br>smooth                 |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1554.8': 78° Undulating<br>smooth               |                        |                            |                |       | UCS = 8,017.32             |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1557.2': 82° Undulating<br>smooth               |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1559': 65° Undulating<br>smooth                 |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1559.35': 0° Planar<br>rough                    | C                      | 100                        | 21             |       | PL(D) = 18.37              |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1560.5' to 1561.3':<br>Rubble              |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1562.1': 70° Undulating<br>smooth               |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1563': 75° Planar<br>smooth                     |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1564' to 1564.3':<br>45° Undulating smooth |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1564.4' to 1567.2':<br>Rubble              |                        |                            |                |       | UCS = 1,427.61             |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1569.5': 45° Undulating<br>smooth               |                        |                            |                |       | PL(D) = 18.98              |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1570.7': 45° Undulating<br>smooth               |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1571.8': 78° Undulating<br>rough                | C                      | 100                        | 30             |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1573': 75° Planar rough                         |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1574': 60° Undulating                           |                        |                            |                |       |                            |

BORING TYPE: HQ3  
HOLE DEPTH (ft): 2280  
REMARKS: \_\_\_\_\_

DRILLER: Crux  
WATER OBSERVATIONS: 1006 ft.

LOGGED BY: Chris Messenger  
CASING: HW to 20 ft.

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                    |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|------------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type _____) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)         |
| W                                 | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)         |



CLIENT: Lane Power & Energy Solutions  
PROJECT: Hydrostor Zevsar  
PROJECT LOCATION: Rosamod, CA

SURFACE ELEVATION (ft): 2548.8  
NORTHING: 2153392.317  
EASTING: 6514888.703

PROJECT No: 951-20  
DATE: 8/10/2024 - 10/13/2024  
DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities                                       |                        | Sampling & In Situ Testing |                |       |                              |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|-------------------------------------------------------|------------------------|----------------------------|----------------|-------|------------------------------|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear                              | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments   |
| 1580                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | rough                                                 |                        |                            |                |       | ITS = 130.25<br>PL(A) = 4.48 |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | -1574.8': 55° Planar rough                            |                        |                            |                |       |                              |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | -1575.55': 40° Undulating smooth                      |                        |                            |                |       |                              |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | -1576.1': 40° Undulating smooth                       |                        |                            |                |       |                              |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1577.7' to 1578.5': 90° Planar rough             |                        |                            |                |       |                              |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | -1578.6': 53° Undulating smooth                       |                        |                            |                |       | C 100 36                     |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | -1578.8': 65° Undulating rough                        |                        |                            |                |       |                              |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | -1579.5': 40° Undulating rough                        |                        |                            |                |       |                              |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | -1580.25': 53° Undulating rough                       |                        |                            |                |       |                              |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | -1581.35': 20° Planar rough                           |                        |                            |                |       |                              |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1581.8' to 1582': 30° Undulating smooth          |                        |                            |                |       | C 100 39                     |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | -1584.1': 55° Undulating smooth                       |                        |                            |                |       |                              |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | -1584.4': 67° Undulating smooth                       |                        |                            |                |       |                              |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1584.7' to 1585.5': 90° Planar rough, rubble     |                        |                            |                |       |                              |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | -1586.2': 45° Planar rough                            |                        |                            |                |       |                              |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | -1586.7': 45° Undulating smooth                       |                        |                            |                |       | C 100 41                     |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | -1588.5': 60° Undulating rough                        |                        |                            |                |       |                              |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | -1588.85': 45° Undulating smooth                      |                        |                            |                |       |                              |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | -1589.6': 60° Undulating smooth                       |                        |                            |                |       |                              |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | -1591.8': 30° Planar rough                            |                        |                            |                |       |                              |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | -1592.3': 63° Undulating smooth                       |                        |                            |                |       | C 100 41                     |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | -1592.8': 45° Undulating smooth                       |                        |                            |                |       |                              |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | -1593.3': 55° Undulating smooth                       |                        |                            |                |       |                              |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | -1593.8': 70° Undulating smooth                       |                        |                            |                |       |                              |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | -1594.25': 59° Undulating smooth                      |                        |                            |                |       |                              |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1595.2' to 1596': 30° - 45° J. Undulating smooth |                        |                            |                |       | C 100 41                     |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | -1596': 45° Undulating rough                          |                        |                            |                |       |                              |

BORING TYPE: HQ3  
HOLE DEPTH (ft): 2280  
REMARKS: \_\_\_\_\_

DRILLER: Crux  
WATER OBSERVATIONS: 1006 ft.

LOGGED BY: Chris Messenger  
CASING: HW to 20 ft.

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                   |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|-----------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type ____) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)        |
| WL                                | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)        |



CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2548.8

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2153392.317

DATE: 8/10/2024 - 10/13/2024

PROJECT LOCATION: Rosamod, CA

EASTING: 6514888.703

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities                              |                        | Sampling & In Situ Testing |                |       |                            |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|----------------------------------------------|------------------------|----------------------------|----------------|-------|----------------------------|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear                     | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments |
| 935<br>1615         |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1596.25': 50° Undulating rough               |                        |                            |                |       | UCS = 2,585.58             |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1596.55': 45° Undulating smooth              |                        | C                          | 100            | 39    | SLK = Type II              |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1596.95' to 1597.8': Rubble             |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1598' to 1598.75': 90° Planar rough     |                        |                            |                |       | PL(A) = 159.76             |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1599.1': 45° Planar smooth                   |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1599.6': 55° Undulating smooth               |                        |                            |                |       |                            |
| 930<br>1620         |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1603.6': 10° Undulating rough                |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1604.65': 62° Planar rough                   |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1605.4': 45° Undulating rough                |                        |                            |                |       | PL(D) = 59.30              |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1607.25' to 1607.45': 45° Planar smooth |                        | C                          | 100            | 32    |                            |
| 925<br>1625         |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1608.1': 45° Planar smooth                   |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1608.4': 30° Planar smooth                   |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1609' to 1611': Rubble                  |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1613.6': 45° Undulating smooth               |                        |                            |                |       |                            |
| 920<br>1630         |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1614.35': 45° Planar smooth                  |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1615.4': 62° Undulating smooth               |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1616': 25° Planar smooth                     |                        | C                          | 100            | 42    | PL(A) = 13.34              |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1616.4' to 1617.4': 90° Planar rough    |                        |                            |                |       |                            |
| 915<br>1635         |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1618.45': 45° Undulating smooth              |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1619.3': 55° Undulating rough                |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1619.65': 45° Undulating rough               |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1620.1': 45° Undulating rough                |                        |                            |                |       | PL(D) = 39.27              |
| 910<br>1640         |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1622.1': 58° Undulating rough                |                        |                            |                |       | UCS = 656.58               |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1622.8': 65° Undulating rough                |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1623.9': 70° Undulating smooth               |                        | C                          | 100            | 51    |                            |
| 905                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1628.3': 59° Undulating rough                |                        |                            |                |       |                            |

BORING TYPE: HQ3

DRILLER: Crux

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 2280

WATER OBSERVATIONS: 1006 ft.

CASING: HW to 20 ft.

REMARKS: \_\_\_\_\_

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                   |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|-----------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type ____) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)        |
| L                                 | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)        |

(Continued Next Page)



CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2548.8

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2153392.317

DATE: 8/10/2024 - 10/13/2024

PROJECT LOCATION: Rosamod, CA

EASTING: 6514888.703

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities                                |                        | Sampling & In Situ Testing |                |       |                                  |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|------------------------------------------------|------------------------|----------------------------|----------------|-------|----------------------------------|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear                       | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments       |
| 900                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1631.6': 0° Planar<br>smooth                   |                        |                            |                |       | PL(A) = 373.66                   |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1632': 13° Undulating<br>rough                 |                        |                            |                |       |                                  |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1633': 47° Planar rough                        |                        |                            |                |       |                                  |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1634': 16° Planar rough                        |                        |                            |                |       |                                  |
| 1650                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1634.9': 37° Undulating<br>rough               |                        |                            |                |       | PL(A) = 107.43                   |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1635.9': 28° Undulating<br>smooth              |                        |                            |                |       | SLK = Type I                     |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1636.6' to 1637.1':<br>Rubble             | C                      | 100                        | 54             |       |                                  |
| 1655                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1637.4': 60° Undulating<br>rough               |                        |                            |                |       |                                  |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1637.5': 40° Planar<br>rough                   |                        |                            |                |       | PL(D) = 140.73                   |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1638.2': 22° Planar<br>smooth                  |                        |                            |                |       |                                  |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1638.3': 68° Undulating<br>smooth              |                        |                            |                |       |                                  |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1640.5': 62° Undulating<br>smooth              |                        |                            |                |       |                                  |
| 1660                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1656' to 1657': 62°<br>Healed fracture    |                        |                            |                |       |                                  |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1657.8': 53° Planar<br>smooth                  |                        |                            |                |       | PL(A) = 185.37<br>PL(D) = 243.07 |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1658.4': 40° Planar<br>smooth                  | C                      | 100                        | 72             |       |                                  |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1659.1': 10° Planar<br>smooth                  |                        |                            |                |       |                                  |
| 1665                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1659.4': 12° Planar<br>smooth                  |                        |                            |                |       |                                  |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1660.5': 5° Planar rough                       |                        |                            |                |       |                                  |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1661.5' to 1662.6':<br>Undulating rough   |                        |                            |                |       |                                  |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1663': 55° Planar<br>smooth                    |                        |                            |                |       |                                  |
| 1670                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1665': 45° Planar<br>smooth                    |                        |                            |                |       |                                  |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1666.5': 54° Undulating<br>rough               |                        |                            |                |       | UCS = 4,306.62                   |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1668' to 1668.5':<br>80° Undulating rough | C                      | 100                        | 69             |       | PL(D) = 339.72                   |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1669': 67° Planar<br>smooth                    |                        |                            |                |       |                                  |
| 1675                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1670.3': 65° Planar<br>smooth                  |                        |                            |                |       |                                  |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1673.5': 33° Planar<br>smooth                  |                        |                            |                |       |                                  |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1675.3': 12° Planar<br>rough                   |                        |                            |                |       |                                  |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1678.6' to 1679':<br>66° Undulating rough |                        |                            |                |       |                                  |

BORING TYPE: HQ3

DRILLER: CruX

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 2280

WATER OBSERVATIONS: 1006 ft.

CASING: HW to 20 ft.

REMARKS:

| <b>SAMPLING &amp; IN SITU TESTING LEGEND</b> |               |       |                                                  |     |                                   |
|----------------------------------------------|---------------|-------|--------------------------------------------------|-----|-----------------------------------|
| C                                            | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type ____) |
| W                                            | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)        |
| L                                            | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)        |

(Continued Next Page)



CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2548.8

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2153392.317

DATE: 8/10/2024 - 10/13/2024

PROJECT LOCATION: Rosamod, CA

EASTING: 6514888.703

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities                                   |                        | Sampling & In Situ Testing |                |       |                                                         |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|---------------------------------------------------|------------------------|----------------------------|----------------|-------|---------------------------------------------------------|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear                          | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments                              |
| 1685                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1679.2' to 1680':<br>Undulating smooth       |                        |                            |                |       |                                                         |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1680.2': 45° Planar<br>smooth                     |                        | C                          | 100            | 71    | PL(A) = 76.06<br>UCS = 6,448.04<br><br>ITS = 291.72     |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1681' to 1682':<br>Undulating smooth         |                        |                            |                |       |                                                         |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1682.8': 35° Planar<br>smooth                     |                        |                            |                |       |                                                         |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1683.2': 31° Planar<br>rough                      |                        |                            |                |       |                                                         |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1683.9': 26° Planar<br>smooth                     |                        |                            |                |       |                                                         |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1687.2': 9° Planar rough                          |                        |                            |                |       |                                                         |
| 1690                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1689.6': 70° Undulating<br>rough                  |                        |                            |                |       |                                                         |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1690.2': 27° Planar<br>rough                      |                        |                            |                |       |                                                         |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1692.3': 57° Planar<br>smooth                     |                        | C                          | 100            | 81    | TRI = 30,345.96<br><br>PL(A) = 183.25<br>PL(D) = 190.59 |
| 1695                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1696.3': 15° Undulating<br>rough                  |                        |                            |                |       |                                                         |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1696.7': 42° Undulating<br>rough                  |                        |                            |                |       |                                                         |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1698.7': 33° Planar<br>rough                      |                        |                            |                |       |                                                         |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1699.6': 35° Planar<br>smooth                     |                        |                            |                |       |                                                         |
| 1700                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1701.6' to 1701.7':<br>72° Undulating smooth |                        |                            |                |       |                                                         |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1703' to 1703.5':<br>84° Undulating smooth   |                        | C                          | 100            | 76    | UCS = 9,914.34<br>TRI = 18,406.05                       |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1703.9': 9° Planar<br>smooth                      |                        |                            |                |       |                                                         |
| 1705                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1705.5': 6° Undulating<br>smooth                  |                        |                            |                |       |                                                         |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1706.4': 9° Undulating<br>rough                   |                        |                            |                |       |                                                         |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1708.9': 12° Planar<br>rough                      |                        |                            |                |       | TRI = 26,823.59<br>SLK = Type II                        |
| 1710                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                   |                        |                            |                |       |                                                         |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1713': 28° Planar<br>smooth                       |                        | C                          | 100            | 81    | ITS = 495.87<br>PL(A) = 92.12<br>PL(D) = 117.99         |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1713.8': 54° Planar<br>smooth                     |                        |                            |                |       |                                                         |

BORING TYPE: HQ3

DRILLER: Crux

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 2280

WATER OBSERVATIONS: 1006 ft.

CASING: HW to 20 ft.

REMARKS: \_\_\_\_\_

| <b><u>SAMPLING &amp; IN SITU TESTING LEGEND</u></b> |               |       |                                                  |     |                                    |
|-----------------------------------------------------|---------------|-------|--------------------------------------------------|-----|------------------------------------|
| C                                                   | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type _____) |
| W                                                   | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)         |
| L                                                   | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)         |

(Continued Next Page)



CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2548.8

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2153392.317

DATE: 8/10/2024 - 10/13/2024

PROJECT LOCATION: Rosamod, CA

EASTING: 6514888.703

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata                                                                                    | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities                                  |                        | Sampling & In Situ Testing |                |       |                                                     |
|---------------------|----------------------------------------------------------------------------------------------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|--------------------------------------------------|------------------------|----------------------------|----------------|-------|-----------------------------------------------------|
|                     |                                                                                                                | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear                         | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments                          |
| 1716                | QTZ MONZONITE, light gray to pink to white, phaneritic, with Na-Ca-K feldspar, biotite, hornblende, and pyrite |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | -1716.9': 14° Planar smooth                      |                        |                            |                |       | PL(A) = 48.66                                       |
|                     |                                                                                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | -1718': 31° Planar smooth                        |                        |                            |                |       |                                                     |
|                     |                                                                                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | -1718.6': 52° Planar smooth                      |                        |                            |                |       |                                                     |
| 1720                |                                                                                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | -1721.6': 30° Planar smooth                      |                        |                            |                |       | PL(D) = 171.87                                      |
|                     |                                                                                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | -1722.7': 21° Planar smooth                      |                        | C                          | 100            | 62    |                                                     |
|                     |                                                                                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1722.8' to 1723.3': 79° Undulating smooth   |                        |                            |                |       |                                                     |
| 1725                |                                                                                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | -1724.6': 30° Planar smooth                      |                        |                            |                |       | ITS = 620.76                                        |
|                     |                                                                                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | -1725.4': 50° Planar smooth                      |                        |                            |                |       |                                                     |
|                     |                                                                                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | -1725.5': 32° Planar smooth                      |                        |                            |                |       |                                                     |
|                     |                                                                                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | -1728.6': 42° Planar smooth                      |                        |                            |                |       | UCS = 10,273.03                                     |
| 1730                |                                                                                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                  |                        |                            |                |       |                                                     |
|                     |                                                                                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | -1732': 60° Undulating rough                     |                        | C                          | 100            | 74    |                                                     |
|                     |                                                                                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | -1736.6': 36° Planar rough                       |                        |                            |                |       | PL(A) = 239.46<br>UCS = 18,527.74<br>PL(D) = 179.57 |
| 1735                |                                                                                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | -1738.7': 30° Undulating rough                   |                        |                            |                |       |                                                     |
|                     |                                                                                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | -1739.7': 45° Planar smooth                      |                        |                            |                |       |                                                     |
|                     |                                                                                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                  |                        |                            |                |       | SLK = Type II                                       |
| 1740                |                                                                                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | -1742.9': 62° Undulating rough                   |                        | C                          | 100            | 58    |                                                     |
|                     |                                                                                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | -1743.9': 40° Planar rough                       |                        |                            |                |       |                                                     |
|                     |                                                                                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1744.3' to 1744.7': 80° Undulating rough    |                        |                            |                |       |                                                     |
| 1745                |                                                                                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1746' to 1753': (6) 20° - 40° Planar smooth |                        |                            |                |       | ITS = 48.04                                         |
| 1746                | QTZ MONZONITE, light gray to white to pink, phaneritic                                                         |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                  |                        |                            |                |       |                                                     |

BORING TYPE: HQ3

DRILLER: Crux

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 2280

WATER OBSERVATIONS: 1006 ft.

CASING: HW to 20 ft.

REMARKS:

| <b><u>SAMPLING &amp; IN SITU TESTING LEGEND</u></b> |               |       |                                                  |     |                               |
|-----------------------------------------------------|---------------|-------|--------------------------------------------------|-----|-------------------------------|
| C                                                   | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type _ |
| W                                                   | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)    |
| WL                                                  | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)    |

(Continued Next Page)



CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2548.8

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2153392.317

DATE: 8/10/2024 - 10/13/2024

PROJECT LOCATION: Rosamod, CA

EASTING: 6514888.703

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata                                                                                                   | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities          |                       | Sampling & In Situ Testing |                |       |                            |                                                        |
|---------------------|-------------------------------------------------------------------------------------------------------------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|--------------------------|-----------------------|----------------------------|----------------|-------|----------------------------|--------------------------------------------------------|
|                     |                                                                                                                               | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear | J - Joint<br>F- Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments |                                                        |
| 795<br>1755         | QTZ MONZONITE, light gray to white, phaneritic, with feldspar, biotite, and hornblende, trace amounts of muscovite and pyrite |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            | C              | 100   | 70                         | PL(A) = 46.99<br>PL(D) = 50.21<br>UCS = 5,320.66       |
| 790<br>1760         |                                                                                                                               |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            | C              | 100   | 76                         | PL(A) = 475.68<br><br>PL(D) = 221.99<br>UCS = 1,376.27 |
| 785<br>1765         |                                                                                                                               |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            | C              | 100   | 76                         | UCS = 471.28<br><br>PL(D) = 44.70                      |
| 780<br>1770         |                                                                                                                               |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            | C              | 100   | 60                         | PL(A) = 5.56                                           |
| 775<br>1775         |                                                                                                                               |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            | C              | 100   | 76                         |                                                        |
| 770<br>1780         |                                                                                                                               |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                       |                            |                |       |                            |                                                        |

BORING TYPE: HQ3

DRILLER: Crux

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 2280

WATER OBSERVATIONS: 1006 ft.

CASING: HW to 20 ft.

REMARKS:

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                  |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|----------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type ___) |
| W                                 | Water seep    | PL(A) | Point load axial test (50) (psi)                 | TRI | Triaxial stress test (psi)       |
| WL                                | Water level   | PL(D) | Point load diametral test (50) (psi)             | UCS | Uniaxial stress test (psi)       |





CLIENT: Lane Power & Energy Solutions  
PROJECT: Hydrostor Zevsar  
PROJECT LOCATION: Rosamod, CA

SURFACE ELEVATION (ft): 2548.8  
NORTHING: 2153392.317  
EASTING: 6514888.703

PROJECT No: 951-20  
DATE: 8/10/2024 - 10/13/2024  
DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata                    | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities                                     |                        | Sampling & In Situ Testing |                |       |                                                   |
|---------------------|------------------------------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|-----------------------------------------------------|------------------------|----------------------------|----------------|-------|---------------------------------------------------|
|                     |                                                | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear                            | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments                        |
| 1790                | QTZ MONZONITE, light gray to white, phaneritic |                         |    |    |    |    |                |               |      |          |      |           |         |       | 0.05                        | -1790': 40° - 42° Reverse angle Planar smooth       |                        |                            |                |       | PL(D) = 56.95<br>PL(A) = 595.72<br>PL(D) = 522.09 |
| 1792                |                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       | 0.25                        | -1791.3': 42° Planar rough                          |                        | C                          | 100            | 66    |                                                   |
| 1795                |                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       | 0.50                        | From 1794' to 1796.3': (4) 45° Planar smooth        |                        |                            |                |       |                                                   |
| 1800                |                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       | 2.50                        | -1798.45': 61° Undulating rough                     |                        |                            |                |       | SLK = Type I                                      |
| 1805                |                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       | 5.00                        | From 1802' to 1803': 47° - 74° Undulating           |                        | C                          | 100            | 58    | ITS = 239.83<br>PL(D) = 186.30                    |
| 1810                |                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1804.3': Rubble                                     |                        |                            |                |       |                                                   |
| 1815                |                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1805': 50° Undulating smooth                        |                        |                            |                |       |                                                   |
|                     |                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1808.3' to 1811': (6) 30° - 40° Planar smooth  |                        |                            |                |       | ITS = 802.74                                      |
|                     |                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | -1812.7': 90° S. Planar rough                       |                        | C                          | 100            | 42    |                                                   |
|                     |                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1814' to 1818': (7) 47° - 58° J. Planar smooth |                        |                            |                |       |                                                   |
|                     |                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1818' to 1817.4': 90° Stepped smooth, healed   |                        |                            |                |       | UCS =                                             |

BORING TYPE: HQ3  
HOLE DEPTH (ft): 2280  
REMARKS: \_\_\_\_\_

DRILLER: CruX  
WATER OBSERVATIONS: 1006 ft.

LOGGED BY: Chris Messenger  
CASING: HW to 20 ft.

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                   |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|-----------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type ____) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)        |
| L                                 | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)        |





CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2548.8

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2153392.317

DATE: 8/10/2024 - 10/13/2024

PROJECT LOCATION: Rosamod, CA

EASTING: 6514888.703

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities                                                        |                        | Sampling & In Situ Testing |                |       |                            |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|------------------------------------------------------------------------|------------------------|----------------------------|----------------|-------|----------------------------|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear                                               | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments |
| 1825                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1821' to 1823': 90°<br>Undulating rough, 45°<br>Undulating smooth |                        | C                          | 100            | 32    | 12,786.46                  |
| 1830                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1824' to 1827.7':<br>Multiple 90° Radial<br>fractures             |                        |                            |                |       |                            |
| 1835                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1829' to 1831':<br>Rubble                                         |                        |                            |                |       |                            |
| 1840                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1832' to 1836': 17°<br>- 31° Planar smooth                        |                        | C                          | 100            | 41    | PL(D) = 382.40             |
| 1845                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1836' to 1844': (3)<br>0° - 7° Planar smooth                      |                        |                            |                |       | ITS = 488.40               |
| 1850                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1844' to 1866':<br>Rubble                                         |                        | C                          | 100            | 47    |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                                        |                        | C                          | 100            | 45    | UCS = 2,686.37             |

BORING TYPE: HQ3

DRILLER: Crux

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 2280

WATER OBSERVATIONS: 1006 ft.

CASING: HW to 20 ft.

REMARKS: \_\_\_\_\_

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                  |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|----------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type ___) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)       |
| WL                                | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)       |

(Continued Next Page)



CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2548.8

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2153392.317

DATE: 8/10/2024 - 10/13/2024

PROJECT LOCATION: Rosamod, CA

EASTING: 6514888.703

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata                                                                  | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities                                          |                        | Sampling & In Situ Testing |                |       |                            |
|---------------------|----------------------------------------------------------------------------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|----------------------------------------------------------|------------------------|----------------------------|----------------|-------|----------------------------|
|                     |                                                                                              | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear                                 | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments |
| 1860                | QTZ MONZONITE, light gray to white,<br>phaneritic, with feldspar, biotite, and<br>hornblende |                         |    |    |    |    |                |               |      |          |      |           |         |       | 0.05                        |                                                          |                        |                            |                |       | SLK = Type I               |
| 1865                |                                                                                              |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                          |                        | C                          | 100            | 51    |                            |
| 1870                |                                                                                              |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1866' to 1871': (4)<br>45° Planar smooth            |                        |                            |                |       |                            |
| 1875                |                                                                                              |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1873' to 1874.5':<br>90° S. Undulating rough        |                        | C                          | 100            | 63    |                            |
| 1880                |                                                                                              |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1874.5' to 1881':<br>(6) 20° - 40° Planar<br>smooth |                        |                            |                |       |                            |
| 1885                |                                                                                              |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1881' to 1885': 30°<br>- 40° Undulating smooth      |                        | C                          | 100            | 56    | UCS = 6,774.61             |
|                     |                                                                                              |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1886.3': 27° Planar<br>smooth                            |                        |                            |                |       | ITS = 790.37               |
|                     |                                                                                              |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1889.1': 7° Undulating<br>rough                          |                        |                            |                |       |                            |

BORING TYPE: HQ3

DRILLER: Crux

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 2280

WATER OBSERVATIONS: 1006 ft.

CASING: HW to 20 ft.

REMARKS: \_\_\_\_\_

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                   |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|-----------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type ____) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)        |
| WL                                | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)        |

(Continued Next Page)



CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2548.8

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2153392.317

DATE: 8/10/2024 - 10/13/2024

PROJECT LOCATION: Rosamod, CA

EASTING: 6514888.703

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities          |                        | Sampling & In Situ Testing |                                                                          |       |                            |    |                 |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|--------------------------|------------------------|----------------------------|--------------------------------------------------------------------------|-------|----------------------------|----|-----------------|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear | J - Joint<br>F - Fault | Type                       | Core<br>Rec. %                                                           | RQD % | Test Results<br>& Comments |    |                 |
| 655<br>1895         |                             |                         |    |    |    |    |                |               |      |          |      |           |         | 0.05  | 0.25                        | 0.50                     | 2.50                   | 5.00                       | 1889.9': 29° Planar smooth                                               | C     | 100                        | 36 | UCS = 10,538.42 |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            | From 1892' to 1893': 38° - 52° Reverse angle wedge                       |       |                            |    |                 |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            | 1894': (2) 50° - 52° Undulating rough                                    |       |                            |    |                 |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            | From 1894.7' to 1896': (1) 90° Planar smooth, (3) 45° - 47° Planar rough |       |                            |    |                 |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            | From 1896.6' to 1897.2': Reverse angle wedge, Undulating rough           |       |                            |    |                 |
| 650<br>1900         |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            | 1898.3': 39° Undulating rough                                            |       |                            |    |                 |
| 645<br>1905         |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            | From 1902' to 1906': (11) 35° - 47° J. Planar rough                      |       |                            |    |                 |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            | From 1906.2' to 1906.8': (2) 7° - 9° Planar                              |       |                            |    |                 |
| 640<br>1910         |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            | 1908.6': Undulating rough                                                |       |                            |    |                 |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            | 1909.5': 17° Stepped rough                                               |       |                            |    |                 |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            | 1910': 4° Undulating rough                                               |       |                            |    |                 |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            | 1912': 4° Planar rough                                                   |       |                            |    |                 |
| 635<br>1915         |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            | From 1914' to 1914.3': Rubble                                            |       |                            |    |                 |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            | From 1916' to 1917.7': Rubble                                            |       |                            |    |                 |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            | From 1918' to 1919': (4) 20° - 40° Planar smooth                         |       |                            |    |                 |
| 630<br>1920         |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            | 1920': 57° Planar smooth                                                 |       |                            |    |                 |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            | 1922': 1° Planar smooth                                                  |       |                            |    |                 |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            | 1923': (3) 40° - 42° Planar smooth                                       |       |                            |    |                 |
| 625                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            | From 1924.6' to 1925':                                                   |       |                            |    |                 |

BORING TYPE: HQ3

DRILLER: Crux

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 2280

WATER OBSERVATIONS: 1006 ft.

CASING: HW to 20 ft.

REMARKS: \_\_\_\_\_

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                   |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|-----------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type ____) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)        |
| WL                                | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)        |

(Continued Next Page)



CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2548.8

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2153392.317

DATE: 8/10/2024 - 10/13/2024

PROJECT LOCATION: Rosamod, CA

EASTING: 6514888.703

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata                       | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities                                           |                        | Sampling & In Situ Testing |                |       |                            |
|---------------------|---------------------------------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|-----------------------------------------------------------|------------------------|----------------------------|----------------|-------|----------------------------|
|                     |                                                   | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear                                  | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments |
| 620                 |                                                   |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 37° - 40° Planar smooth                                   |                        |                            |                |       |                            |
| 1930                |                                                   |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1926.3': 47° and 90°<br>Undulating smooth                 |                        |                            |                |       |                            |
|                     |                                                   |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1928.3': 27° Planar<br>smooth                             |                        |                            |                |       |                            |
|                     |                                                   |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1929.5' to 1931':<br>(7) 7° - 17° Planar<br>smooth   |                        |                            |                |       |                            |
|                     |                                                   |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1931' to 1931.5':<br>Rubble                          |                        |                            |                |       |                            |
| 1935                |                                                   |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1932' to 1934.5':<br>90° Undulating, healed          | C                      | 100                        | 39             |       |                            |
|                     |                                                   |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1936' to 1939': (6)<br>40° - 52° J. Planar rough     |                        |                            |                |       |                            |
| 1940                |                                                   |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1939' to 1941': 90°<br>Planar smooth                 |                        |                            |                |       |                            |
|                     |                                                   |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1943': 41° Undulating<br>rough                            | C                      | 100                        | 48             |       | UCS =<br>11,065.70         |
| 1945                |                                                   |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1945.3': 47° Undulating<br>rough                          |                        |                            |                |       |                            |
|                     |                                                   |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1948' to 1949.5':<br>90° Undulating rough,<br>healed |                        |                            |                |       |                            |
| 1950                |                                                   |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1951' to 1952': 90°<br>Undulating rough              |                        |                            |                |       |                            |
|                     |                                                   |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1952': 67° Undulating<br>smooth                           | C                      | 100                        | 32             |       | ITS = 1,014.78             |
| 1955                |                                                   |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1954.5': (3) 17° - 30°<br>Planar rough                    |                        |                            |                |       |                            |
|                     |                                                   |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1956': 10° Planar<br>smooth                               |                        |                            |                |       |                            |
|                     |                                                   |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1957': 60° Planar<br>smooth                               |                        |                            |                |       | SLK = Type I               |
| 1958                | QTZ MONZONITE, light gray to white,<br>phaneritic |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1958': 80° Planar<br>smooth                               |                        |                            |                |       | PL(A) = 673.00             |

BORING TYPE: HQ3

DRILLER: Crux

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 2280

WATER OBSERVATIONS: 1006 ft.

CASING: HW to 20 ft.

REMARKS:

| <b><u>SAMPLING &amp; IN SITU TESTING LEGEND</u></b> |               |       |                                                  |     |                                 |
|-----------------------------------------------------|---------------|-------|--------------------------------------------------|-----|---------------------------------|
| C                                                   | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type __) |
| W                                                   | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)      |
| WL                                                  | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)      |

(Continued Next Page)



CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2548.8

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2153392.317

DATE: 8/10/2024 - 10/13/2024

PROJECT LOCATION: Rosamod, CA

EASTING: 6514888.703

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities                                               |                        | Sampling & In Situ Testing |                |       |                            |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|---------------------------------------------------------------|------------------------|----------------------------|----------------|-------|----------------------------|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear                                      | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments |
| 585                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1958.2' to 1959.4':<br>20° - 40° Planar smooth           |                        |                            |                |       |                            |
| 1965                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1959.9' to 1960.3':<br>59° - 63° Planar rough            |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1961.1': 50° Planar<br>smooth                                 |                        | C                          | 100            | 48    |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1961.7': 65° Undulating<br>smooth                             |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1963.2': 5° Planar<br>smooth                                  |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1963.4': 67° Planar<br>smooth                                 |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1963.8' to 1964.5':<br>Undulating smooth                 |                        |                            |                |       |                            |
| 1970                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1965.3': 12° Planar<br>smooth                                 |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1967.3': 45° Planar<br>smooth                                 |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1968.2': 45° Planar<br>smooth                                 |                        | C                          | 100            | 57    |                            |
| 1974                | QTZ MONZONITE               |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1970.4' to 1971.4':<br>15° - 35° Planar smooth           |                        |                            |                |       |                            |
| 1975                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1972.4': 18° Undulating<br>smooth                             |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1973.2' to 1973.8':<br>(4) 15° - 25° J. Planar<br>smooth |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1974.5': 40° Planar<br>smooth                                 |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1975.8': 65° Undulating<br>smooth                             |                        |                            |                |       |                            |
| 1980                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1976.7': 50° Planar<br>smooth                                 |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1977.3': 40° Planar<br>smooth                                 |                        | C                          | 100            | 47    |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1978.4': 48° Undulating<br>smooth                             |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1978.7' to 1979.7':<br>30° - 35° Planar smooth           |                        |                            |                |       |                            |
| 1985                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1980.8': 5° Undulating<br>rough                               |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1981.9': 55° Undulating<br>rough                              |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1982.5' to 1982.7':<br>30° - 45° Undulating<br>smooth    |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1983.2': 35° Undulating<br>smooth                             |                        |                            |                |       |                            |
| 1990                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 1983.6' to 1983.8':<br>45° Undulating smooth             |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1984.9': 63° Undulating<br>rough                              |                        | C                          | 100            | 43    |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1985.4': 57° Planar<br>smooth                                 |                        |                            |                |       |                            |

BORING TYPE: HQ3

DRILLER: Crux

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 2280

WATER OBSERVATIONS: 1006 ft.

CASING: HW to 20 ft.

REMARKS:

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                         |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|-----------------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type <u>  </u> ) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)              |
| L                                 | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)              |

(Continued Next Page)

**CLIENT:** Lane Power & Energy Solutions

**SURFACE ELEVATION (ft):** 2548.8

**PROJECT No:** 951-20

**PROJECT:** Hydrostor Zevsar

**NORTHING:** 2153392.317

**DATE:** 8/10/2024 - 10/13/2024

**PROJECT LOCATION:** Rosamod, CA

**EASTING:** 6514888.703

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata                                                                                                                              | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) |                                                       | Discontinuities                              |                        | Sampling & In Situ Testing |                |                                |                            |
|---------------------|----------------------------------------------------------------------------------------------------------------------------------------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|-------------------------------------------------------|----------------------------------------------|------------------------|----------------------------|----------------|--------------------------------|----------------------------|
|                     |                                                                                                                                                          |                         |    |    |    |    |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex-Hard |       |                             |                                                       | B - Bedding<br>S - Shear                     | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD %                          | Test Results<br>& Comments |
|                     |                                                                                                                                                          | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex-Hard |       | 0.05                        | 0.25                                                  | 0.50                                         | 2.50                   | 5.00                       |                |                                |                            |
| 550'                | QTZ MONZONITE, light gray to white to purple, phaneritic, with Na-Ca feldspar, biotite, and hornblende, trace amounts of chlorite, pyrite, and muscovite |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                       | 1987.3': 5° Planar smooth                    |                        |                            |                | UCS = 4,657.95<br>ITS = 493.63 |                            |
| 2000                |                                                                                                                                                          |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                       | 1988.3': 35° Planar smooth                   |                        |                            |                |                                |                            |
|                     |                                                                                                                                                          |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                       | 1988.6': 12° Planar rough                    |                        |                            |                |                                |                            |
|                     |                                                                                                                                                          |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                       | From 1988.8' to 1990.3': 90° Healed fracture |                        |                            |                |                                |                            |
|                     |                                                                                                                                                          |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                       | 1991.4': 25° Planar rough                    |                        |                            |                |                                |                            |
|                     |                                                                                                                                                          |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                       | 1991.6': 32° Planar smooth                   |                        |                            |                |                                |                            |
|                     |                                                                                                                                                          |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                       | 1992.1': 35° Undulating smooth               | C                      | 100                        | 38             |                                |                            |
| 545'                |                                                                                                                                                          |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                       | 1992.3': 35° Planar smooth                   |                        |                            |                |                                |                            |
| 2005                |                                                                                                                                                          |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                       | 1994.4': 70° Undulating rough                |                        |                            |                |                                |                            |
|                     |                                                                                                                                                          |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                       | 1996.8': 70° - 80° Planar rough              |                        |                            |                |                                |                            |
|                     |                                                                                                                                                          |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 1998.3': 55° Planar smooth                            |                                              |                        |                            |                |                                |                            |
| 540'                |                                                                                                                                                          |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2000.5': 57° Undulating rough                         |                                              |                        |                            |                |                                |                            |
| 2010                |                                                                                                                                                          |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2000.7' to 2001': Rubble                         |                                              |                        |                            |                |                                |                            |
| 2011                |                                                                                                                                                          |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2001.4': 67° Undulating rough                         | C                                            | 100                    | 43                         |                |                                |                            |
|                     |                                                                                                                                                          |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2002.5': 45° Undulating smooth                        |                                              |                        |                            |                |                                |                            |
| 535'                |                                                                                                                                                          |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2002.7': 18° Planar smooth                            |                                              |                        |                            |                |                                |                            |
| 2015                |                                                                                                                                                          |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2003.7': 72° Undulating smooth                        |                                              |                        |                            |                |                                |                            |
|                     |                                                                                                                                                          |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2004.8': 70° Undulating smooth                        |                                              |                        |                            |                |                                |                            |
|                     |                                                                                                                                                          |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2005.6': 75° Planar rough                             |                                              |                        |                            |                |                                |                            |
| 530'                |                                                                                                                                                          |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2006': 80° Planar rough                               |                                              |                        |                            |                |                                |                            |
| 2020                |                                                                                                                                                          |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2006.4' to 2007.1': Rubble                       |                                              |                        |                            |                |                                |                            |
|                     |                                                                                                                                                          |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2008.2': 80° Planar rough                             | C                                            | 100                    | 60                         |                |                                |                            |
| 2023                |                                                                                                                                                          |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2009.6': 45° Planar rough                             |                                              |                        |                            |                |                                |                            |
| 525'                |                                                                                                                                                          |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2010' to 2010.6': Multiple fractures             |                                              |                        |                            |                |                                |                            |
| 2025                |                                                                                                                                                          |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2012' to 2012.4': 50° - 55° (2) J. Planar smooth |                                              |                        |                            |                |                                |                            |
|                     |                                                                                                                                                          |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2013.4': 55° Planar smooth                            |                                              |                        |                            |                |                                |                            |
| 520'                |                                                                                                                                                          |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2014.2': 40° Planar smooth                            |                                              |                        |                            |                |                                |                            |

**BORING TYPE:** HQ3

**DRILLER:** Crux

**LOGGED BY:** Chris Messenger

**HOLE DEPTH (ft):** 2280

WATER OBSERVATIONS: 1006 ft.

**CASING:** HW to 20 ft.

REMARKS:

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |
|-----------------------------------|---------------|-------|--------------------------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               |
| W                                 | Water level   | PL(D) | Point load diametral test Is(50) (psi)           |
|                                   |               | SLK   | Slake durability test (Type _____)               |
|                                   |               | TRI   | Triaxial stress test (psi)                       |
|                                   |               | UCS   | Uniaxial stress test (psi)                       |

(Continued Next Page)



CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2548.8

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2153392.317

DATE: 8/10/2024 - 10/13/2024

PROJECT LOCATION: Rosamod, CA

EASTING: 6514888.703

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata                                                                                        | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities          |                        | Sampling & In Situ Testing |                |       |                            |
|---------------------|--------------------------------------------------------------------------------------------------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|--------------------------|------------------------|----------------------------|----------------|-------|----------------------------|
|                     |                                                                                                                    | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments |
| 2032                | QTZ MONZONITE                                                                                                      |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        | C                          | 100            | 38    | SLK = Type I               |
| 2033                |                                                                                                                    |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 2035                |                                                                                                                    |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 2037.7              |                                                                                                                    |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 2040                | QTZ MONZONITE, light gray to white, phaneritic, with feldspar, biotite, and hornblende, trace muscovite and pyrite |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       | UCS = 4,721.11             |
| 2045                |                                                                                                                    |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 2046                |                                                                                                                    |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       | ITS = 590.53               |
| 2050                |                                                                                                                    |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       | UCS = 5,559.64             |
| 2055                |                                                                                                                    |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 2060                |                                                                                                                    |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 2064                |                                                                                                                    |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 2064                |                                                                                                                    |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 2064                |                                                                                                                    |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 2064                |                                                                                                                    |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |
| 2064                | CORE LOSS                                                                                                          |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                          |                        |                            |                |       |                            |

BORING TYPE: HQ3

DRILLER: Crux

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 2280

WATER OBSERVATIONS: 1006 ft.

CASING: HW to 20 ft.

REMARKS:

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                               |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|-------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type ) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)    |
| W                                 | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)    |

(Continued Next Page)





CLIENT: Lane Power & Energy Solutions  
PROJECT: Hydrostor Zevsar  
PROJECT LOCATION: Rosamod, CA

SURFACE ELEVATION (ft): 2548.8  
NORTHING: 2153392.317  
EASTING: 6514888.703

PROJECT No: 951-20  
DATE: 8/10/2024 - 10/13/2024  
DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities                                                                   |                        | Sampling & In Situ Testing |                |       |                            |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|-----------------------------------------------------------------------------------|------------------------|----------------------------|----------------|-------|----------------------------|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear                                                          | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments |
| 2065                | QTZ MONZONITE               |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2042.2' to 2042.5':<br>65° - 75° Planar smooth,<br>healed                    |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2044': 60° Planar<br>smooth                                                       |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2044.9': 70° Undulating<br>rough                                                  |                        |                            |                |       |                            |
| 2070                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2048.9': 47° Undulating<br>rough                                                  |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2050' to 2051':<br>Rubble                                                    |                        |                            |                |       |                            |
| 2072                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2051.3': 74° Stepped<br>rough                                                     | C                      | 100                        | 74             |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2052' to 2052.6':<br>(1) 30° (1) 79° Undulating<br>rough                     |                        |                            |                |       |                            |
| 2074.3              | QTZ MONZONITE               |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2053.75' to<br>2054.78': 90° Planar<br>smooth                                |                        |                            |                |       | UCS = 2,492.14             |
| 2075                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2057.6': 74° Undulating<br>smooth                                                 |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2059' to 2060': 67°<br>Undulating rough, 38° -<br>80° Planar smooth<br>wedge |                        |                            |                |       |                            |
| 2080                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2061': 76° Undulating<br>smooth                                                   |                        |                            |                |       |                            |
| 2081                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2063': (3) 74° - 79° - 90°<br>Undulating rough                                    | C                      | 100                        | 62             |       | ITS = 400.41               |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2065': 90° Planar<br>smooth                                                       |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2066' to 2072':<br>Rubble                                                    |                        |                            |                |       |                            |
| 2085                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2073.8': 79° Planar<br>rough                                                      |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2075': 67° Planar<br>smooth                                                       |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2076' to 2079': 45°<br>J. Planar smooth                                      |                        |                            |                |       | PL(D) = 403.19             |
| 2090                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2082.6': 67° Planar<br>smooth                                                     |                        |                            |                |       | SLK = Type I               |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2084' to 2086':<br>Rubble                                                    |                        |                            |                |       | UCS =<br>13,124.24         |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2086.9': 51° Undulating<br>smooth                                                 | C                      | 100                        | 46             |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2088' to 2088.5':<br>7° - 15° Planar smooth                                  |                        |                            |                |       |                            |
| 2095                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2091' to 2094': 90°<br>Healed fracture                                       |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2092.1': 80° - 90°<br>Stepped smooth                                              |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2094' to 2096.4':<br>Rubble                                                  |                        |                            |                |       |                            |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2097.4': 32° Planar<br>smooth                                                     |                        |                            |                |       |                            |

BORING TYPE: HQ3  
HOLE DEPTH (ft): 2280  
REMARKS: \_\_\_\_\_

DRILLER: Crux  
WATER OBSERVATIONS: 1006 ft.

LOGGED BY: Chris Messenger  
CASING: HW to 20 ft.

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                   |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|-----------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type ____) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)        |
| WL                                | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)        |

(Continued Next Page)





CLIENT: Lane Power & Energy Solutions  
PROJECT: Hydrostor Zevsar  
PROJECT LOCATION: Rosamod, CA

SURFACE ELEVATION (ft): 2548.8  
NORTHING: 2153392.317  
EASTING: 6514888.703

PROJECT No: 951-20  
DATE: 8/10/2024 - 10/13/2024  
DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities                                            |                        | Sampling & In Situ Testing |                |       |                                |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|------------------------------------------------------------|------------------------|----------------------------|----------------|-------|--------------------------------|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear                                   | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments     |
| 445'                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2097.7' to 2099':<br>79° Planar rough                 |                        |                            |                |       |                                |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2099' to 2099.8':<br>74° Planar smooth                |                        |                            |                |       |                                |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2099.8' to 2101':<br>90° Undulating rough,<br>healed  |                        | C                          | 100            | 33    |                                |
| 2105                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2102.4': 45° Planar<br>smooth                              |                        |                            |                |       |                                |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2102.5' to 2104.1':<br>87° - 90° Stepped rough        |                        |                            |                |       |                                |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2104.5' to 2106':<br>Rubble                           |                        |                            |                |       |                                |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2107.7' to 2108':<br>(3) 34° Planar rough             |                        |                            |                |       |                                |
| 2110                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                            |                        |                            |                |       |                                |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2111' to 2113': (4)<br>20° - 40° Planar smooth        |                        | C                          | 100            | 63    | ITS = 664.64                   |
| 2115                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2113.8': 42° Planar                                        |                        |                            |                |       |                                |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2115' to 2115.7':<br>(2) 40° Planar rough             |                        |                            |                |       |                                |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                            |                        |                            |                |       |                                |
| 2120                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2119': 45° Stepped<br>rough                                |                        |                            |                |       | UCS =<br>10,645.72             |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2120' to 2121': 79°<br>- 84° Undulating smooth        |                        |                            |                |       |                                |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2121' to 2123.4':<br>(5) 30° - 41° Planar<br>smooth   |                        | C                          | 100            | 52    |                                |
| 2125                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2125': (2) 45° - 57° J.<br>Planar smooth                   |                        |                            |                |       |                                |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2126.3' to 2127.7':<br>(2) 32° - 41° Planar<br>smooth |                        |                            |                |       |                                |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2128.1': 74° Planar<br>rough                               |                        |                            |                |       | SLK = Type I<br>UCS = 7,271.81 |
| 2130                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2130' to 2131': (2)<br>45° Undulating smooth          |                        |                            |                |       |                                |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2131.4' to 2134':<br>90° Planar smooth                |                        | C                          | 100            | 21    | ITS = 698.66                   |
| 415'                |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                            |                        |                            |                |       |                                |

BORING TYPE: HQ3  
HOLE DEPTH (ft): 2280  
REMARKS: \_\_\_\_\_

DRILLER: Crux  
WATER OBSERVATIONS: 1006 ft.

LOGGED BY: Chris Messenger  
CASING: HW to 20 ft.

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                    |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|------------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type _____) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)         |
| WL                                | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)         |



CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2548.8

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2153392.317

DATE: 8/10/2024 - 10/13/2024

PROJECT LOCATION: Rosamod, CA

EASTING: 6514888.703

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata                                                                                                   | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities                                   |                        | Sampling & In Situ Testing |                |       |                            |
|---------------------|-------------------------------------------------------------------------------------------------------------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|---------------------------------------------------|------------------------|----------------------------|----------------|-------|----------------------------|
|                     |                                                                                                                               | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear                          | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments |
| 2136                | QTZ MONZONITE, light gray to white, phaneritic                                                                                |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2135' to 2136': Rubble                       |                        |                            |                |       |                            |
| 2140                |                                                                                                                               |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2136' to 2151': Rubble                       |                        |                            |                |       |                            |
| 2145                |                                                                                                                               |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                   |                        | C                          | 100            | 3     |                            |
| 2150                |                                                                                                                               |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2151' to 2156': (3) 40° - 45° Planar smooth  |                        | C                          | 100            | 25    | UCS = 2,905.54             |
| 2155                |                                                                                                                               |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2156' to 2163': Rubble                       |                        |                            |                |       |                            |
| 2160                |                                                                                                                               |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2163' to 2166': 47° - 48° Planar rough wedge |                        | C                          | 100            | 40    |                            |
| 2165                |                                                                                                                               |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2166.8': 4° Planar rough                          |                        |                            |                |       |                            |
| 2166                | QTZ MONZONITE, light gray to white, phaneritic, with feldspar, biotite, and hornblende, trace amounts of muscovite and pyrite |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2167.5': 57° Planar smooth                        |                        |                            |                |       | ITS = 95.21                |
|                     |                                                                                                                               |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2168.5': 55° Planar rough                         |                        |                            |                |       |                            |

BORING TYPE: HQ3

DRILLER: Crux

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 2280

WATER OBSERVATIONS: 1006 ft.

CASING: HW to 20 ft.

REMARKS:

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                  |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|----------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type ___) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)       |
| L                                 | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)       |

(Continued Next Page)



CLIENT: Lane Power & Energy Solutions  
PROJECT: Hydrostor Zevsar  
PROJECT LOCATION: Rosamod, CA

SURFACE ELEVATION (ft): 2548.8  
NORTHING: 2153392.317  
EASTING: 6514888.703

PROJECT No: 951-20  
DATE: 8/10/2024 - 10/13/2024  
DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities                                     |                        | Sampling & In Situ Testing |                |       |                                                 |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|-----------------------------------------------------|------------------------|----------------------------|----------------|-------|-------------------------------------------------|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear                            | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments                      |
| 375<br>2175         |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2169.9': 55° Planar smooth                          |                        |                            |                |       |                                                 |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2172.1': 65° Undulating smooth                      |                        | C                          | 100            | 57    |                                                 |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2172.6': 57° Planar smooth                          |                        |                            |                |       |                                                 |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2173.7' to 2173.9':<br>55° - 65° Planar smooth |                        |                            |                |       |                                                 |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2175.25': 35° Planar smooth                         |                        |                            |                |       |                                                 |
| 370<br>2180         |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2179': 0° Planar rough                              |                        |                            |                |       |                                                 |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2179.1' to 2179.9':<br>90° Healed fracture     |                        |                            |                |       |                                                 |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2180.1': 3° Planar rough                            |                        | C                          | 100            | 58    | SLK = Type II<br>ITS = 210.84<br>UCS = 2,653.69 |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2183.1': 0° Planar rough                            |                        |                            |                |       |                                                 |
| 365<br>2185         |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2185.1': 65° Planar rough                           |                        |                            |                |       |                                                 |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2185.85': 0° Planar rough                           |                        |                            |                |       |                                                 |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2186.1' to 2186.7':<br>90° Healed fracture     |                        |                            |                |       |                                                 |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2187': 60° Planar rough                             |                        |                            |                |       |                                                 |
| 360<br>2190         |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2188.55' to<br>2189.85': Rubble                |                        |                            |                |       |                                                 |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2190.2' to 2190.4':<br>50° - 55° Planar rough  |                        |                            |                |       |                                                 |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2191.4' to 2193':<br>90° Healed fracture       |                        | C                          | 100            | 32    |                                                 |
| 355<br>2195         |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2193.4': 45° Planar smooth                          |                        |                            |                |       |                                                 |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2194.5' to 2196':<br>90° Healed fracture       |                        |                            |                |       |                                                 |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2196.2' to 2197.3':<br>90° Healed fracture     |                        |                            |                |       |                                                 |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2197.65': 60° Planar smooth                         |                        |                            |                |       |                                                 |
| 350<br>2200         |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2198.7': 80° Planar smooth                          |                        |                            |                |       |                                                 |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2199.2': 45° Planar rough                           |                        |                            |                |       |                                                 |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2199.6': 70° Undulating rough                       |                        | C                          | 100            | 61    |                                                 |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2199.9': 45° Planar rough                           |                        |                            |                |       |                                                 |
| 345                 |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2200.5': 67° Undulating rough                       |                        |                            |                |       |                                                 |

BORING TYPE: HQ3  
HOLE DEPTH (ft): 2280  
REMARKS:

DRILLER: Crux  
WATER OBSERVATIONS: 1006 ft.

LOGGED BY: Chris Messenger  
CASING: HW to 20 ft.

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                         |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|-----------------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type <u>  </u> ) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)              |
| WL                                | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)              |

(Continued Next Page)



CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2548.8

PROJECT No: 951-20

PROJECT: Hydrostor Zevsar

NORTHING: 2153392.317

DATE: 8/10/2024 - 10/13/2024

PROJECT LOCATION: Rosamod, CA

EASTING: 6514888.703

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) |                       | Discontinuities |                | Sampling & In Situ Testing |                            |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|-----------------------|-----------------|----------------|----------------------------|----------------------------|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       | B - Bedding<br>S - Shear    | J - Joint<br>F- Fault | Type            | Core<br>Rec. % | RQD %                      | Test Results<br>& Comments |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 340<br>2210         |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                       |                 |                |                            |                            |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |

BORING TYPE: HQ3

DRILLER: Crux

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 2280

WATER OBSERVATIONS: 1006 ft.

CASING: HW to 20 ft.

REMARKS:

| <b><u>SAMPLING &amp; IN SITU TESTING LEGEND</u></b> |               |       |                                                  |     |                                 |
|-----------------------------------------------------|---------------|-------|--------------------------------------------------|-----|---------------------------------|
| C                                                   | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type __) |
| W                                                   | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)      |
| L                                                   | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)      |

(Continued Next Page)



CLIENT: Lane Power & Energy Solutions

SURFACE ELEVATION (ft): 2548.8

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EASTING: 6514888.703

DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities                           |                        | Sampling & In Situ Testing |                |       |                                                   |
|---------------------|-----------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|-------------------------------------------|------------------------|----------------------------|----------------|-------|---------------------------------------------------|
|                     |                             | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear                  | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments                        |
| 305'<br>-2245       |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2229': 33° Planar smooth                  |                        |                            |                |       | UCS = 9,829.09<br>ITS = 891.80<br>UCS = 15,398.92 |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2229.8': Planar rough                     |                        |                            |                |       |                                                   |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2230': 9° Planar smooth                   | C                      | 100                        | 42             |       |                                                   |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2230.6': 20° Planar smooth                |                        |                            |                |       |                                                   |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2231.8': 35° Planar rough                 |                        |                            |                |       |                                                   |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2232': 22° Planar rough                   |                        |                            |                |       | SLK = Type I                                      |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2232.6': 40° Planar smooth                |                        |                            |                |       |                                                   |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2233.2': 25° Planar smooth                |                        |                            |                |       |                                                   |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2233.3': 65° Planar smooth                |                        |                            |                |       |                                                   |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2234.7': 58° Planar smooth                |                        |                            |                |       |                                                   |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2235.7': Undulating smooth                | C                      | 100                        | 13             |       | ITS = 1,364.45                                    |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2236.5': 20° Planar rough                 |                        |                            |                |       |                                                   |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2236.7': 10° Planar smooth                |                        |                            |                |       |                                                   |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2238.2': 3° - 6° Planar rough             |                        |                            |                |       |                                                   |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2238.7': 60° Planar smooth                |                        |                            |                |       |                                                   |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2239': 15° Undulating rough               |                        |                            |                |       | ITS = 1,364.45                                    |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2240': 60° Planar smooth                  |                        |                            |                |       |                                                   |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2242.6': 25° Undulating rough             |                        |                            |                |       |                                                   |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2242.9': 32° Planar rough                 | C                      | 100                        | 26             |       |                                                   |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2244.7': 9° Planar smooth                 |                        |                            |                |       |                                                   |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2245.5': 45° Planar smooth                |                        |                            |                |       | ITS = 1,364.45                                    |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2246.8': 73° Planar smooth                |                        |                            |                |       |                                                   |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2248.6': 15° Planar smooth                |                        |                            |                |       |                                                   |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2249': 20° Planar smooth                  |                        |                            |                |       |                                                   |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2249.5': 75° Planar smooth                |                        |                            |                |       |                                                   |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2251' to 2252': Stepped rough        | C                      | 100                        | 19             |       | ITS = 1,364.45                                    |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2252.5' to 2253.2': Undulating rough |                        |                            |                |       |                                                   |
|                     |                             |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2253.3': 75° Planar                       |                        |                            |                |       |                                                   |

BORING TYPE: HQ3

DRILLER: Crux

LOGGED BY: Chris Messenger

HOLE DEPTH (ft): 2280

WATER OBSERVATIONS: 1006 ft.

CASING: HW to 20 ft.

REMARKS: \_\_\_\_\_

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                   |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|-----------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type ____) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)        |
| L                                 | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)        |

(Continued Next Page)



CLIENT: Lane Power & Energy Solutions  
PROJECT: Hydrostor Zevsar  
PROJECT LOCATION: Rosamod, CA

SURFACE ELEVATION (ft): 2548.8  
NORTHING: 2153392.317  
EASTING: 6514888.703

PROJECT No: 951-20  
DATE: 8/10/2024 - 10/13/2024  
DIP/AZIMUTH: -90 /

| EL<br>DEPTH<br>(ft) | Description<br>of<br>Strata        | Degree of<br>Alteration |    |    |    |    | Graphic<br>Log | Rock Strength |      |          |      |           |         | Water | Fracture<br>Spacing<br>(ft) | Discontinuities                                    |                        | Sampling & In Situ Testing |                |       |                            |
|---------------------|------------------------------------|-------------------------|----|----|----|----|----------------|---------------|------|----------|------|-----------|---------|-------|-----------------------------|----------------------------------------------------|------------------------|----------------------------|----------------|-------|----------------------------|
|                     |                                    | Fr                      | SA | MA | HA | CA |                | Very Soft     | Soft | Med-Hard | Hard | Very Hard | Ex Hard |       |                             | B - Bedding<br>S - Shear                           | J - Joint<br>F - Fault | Type                       | Core<br>Rec. % | RQD % | Test Results<br>& Comments |
| 270                 |                                    |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             |                                                    |                        |                            |                |       |                            |
| 2280                | Bottom of borehole at 2280.0 feet. |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | rough                                              |                        |                            |                |       | UCS =<br>13,063.97         |
|                     |                                    |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2254' to 2254.9':<br>76° Planar smooth        |                        |                            |                |       |                            |
|                     |                                    |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2255': 12° Planar<br>smooth                        |                        |                            |                |       |                            |
|                     |                                    |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2256' to 2256.5':<br>Rubble                   |                        |                            |                |       |                            |
|                     |                                    |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2257': 45° Planar<br>smooth                        |                        |                            |                |       |                            |
|                     |                                    |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2257.7': 85° Undulating<br>smooth                  |                        |                            |                |       |                            |
|                     |                                    |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2259': 25° Planar<br>smooth                        |                        |                            |                |       |                            |
|                     |                                    |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2260.1': 20° Planar<br>smooth, healed              |                        |                            |                |       |                            |
|                     |                                    |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2261.4': 15° Planar<br>smooth                      |                        |                            |                |       |                            |
|                     |                                    |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2262': 12° Undulating<br>smooth                    |                        |                            |                |       |                            |
|                     |                                    |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2262.9': 40° Planar<br>smooth                      |                        |                            |                |       |                            |
|                     |                                    |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2263': 8° Planar smooth                            |                        |                            |                |       |                            |
|                     |                                    |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2263.4': 20° Planar<br>smooth                      |                        |                            |                |       |                            |
|                     |                                    |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2264': 60° Planar<br>smooth                        |                        |                            |                |       |                            |
|                     |                                    |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2264.9': Planar smooth                             |                        |                            |                |       |                            |
|                     |                                    |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2266': 50° Planar rough                            |                        |                            |                |       |                            |
|                     |                                    |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2266.1' to 2267.7':<br>Multiple planar smooth |                        |                            |                |       |                            |
|                     |                                    |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2270.6': 40° Planar<br>smooth                      |                        |                            |                |       |                            |
|                     |                                    |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2271.1': 6° Planar<br>smooth                       |                        |                            |                |       |                            |
|                     |                                    |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2271.3': 15° Planar<br>smooth                      |                        |                            |                |       |                            |
|                     |                                    |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2272': 50° Planar rough                            |                        |                            |                |       |                            |
|                     |                                    |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2273.1': 50° Planar<br>smooth                      |                        |                            |                |       |                            |
|                     |                                    |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2273.6': Undulating<br>rough                       |                        |                            |                |       |                            |
|                     |                                    |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | From 2275' to 2279.2':<br>Rubble                   |                        |                            |                |       |                            |
|                     |                                    |                         |    |    |    |    |                |               |      |          |      |           |         |       |                             | 2279.3': 50° Planar<br>smooth                      |                        |                            |                |       |                            |

BORING TYPE: HQ3  
HOLE DEPTH (ft): 2280  
REMARKS: \_\_\_\_\_

DRILLER: Crux  
WATER OBSERVATIONS: 1006 ft.

LOGGED BY: Chris Messenger  
CASING: HW to 20 ft.

| SAMPLING & IN SITU TESTING LEGEND |               |       |                                                  |     |                                   |
|-----------------------------------|---------------|-------|--------------------------------------------------|-----|-----------------------------------|
| C                                 | Core drilling | ITS   | Indirect tensile strength (Brazilian) test (psi) | SLK | Slake durability test (Type ____) |
| W                                 | Water seep    | PL(A) | Point load axial test Is(50) (psi)               | TRI | Triaxial stress test (psi)        |
| WL                                | Water level   | PL(D) | Point load diametral test Is(50) (psi)           | UCS | Uniaxial stress test (psi)        |